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PHASE I RFI/RI REPORT

**WOMAN CREEK PRIORITY DRAINAGE
OPERABLE UNIT NO 5**

**ROCKY FLATS ENVIRONMENTAL
TECHNOLOGY SITE, COLORADO**



TEXT

Prepared For

U S DEPARTMENT OF ENERGY
Rocky Flats Environmental Technology Site
Golden Colorado



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ACRONYMS

µg/kg	micrograms per kilogram
µg/L	micrograms per liter
1 1 DCE	1 1 dichloroethene
1 2 DCE	1 2 dichloroethene
1 1 1 TCA	1 1 1 trichloroethane
ac ft	acre feet
ACGIH	American Conference of Governmental Industrial Hygienists
ACM	asbestos containing material
AEC	Atomic Energy Commission
AOC	Area of Concern
ARAR	Applicable or Relevant and Appropriate Requirement
BAT®	Bengt Arne Tortensson
BGCR	Background Geochemical Characterization Report
BOD	biochemical oxygen demand
bQ	becquerel
BRA	Baseline Risk Assessment
BUTL	Background Upper Tolerance Limit
CDPHE	Colorado Department of Public Health and Environment
CEDE	committed effective dose equivalent
CERCLA	Comprehensive Environmental Response Compensation and Liability Act
cfs	cubic feet per second
CLP	Contract Laboratory Program
CMP	corrugated metal pipe
cm/sec	centimeters per second
cm ² /sec	square centimeters per second
cm ³ /sec	cubic centimeters per second
COC	chemical of concern
cpm	counts per minute
CPT	cone penetrometer testing
CRAVE	Carcinogenic Risk Assessment Verification Endeavor
CRQL	contract required quantitation limit
CSF	cancer slope factor
CSM	conceptual site model
CSU	Colorado State University
CT	central tendency
DCF	dose conversion factors
DCN	Document Change Notice
DCM	dichloromethane
DLG	Digital Line Graph
DMR	Document Modification Request
DOE	U S Department of Energy

ACRONYMS (Continued)

DQO	data quality objective
ECAO	Environmental Criteria and Assessment Office
ECOC	ecological chemicals of concern
EDE	effective dose equivalent
EM	electromagnetic
EPA	U S Environmental Protection Agency
ER	Environmental Restoration
ERA	Ecological Risk Assessment
ERAM	ecological risk assessment methodology
ERDA	Energy Research and Development Administration
f_1	fractional uptake
FB	field blank
FDM	Fugitive Dust Model
FIDLER	Field Instrument for the Detection of Low Energy Radiation
FS	Feasibility Study
FSP	Field Sampling Plan
ft	feet
ft/day	feet per day
ft^2	square feet
ft^3/m	cubic feet per minute
g	gram
g/m^2	grams per square centimeter
gpm	gallons per minute
GRRASP	General Radiochemistry and Routine Analytical Services Protocol
Gy	Gray (u/l case)
H&S	health and safety
HEAST	Health Effects Assessment Summary Tables
HHRA	Human Health Risk Assessment
HI	hazard index
HPGe	high purity germanium
HQ	hazard quotient
HRR	Historical Release Report
HSA	hollow stem auger
HSPF10	Hydrologic Simulation Program Fortran Version 10
IAG	Interagency Agreement
IHSS	Individual Hazardous Substance Site
IHSS 115	Original Landfill
IHSS 133 1	Ash Pit 1
IHSS 133 2	Ash Pit 2
IHSS 133 3	Ash Pit 3
IHSS 133 4	Ash Pit 4
IHSS 133 5	Incinerator

ACRONYMS (Continued)

IHSS 133 6	Concrete Wash Pad
IHSS 142 10	Pond C 1
IHSS 142 11	Pond C 2
IHSS 196	Water Treatment Plant Backwash Pond
IHSS 209	Surface Disturbances
IM	interim measure
IRA	interim remedial action
IRIS	Integrated Risk Information System
kg	kilogram
LHSU	lower hydrostratigraphic unit
LR	laboratory replicate
m	meter
m/s	meters per second
mg/l	milligrams per liter
mg/kg	milligrams per kilogram
mph	miles per hour
mm	millimeter
mmhos/m	millimhos per meter
MS	matrix spike
MSD	matrix spike duplicate
MSL	mean sea level
nCi/g	nanocuries per gram
NCP	National Contingency Plan
n d	no date
NOAEL	No Observed Adverse Effects Level
NPDES	National Pollutant Discharge Elimination System
OU	Operable Unit
OU 5	Operable Unit No 5
PAH	polynuclear aromatic hydrocarbon
PARCC	precision accuracy representativeness completeness and comparability
PCB	polychlorinated biphenyl
PCE	tetrachloroethene
pCi/L	picocuries per liter
pCi/g	picocuries per gram
PCOC	potential chemical of concern
PET	potential evapotranspiration
ppm	parts per million
PVC	polyvinyl chloride
QA	quality assurance
QAA	Quality Assurance Addendum
QC	quality control
RAAMP	Radioactive Ambient Air Monitoring Program

ACRONYMS (Continued)

RAGS	Risk Assessment Guidance Superfund
RBC	risk based concentration
RCA	radiologically controlled area
RCRA	Resource Conservation and Recovery Act
RFA	Rocky Flats Alluvium
RfC	reference concentration
RfD	reference dose
RFEDS	Rocky Flats Environmental Database System
RFETS	Rocky Flats Environmental Technology Site
RFI/RI	RCRA Facility Investigation/Remedial Investigation
RFP	Rocky Flats Plant
RME	reasonable maximum exposure
RPD	relative percent difference
s	seconds
SBDC	South Boulder Diversion Canal
SEP	Systematic Evaluation Program
SID	South Interceptor Ditch
SOP	standard operating procedure
SVOC	semi volatile organic compound
TAL	target analyte list
TB	trip blank
TCE	trichloroethene
TCL	toxic compound list
TDEM	time domain electromagnetic
TEDE	total effective dose equivalent
TIC	tentatively identified compound
TM	Technical Memorandum
TRV	toxicity reference values
TSS	total suspended solids
UCL	upper confidence limit
UHSU	upper hydrostratigraphic unit
USCS	Unified Soil Classification System
USGS	United States Geological Survey
UTL	Upper Tolerance Limit
VOC	volatile organic compound
WDM	Watershed Data Management

EXECUTIVE SUMMARY

This report presents the results obtained during implementation of the Work Plan for the Phase I Resource Conservation and Recovery Act (RCRA) Facility Investigation/Remedial Investigation (RFI/RI) of the Woman Creek Priority Drainage (Operable Unit No. 5 (OU 5)) at the Rocky Flats Environmental Technology Site (RFETS) formerly known as the Rocky Flats Plant (RFP) Jefferson County Colorado as amended. This investigation is pursuant to a Compliance Agreement among the U.S. Department of Energy (DOE), the U.S. Environmental Protection Agency (EPA), and the Colorado Department of Public Health and the Environment (CDPHE) dated July 31, 1986 and an Interagency Agreement (IAG) among DOE, EPA, and CDPHE dated January 22, 1991.

The purpose of the OU 5 Phase I RFI/RI is to assess the potential contamination associated with the Individual Hazardous Substance Sites (IHSSs) that are located within the Woman Creek drainage. Data collected under the field investigation portion of the RFI/RI were used to estimate risks to human health and the environment, to begin developing and screening remedial alternatives, and to evaluate the need for further studies of the OU 5 IHSSs.

Eleven IHSSs geographically located along or within the drainage areas of Woman Creek, have been designated as OU 5. These IHSSs include the Original Landfill (IHSS 115), Ash Pits, Former Incinerator Area, and Concrete Wash Pad (IHSSs 133.1 through 133.6), Detention Ponds C 1 and C 2 (IHSSs 142.10 and 142.11), and a Surface Disturbance (IHSS 209). Ponds C 1 and C 2 are the only IHSSs located on Woman Creek. The remaining IHSSs are located along the banks and/or upland areas that drain into Woman Creek or into the South Interceptor Ditch (SID). In addition to these IHSSs, two additional surface disturbances are being investigated in the Phase I OU 5 investigation: a Surface Disturbance West of IHSS 209 and a Surface Disturbance South of the Ash Pits. See Figure 1.2.

On May 27, 1993, EPA and CDPHE notified DOE that IHSS 196, Water Treatment Plant Filter Backwash Pond, was to be included in the OU 5 investigation. This IHSS was previously scheduled to be investigated as part of OU 16, Low Priority Sites. Because of its proximity to IHSS 115, the investigation of IHSS 196 was conducted concurrently with that of IHSS 115.

The OU 5 Phase I RFI/RI was conducted in two phases of distinct field programs. The first program was the field investigation specified in the OU 5 Phase I RFI/RI Work Plan. This investigation was conducted from September 1992 through August 1993 and included as many as four phases of work performed at each IHSS. During the course of this investigation, ten technical memoranda (TMs) were prepared to evaluate the data collected under each stage of the investigation and to further define the activities to be performed in subsequent investigations.

Upon completion of the field investigation specified in the OU 5 Phase I RFI/RI Work Plan, as amended by the TMs, the data collected under this investigation were evaluated. It was determined from this evaluation that additional data were required to assist in the definition of the nature and extent of contamination associated with each IHSS and to collect data required for the evaluation of potential remedial alternatives for the OU 5 Feasibility Study (FS). Technical Memorandum No. 15 (TM15) was prepared to document the evaluation of the data collected during the OU 5 Work Plan investigation and to provide an amended Field Sampling Plan (FSP). This TM enabled the additional data required to be collected under the Phase I RFI/RI for OU 5 rather than proceeding with a Phase II RFI/RI. This additional field program was conducted from September 1994 through August 1995.

The Phase I RFI/RI Work Plan for OU 5 Woman Creek Priority Drainage is a Controlled Document available for viewing in the Public Reading Rooms as specified in the IAG. TM 15, Amended Field Sampling Plan, is included as Volume III, IV, and V of the Phase I RFI/RI Work Plan of OU 5 Woman Creek Priority Drainage. Text to TM15, Amended Field Sampling Plan (Vol. I, Text); Text to TM15, Amended Field Sampling Plan (Vol. II, Text); Text to TM15, Amended Field Sampling Plan (Vol. III, Appendices A-G).

Field investigations indicate that the site physical characteristics are complex. Site meteorologic, geologic, hydrologic, and hydrogeologic processes combined interactively to provide mechanisms and pathways for surface and subsurface constituents to migrate through the environment. For example, because some upper hydrostratigraphic unit groundwater pathways discharge to surface water within OU 5, there is limited potential for migration of volatile organic compounds (VOCs) to offsite locations.

The nature and extent of environmental contamination within OU 5 have been characterized through the collection, analysis, and assessment of hundreds of samples (Tables 2.1 through 2.10) of various environmental media. Environmental samples were analyzed for a comprehensive suite of chemicals to

help characterize potential contamination associated with waste handling and disposal practices conducted during the operating history of the Site. The OU 5 data assessment process including rigorous data validation was designed to be conservative to ensure a comprehensive understanding of potential contamination conditions in OU 5.

The results of the OU 5 data assessment indicated the presence of potential chemicals of concern (PCOCs) in surface soil, subsurface soil, groundwater, pond seep, and stream water, and pond, seep, and stream sediments. PCOCs identified in one or more of these environmental media include VOCs, semi-volatile organic compounds (SVOCs), polychlorinated biphenyls (PCBs)/pesticides, metals, and other nonradioactive inorganic constituents, and radionuclides. The list of PCOCs for each medium was then screened using risk-based and other screening methods to identify chemicals of concern (COCs) for both the Human Health Risk Assessment (HHRA) and the Ecological Risk Assessment (ERA). COCs were identified as the chemicals in each medium that were likely to contribute at least one percent of overall risk. For the HHRA, COCs were selected on an OU-wide basis; for the ecological risk assessment (ERA), the COCs were identified for the Woman Creek watershed. In groundwater and surface water, metals and radionuclides are the primary COCs; however, in seep water, the COCs are all VOCs. The COCs in surface soil and subsurface soil include uranium isotopes, several metals, polynuclear aromatic hydrocarbons (PAHs), and PCBs. The COCs identified in stream and pond sediments are radionuclides and metals. Table 6-25 in Section 6 presents the COCs identified for OU 5.

The presence of COCs in all media is a result of historical releases to the environment. Under the hydrogeochemical conditions of OU 5, metals and radionuclides are not expected to be very mobile via the groundwater pathway. However, storm water runoff may transport contaminated soils to surface waters with subsequent transport to downstream receptors. The presence of COCs in stream, seep, and pond sediments is likely a result of surface water transport of contaminated surface soils to Woman Creek. Fugitive dust emissions from OU 5 surface soils and dry sediments may contribute contaminated particulates to future onsite receptors. Exposure to subsurface soils by future onsite construction workers may result in contaminant inhalation and ingestion. Numerical modeling was used to examine the migration of COCs along pathways in groundwater, surface water, and air. The numerical models provided COC concentration tables for the HHRA.

The OU 5 HHRA indicate that there are estimated health risks and annual radiation doses for current and future onsite receptors as a result of indirect or direct exposure from sources in OU 5. The following

exposure scenarios were evaluated a current industrial worker (security guard) a future industrial/office worker a future ecological researcher a future open space recreational user and a future construction worker Future onsite residential receptors were not considered in the HHRA because future land use plans do not include residential use It was determined during HHRA negotiations with the regulatory agencies that health risks to offsite receptors would not be addressed on an OU specific basis but on a sitewide basis

For the HHRA exposure media that were evaluated included surface soil subsurface soil outdoor and indoor air stream seep and pond water and stream seep and pond sediments Groundwater was not evaluated as an exposure pathway because there are no current or future receptors

Risks were evaluated for three Areas of Concern (AOCs) AOC No 1 is the Original Landfill (IHSS 115/196 Source Area) AOC No 2 includes the Ash Pits (IHSS 133 Source Area) AOC No 3 includes the SID Ponds C 1 and C 2 Source Areas and the Woman Creek. See Figure 6 1

The risk characterization process combines average and reasonable maximum estimates of exposure with upperbound estimates of toxicity to yield conservative (protective) estimates of health risk. Estimates of health risk for average (central tendency or CT) and reasonable maximum exposure (RME) conditions are provided so that risk management decisions can be based on a range of potential risks for different exposure scenarios

The following are the major conclusions of the HHRA

- AOC1 Cumulative hazard indices (HIs) were below 1 and RME cancer risk estimates were $3\text{E-}05$ or below for all receptors The maximum cancer risk estimate of $3\text{E-}05$ is for both the current worker (security guard) and the future office worker This risk is still within EPA's acceptable risk range of $1\text{E-}06$ to $1\text{E-}04$ External irradiation due to exposure of uranium 238 in surface soil is the primary contributor to this estimate of cancer risk
- AOC2 Cumulative HIs were below 1 and RME cancer risk estimates were $4\text{E-}06$ or below for all receptors The maximum cancer risk estimate of $4\text{E-}06$ is for both the current worker (security guard) and the future office worker This risk is at the low end of EPA's acceptable risk range of $1\text{E-}06$ to $1\text{E-}04$ External irradiation due to exposure of uranium 238 in surface soil is the primary contributor to this estimate of cancer risk

• AOC3 Cumulative HIs were below 1 and the RME cancer risk estimates were below EPA's point of departure of 1×10^{-6} for both receptors. These results indicate that no adverse noncarcinogenic health hazards and negligible cancer risk are expected for all receptors evaluated.

The ERA for Woman Creek was conducted for aquatic and terrestrial biota exposed to contaminants in OUs 1, 2, and 5. Assessment of ecological risks was based on evaluating exposure of biological receptors to PCOCs in designated ERA source areas. Source areas include individual or groups of IHSSs within an OU and were based on abiotic and biotic sampling locations in and around IHSSs. A preliminary exposure and risk calculation was conducted for PCOCs in source areas. The analysis was conducted to estimate the contribution of each PCOC and each source area to overall risk in the watershed. Ecological chemicals of concern (ECOCs) were identified from preliminary risk calculations and evaluated further in risk characterization.

Ecotoxicological risk to terrestrial receptors in OU 5 was minimal. Concentrations (activities) of uranium 233/234 and uranium 238 in soils exceeded the risk based screening criteria developed for the Site. However, the criteria were exceeded in only two locations, both of which are in the Old Landfill source area and which represent a negligible portion of habitat in the watershed. Maximum concentrations of radionuclides in small mammals were not associated with levels that exceed the benchmarks for safe radiological doses. Thus, risk from exposure to radionuclides appears to be minimal.

The screening level assessment also indicated that concentrations of mercury, antimony, and Aroclor 1254 could represent risks to aquatic feeding birds if they acquired all of their food from the SID Pond C 1 and segments of Woman Creek. However, it is unlikely that birds would spend all of the time in the areas of concern, because the size and quality of habitat in these areas is inadequate to support their needs.

The results of the HHRA and the ERA support the conclusions that environmental contamination within OU 5 does not pose a threat to public health or the environment under the evaluated exposure scenarios and that remediation of environmental media to address risk to public health and the environment is not warranted.

1 0 INTRODUCTION

This report presents the results obtained during implementation of the Work Plan (DOE 1992a) for the Phase I Resource Conservation and Recovery Act (RCRA) Facility Investigation/Remedial Investigation (RFI/RI) of the Woman Creek Priority Drainage (Operable Unit No 5 [OU 5]) at the Rocky Flats Environmental Technology Site (RFETS) formerly known as the Rocky Flats Plant (RFP) Jefferson County Colorado as amended (DOE 1992a,1994a) This investigation is pursuant to a Compliance Agreement among the U S Department of Energy (DOE) the U S Environmental Protection Agency (EPA) and the Colorado Department of Public Health and the Environment (CDPHE) dated July 31 1986 and an Interagency Agreement (IAG) among DOE EPA and CDPHE dated January 22 1991 The IAG addresses RCRA and Comprehensive Environmental Response Compensation and Liability Act (CERCLA) issues and has been integrated with DOE's Environmental Restoration (ER) Program (IAG 1991)

1 1 PURPOSE OF PROJECT

The purpose of the OU 5 Phase I RFI/RI is to assess the potential contamination associated with the Individual Hazardous Substance Sites (IHSSs) that are located within the Woman Creek drainage The data collected under the field investigation portion of the RFI/RI are used to estimate risks to human health and the environment begin developing and screening remedial alternatives and to evaluate the need for further studies of the OU 5 IHSSs

1 2 BACKGROUND

1 2 1 Plant Operations

The site (Figure 1 1) is a government-owned and contractor operated facility that is part of the nationwide nuclear weapons production complex RFP was operated for the U S Atomic Energy Commission (AEC) from construction in 1951 until the AEC was dissolved in January 1975 At that time responsibility for the RFP was assigned to the Energy Research and Development Administration (ERDA) which was succeeded by the DOE in 1977 Dow Chemical USA an operating unit of the DOW Chemical Company was the prime operating contractor of the facility from 1951 until June 30 1975 Rockwell

International succeeded Dow Chemical USA from July 1 1975 to January 1 1990 when EG&G Rocky Flats Inc succeeded Rockwell International On July 1 1995 Kaiser Hill LLC succeeded EG&G Rocky Flats Inc as the prime operating contractor

Currently the primary mission at the Site is environmental restoration The name was changed from RFP to Rocky Flats Environmental Technology Site in September 1994 Historically the primary mission was to produce metal components for nuclear weapons These components were fabricated from plutonium uranium and nonradioactive metals principally beryllium and stainless steel Metal components were shipped elsewhere for final assembly When nuclear weapons were determined to be obsolete components of the weapons were returned for special processing to recover plutonium and americium Other activities included research and development in metallurgy machining nondestructive testing coatings remote engineering chemistry and physics Both radioactive and nonradioactive wastes have been and are generated in these research and production processes Current waste handling practices involve onsite and offsite recycling of hazardous materials onsite storage of hazardous and radioactive mixed wastes and disposal of solid radioactive materials at other DOE facilities However historically the site operating procedures included both onsite storage and disposal of hazardous and radioactive wastes

1 2 2 OU 5 (Woman Creek)

Eleven IHSSs geographically located along or within the drainage areas of Woman Creek (Figure 1 2) have been designated as OU 5 These IHSSs include the Original Landfill (IHSS 115) Ash Pits Incinerator and Concrete Wash Pad (IHSSs 133 1 through 133 6) Detention Ponds C 1 and C 2 (IHSSs 142 10 and 142 11) and a Surface Disturbance (IHSS 209) Ponds C 1 and C 2 are the only IHSSs located on Woman Creek The remaining IHSSs are located along the banks and/or upland areas that drain into Woman Creek or into the South Interceptor Ditch (SID) In addition to these IHSSs two additional surface disturbances are being investigated in the Phase I OU 5 investigation a Surface Disturbance West of IHSS 209 and a Surface Disturbance South of the Ash Pits

In 1980 the SID (Figure 1 7) was constructed upslope (to the north) of Woman Creek to intercept surface water run off from the southern portion of the Industrialized Area, and more specifically from the

881 Hillside The SID begins near the east end of an Ash Pit (IHSS 133 2) parallels the creek cuts through the toe of the Original Landfill (IHSS 115) and continues below the 881 Hillside French Drain. The SID crosses under the Woman Creek Diversion Ditch then empties into Pond C 2. A berm was constructed on the downslope side of the SID to contain the water flowing into the ditch. The construction of the SID through the toe of the Original Landfill has contributed to the formation of slump features that are apparent within that area.

On May 27, 1993, EPA and CDPHE notified DOE that IHSS 196, Water Treatment Plant Filter Backwash Pond, was to be included in the OU 5 investigation. This IHSS was previously scheduled to be investigated as part of OU 16, Low Priority Sites. Because of its proximity to IHSS 115, the investigation of IHSS 196 was conducted concurrently with that of IHSS 115.

1.2.2.1 OU 5 IHSS Descriptions and Histories

The following sections describe the locations, physical features, and histories of each of the OU 5 IHSSs. These discussions are primarily based on the information provided in the OU 5 Work Plan (DOE 1992a) and additional information that was obtained during the course of the investigation of the IHSSs and that provide further detail regarding the location, description, and history of the IHSSs.

IHSS 115 (Original Landfill) and IHSS 196 (Filter Backwash Pond) The Original Landfill is located within the buffer zone just south of the site industrialized area and south of the west access road (Figure 1.3). It is located north of Woman Creek on a moderately to steeply sloping south-facing hillside.

The Original Landfill was in operation from 1952 to 1968 and was used to dispose of general wastes generated at the Site. It is estimated that 2 million cubic feet of miscellaneous Site wastes are buried in the landfill, including such things as solvents, paints, paint thinners, oil, pesticides, cleaners (Rockwell 1988), construction-related debris, waste metal, and glass. These wastes were not considered hazardous prior to 1968 when they were placed in the landfill. The landfill also received beryllium and/or uranium wastes and used graphite. It has been reported that ash containing an estimated 20 kilograms (kg) of depleted uranium (DOE 1986) produced when 60 kg of depleted uranium were inadvertently burned and only 40 kg were recovered, was buried within the landfill. Chemicals that may have been placed in this landfill include commonly used solvents such as trichloroethene (TCE), carbon tetrachloride, tetrachloroethene,

(PCE) petroleum distillates 1 1 1 trichloroethane (1 1 1 TCA) dichloromethane (DCM) benzene paint and paint thinners Metals such as beryllium uranium lead and chromium may also be present (Rockwell 1988) Accurate records of any further wastes placed in this landfill are not available

IHSS 196 an evaporation/settling pond that was used for backflushing sand filters from the water treatment facility (Building 124) was located within the boundaries of the Original Landfill near the western edge (Figure 1 3) It appears that a second pond (visible in a 1955 aerial photograph in the approximate location of the SID) was constructed but by 1964 this pond was no longer present and the area had been covered by fill (DOE 1992a)

By 1980 the SID had been built across the southern part of the landfill Several other activities at the landfill are apparent from aerial photographs of the area presented in EPA (1988a) A 1964 aerial photograph shows an active area of surface disturbance east of the landfill Little documented historical information is available concerning this area however this area may have served as a storage yard for pipes and scrap metal In addition soil appears to have been placed in this area as substantial mounds of debris are noted in this area, as shown in 1969 and 1971 aerial photographs (EPA 1988a)

The landfill was closed with a soil cover however a bottom liner was not installed Details of the construction of the surface cover are not available nor is the year the cover was installed The slope on the south side of the landfill was regraded to correct sloughing and erosion related problems

Two storm sewer pipes protrude from the landfill area (Figure 1 3) The west pipe is no longer connected to a drainage system The pipe which cuts diagonally across the landfill from west to east, appears to be connected to storm drains and possibly to foundation drains in the 400 Area (Section 2 4 5) This pipe discharges to the SID just east of the surface disturbance east of the landfill

IHSS 133 (Ash Pits, Former Incinerator Area, and Concrete Wash Pad) The Former Incinerator Area, Ash Pits and Concrete Wash Pad are located south southwest of the industrialized area of the site south of the west access road and north of Woman Creek (Figure 1 4) The locations of these IHSSs are defined from historic aerial photographs The Former Incinerator which had a 10 to 20-foot stack, was located along the original western boundary of the site off the west access road Ash Pits 1 2 3 4 (IHSSs 133 1 133 2 133 3 133 4) and time domain electromagnetic area (TDEM) 1 and TDEM 2 are approximately 20 feet

(ft) wide by 150 ft long and 8 18 ft deep Two additional ash pits were identified and are referred to as TDEM 1 and TDEM 2 in this report The Ash Pits are located on a relatively flat surface and are currently covered by tall grasses

The Former Incinerator Area (IHSS 133 5) occupies approximately 4 000 square feet (ft²) and the Concrete Wash Pad (IHSS 133 6) covers an area of about 33 000 ft² These two IHSSs are located west of the four original Ash Pits The area surrounding the Concrete Wash Pad has an extremely irregular hummocky surface that slopes gently to the south toward Woman Creek

The Incinerator was used to burn general site wastes between the 1950s and 1968 Depleted uranium is also believed to have been burned in the Incinerator (Rockwell 1988) A review of aerial photographs revealed that the Incinerator was removed by 1971 and the entire area was beginning to revegetate (EPA 1988a) Ashes from the Incinerator were placed into the Ash Pits or were pushed over the side of the hill into the Woman Creek drainage and/or onto the Concrete Wash Pad (Rockwell 1988) Following the shutdown of the Incinerator after 1968 the Ash Pits were covered with fill (Rockwell 1988) however information about the material used in the construction of the cover is unavailable

The history of the Concrete Wash Pad has not been as well documented as the Ash Pits or Former Incinerator area. It appears that this area was used to dispose of waste concrete from the concrete trucks involved in the construction activities of the site It is also likely that the concrete trucks were washed down in this area after delivering concrete

The histories of the Ash Pits Incinerator and Concrete Wash Pad are not entirely known because few records were kept of their operations It is known however that general combustible wastes from the site were burned in the Incinerator along with an estimated 100 grams of depleted uranium (Owen and Steward 1973) which were disposed of into the ash pits and 60 kg was burned of which 20 kg was disposed into the original landfill The ashes from the Incinerator were disposed in the Ash Pits At the Concrete Wash Pad, potentially contaminated materials consist of concrete debris and small amounts of ash from the Incinerator that were reported to have been pushed over the side of the hill onto the Concrete Wash Pad area (Rockwell 1988)

A rayscope survey (an unknown type of survey) was conducted over Ash Pit 3 (IHSS 133 3) prior to 1973 and the results of this survey detected metals (type unknown) (DOE 1987) No documentation exists as to whether the other Ash Pits (IHSSs 133 1 133 2 and 133 4) had a rayscope survey done over their surfaces

IHSS 142.10 and 142.11 (C Ponds) Ponds C 1 (IHSS 142 10) and C 2 (IHSS 142 11) are located along Woman Creek southeast of the industrialized area of the site and within the Buffer Zone (Figure 1 2) These ponds are approximately 2 000 ft apart with Pond C 1 to the west of Pond C 2 The estimated capacities for Ponds C 1 and C 2 are approximately 5 acre feet (ac ft) and 69 8 ac ft, respectively

The natural drainage of Woman Creek has been somewhat modified in the OU 5 area by the construction of Ponds C 1 and C 2 and the SID south of the industrial area. Currently Woman Creek flows eastward through OU 5 in its natural stream channel to Pond C 1 (Figure 1 2) Filter backwash water from the water treatment facility was discharged in Pond C 1 between the site start up in 1952 and December 21 1973 (DOE 1980) In addition the cooling tower blowdown water was discharged to Pond C 1 until the latter part of 1974 In the early 1970s the site operations were changed and Pond C 1 was used principally to manage the surface water runoff in the Woman Creek drainage Water is rarely retained within this pond because the outlet or gate is usually open and the water is allowed to flow through the pond The water consequently flows in its natural channel until just west of Pond C 2 where it is diverted around Pond C 2 by a diversion canal During low flows downgradient and to the east of Pond C 2 all of the water is diverted from Woman Creek's main channel into an unnamed ditch that flows into Mower Reservoir During high flows some flow continues to flow downstream in Woman Creek and into Standley Lake Reservoir

In 1980 the SID was constructed upslope (to the north) of Woman Creek (Figure 1 2) to intercept surface runoff from the site A berm was constructed on the downslope side of the SID to contain the water flowing in this ditch Since construction of the SID in 1980 Woman Creek has not received runoff directly from the southern part of the site Surface water flow in the SID is intermittent and usually occurs only following precipitation events or snow melt. When flow is low water tends to pond in several areas of the ditch The SID begins approximately 200 ft east of the Ash Pits and runs for almost two miles to Pond C 2 (Figure 1 2) The SID is approximately 4 to 8 ft in depth and is not lined Just upslope of Pond C 2 the water flowing in the SID crosses over Woman Creek and flows into Pond C 2 In Pond C 2 the

water is sampled analyzed and discharged into the Broomfield Diversion Ditch that diverts water around Great Western Reservoir according to a National Pollutant Discharge Elimination System (NPDES) agreement (Permit No. CO 0001333)

IHSS 209 and Other Surface Disturbances Three separate surface disturbances are described in this section: (1) IHSS 209, (2) the Surface Disturbance West of IHSS 209, and (3) the Surface Disturbance South of the Ash Pits. IHSS 209 is located to the southeast of the site industrialized area, south of Woman Creek and approximately 1,000 ft southeast of Pond C-1 (IHSS 142-10) (Figure 1-5). This area was included as an IHSS because unknown activities took place in this area of shallow excavations and surface disturbances (DOE 1992a). IHSS 209 covers approximately 225,000 ft² (5.2 acres) and is located on a long narrow plateau bounded to the north, east, and south by a slope leading into the Woman Creek drainage. A dirt road transects this IHSS and loops near the eastern boundary. Three excavations are located within the boundary of this IHSS. Two depressions, which periodically retain water, are present near the northern and southwestern boundary of the IHSS.

A second surface disturbance, the Surface Disturbance West of IHSS 209, located approximately 1,500 ft west of IHSS 209, is also included in the OU 5 investigation. The area consists of several small disturbed areas in a somewhat symmetric arrangement (Figure 1-5). This disturbance covers an area of approximately 62,500 ft² (approximately 1.4 acres).

A third surface disturbance area, the Surface Disturbance South of the Ash Pits, is also being investigated under the OU 5 RFI/RI. This area is located 1,200 ft south of IHSS 133 and south of Woman Creek. This area consists of several former excavation areas (Figure 1-6). These surface disturbances were identified in aerial photographs taken between 1955 and 1988 (see EPA 1988a). There is still surface evidence of some of these disturbances. Two former excavations trend along northeast-southwest axes. Each excavation is approximately 30 ft wide by 400 ft long. A third area is located northeast of the parallel excavations and a fourth excavation (3 ft wide by approximately 2 ft deep) is located to the southwest. This excavation trends in a north-south direction across the plateau. An additional disturbed area is approximately 150 ft wide by 600 ft long and is located upslope (southwest) from the other disturbances.

It is not known what activity or activities may have taken place at IHSS 209 or at the other surface disturbances. However, the time period in which these areas were disturbed has been estimated from aerial photographs (EPA 1988a).

IHSS 209 first appears as a disturbed area seen in a 1955 aerial photograph (EPA 1988a). The ground was disturbed both west and east of the dirt road; however, no obvious features or equipment can be seen in the photo. By 1961, three excavations existed within this IHSS. The depression located near the southwestern boundary of this IHSS appears as a pond in 1980, 1983, and 1988 aerial photographs (EPA 1988a). A 1980 aerial photograph also reveals that the western half of the IHSS was beginning to revegetate. By 1988, the only recognizable features on or near this surface disturbance were the presence of the easternmost excavation and the pond located near the northern boundary of this IHSS (Figure 1.5).

The OU 5 Work Plan stated that the Surface Disturbance West of IHSS 209 appears to have been the location of a radio tower installation based on the geometry of the five disturbances at this site. This surface disturbance was observed in a 1955 aerial photograph and was still evident on photographs until about 1971, when the area started revegetating. A radio tower, however, was never viewed in the aerial photographs.

The east excavation area was the first area to be noted as active in the Surface Disturbance South of the Ash Pits. This was observed in a 1955 aerial photograph. The two parallel excavations became active prior to 1978, and they are visible in a 1978 photo (EPA 1988a). After 1983, the excavated areas started to revegetate. The west area, located approximately 400 ft southwest of the parallel excavations, became active prior to 1969 (EPA 1988a) and is now backfilled with large rocks. It is not known when these rocks were placed.

1.2.3 Other Investigations

To the extent they are applicable, the results of other site investigations were incorporated into this investigation. The scope of these other investigations is briefly described in the following sections:

1 2 3 1 Sitewide Geological Characterization

The Sitewide Geoscience Characterization Study was performed to compile and integrate all available information in order to develop a conceptual model of the geologic hydrogeologic and geochemical conditions at the site. The results of this study were documented in three reports: the Geologic Characterization Report (EG&G 1995a), the Hydrogeologic Characterization Report (EG&G 1995b), and the Groundwater Geochemistry Report (EG&G 1995c). The information presented in these reports was integrated into the discussions of the geology and hydrogeology of OU 5 presented in Chapter 3.0.

1 2 3 2 Sitewide Background Geochemical Characterization

The IAG required DOE to conduct a background study to establish representative background concentrations for various environmental media and to prepare background study reports periodically to document the results of this study. The 1993 Background Geochemical Characterization Report (BGCR) (DOE 1993a) presents the final results of this program and provides background data for surface water, sediments, groundwater, and borehole materials. These data are necessary to support RFI/RI, as well as RCRA interim measures (IMs) and CERCLA interim remedial actions (IRAs).

Analytical results for samples collected under the OU 5 RFI/RI were compared to the background data provided in the 1993 BGCR to determine whether or not the concentrations detected in OU 5 environmental media statistically exceeded those of background. Section 4.2 discusses the methodology used for this comparison.

1 2 3 3 Sitewide Surface Water Studies

Several studies have been or continue to be conducted pertaining to analyses of surface water, stream sediments, and pond sediments in the Woman Creek drainage and Ponds C 1 and C 2. The historical data for these media were evaluated in Technical Memorandum No. 1 (TM1) to assist in the design of a monitoring network for the OU 5 Phase I RFI/RI (DOE 1993b; also see Section 1.3.2.1) and were also used to determine the nature and extent of contamination within the Woman Creek drainage. The surface water and sediment investigations and associated results are described in detail in Appendix A and are discussed in the applicable sections of Chapters 2.0, 3.0, and 4.0.

1 2 3 4 Sitewide Groundwater Characterization

Prior to the OU 5 Phase I RFI/RI field investigations a total of 64 alluvial and bedrock wells existed in the vicinity of the Woman Creek drainage. Many of these wells have been or continue to be sampled as part of the sitewide groundwater monitoring program or for the investigation of other operable units (OUs) in the vicinity of OU 5. In addition, water levels are routinely measured in most of these wells. To the extent that the data from these wells met the quality requirements of the OU 5 RFI/RI, they were incorporated into this investigation. Appendix A provides a discussion of the available historical data from these wells. These data are also discussed where appropriate in the Chapters 2 0 3 0 and 4 0.

1 3 SUMMARY OF PHASE I RFI/RI WORK PLAN AND TECHNICAL MEMORANDA

The Phase I RFI/RI Work Plan for OU 5 presents a Field Sampling Plan (FSP) that defines a staged approach to investigating each IHSS. The Work Plan outlines the use of an Observational Approach to achieve the objectives of the RFI/RI. This technique provides for continually reassessing site conditions as additional data are obtained. Sampling plans for subsequent stages of investigation are formulated to build on existing information. These sampling plans are submitted as TMs to EPA and CDPHE for review prior to implementation. The OU 5 Work Plan contains nine TMs to be prepared to outline sampling plans for investigations of the OU 5 IHSSs and four TMs to be prepared to discuss Human Health Risk Assessment (HHRA) activities. A total of eleven TMs were prepared to describe planned field investigations during the implementation of the Phase I FSP at OU 5 (TMs 1 10 and 15). Three TMs were also prepared to describe specific phases of the HHRA. The following paragraphs summarize the FSP outlined by the OU 5 Work Plan and as amended by each of the TMs, as well as the scope of the TMs prepared for the HHRA.

1 4 ENVIRONMENTAL EVALUATION

The ecological risk assessment (ERA) portion of the baseline risk assessment was completed as part of an overall ERA conducted for the Walnut Creek and Woman Creek watershed. The complete ERA report for both watersheds is presented in Appendix N. An overview of the scope, approach, results, and conclusions for the Woman Creek watershed is presented in Section 7 0.

1 4 1 Phase I RFI/RI Work Plan for OU 5 (Woman Creek)

The OU 5 Work Plan identified site specific data needs based on preliminary identification of contaminants potentially present at each IHSS in addition to the data needs for the Phase I Baseline Risk Assessment and Environmental Evaluation. The FSP presented in the OU 5 Work Plan was based on these data needs and the requirements of the IAG between DOE, EPA, and CDPHE. The FSP for each IHSS required a combination of screening activities, sampling of soils, sediments, and surface water, and well installation and sampling. Table 1 1A is a matrix showing the IAG required tasks and how these tasks were implemented as defined in the OU 5 Work Plan, as amended by the TMs. Table 1 1B is a matrix showing TM15 required tasks and Document Modification Requests (DMRs) to the FSP.

Stage 1 activities at each IHSS consisted primarily of the review of existing data, such as the results of previous investigations, aerial photographs, and other historical documents. Stage 2 activities were screening activities that included radiological, geophysical, and soil gas surveys. Sampling of surface and subsurface soils were the predominant Stage 3 activities, and Stage 4 activities were primarily associated with groundwater investigations. If other activities were to be performed that did not fall into Stages 1 to 4, these activities were conducted under Stage 5. The site specific FSPs outlined in the OU 5 Work Plan are briefly summarized below.

IHSS 115 (Original Landfill) and IHSS 196 (Filter Backwash Pond) Review and screening activities specified for the Original Landfill, including the area of IHSS 196, consisted of a review of a gamma radiation survey completed in 1990, review of aerial photographs, and completion of a soil gas survey and geophysical surveys. Sampling identified included surface soil sampling, subsurface soil sampling in borings, and sediment and surface water sampling adjacent to the IHSS. The OU 5 Work Plan also specified that cone penetrometer testing (CPT) and Bengt Arne Tortensson (BAT®) sampling be performed, and wells be installed and sampled downgradient of the IHSS and in selected soil borings if plumes were encountered. Additionally, pipes protruding from the landfill were to be investigated and, if present, effluent sampled. The OU 5 Work Plan specified that TMs be prepared to present site specific FSPs for the soil gas survey, geophysical surveys, surface soil sampling, CPT, and monitoring well installation and sampling.

IHSS 133.1.6 (Ash Pits 1.4, Incinerator, and Concrete Wash Pad) Tasks specified by the FSP for the IHSS 133 sites included a review of aerial photographs and radiological and geophysical surveys to identify the extent of these IHSS sites. Sampling activities specified included surface soil sampling, subsurface soil sampling in borings, and installation and sampling of wells. The preparation of TMs was specified for the geophysical surveys, surface soil sampling, subsurface soil sampling, and monitoring well installation and sampling.

IHSS 142 (C Ponds) Activities specified by the FSP for IHSS 142.10 (C 1 Pond) and IHSS 142.11 (C 2 Pond) included a review of existing data collected by ongoing monitoring activities to assess potential overlap between the ongoing programs and the proposed OU 5 specific program. Contingent upon the results of the review of ongoing monitoring programs, the FSP also specified that surface water and sediment samples be collected from the ponds, Woman Creek, and the SID. In addition, monitoring wells were to be installed and sampled downgradient of each pond.

IHSS 209 (Surface Disturbance Southeast of Building 881), the Surface Disturbance West of IHSS 209, and the Surface Disturbance South of the Ash Pits Screening activities to be conducted at these sites included reviews of historical use information pertaining to these sites, visual inspections, and radiological surveys. Sampling activities specified by the FSP included surface soil sampling from the excavations present at each site, subsurface soil sampling from borings, and collection of sediment and/or surface water samples from each of the former pond areas at IHSS 209.

The FSP defined in the OU 5 Work Plan was amended by ten TMs at various stages during the field investigation. As is discussed in detail below, the scope of each TM does not agree in all cases with that described in the Work Plan. Because some of the activities to be described in the TMs specified by the Work Plan were similar, a single TM to address the same activity at more than one IHSS was prepared rather than preparing individual TMs for each IHSS. In addition, during the course of investigating each IHSS, it became apparent that the scope of subsequent Work Plan activities was not appropriate or adequate, thus necessitating the preparation of additional TMs. Similarly, the scope of several field investigation activities was clarified in letters submitted to EPA and CDPHE prior to implementing these activities. These letters were prepared for activities where the Work Plan did not require a TM, but additional definition or clarification of the scope of the activity was necessary. The scope of each TM and letter prepared during the implementation of the Phase I RFI/RI is summarized below.

1 4 2 Addenda to the Phase I RFI/RI Work Plan

1 4 2 1 Technical Memorandum 1 Revised Network Design (Surface Water and Sediment)

TM1 (DOE 1993b) documented the results of the review and assessment of ongoing surface water and sediment monitoring programs discussed under IHSS 142 above. Based upon this assessment of the ongoing programs, this TM provided an amended FSP for the collection and analysis of surface water and sediment samples from the C 1 and C 2 Ponds, Woman Creek and its tributaries, and the SID. In addition to addressing sampling activities for the ponds, this TM also addressed surface water and sediment sampling activities for all other OU 5 IHSSs. This TM also specified the installation of shallow well points along Woman Creek to augment ongoing groundwater/surface water interaction studies. The sampling and monitoring programs defined by this TM are summarized in Section 2 2 3 3.

1 4 2 2 Technical Memorandum 2 Surface Geophysical Surveys (Original Landfill and Ash Pits)

TM2 (DOE 1992b) described the approach for performing magnetic and electromagnetic (EM) surveys at IHSS 115 and the IHSS 133 sites. Due to similarities in these surveys at both IHSSs, one TM was prepared to describe these surveys rather than the two TMs identified in the Work Plan. This TM documented the results of the review of the 1990 radiological survey of IHSS 115 and reviews of existing information, including aerial photographs, for both IHSS 115 and the IHSS 133 sites. It also provided the details of the procedures to be followed for performing geophysical surveys at both IHSSs. The methodology for and results of these surveys are summarized in Sections 2 2 1 2 and 2 2 2 2.

1 4 2 3 Technical Memorandum 3 Surface-Soil Sampling Plan (Original Landfill)

TM3 (DOE 1993c) presented the sampling and analytical program for surface soils within IHSS 115. The sampling and analytical program defined in this TM consisted of collection of samples for analysis of radionuclides from anomalies identified by the 1990 radiological survey of IHSS 115 and collection of samples for analyses of chemicals and radionuclides from the disturbed area east of the landfill and from landfill cover material. The surface soil sampling program is summarized in Section 2 2 1 3.

1 4 2 4 Technical Memorandum 4 Surface Soil Sampling (Ash Pits Incinerator and Concrete Wash Pad)

TM4 (DOE 1993d) specified the sampling and analytical program for surface soils within the IHSS 133 sites. Similar to the program defined by TM3 for IHSS 115, the program defined by this TM included sample collection for analysis of radionuclides from anomalies identified by a radiological survey of these sites conducted as part of the OU 5 RFI/RI (see Section 2 5 2). It also involved sample collections for analyses of chemicals and radionuclides from areas believed to have been impacted by disposal operations at the IHSS 133 sites. Section 2 2 2 3 summarizes the methodology and results of this sampling program.

1 4 2 5 Technical Memorandum 5 Soil Gas Survey (Original Landfill)

Based on the results of other soil gas surveys conducted at the site and on the review of historical data and other screening activities at IHSS 115, it was determined that modification of the soil gas sampling plan proposed in the OU 5 Work Plan was necessary. TM5 (DOE 1993e) presented the results of the previous investigations at IHSS 115 and provided a revised sampling and analysis plan for the soil gas survey. The results of this survey are summarized in Section 2 2 1 2.

1 4 2 6 Technical Memorandum 6 Cone Penetrometer Testing (Original Landfill)

The OU 5 Work Plan proposed the performance of CPT and collection of groundwater samples with a BAT® (or equivalent) sampling device. The Work Plan specified that a TM be prepared that would define the specific procedures and locations for these activities. TM6 (DOE 1993f) specified the procedures and locations for CPT and provided a methodology for selecting locations for collection of groundwater samples contingent upon the results of the CPT and other previous and ongoing investigations at IHSS 115. Due to several advantages of this technique, this TM also specified the collection of groundwater samples from well points rather than with the BAT® sampling device. The implementation and results of these activities are summarized in Section 2 2 1 4.

1 4 2 7 Technical Memorandum 7 Soil Borehole Sampling (Ash Pits Incinerator and Concrete Wash Pad)

Soil borings to be drilled in the areas of the IHSS 133 sites were proposed by the OU 5 Work Plan. The Work Plan also specified that a TM be prepared to better define the locations of these borings based on the results of preceding investigations. TM7 (DOE 1993g) provided an FSP for the drilling and sampling of borings at the IHSS 133 sites. It also specified the collection of groundwater samples from within borings using the Hydropunch II or BAT® samplers where groundwater was present. The soil boring program and its results are summarized in Section 2 2 2 3.

1 4 2 8 Technical Memorandum 8 Groundwater Monitoring Well Installation (Original Landfill)

This TM provided a revised FSP for the installation and sampling of monitoring wells in the vicinity of IHSS 115 and IHSS 196 as prescribed by the OU 5 Work Plan. Subsequent to the preparation of the draft version of this TM, it was determined that the intent of the Work Plan was such that a TM was no longer required to define the locations of these monitoring wells. Therefore, a letter was prepared that described the plan for installing and sampling monitoring wells at IHSS 115. This letter is found in the appendices to TM15 (DOE 1994a). The groundwater monitoring program is summarized in Section 2 2 1 4.

1 4 2 9 Technical Memorandum 9 Groundwater Monitoring Well Installation (Ash Pits Incinerator and Concrete Wash Pad)

The installation of monitoring wells in the area of the IHSS 133 sites was proposed in the OU 5 Work Plan, and the Work Plan specified that a TM be prepared to define the locations of these wells. TM9 (DOE 1993h) provided a monitoring well installation and sampling program for the installation of wells based on the results of previous investigations in the IHSS 133 area. The implementation of this TM and the results of this investigation are summarized in Section 2 2 2 4.

1 4 2 10 Technical Memorandum 10 Surface Soil and Soil Borehole Sampling (IHSS 209 and Other Surface Disturbances)

TM10 (DOE 1993i) presented a FSP for the collection of surface and subsurface soils at IHSS 209 the Surface Disturbance West of IHSS 209 and the Surface Disturbance South of the Ash Pits The OU 5 Work Plan did not indicate that a TM would be required for these sampling programs but information obtained in previous stages of the investigation of these areas necessitated that the soil sampling program described in the Work Plan be modified This information indicated that there was no evidence of waste disposal in these areas and the soil sampling programs were reduced in scope so as to only confirm the results of the preceding investigations The results of the implementation of TM10 are summarized in Section 2 2 4 3

1 4 2 11 Technical Memorandum 11 Chemicals of Concern

TM11 (DOE 1995a) identified the chemicals of concern (COCs) that were included in the HHRA to assess potential health risks from assumed exposure to the COCs detected in soil groundwater and other media sampled in OU 5 COCs are metals or radionuclides whose concentrations exceed background concentrations (or organic chemicals that are not naturally occurring) but that could pose a health risk under the assumed exposure conditions COCs are selected from all analytes detected in each medium using risk based and other screening methods that identify chemicals that would pose the greatest risk and therefore warrant inclusion in the HHRA COCs also provide the focus for fate and transport modeling and remedy selection Section 4 2 provides a discussion of the comparison of data for OU 5 sampling locations with background values and Section 6 2 discusses the selection of COCs

1 4 2 12 Technical Memorandum 12 Exposure Scenarios

TM 12 (DOE 1995b) was prepared to identify potentially complete exposure pathways and human receptors at OU 5 and if presents quantitative values for exposure parameters and equations for estimating central tendency (CT) and reasonable maximum exposures (RMEs) to be used in the HHRA The scenarios identified in TM12 are discussed in detail in Section 6 3

1 4 2 13 Technical Memorandum 13 Model Description

Fate and transport modeling was required to support the HHRA and the evaluation of potential remedial alternatives for the Feasibility Study (FS) at OU 5. TM13 (DOE 1994b) provided a description of the models selected to perform groundwater, surface water, and air modeling for OU 5. A Conceptual Site Model (CSM) of chemical release and transport to potential human receptors was presented in TM13. This CSM identifies the rationale for the selection of mathematical models that were used to estimate exposure point concentrations for the HHRA. The model selection process is summarized and the model results are detailed in Section 5.0.

1 4 2 14 Technical Memorandum 14 Toxicity

The OU 5 Work Plan also specified that a TM be prepared that identifies the toxicological information that would be used in the risk assessment. During the course of performing the OU 5 HHRA, however, it was determined that all necessary toxicological information for the identified COCs was available in the regulatory databases. Therefore, DOE, EPA, and CDPHE agreed that this TM would not be required.

1 4 2 15 Technical Memorandum 15 Amended Field Sampling Plan

Subsequent to completion of the field program specified in the OU 5 Work Plan, it was determined that additional data were required to fully describe the nature and extent of contamination associated with all of the OU 5 IHSSs and to provide the information necessary for the evaluation of potential remedial alternatives in the OU 5 FS. Rather than proceeding with a Phase II RFI/RI (as is the traditional approach outlined in the IAG), DOE, EPA, and CDPHE agreed to performing an additional stage of field investigations under the Phase I RFI/RI. Therefore, TM15 (DOE 1994a) was prepared to present the results obtained during the implementation of the OU 5 Work Plan, identify gaps in the data obtained during the Work Plan investigation, and to provide an amended Phase I FSP for obtaining the information necessary to fill those gaps.

1 5 REPORT ORGANIZATION

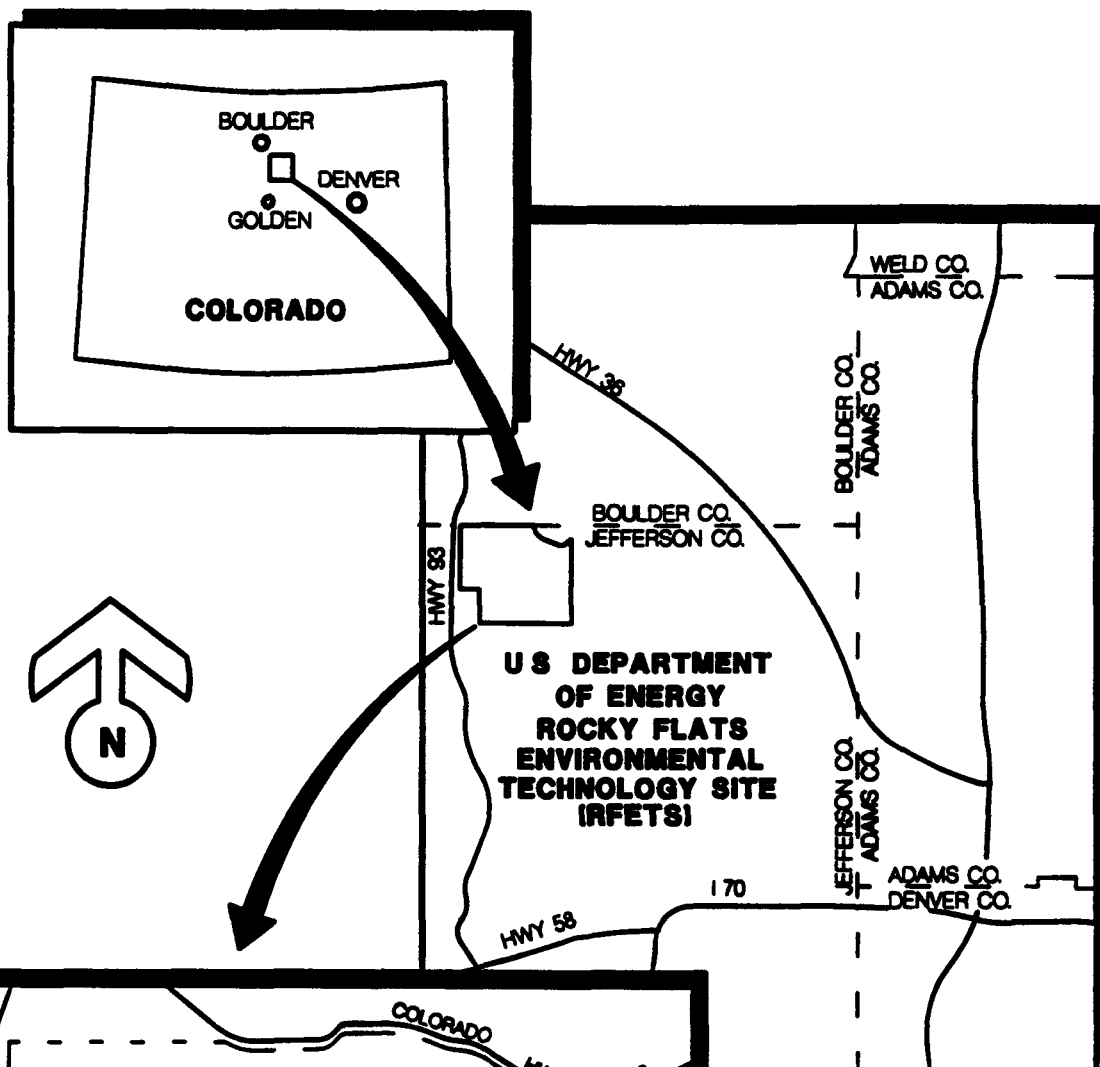
The following chapters of this report describe the field investigations performed at OU 5 and the results of those investigations provide a description of the nature and extent of contamination associated with each IHSS and to discuss the risk to human health and the environment posed by contamination at each IHSS Chapter 2 0 describes the stages of field investigation at each IHSS and presents the results of these investigations Those stages of the field investigation that were completed prior to the preparation of TM15 are only summarized in this report Detailed discussions of these investigations are presented in TM15 (DOE 1994a) The implementation of TM15 and the results of those activities are presented in detail for each IHSS in Chapter 2 0

Chapters 3 0 and 4 0 present discussions of the physical characteristics and nature and extent of contamination respectively at each IHSS These chapters draw information from all stages of the Phase I RFI/RI as well as information collected by other the site programs to provide a description of the physical setting and nature and extent of contamination at each IHSS This information is used to develop a conceptual understanding of the contamination associated with each IHSS and the potential for contaminant release and subsequent exposure to human receptors and/or the environment.

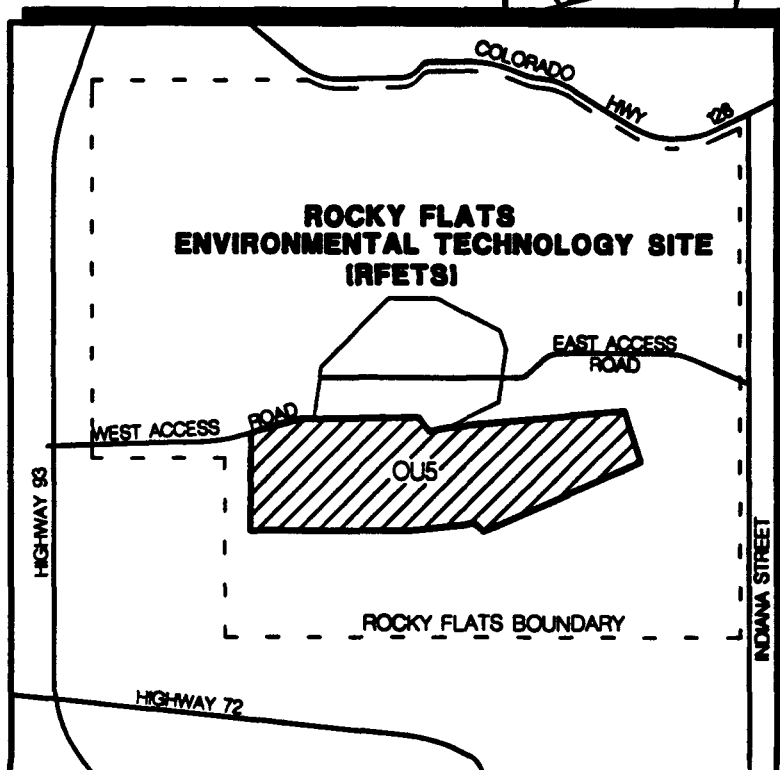
Chapter 5 0 discusses the results of contaminant fate and transport modeling in groundwater surfacewater and air This chapter provides a detailed discussion of the modeling process in each medium and of the results of the modeling particularly where applicable to the Baseline Risk Assessment (BRA) Chapters 6 0 and 7 0 provide discussions of the BRA The HHRA is discussed in detail in Chapter 6 0 and the Environmental Risk Assessment (ERA) is discussed in Chapter 7 0

A discussion of the process to be used for the evaluation of remedial alternatives is provided in Chapter 8 0 However presentation of the evaluation of remedial alternatives will be completed under the CMS/FS process Chapter 9 0 discusses the preliminary identification of data gaps and Chapter 10 0 provides a summary and conclusions of the Phase I RFI/RI

Appendix A the Hydrologic Data Summary Report, provides a detailed evaluation of surface water stream sediment pond sediment and groundwater data obtained from the sitewide and historical programs discussed in Section 1 2 3 and the data for these media obtained from the OU 5 Phase I RFI/RI This appendix was issued under separate cover previously The remaining Appendices B through N provide supporting data for the discussions provided in Chapters 2 0 through 7 0



Approximate Scale: 1 = 5 Miles



Approximate Scale: 1 = 1 Mile

Drawn	NM 8/1/95
Checked	729 8/1/95
Approved	
Date	
Date	

FILE OU5-1-1 DWG

GENERAL LOCATION OF RFETS

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 1-1

TABLE 1 1A MATRIX OF OUS RFI/RI FSP REQUIREMENTS FROM IAG WORK PLAN AND TECHNICAL MEMORANDA

IHSS	ACTIVITY	IAG		WORK PLAN		MODIFIED BY TM		Comments
		TASK	Analytes ⁽¹⁾	TASK	Analytes ⁽¹⁾	TASK	Analytes ⁽¹⁾	
115 Original Landfill (OI F)	Rad Survey	FIDLER	N/A	HPGe Fall 90	N/A	Data reviewed in TM 2 FIDLER SURVEY over hot spots	N/A	
	Magnetometer	Not addressed	N/A	2490 points	N/A	Data reviewed in TM 2	N/A	
	1 M Survey	Not addressed	N/A	2490 points	N/A	Data reviewed in TM 2	N/A	
	Soil Gas (SG) Survey	Over OLF	Not addressed	Not Determined	28 33	TM 4 343 samples 10% resampled for a maximum of 27	28 33	
	Surficial Soil	Not addressed	Not addressed	2 per Rad Anomaly in OLF	Random 1-4 8 11 12x 21 Rad Anomalies 4	TM 3 Min 11 locations @ Hot Spots 3 Locations least of OLF & 51 Locations over OLF	Hot Spots 1 7 East of OLF 1 8 8y 11 16 21 over OLF 1 4 6 8 11 17 21	A total of 67 samples were collected along with 5 dups for a total of 72
	Soil Cores	1 per/50 SGS pls	Not addressed	1/15 SG Sam	not addressed	TM 5 Deleted p ogram	N/A	
	Soil Borings	If (+) SG results drill soil borings at locations which may have GW	1-4 6 7 8y 10 11x 14	3 per SG plume 1 at each of 2 ponds 6 Distributed Area	2 FT Grab 9 6Ft 1-4 11 12x SG Borings 9 12x	In Monitoring Well File	N/A	TM 8 Canceled/Replaced by two letters which specify number and location of samples
	Monitoring Wells	If GW is found in Soil Borings	1-4 6 7 8y 10 11x	3 wells	1 2 2x 3 3x 4 4x, 6x 7x 8 8y 9 11 36, 38	In Monitoring Well File	Not addressed see Work Plan	TM 8 Canceled/Replaced
	Alluvial Wells	3 Wells	2 2x, 3 3x, 6x 7 8y 10 11x, 37	4 wells	1 2 2x, 3 3x, 4 4x, 6x 7x 8 8y 9 11 36, 38	6 wells	Not addressed see Work Plan	
	Pipe Outfall	If water then sample quarterly	2 2x 3 3x 6x 7 8y 10 11x, 37	1 Sample from both pipes	1-4 1x-4x 6x 7x 8 8y 9 10 12x 36 38	Not addressed	N/A	
	Cone Penetrometer Testing (CPT)	Not addressed	n/a	To be determined in TM 6	N/A	TM 6 22 CPT points 15 well points GW samples taken from well points	Ground Water 1 7 10 12 18 27	BAT® Sampling replaced by Well Points

(1) See Page 6 for key to codes

TABLE 1 1A MATRIX OF OUS RFI/RI FSP REQUIREMENTS FROM IAG, WORK PLAN, AND TECHNICAL MEMORANDA

IHSS	ACTIVITY	IAG		WORK PLAN		MODIFIED BY TM		Comments
		TASK	Analytes ⁽¹⁾	TASK	Analytes ⁽¹⁾	TASK	Analytes ⁽¹⁾	
133 1 133 6 Ash Pits Incinerator and Concrete Wash Pad	Rad Survey	FIDLER	N/A	HPGe Survey	N/A	Reviewed in TM 2 FIDLER Survey over Hot Spots	N/A	Work Plan 100 / HPGe
	Soil Borings	Does not specify	1 2	Estimated 85 Soil Borings	1-4 8	TM 7 46 Total 28 Loc with exploratory boreholes	1 4 8	Coverage 17 Exploratory Boreholes and 1 HPGe Anomaly completed
	Groundwater sampled from Soil Borings if water encountered	Not addressed	N/A		N/A	TM 7 Maximum of 10 samples	1 4 8	Field Parameters pH S C DO Barometric Pressure
	Magnetometer	Not addressed	N/A	4864 points	N/A	Reviewed in TM 2	N/A	
	EM Survey	Not addressed	N/A	4864 points	N/A	Reviewed in TM 2	N/A	
	Surficial Soil	At hot spots	1 2	To be determined	Random 1-4 8 21 Rad Anomalies 1-4	TM 4 20 samples 8 previously sampled for environmental evaluation	1 4 8 21	
	Alluvial GW Wells	3 Locations	2 2x 3 3x 6x 7 8y 10 11x	3 Locations	1 4 1x-4x 6x 7x 8 9 11	TM 9 4 Locations	Soil Samples 1 4 8 GW Samples 1 2 8	Field Measurements pH S C Temp DO Bar Pressure

(1) See Page 6 for key to codes

TABLE 1 1A MATRIX OF OUS RFI/RI FSP REQUIREMENTS FROM IAG WORK PLAN AND TECHNICAL MEMORANDA

IHSS	ACTIVITY	IAG		WORK PLAN		MODIFIED BY TM		Comments
		TASK	Analytes (')	TASK	Analytes (')	TASK	Analytes (')	
142 10 11 C 1 and C 2 Ponds	Pond Surface Water	5 Locations at each pond	1 7 1x-4x 6 6x, 7x 8y 8z, 10 11x 38	5 Locations at each pond	1-4 1x-4x 5 6 7x 8 8y 9 11 38	TM 1 C 1 Field Parameters no field work in Pond C 2	Field Parameters Temp S C pH D O	NPDES data used for characterization of both ponds
	Pond Sediment	5 Locations at each pond	1 7 8y 10 11 38	5 Locations at each pond	1 5 8 9 11 12x 38	TM 1 3 Locations in each pond	5 8 9 11 37 38	These analy/ses only apply to the top 6 Note the maximum amount of sediment sampled was less than 6
	GW Wells	4 Wells	1-4 1x-4x 5 6 6x 7 7x 8y 10 11x 38	Min of 4	1 5 1x 4x 6x 7x 8 8y 9 11 37 38	Not address d	N/A	

(1) See Page 6 for key to codes

TABLE 1 1A MATRIX OF OUS RFI/RI FSP REQUIREMENTS FROM IAG WORK PLAN AND TECHNICAL MEMORANDA

IHSS	ACTIVITY	IAG		WORK PLAN		MODIFIED BY TM		Comments
		TASK	Analytics (1)	TASK	Analytics (1)	TASK	Analytics (1)	
209 Surface Disturbanc s	Rad Survey	Not addressed	N/A	FIDLER Survey	N/A	Not addressed	N/A	
	Soil in Sample in former ponds	Not Addressed	N/A	1 Location in each pond	1 4 8 9 11 12x	Not addresscd	N/A	
	SW if present in former ponds	Not addressed	N/A	1 Location in each pond	1 4 8 9 11	Not addressed	N/A	
	Surface Soil	Not addressed	N/A	191 Locations	1 4 8 9 11 21	TM 10 191 Locations	2 4 8 11 12x 13 15 17 21	
	Boreholes	Not addressed	N/A	19 Boreholes	2 ft Intervals 9 6 ft intervals 1 4 8 9 11 21	TM 10 4 Boreholes	2 ft Intervals 9 6 ft intervals 1 4 8 9 11	
	Soil in Small Depressions	Not addressed	N/A	Not determined	1 4 8 9 11 12x 21	TM 10	N/A	Include with Surface Soil Sampling in TM 10

(1) See Page 6 for key to codes

TABLE 1 1A MATRIX OF OUS RFI/RI FSP REQUIREMENTS FROM IAG, WORK PLAN, AND TECHNICAL MEMORANDA

IHSS	ACTIVITY	IAG		WORK PLAN		MODIFIED BY TM		Comments	
		TASK	Analytes ⁽¹⁾	TASK	Analytes ⁽¹⁾	TASK	Analytes ⁽¹⁾		
Stream Sampling Program									
115	Stream SW	Not Determined	2 2x 3 3x 6x, 7 8y 10 11x 37	6 Locations	1-4 1x-4x, 6x 7x 8 8y 9 11 12x 36	see TM 1 below	N/A	TM 1 specifies 4 synoptic	
	Stream Sed	Not Determined	2 3 8y 6 7,10,11x, 37	4 Locations	1-4 8 9 11 12x	see TM 1 below	N/A		
133	Seds Down stream of Ash Pits	Not Addressed	N/A		1 5 8 21 38	see TM 1 below	N/A		
142		28 Locations	1 7 8y 10 11x 38	12 Locations, and 18 from Site Wide	1 5 8 21 38	see TM 1 below	N/A		
TM 1 for all OUS	Stream Surface Water	N/A	N/A	N/A	N/A	14 Locations per TM 1 9 for storm e ents	1-4 2x-4x 6x 7x 8 8x 9 11 12x 36 39		
							9 11 12x	These analytes for base flow events only	
	Stream Sediments	N/A	N/A	N/A	N/A	9 Locations per TM1	1-4 8 21 38		All Locations
							5		SW027 SW024 Only
							39		Only Analyte collected at SED501 505 & 506

(1) See Page 6 for key to codes

TABLE 1 1A MATRIX OF OUS RF/RI FSP REQUIREMENTS FROM IAG, WORK PLAN AND TECHNICAL MEMORANDA

ANALYTE	Code	ANALYTE	Code
Gross A/B	1	COB	22
Filtered A/B	1x	Orthophosphate	23
U 233/234/235/238	2	NO ₃ /NO ₂ as N	24
Dissolved U 233/234/235/238	2x	Ra 226/228	25
Plutonium 239/240	3	TDS Cl SO ₄ CO ₃ HCO ₃	26
Dissolved Plutonium 239/240	3x	Cyanid	27
Americium 241	4	1,1,1 Trichloroethan (1,1,1)	28
Dissolved Americium 241	4x	Dichloromethane	29
Tritium	5	Benzene	30
Cesium 137	6	Carbon Tetrachloride (CCl ₄)	31
Dissolved Cesium 137	6x	Tetrachloroethene (PCE)	32
Strontium	7	Trichloroethene (1,1,1)	33
Dissolved Strontium	7x	Dissolved Anions TDS	36
TAI Metals	8	Chromium	37
Dissolved TAI Metals	8x	Nitrate	38
HSL Metals	8y	Micro/Acute Toxicity	39
Dissolved HSL Metals	8z		
TCL Volatiles	9		
HSL Volatiles	10		
TCL Semivolatiles	11		
HSL Semivolatiles	11x		
TCL Pesticides PCBs	12		
TCL Pesticides	12x		
Bulk Density	13		
Particle Size Analysis	14		
Specific Conductance	15		
Carbonate	16		
pH	17		
CLP Metals w/ Cs, Li, Sn, Mo, Si	18		
BNA	19		
TSS	20		
TOC	21		

TABLE 1 IB MATRIX OF OUS FSP REQUIREMENTS FROM TMIS

<p align="center">ORIGINAL SCOPE OF TM15 WORK PLAN AUGUST 1994</p>	<p align="center">94 DMR(1) ERM 0139 11/10/94 DEEP BEDROCK WELL LOCATIONS REVISED GEOTECHNICAL PROGRAM AND IHSS133 DRILLING</p>	<p align="center">94 DMR(1) ERM 0144 12/16/94 TEMPORARY FILL ROAD</p>	<p align="center">94 DMR(1) ERM 0146 12/21/94 TRIP BLANK QA/QC REQUIREMENTS</p>	<p align="center">94 DMR(1) ERM 0148 12/20/94 CONVERT GEOTECH BORINGS TO DEEP MONITORING WELL</p>
<p>GEOTECHNICAL PROGRAM. IHSS 115</p> <p>5 HSA BOREHOLES (one with a piezometer installed) 8 Kansas Sampler Boreholes (one with a piezometer installed) two piezometers to be checked for water levels monthly</p> <p>Install 3 deep bedrock monitoring wells at locations to be specified in a future letter</p>	<p>19 HSA BOREHOLES (up to 9 piezometers/monitoring wells installed) Addressed changes to the geotechnical sample parameters to be collected</p> <p>Piezometers/monitoring wells to have water levels checked monthly and sampled quarterly for one year for TCL VOCs SVOC Pesticides and PCBs TAL metals and radionuclides</p>	<p>Addressed access to boring locations by constructing a temporary fill road into IHSS 115</p>	<p>Addressed trip blank QC requirement of one VOC trip blank per groundwater VOC collection per day</p>	<p>Addressed EPA concerns regarding UHSU and LHSU interaction in the area of the former ponds (IHSS 196) Location also selected to evaluate possible inferred fault zone</p> <p>Converted the geotechnical boring to be located in the area of the former ponds into a deep bedrock monitoring well and revised the workplan to allow construction of a shallow UHSU well adjacent to the LHSU well</p> <p>The UHSU well to be constructed within a second geotechnical boring drilled in the area due to the historical landslide present and the need for additional geotechnical data</p>

TABLE 1 1B MATRIX OF OUS FSP REQUIREMENTS FROM TM15

ORIGINAL SCOPE OF TM15 WORK PLAN AUGUST 1994	95 DMR(1) ERM-0015 2/7/95 MODIFY GEOTECH LOCATIONS CONVERT GEOTECH BORINGS TO DEEP WELL/IHSS 209 SOIL SAMPLING	95 DMR(1) ERM 0022 2/10/95 ADD ONE SHALLOW LHSU WELL IN IHSS 115	95 DMR(1) ERM 0151 4/5/95 DELETE PESTICIDES AND PCBs FROM GROUNDWATER ANALYTE LIST	TM15 WORK COMPLETED
GEOTECHNICAL PROGRAM. IHSS 115 5 HSA BOREHOLES (one with a piezometer installed) 8 Kansas Sampler Boreholes (one with a piezometer installed) two piezometers to be checked for water levels monthly Install 3 deep bedrock monitoring wells at locations to be specified in a future letter	Address FS team proposed changes to remaining geotech boring locations Convert locations at western end of temporary fill road to a fifth deep bedrock monitoring well on the basis of the results of the LHSU well 71194 Location selected to evaluate possible inferred fault zone Attempt to collect Shelby tube sample of slide plane at 4 ft in shallow UHSU well offset	Address upper water bearing interval observed in geotech/fifth deep well at west end of temp road also try and collect shelly tube sample of slide plane at 4 previous attempt did not succeed		Completed 20 geotechnical borings 8 converted to monitoring wells and three for surface casings for three deep bedrock monitoring wells in IHSS 115 Completed the location adjacent to IHSS 196 one UHSU well (59794) and one LHSU well (71194) Located at west end of temporary fill road completed with one UHSU well (58394) and two LHSU wells (57194 deep LHSU and 71494 shallow LHSU)

TABLE 1 1B MATRIX OF OUS FSP REQUIREMENTS FROM TM15

<p align="center">ORIGINAL SCOPE OF TM15 WORK PLAN AUGUST 1994</p>	<p align="center">94 DMR(1) ERM 0139 11/10/94 DEEP BEDROCK WELL LOCATIONS REVISED GEOTECHNICAL PROGRAM AND IHSS133 DRILLING</p>	<p align="center">94 DMR(1) ERM 0144 12/16/94 TEMPORARY FILL ROAD</p>	<p align="center">94 DMR(1) ERM-0146 12/21/94 TRIP BLANK QA/QC REQUIREMENTS</p>	<p align="center">94 DMR(1) ERM 0148 12/20/94 CONVERT GEOTECH BORINGS TO DEEP MONITORING WELL</p>
<p align="center">GROUNDWATER INVESTIGATION, IHSS 115</p> <p>Install and sample 5 miniwells Sample quarterly for TCL VOC s SVOCs Pesticides and PCBs TAL metals and radionuclides</p>	<p>Three borehole/deep bedrock monitoring well locations are addressed Deep wells are to have water levels monitored and water quality samples collected quarterly for one year for TCL VOCs SVOCs Pesticides and PCB s TAL metal and r dionuclides Locations selected as closure/ compliance monitoring points and to collect subsurface data for the evaluation of a possible inferred fault in IHSS 115</p>			
<p>Measure 46 water levels monthly Sample existing well points/miniwells quarterly for TCL VOCs SVOCs Pesticides and PCBs TAL metals and radionuclides Installed three piezometers to characterize bedrock surface Perform one aquifer test</p>				

TABLE 1 IB MATRIX OF OUS FSP REQUIREMENTS FROM TM15

<p align="center">ORIGINAL SCOPE OF TM15 WORK PLAN AUGUST 1994</p>	<p align="center">95 DMR(1) ERM 0015 2/7/95 MODIFY GEOTECH LOCATIONS CONVERT GEOTECH BORINGS TO DEEP WELL/IHSS 209 SOIL SAMPLING</p>	<p align="center">95 DMR(1) ERM-0022 2/10/95 ADD ONE SHALLOW LHSU WELL IN IHSS 115</p>	<p align="center">95 DMR(1) ERM 0151 4/5/95 DELETE PESTICIDES AND PCBs FROM GROUNDWATER ANALYTE LIST</p>	<p align="center">TM15 WORK COMPLETED</p>
<p align="center">GROUNDWATER INVESTIGATION, IHSS 115</p> <p>Install and sample 5 miniwells Sample quarterly for TCL VOC's SVOCs Pesticides and PCBs TAL metals and radionuclides</p>	<p>Deleted tritium TOC and COD from groundwater analyte list</p>		<p>Delete Pesticides and PCBs from Groundwater Analyte List to conform to OUS Work Plan</p>	<p>Completed 3 LHSU bedrock monitoring wells converted three geotechnical borings to three LHSU wells installed 8 miniwells Completed first and second quarter groundwater sampling Collected No through June water samples</p>
<p>Measure 46 water levels monthly Sample existing well points/miniwells quarterly for TCL VOCs SVOCs Pesticides and PCBs TAL metals and radionuclides Installed three piezometers to characterize bedrock surface Perform one aquifer test</p>				

TABLE 1 IB MATRIX OF OUS FSP REQUIREMENTS FROM TMIS

ORIGINAL SCOPE OF TM15 WORK PLAN AUGUST 1994	94 DMR(1) ERM 0139 11/10/94 DEEP BEDROCK WELL LOCATIONS REVISED GEOTECHNICAL PROGRAM AND IHSS133 DRILLING	94 DMR(1) ERM 0144 12/16/94 TEMPORARY FILL ROAD	94 DMR(1) ERM 0146 12/21/94 TRIP BLANK QA/QC REQUIREMENTS	94 DMR(1) ERM 0148 12/20/94 CONVERT GEOTECH BORINGS TO DEEP MONITORING WELL
ASH PITS, IHSS 133 Additional work to characterize TDEM anomalies to be proposed in a future letter based on visual survey Seven Kansas Sampler soil borings collection of one groundwater sample from borehole (location to be determined)	Addressed collection of soil sample for solidification treatability study			
GROUNDWATER INVESTIGATION, IHSS 133 Install 9 miniwells Measure monthly water levels Sample piezometers quarterly for TAL metals SVOC Pesticides and PCB s and radionuclides Perform one aquifer test				
HPGe SURVEY, IHSS 209 AND OTHER SURFACE DIST. Perform HPGe survey perform FIDLER Survey collect surface soil samples on basis of FIDLER Survey results				

TABLE 1 1B MATRIX OF OUS FSP REQUIREMENTS FROM TM15

<p align="center">ORIGINAL SCOPE OF TM15 WORK PLAN AUGUST 1994</p>	<p align="center">95 DMR(1) ERM 0015 2/7/95 MODIFY GEOTECH LOCATIONS CONVERT GEOTECH BORINGS TO DEEP WELL/IHSS 209 SOIL SAMPLING</p>	<p align="center">95 DMR(1) ERM-0022 2/10/95 ADD ONE SHALLOW LHSU WELL IN IHSS 115</p>	<p align="center">95 DMR(1) ERM-0151 4/5/95 DELETE PESTICIDES AND PCBs FROM GROUNDWATER ANALYTE LIST</p>	<p align="center">TM15 WORK COMPLETED</p>
<p align="center">ASH PTS. IHSS 133</p> <p>Additional work to characterize TDEM anomalies to be proposed in a future letter based on visual survey Seven Kansas Sampler soil borings collection of one groundwater sample from borehole (location to be determined)</p>	<p>Addresses one additional boring in TDEM anomaly west side of IHSS 133</p>			<p>Completed original 7 plus 3 Kansas Sampler borings two borings mislocated one converted to miniwell Two borings were drilled to replace mislocated borings Collected 25 real 6 rinse and 1 dup sample</p>
<p align="center">GROUNDWATER INVESTIGATION. IHSS 133</p> <p>Install 9 miniwells Measure monthly water levels Sample piezometers quarterly for TAL metals SVOC Pesticides and PCB s and radionuclides Perform one aquifer test</p>				<p>Installed 9 miniwells completed 1st and 2nd quarter groundwater sampling collected Nov through June water levels collected 11 moisture content samples Collected rinse from 55594 for analysis Did not collect a sample from 57894.</p>
<p align="center">HPGe SURVEY. IHSS 209 AND OTHER SURFACE DIST.</p> <p>Perform HPGe survey perform FIDLER Survey collect surface soil samples on basis of FIDLER Survey results</p>	<p>Provided results of HPGe and FIDLER Surveys Proposed 8 surface soil sample locations</p>			<p>Completed HPGe Survey of 24 points completed FIDLER survey of 24 points Collected 8 surface soil samples and 2 QC samples to verify HPGe and FIDLER survey results</p>

(1) DMR = Document
Modification Request

2 0 OU 5 FIELD OPERATIONS AND INVESTIGATIONS

This chapter discusses the methods and results of the field investigations performed under the Phase I RFI/RI of OU 5. As discussed in Chapter 1 0, the performance and results of the field investigations outlined in the OU 5 Work Plan (DOE 1992a) are described in detail in TM15 (DOE 1994a). The FSP was implemented in stages (Figure 2 18): Historical Review, Screening Level Surveys, Intrusive Sampling, and Well Installation and Groundwater Sampling. These investigations are summarized briefly in this chapter.

2 1 FIELD INVESTIGATION PROCEDURES

All field investigations conducted during the OU 5 Phase I RFI/RI were performed in accordance with the applicable RFETS Standard Operating Procedures (SOPs). More specifically, the procedures followed are those contained in the following volumes of the Environmental Management Division Operating Procedures Manual (5 21000 OPS):

- Volume I: Field Operations (5 21000 OPS FO) (EG&G 1992a)
- Volume II: Groundwater (5 21000 OPS GW) (EG&G 1992b)
- Volume III: Geotechnical (5 21000 OPS GT) (EG&G 1992c) and
- Volume IV: Surface Water (5 21000 OPS SW) (EG&G 1992d)

During the course of this project, several Document Modification Requests (DMRs, formerly known as Document Change Notices (DCNs)) were prepared to modify the existing procedures for specific application to the OU 5 sites.

2 2 PHASE I RFI/RI FIELD INVESTIGATION

This section provides a summary of the work conducted during implementation of the FSP defined by the OU 5 Work Plan (DOE 1992a) and as amended by several TMs during various stages of the field investigation. Work conducted prior to January 1994 is discussed in detail in TM15 (DOE 1994a), and a summary of that work is provided in this section. Results of additional work proposed and outlined in TM15 are discussed in more detail herein. The objectives of the Phase I RFI/RI were to

- Characterize the physical and hydrogeological setting of the IHSSs
- Assess the presence or absence of contamination at the IHSSs
- Characterize the nature and extent of contamination at the IHSSs if present
- Determine contamination migration rate and transport characteristics
- Support the Phase I Human and Environmental Risk Assessment, and
- Provide a basis for the Feasibility Study if required

Preliminary evaluation of data collected during the first phase of work consisted of comparisons with background upper tolerance limits (UTLs) presented in the BGCR (DOE 1993a). However, those UTLs were calculated with outliers being excluded (see Appendix E of DOE 1993a). Comparisons with those UTLs were performed and documented in TM15. That step was an initial one, and as the project has progressed, the data cleanup process has evolved, as have the evaluation processes. Since the preliminary evaluations, background UTLs have been recalculated without excluding outliers for both lognormal and normal distributions. This was done so that site data and background data were treated similarly for the risk assessment. Therefore, calculated values of background UTLs have changed since TM15 was finalized, which has resulted in comparisons of site data to two sets of background UTLs through time. As a consequence, this section is primarily a summary of the work completed and the analytical results of that work are discussed in general terms. However, where background UTLs are referenced in this section, the values presented in Appendix C of the BGCR values are used. Analytical data are discussed in additional detail in Chapter 4.0 Nature and Extent of Contamination.

The discussions of analytical data provided in the following sections reference a series of tables (Tables 2.3 through 2.11) that summarize the data collected during all stages of this investigation. The data presented in these tables were generally organized so that the data generated by the investigation specified by the OU 5 Work Plan (DOE 1992a) were provided for comparison to data generated by the investigation outlined in TM15 (DOE 1994a). As noted previously, the value substituted for nondetects in those data sets with relatively high (>50%) non-detect rates will strongly affect the calculated value of the apparent mean. Both the data analyst and the reader should keep in mind the uncertainty of statistical parameters calculated for any data set containing a high proportion of nondetect data. In the case of TM15, those constituents (metals, in particular) detected at relatively low to very low frequencies (<50% to <20% detects) tend to have mean concentrations that are artificially higher than those reported for pre-TM15 data. This apparent increase in mean values is the result of higher values substituted for nondetects.

In these cases the range of detected concentrations (reported in Tables 2 3 to 2 10) gives a better indication of the comparability of metal concentrations in TM15 and pre TM15 samples In these cases the range of detected concentrations reported on Tables 2 3 through 2 10 gave a better indication of whether the samples collected under TM15 contain similar concentrations to the pre TM15 samples

The data generated by the OU 5 Work Plan field investigation were used for the HHRA (Chapter 6 0) Therefore a comparison of the data generated under the TM15 investigation to the data used for the HHRA was necessary to evaluate any potential impacts to the conclusions of the HHRA that result from the collection of additional data A discussion of the potential impacts is provided in Section 2 3

2 2 1 IHSS 115 (Original Landfill) and IHSS 196 (Filter Backwash Pond)

Volume II of TM15 (DOE 1994a) provides detailed discussions of the methodology for and results of the Phase I investigation conducted at IHSSs 115 and 196 (IHSS 115/196) prior to implementation of work outlined in Volume I of TM15 (DOE 1994a) A summary of the information related to IHSS 115/196 and presented in Volume II of TM15 (DOE 1994a) is also presented in this section, along with a discussion of the results of implementation of the activities proposed in TM15 Figure 1 2 shows the relation of these IHSSs to RFETS Figure 2 1 is a larger scale map of the IHSS 115/196 area showing locations sampled prior to the implementation of TM15

2 2 1 1 Stage 1

Stage 1 activities conducted for IHSS 115/196 included reviewing vertical aerial photographs from the Aerial Photographic Analysis Comparison Report (EPA 1988a) and a series of oblique aerial photographs obtained from the RFETS archives taken during the operation of the Original Landfill Review of these aerial photographs resulted in some modifications to the dimensions and boundaries of IHSS 115/196 shown in the OU 5 Work Plan These modifications are discussed in detail in TM15 (DOE 1994a) and the current boundaries are shown on Figure 2 1

Stage 1 also involved review of the results of a gamma radiation survey conducted from October 25 1990 through December 8 1990 The survey was conducted using a 20 percent N type high purity germanium (HPGe) detector (DOE 1992a) These activities are discussed in detail in Section 2 4 1 of Volume II of

TM15 (DOE 1994a) This investigation found that radiation in the soil was contributed from potassium uranium and thorium. Review of these data indicated that activities from these radioisotopes were consistent with natural background activities. However, there were areas that exhibited elevated uranium 238 activity (hot spots). These hot spots were surveyed and marked with stakes for subsequent sampling activities (Section 2.2.1.3) and radiological surveys (Section 2.2.1.2).

2.2.1.2 Stage 2

Stage 2 activities at IHSS 115/196 consisted of geophysical and soil gas surveys as specified in the OU 5 Work Plan. In addition, a radiological survey with a Field Instrument for the Detection of Low Energy Radiation (FIDLER) was conducted to supplement the 1990 HPGe survey discussed in the previous section. Section 2.4.2 of Volume II of TM15 (DOE 1994a) discusses the Stage 2 activities in detail, and they are summarized in this section.

Geophysical Surveys Frequency-domain EM and magnetometer geophysical surveys were conducted in IHSS 115/196 from October through December 1992. Results of these surveys confirmed the known location of the Original Landfill and did not identify additional areas requiring investigation. Useful data could not be acquired beneath the power lines near the southern boundary of the Original Landfill due to the overriding EM interference produced by the lines.

Soil Gas Survey A real time soil gas survey was performed at IHSS 115/196 as proposed by the OU 5 Work Plan. The survey involved the collection and analysis of more than 300 soil gas samples. Anomalous readings encountered during the survey were further investigated by additional soil gas sampling. Plumes of volatile organic compounds (VOCs) identified by the soil gas survey were further assessed by the subsequent drilling of boreholes within the plumes and installation of groundwater monitoring wells downgradient of the plumes (Section 2.2.1.3). Results of the soil gas survey are discussed in detail in Section 2.4.2.2 of Volume II of TM15 (DOE 1994a). Briefly, the survey resulted in the identification of three areas of anomalous concentrations of 1,1,1-TCA, TCE, and PCE as shown on Figure 2.2.

In July 1993 (subsequent to completion of the soil gas survey) a small scale intrinsic air permeability study was conducted in and adjacent to IHSS 115/196. Evaluation of results of the intrinsic air permeability study are presented in Section 2.2.1.7.

FIDLER Surveys Several areas of IHSS 115/196 were surveyed with a FIDLER during March to June 1993. The purpose of this survey was to further characterize anomalies identified by the 1990 HPGe survey discussed in Section 2.2.1.1. Section 2.4.2.3 of Volume II of TM15 (DOE 1994a) details the performance and results of this survey.

The FIDLER surveys identified nine areas of anomalous radioactivity. Each of these areas has been posted as a radiologically controlled area (RCA). In areas where a piece of landfilled material was not identified as the source of the detected radiation, surface soil samples were collected to characterize the contamination present. Several pieces of radioactive material were removed from these areas on May 28, 1993 during an emergency removal action. This material was placed in an area designated for the storage of radioactive material. Measurements performed by EG&G Radiological Engineering indicated that the principal isotope present in these materials was uranium 238, although no quantification of the activity present was provided.

2.2.1.3 Stage 3

Stage 3 activities at IHSS 115/196 consisted of the collection and analysis of surface soil samples, drilling and sampling characterization boreholes, and further investigation of the soil gas anomalies. The results of Stage 3 activities are discussed in detail in Section 2.4.3 of Volume II of TM15 (DOE 1994a) and are summarized in this section.

Surface Soil Sampling Details of surface soil sampling at IHSS 115/196 are presented in Section 2.4.3.1 of Volume II of TM15 (DOE 1994a). Surface soil samples were collected at 66 locations in IHSS 115/196 (Figure 2.3). Analyses of surface soil samples identified samples with elevated concentrations of a limited number of metals, and several radionuclides were identified with activities that exceeded background activities. Pesticides, polychlorinated biphenyls (PCBs), and a wide variety of semi-volatile organic compounds (SVOCs) were also detected in several surface soil samples. Locations where the concentrations of both inorganic and organic compounds exceeding background concentrations were

detected are centered around the abandoned storm sewer outfall near the center of the Original Landfill. These findings may be the result of the surface soil being disturbed during installation of the outfall pipe.

Characterization Boreholes Eight boreholes were installed in IHSS 115/196 for subsurface characterization. The results of this work are discussed in detail in Section 2.4.3.2 of Volume II of TM15 (DOE 1994a). Briefly, metals analyses resulted in the detection of a limited number of metals at concentrations exceeding background UTLs. Radiological analyses identified several samples from the upper six feet with activities greater than background. Also, a variety of SVOCs, VOCs, pesticides, and PCBs were detected in samples from these boreholes.

Investigation of Soil Gas Anomalies Four boreholes were installed within the soil gas anomalies located adjacent to the former ponds (IHSS 196) and two 0.5 inch diameter wells (small diameter wells) (60993 and 61093) were installed within the anomaly near the center of the Original Landfill. Details of installation, sampling, and results of these activities are discussed in Section 2.4.3.3 of Volume II of TM15 (DOE 1994a).

Results of the analyses of the soil and groundwater samples collected from the boreholes and small diameter wells drilled within each soil gas anomaly confirmed the results of the soil gas survey. In addition, several metals and radionuclides were detected at concentrations exceeding background UTLs. Some pesticides, PCBs, and SVOCs were detected at these soil gas anomaly locations.

Surface Water and Sediment Sampling Results of surface water sampling are discussed in Section 2.2.3.3 because these sampling locations are all part of a single system.

2.2.1.4 Stage 4

Stage 4 activities conducted at IHSS 115/196 consisted of a CPT program and the investigation of groundwater quality through the use of wellpoints and monitoring wells. Implementation and results of these activities are discussed in detail in Section 2.4.4 of Volume II of TM15 (DOE 1994a) and are summarized in this section.

Cone Penetrometer Testing Specifics of the proposed CPT program are provided in TM6 (DOE 1993f). TM6 was prepared based upon evaluation of work conducted during Stages 1, 2, and 3. Section 2.4.4.1 of Volume II of TM15 (DOE 1994a) discusses the CPT program and its results in detail. Five significant topographic lows in the bedrock surface (or migration pathways) were identified by the CPT program. Water was found to be present in three of the topographic lows in the bedrock surface; the other two topographic lows in the bedrock were dry. Water was also found at two areas identified as topographic highs in the bedrock surface. Information provided by CPT was used to subsequently locate wellpoints (Section 2.2.1.4) and monitoring wells (Section 2.2.1.4).

Wellpoints Ten wellpoints were installed along the downgradient perimeter of IHSS 115/196 and are discussed in Section 2.4.4.2 of Volume II of TM15 (DOE 1994a). Elevated concentrations of a few metals, common anions, radionuclides, and water quality parameters were detected in unfiltered groundwater samples from within the footprint of the Original Landfill. VOCs including acetone, 1,1-dichloroethene (1,1 DCE), 1,2-dichloroethene (1,2 DCE), 1,1,1-TCA, TCE, and PCE were also detected in these samples.

Groundwater Investigation Details of five monitoring wells (59393, 59493, 59593, 59793, and 61293) and two boreholes (59193 and 59293) installed as part of the groundwater investigation of IHSS 115/196 are provided in Section 2.4.4.3 of Volume II of TM15 (DOE 1994a). The two boreholes were drilled at locations originally intended for monitoring wells, but groundwater was not encountered during drilling and the boreholes were plugged and abandoned.

Several metals were detected in subsurface soil samples collected from these wells and boreholes at concentrations exceeding background UTLs. Plutonium 239/240 was also detected at activities exceeding the background UTL. The PCB Aroclor 1254 was detected in a subsurface soil sample from well 59493, which was installed within IHSS 196. A variety of SVOCs and VOCs were also detected in several subsurface soil samples from these wells and boreholes.

Groundwater samples collected from these five wells have contained a number of metals at concentrations exceeding background UTLs. A few radionuclides were also detected at activities exceeding background UTLs. No pesticides or PCB constituents were detected in the groundwater samples collected in the IHSS 115/196 monitoring wells. A variety of SVOCs have been detected in groundwater samples, primarily

those from well 59493 which was installed within IHSS 196. Also the VOC methylene chloride, a common laboratory contaminant, was detected in one sample from well 59493.

Two of the five wells installed at IHSS 115/196 were selected for aquifer testing. A multiple well pumping test was performed at IHSS 196 in well 59493, and a single well slug test was performed in one well (59593) downgradient of IHSS 115. The multiple well test appears to have been successful; however, the slug test data indicated that the results at that location may not be representative of the formation characteristics but may instead represent the hydraulic conductivity of the filter pack (see Section 2.4.4.3 of Volume II of TM15 (DOE 1994a)). The slug test was repeated during the implementation of TM15 (DOE 1994a). Six of the wells installed in IHSS 115/196 during the implementation of TM15 were tested as part of the 1995 Aquifer Testing Program (EG&G 1995). The results are discussed in Sections 2.2.1.7 and 3.8.1.

2.2.1.5 Stage 5 Investigation of Storm Sewer Pipelines

Stage 5 activities at IHSS 115/196 involved investigation of the storm sewer pipelines that protrude from the Original Landfill area. These activities are discussed in detail in Section 2.4.5 of Volume II of TM15 (DOE 1994a) and are summarized below.

Activities performed to investigate the storm sewer pipelines included collecting a one-time sample of the water discharging from the active pipeline and performing a video-camera survey of the storm sewer system to determine and/or verify the connections and source of the constant discharge from the system.

Analytical results of the single sample obtained during dry weather from the storm sewer outfall did not indicate elevated concentrations for radionuclides, metals, or organic constituents.

The video camera survey of the pipeline indicated that, for the most part, the storm sewer system had only small rocks and sediment along its invert. There were some slight groundwater inflows at joints and manholes, and an occasional 6-inch polyvinyl chloride (PVC) roof drain connection entering through the top portion of the pipe. However, a continuous dry weather discharge was seen entering the system through a 12-inch corrugated metal pipe (CMP) at a manhole from the Building 447 foundation underdrain system (Jacobs 1994). Another manhole had an intermittent high velocity inflow that entered the

manhole through a 6 inch PVC pipe located at the southeast corner of the manhole. This inflow appeared to be pumped into the manhole from a sump pump. Based on the location of the pipe, the flow was assumed to be coming from Building 440 or the evaporative cooling tower located along the west side of Building 440.

2 2 1 6 Ambient Air Monitoring

Data from the monitoring network known as the Radioactive Ambient Air Monitoring Program (RAAMP) and from three samplers installed specifically to monitor ambient radionuclide levels around OU 5 were analyzed to evaluate whether airborne releases are significant from IHSS 115/196. Information collected by health and safety (H&S) personnel during the implementation of field investigations was also reviewed. Section 2 5 5 of Volume II of TM15 (DOE 1994a) presents detailed discussions of this analysis. Briefly, the analysis concluded that the presence of multiple sources throughout the facility and the placement of the RAAMP samplers limits the specific applicability of RAAMP data to OU 5.

Examination of the special OU 5 sampler data indicated that the uranium 233/234 and uranium 235 results were within the same order of magnitude for both the sampler downwind of IHSS 115/196 and the sampler upwind of OU 5. The americium 241, plutonium 239/240, and uranium 238 average activities for the downwind sampler were one order of magnitude greater than the average activities of the upwind sampler.

Results of the H&S monitoring that was done during the field investigations of IHSS 115/196 provided a qualitative indication of potential air pathway risks attributable to this source. Elevated organic vapor readings were observed during investigations at only two borehole locations during drilling operations. During field investigation of high purity germanium (HPGe) anomalies B 7 and B 8 near the center of the Original Landfill, beta gamma monitoring registered 60 000 counts per minute (cpm) on one occasion and 10 000 to 80 000 cpm on another.

2 2 1 7 Implementation of TM15

Implementation of field work outlined in TM15 (DOE 1994a) for IHSS 115/196 began in September 1994. In summary, the work consisted of

- Evaluation of Intrinsic Air Permeability Tests
- Geotechnical Evaluation
- Groundwater Investigation and
- Air Programs and Wind Resuspension Investigation

Specific work elements and results of implementing the work are summarized in the following sections. The results of these investigations are presented in additional detail where applicable in Chapters 3.0 and 4.0 of this report.

Evaluation of Intrinsic Air Permeability Tests A small scale intrinsic air permeability study resulted in calculated permeabilities that were orders of magnitude greater than expected for clayey soils. Intrinsic air permeability was estimated by the method presented in *A Practical Approach to the Design, Operation and Monitoring of In Situ Soil Venting Systems* (Johnson *et al.* 1990). Two possible explanations for this discrepancy were that the soils at the test sites were not clayey or that short circuiting of the vapor flow path occurred during the test (e.g., gas flows from surface down along probe and into sampler). Because the test was conducted in the same manner as the soil gas survey, it is possible that short-circuiting occurred during the survey and that the observed soil gas concentrations are lower than those actually occurring in the subsurface formation.

To assess the likelihood of each explanation, recorded survey vacuum pressures were reviewed along with the borehole logs for nearby areas. In those locations where vacuum readings are not greater than background and the soil lithology is known to be of low permeability, short circuiting may have occurred. This situation may also be explained by fractures (e.g., desiccation cracks) or macropores (e.g., worm burrows, root channels). Analytical laboratory data for soils in those areas were also reviewed for correlation.

For each borehole, nearby soil gas survey locations were identified. For each borehole for which a log was available, the data for the soil gas vacuum versus time were analyzed as described in Johnson *et al.* (1990). Calculated values were then compared to values reported (Johnson *et al.* 1990) for similar types of soils as identified on the borehole logs at corresponding depths (see Table 2.1). In each case, the calculated permeability (k) values either concurred with the borehole logs or indicated a less permeable soil type. Therefore, it may be concluded that short circuiting did not occur at locations near boreholes.

Although most of the soil gas samples were collected by the hydraulic probing and purging system several soil gas survey locations were purged with a manual pump. This manual apparatus was not equipped to monitor vacuum levels. However, manual purging took more time than the hydraulic system. Therefore, the gradient of vacuum versus time was less likely to induce short circuiting.

For soil gas sample locations that are not near boreholes, there are no known lithologic data to which calculated k values may be compared. However, the vacuum readings for the entire soil gas survey were reviewed to evaluate occurrences that did not exceed background. Background vacuum (for the probe and tubing system in ambient air) was recorded at 3.5 inches Hg (mercury) during the intrinsic air permeability study. Data from the soil gas survey revealed the lowest 5 minute vacuum reading to be 4.1 inches Hg, a value 17 percent greater than background.

Because background vacuum levels were significantly exceeded at all locations of the soil gas survey where the hydraulic system was used, calculation-derived soil types generally concur with those described in borehole logs, and manual purging is unlikely to induce short circuiting, it was concluded that short circuiting did not occur during the soil gas survey at IHSS 115. Therefore, results of the soil gas survey were considered to be representative of actual field conditions.

Geotechnical Evaluation Section 3.1.2.2 in Volume I of TM15 (DOE 1994a) outlined a geotechnical program to evaluate the stability of the slopes along IHSS 115. The following two work elements were completed:

- Obtain subsurface geometry
- Collect subsurface soil samples to characterize geotechnical properties of subsurface materials

This section describes the methodology for obtaining subsurface data and the collection of geotechnical samples for analysis. Results of the geotechnical sample analysis including the final stability analysis will be presented in subsequent FS reports for OU 5.

The subsurface geometry was evaluated from existing data and from drilling 20 additional boreholes. Locations shown in Figure 2.4 were based on the overall visible width of the existing failures and the

accessibility Soil samples were collected in accordance with SOP GT 2 Drilling and Sampling Using Hollow Stem Auger Techniques Table 2 2 is a summary of borehole information for the TM15 field investigation including the geotechnical borehole program

To facilitate the access of the hollow stem auger drill rig to the geotechnical boreholes located in the central landslide area, a temporary fill road was constructed The temporary fill road was located between the well cluster for 58394 57194 and 71494 and boring 56894 as shown on Figures 2-4 and 3 16 The temporary fill road was placed using clean fill and without excavating the existing hillside

Core samples collected from the geotechnical boreholes were retained in core boxes and logged (Appendix B) Core samples were not submitted for environmental chemical analysis on the basis of the field screening results which indicated no contamination Described in TM15 if field screening results had indicated the potential for contaminants environmental samples would have been collected for analysis for OU 5 target analytes (Table 3 1 2 1 of Volume I of TM15 [DOE 1994a])

Composite samples were obtained from drill cuttings and analyzed for OU 5 target analytes (Table 3 1 2 1 of Volume I of TM15 [DOE 1994a]) These samples were collected to characterize the drummed cuttings in order to determine the proper method for disposal of the cuttings A summary of the data from these composite samples is included in Tables 2 3 through 2 5 This table and all other summary tables in this chapter provide an indication of the difference in concentrations for each constituent in samples collected during the TM15 field investigation and those collected during the investigation outlines in the OU 5 Work Plan (DOE 1992a) this information is provided to assist in evaluating whether the results of the TM15 field investigation would impact the results of the HHRA and ERA which were based on the data collected prior to the implementation of TM15 (see Section 6 0)

With the exception of thallium concentrations of metals in the composite samples were within the range of either the background or pre TM15 data (Table 2 3) Thallium concentrations however are of the same magnitude as those detected in background and pre TM15 samples Detected radionuclide activities were within the ranges of the pre TM15 data (Table 2 4) As listed on Table 2 5 there were several organic compounds detected in these drum characterization samples However these organic compounds were primarily detected at concentrations below those detected in pre TM15 samples or the reporting limit or were common laboratory contaminants (e g acetone methylene chloride and the phthalates)

As part of the groundwater investigation 2 inch nominal diameter PVC piezometers were installed in nine geotechnical borehole locations (Figure 2 4) These piezometers were sampled for OU 5 target analytes (Table 3 1 2 1 of Volume I of TM15 (DOE 1994a) provided sufficient groundwater is present

Groundwater Investigation The groundwater investigation consisted of many activities including characterizing the thickness of alluvial material along Woman Creek and performing aquifer testing However the primary activity of the investigation centered around evaluating the presence and quality of groundwater Various installation types (wellpoints monitoring wells small diameter wells and piezometers) were utilized for these activities Small diameter wells are defined as ½ inch to 1 inch nominal diameter PVC installed in one to 1 5 inch nominal diameter boreholes These work elements and their results are presented in the following paragraphs

To further characterize the bedrock surface and thickness of the valley fill alluvium and colluvium along Woman Creek three small-diameter (nominal 1 inch) boreholes were advanced approximately two feet into weathered bedrock These three locations (58094 58194 and 58594) were located as close to the creek bed as practical (Figure 2 4) Soil samples (core) were collected continuously with a Kansas sampler Core was retained in core boxes and logged (see Appendix B) Because these locations are outside the IHSS boundary core was screened by field instruments and no environmental analytical samples were collected However one soil sample from each location was collected for soil moisture analysis Piezometers were installed in each borehole and subsequently developed

A single well pumping test was performed at well 59593 on May 11 1994 This test was performed when the static water level was higher than at the time of the previous slug test This allowed the hydrostratigraphic unit to be stressed more than in the previous test The results of this test are presented in Appendix D

In order to more completely evaluate the presence and quality of groundwater at and downgradient of IHSS 115/196 additional groundwater samples were obtained Because the presence and quantity of groundwater appeared to be limited this task consisted of three work elements

- Installation and development of nine upper hydrostratigraphic unit (UHSU) monitoring wells/piezometers five small diameter monitoring wells and six bedrock (LHSU) monitoring wells (Figures 2 4 and 3 16)

- Measurement of water levels in all wellpoints small-diameter wells piezometers and monitoring wells that are along or north of Woman Creek, south of the south Buffer Zone access road east of the western edge of IHSS 115 (approximately location CPT07393) and west of the eastern edge of IHSS 115 (approximately location CPT05393) on a monthly basis for one year and
- Collection and analysis of groundwater samples from any location that was downgradient of IHSS 115/196 provided water level measurements indicated the presence of a sufficient quantity of water

Installation of Groundwater Monitoring Locations Nine monitoring wells were installed in geotechnical boreholes where groundwater was or could possibly be encountered

Five small diameter wells (57994 58294 58494 58694 and 58794) were placed in bedrock lows that were identified during the CPT investigation (but where water was not detected during the CPT investigation) and in between existing wellpoints. Of the five small-diameter wells installed four were installed downgradient of IHSS 115/196 and one was installed in the surface disturbance east of the Original Landfill in the vicinity of borehole 50792. These small diameter wells were installed using a small hydraulic drill rig that does not produce soil cuttings. Composite soil samples were collected during drilling and submitted for analysis in accordance with the procedures outlined in TM7 (DOE 1993g). Analytical parameters for soil samples are specified in the OU 5 Work Plan and Table 3.1.2.1 of Volume I of TM15 (DOE 1994a). Twenty five composite samples were collected in this manner. In addition discrete samples were collected at 2 foot intervals for VOC analyses. Forty three VOC samples were obtained. Groundwater was subsequently observed at locations 57994 58494 and a one time measurement from 58794.

Table 2.3 presents summary statistics for metals data from subsurface soil samples obtained from boreholes where monitoring wells were installed. With the exception of selenium metals were detected at concentrations that were within the ranges of both the background and pre TM15 data. Selenium was detected at concentrations that exceeded the pre TM15 data but were within the range of background concentrations. Radionuclides were detected at activities that were within ranges of both background and pre TM15 data except americium 241 and plutonium 239/240 (Table 2.4). Activities of americium 241 and plutonium 239/240 were above those of background data, but were within the pre TM15 data. As listed on Table 2.5 there were several organic compounds detected in subsurface soil samples. However

these organic compounds were primarily detected at concentrations below those detected in pre TM15 samples or the reporting limit, or were common laboratory contaminants

Six bedrock monitoring wells (57194 57594 59394 59894 71194 and 71494) were installed at IHSS 115/196 Three (57194 71194 and 71494) were installed as part of the geotechnical program and the other three (57594 59394 and 59894) were installed specifically as part of the groundwater investigation Figure 2 4 shows the locations of the six bedrock monitoring wells around IHSS 115/196 Data from these monitoring wells have been used to evaluate the hydraulic interaction between the groundwater from the UHSU and the lower hydrostratigraphic unit (LHSU) (see Section 3 8 1)

Five of the six boreholes for bedrock wells were geophysically logged with neutron natural gamma, gamma gamma density EM induction and caliper tools On the basis of the recovered core and the geophysical logs construction details were selected Wells were constructed with 2 inch nominal diameter PVC casing with a 0 01 inch slotted screen Table 2 2 provides a summary of well completion details Bedrock well 59394 was originally scheduled to be installed in borehole 56694 but because 56694 caved in after being geophysically logged 59394 was drilled

Data acquired from all six bedrock monitoring wells were helpful in evaluating the presence of an inferred fault trace in the area of the Original Landfill as presented in section 3 8 1 2 of this report (also in Section 7 of EG&G (1995a) as inferred Fault 2) From the logs it appears that a marker bed is approximately 60 feet higher in location 71194 (west of the inferred fault) than in location 57194 (east of the inferred fault)

Bedrock wells 57194 and 71494 are adjacent to UHSU piezometer 58394 and well 71194 is adjacent to UHSU piezometer 59794 Two potential water bearing intervals were identified on the geophysical logs from well 57194 Well 71494 was installed adjacent to well 57194 to screen this separate water bearing interval Water levels at these locations indicate a downward vertical gradient On the basis of the analytical data, well 71494 appears to be screens across a weathered siltstone that is in apparent hydrolic connection with the UHSU No contaminants were observed in LHSU bedrock wells 57194 57594 or 59894 which had sufficient groundwater for sampling

Measurement of Groundwater Levels Water levels have been measured in all the monitoring wells wellpoints small diameter wells and piezometers located in the immediate vicinity of IHSS 115/196 including the small diameter wells along Woman Creek Appendix C presents a summary of these water

level measurements for the period September 1994 through August 1995. Groundwater contour maps and discussions of groundwater flow are presented in Section 3.8.1.3.

Collection and Analysis of Groundwater Samples Groundwater samples were obtained from any wellpoint or small diameter well that was downgradient of IHSS 115/196 if water level measurements indicated the presence of a sufficient quantity of water. The first quarter of groundwater samples was collected from December 21, 1994 to February 1, 1995 and the results are summarized in this section. Groundwater samples have been collected in the priority listed on Table 3.1.2.3.1 of Volume I of TM15 (DOE 1994a). Table 2.6 presents a summary of locations that were sampled and includes a checklist of requested analyses for each location. Tables 2.7 through 2.10 present summary statistics for data from groundwater samples obtained from wells around IHSS 115/196; these data are discussed below.

With the exception of thallium, total concentrations of metals in unfiltered samples are within the ranges of the background data or the pre TM15 data (Table 2.7). Thallium was detected in only one sample and it was detected at a similar, albeit greater, total concentration than both background and pre TM15 data. The constituents in unfiltered samples that were detected above either the background or pre TM15 data were detected at concentrations of similar magnitude to those data.

Concentration ranges of dissolved antimony, calcium, cobalt, and magnesium in groundwater samples exceeded ranges of both the background and pre TM15 data (Table 2.8). These concentrations were of similar magnitude to both the background and pre TM15 data. Concentrations of the remaining metals were within the ranges of the background or pre TM15 data for groundwater.

Activities of radionuclides in unfiltered groundwater samples at IHSS 115 were within the ranges of the background or pre TM15 data (Table 2.9). The radionuclides that had activities above either the background or pre TM15 data, had activities of similar magnitude to those data. With the exception of strontium 89/90, activities of dissolved radionuclides in groundwater samples were within the ranges of either the background or pre TM15 data (Table 2.9). The maximum activity of dissolved strontium 89/90 activity was 2.2 pCi/L as compared to 1.8 and 1.83 pCi/L for the background and pre TM15 data, respectively.

As listed on Table 2.10, there were 39 organic compounds detected in groundwater samples. Only 17 of these organic compounds were detected with a frequency of detection greater than 5 percent or in more

than three samples. Moreover, these organic compounds were primarily detected at concentrations below the contract required reporting limit.

Air Program and Wind Resuspension Investigation TM15 (DOE 1994a) described four air quality investigations: RAAMP special OU 5 ambient air samplers, an investigation of the wind resuspension potential, and an examination of the volatilization of soil gases. Operation of the RAAMP and OU 5 samplers has continued as part of the routine air quality monitoring programs at RFETS. TM15 (DOE 1994a) recommended the investigation into the volatilization of gases from OU 5 only if inhalation of volatile chemical species was determined to be an exposure pathway of concern. The inhalation of volatile organic compounds by current or future receptors has not been designated a complete exposure pathway (Chapter 6.0).

The remainder of this section discusses the supplemental field investigation into the wind resuspension potential for soils in OU 5, including presentation of the objectives, methods, and results of the study. Wind resuspension potentials for all the OU 5 IHSSs are discussed in Section 5.3.3.2.

2.2.2 IHSS 133 (Ash Pits, Incinerator, and Concrete Wash Pad)

Section 2.5 of Volume II of TM15 (DOE 1994a) provides a detailed discussion of the methodology for and results of the Phase I investigation conducted at the IHSS 133 group prior to implementation of TM15 (DOE 1994a). A summary of the information related to the IHSS 133 group and presented in Volume II of TM15 (DOE 1994a) is provided in this section, along with the results of implementation of the activities proposed in TM15. Figure 1.2 shows the relation of these IHSSs to RFETS. Figure 2.10 is a larger scale map of the IHSS 133 group showing locations sampled prior to the implementation of TM15.

2.2.2.1 Stage 1

Stage 1 activities at the 133 series IHSSs consisted of a review of historical aerial photographs to evaluate the extent of each disposal area. The results of this review are discussed in detail in Section 2.5.1 of Volume II of TM15 (DOE 1994a). In summary, IHSSs 133.1 and 133.3 were incorrectly located on maps prior to TM15 (DOE 1994a). The corrected locations are shown on Figure 2.10.

2 2 2 2 Stage 2

Stage 2 activities at the IHSS 133 sites included surface radiological and geophysical surveys as were specified by the OU 5 Work Plan. These activities are discussed in detail in Section 2 5 2 of Volume II of TM15 (DOE 1994a) and are summarized in the following paragraphs.

HPGe and FIDLER Surveys A radiological survey of the IHSS 133 area was initiated in the summer of 1992 using tripod mounted HPGe gamma ray detector instruments. This initial survey did not cover the entire IHSS 133 area and was followed by a second truck mounted HPGe survey to provide full coverage for each IHSS 133 site. In addition to the HPGe surveys, an instrument for the detection of low energy radiation (FIDLER) was used to focus sampling investigations within anomalies identified by the HPGe surveys.

The 1992 tripod mounted HPGe survey identified two areas of anomalous uranium 238 activity. One of these areas also displayed an elevated uranium 235 activity. The 1993 truck mounted survey corroborated the anomalous activity detected by the 1992 survey at one location but not at the other. The area identified by both HPGe surveys and the FIDLER survey was located immediately to the south and downslope of a small mound and depression. As shown on Figure 2 10, it was identified as an area approximately 35 ft wide and 76 ft long. The area has been posted as an RCA. No historical information regarding the origin of the mound and depression was found during investigation of this area, however borehole (58093) was drilled within the mound and encountered waste fill material (Section 2 2 3 2 in Volume II of TM15 [DOE 1994a]).

The anomaly associated with the 1992 tripod mounted HPGe survey that was not identified by the 1993 truck mounted survey was also not confirmed by the FIDLER survey. However, the FIDLER survey identified an anomalous area in the vicinity of this location.

Geophysical Surveys Frequency domain EM and magnetometer geophysical surveys were conducted in IHSS 133 from October through December 1992. In addition, a time-domain electromagnetic (TDEM) survey was conducted in IHSS 133 from January through February 1994. This TDEM survey was performed with a Geonics EM61 instrument, an instrument that was not available at the time the other

geophysical surveys were performed. The results of these surveys are discussed in detail in Section 2.5.2.2 in Volume II of TM15 (DOE 1994a).

The success of the frequency domain EM and magnetometer surveys in confirming the locations of the known ash pits or identifying unknown disposal sites was limited. The magnetic survey indicated an anomaly on the west side of the IHSS 133 area, with dimensions similar to those of the Ash Pits. The TDEM survey produced excellent results (Figure 2.11). This survey confirmed the locations of several pits previously identified and corroborated results of the borehole program (Section 2.2.2.3). The TDEM survey identified several anomalous areas that required further investigation as specified in Section 3.2.2.1 in Volume I of TM15 (DOE 1994a). The soil borehole program and the investigation of TDEM anomalies are discussed later in this report.

2.2.2.3 Stage 3

Stage 3 activities at the IHSS 133 sites included the collection of surface and subsurface soil samples in and around each IHSS. In addition, subsurface soil samples were collected from within the anomaly west of the IHSS 133 area identified by the magnetic survey. These activities are discussed in detail in Section 2.5.3 in Volume II of TM15 (DOE 1994a) and are summarized in this section.

Surface Soil Sampling The scope of work for the Stage 3 surface soil sampling program is described in TM4 (DOE 1993d). There were two phases of surface soil sampling:

- Characterize concentrations of metals and polynuclear aromatic hydrocarbons (PAHs) and confirm the results of the initial HPGe survey for radionuclides and
- Assess areas of elevated radioactivity that were identified after the second radiation survey was completed.

The surface soil sampling program is discussed in Section 2.5.3.1 of Volume II of TM15 (DOE 1994a). A total of 20 surface soil samples were collected at 20 locations in IHSS 133. Two sediment samples from seeps were also collected. Figure 2.10 shows the locations of the surface soil and seep sediment samples.

Elevated concentrations of zinc and silver were detected in only a few surface soil samples. Gross alpha, uranium 233/234 and uranium 238 were detected with activities exceeding background UTLs. The ratio of Uranium 235 to Uranium 238 indicated that the uranium present in surface soils is primarily depleted Uranium 238. None of the surface soil samples contained detectable concentrations of PAHs.

Zinc, antimony, and uranium 238 were detected at levels exceeding background UTLs in the seep sediment samples. The SVOC bis(2-ethylhexyl)phthalate was detected in one of the seep sediment samples. Neither seep sediment sample contained detectable concentrations of PAHs or VOCs.

Soil Boreholes Based on the results of the aerial photograph review and geophysical survey TM7 (DOE 1993g) proposed a soil borehole program that included drilling 28 boreholes and an undesignated number of shallow offset boreholes to be used in locating the Ash Pit(s). TM7 also proposed placing a borehole in the central location of any anomalous areas detected by the HPGe survey. Section 2.5.3.2 of Volume II of TM15 (DOE 1994a) discusses drilling, sampling, and results of the borehole program.

The completed soil boring program consisted of 53 boreholes (Figure 2.10).

- Two were placed in the mound north of a hot spot that was detected during the HPGe survey.
- Six were originally intended to be wells as part of the groundwater investigation; however, no groundwater was encountered and they were reclassified as boreholes.
- Seventeen were 10 to 12 foot deep offsets drilled to assist in locating the ash pits, and
- The remaining 28 boreholes were drilled in the locations specified in TM7 (DOE 1993g).

Soil samples were collected from all of the boreholes except the offsets, and four one-time groundwater samples were collected with a Hydropunch II sampling device during drilling from boreholes located within waste fill material that contained groundwater.

Soil and groundwater samples from boreholes that encountered waste fill material typically contained concentrations of metals and radionuclides that exceeded background UTLs. One sample contained some asbestos-containing material (ACM). Samples from boreholes that did not encounter waste material generally contained background levels of most constituents.

Investigation of Magnetic Anomaly A magnetic anomaly west of IHSS133 was investigated by drilling three boreholes(64493 64593 and 64693) along the long axis of the anomaly. No ash, waste material or groundwater were encountered in these boreholes. The unconsolidated material encountered appeared to be undisturbed colluvium. The analysis of soil samples collected from these boreholes indicated one barium result, one nickel result, and two plutonium 239/240 results greater than background UTLs.

Results of the drilling investigation of the magnetic anomaly west of IHSS133 indicated that there was no ash pit or other disposal unit in this area. This conclusion was further supported by the results of the TDEM survey which do not indicate the presence of any buried waste material in this area.

2 2 2 4 Stage 4

Stage 4 activities at the IHSS 133 sites consisted of the installation and sampling of groundwater monitoring wells and aquifer testing. The implementation and results of these activities are discussed in Section 2 5 4 of Volume II of TM15 (DOE 1994a) and are summarized in the following paragraphs.

Groundwater Investigation Nine locations were drilled in the IHSS 133 area, in the attempt to install the four proposed monitoring wells. Groundwater was encountered in only three of the nine locations. At the time TM15 was written, groundwater samples were being collected on a quarterly basis from only one well, 58793, which was producing sufficient quantities of groundwater. During the implementation of TM15, the other two wells, 59093 and 63093, were sampled. The results for these wells are included in the paragraphs that follow.

A few metals were detected at levels greater than background UTLs in one or two soil samples collected during drilling operations. Plutonium 239/240 was detected at concentrations exceeding the background UTL in three soil samples taken from these wells/boreholes.

Analyses of unfiltered samples from well 58793 detected 12 to 18 metals at concentrations exceeding background UTLs. Analyses of filtered portions of these same samples resulted in only manganese concentrations greater than the background UTL. This well has also contained above background activities of americium 241 and radium 226 in unfiltered samples.

A multiple well aquifer pumping test was unsuccessfully attempted at well 58793 (see Section 2 5 4 1 of Volume II of TM15 [DOE 1994a]) This test was repeated on May 10 1994 and the results are presented in Appendix D

2 2 2 5 Ambient Air Monitoring

Ambient air monitoring activities associated with the site characterization of IHSS 133 were similar to those conducted for the investigation of IHSS 115 (Section 2 2 1 6) These activities are discussed in Section 2 5 5 of Volume II of TM15 (DOE 1994a) and are summarized in the following paragraphs

The sampling results of the special OU 5 sampler situated downwind of IHSS 133 were similar to those for the IHSS 115 downwind sampler Examination of the data for the special OU 5 sampler indicated that the uranium 233/234 and uranium 235 results were within the same order of magnitude for both the sampler downwind of IHSS 133 and the sampler upwind of OU 5 These data seemed to indicate no discernible contributions to ambient levels of either uranium 233/234 or uranium 235 from IHSS 133 This same analysis appeared to apply also to plutonium 239/240 in the case of IHSS 133 Conversely the americium 241 and uranium 238 average activities for the downwind sampler were one order of magnitude greater than the average activities of the upwind sampler Contributions to ambient levels of americium 241 or uranium 238 by IHSS 133 appeared possible

No elevated organic vapor levels were observed during field investigations of IHSS 133 Elevated beta gamma readings exceeding a background of 250 cpm were encountered during borehole activities at four locations None of the results for ACM monitoring exceeded the American Conference of Governmental Industrial Hygienists (ACGIH) 8 hour Time Weighted Average occupational exposure limit of 2 fibers per cubic centimeter Results indicated that there were some potential for release of ACM during ground disturbance activities

2 2 2 6 Implementation of TM15

Implementation of field work outlined in TM15 (DOE 1994a) for the IHSS 133 area began in September of 1994 and was completed in August 1995 In summary the work consisted of

- Investigation of TDEM Anomalies
- Groundwater Investigation and
- Air Monitoring

Details of this additional work as well as the results are presented in the following subsections

Investigation of TDEM Anomalies The TDEM survey identified many geophysical anomalies throughout IHSS 133. A comprehensive visual inspection was performed over the entire geophysical survey grid to identify areas where surface metallic debris (i.e. cans and fence posts) was present. Nine boreholes (Figure 2.12) were drilled in four anomalous areas identified by the TDEM survey that could not be associated with surface debris. Specifically

- 56194 is located approximately 10 ft southeast of the concrete pad, in the north-central portion of IHSS 133
- 55194, 55294, 59994, and 60094 are located approximately 25 ft north of IHSS 133.6 and 25 ft south of the dirt road underneath the power lines (55194 was converted to a small-diameter well) (59994 and 60094 are located in the anomaly identified as TDEM 1)
- 55694 is at IHSS 133.4 in the center of the TDEM anomaly associated with the northern trench approximately midway between existing boreholes 55993 and 56093C and
- 55894, 55994, and 56094 were advanced on either end and in the center of the geophysical anomaly (TDEM 2) between IHSS 133.3 and IHSS 133.4 approximately 20 ft south of the dirt road beneath the power lines

A tenth borehole (58894) was drilled in an additional TDEM anomaly identified at TDEM survey coordinates 540 East and 180 South (Figure 2.12). The area is approximately 5 by 8 feet in area and described as a small oblong mound. Borehole 57294 was drilled in the northern half of IHSS 133.1 adjacent to boring 56893 to obtain bulk ash samples of the waste fill for treatability studies being conducted for the OU 5 FS. Table 2.2 includes a summary of these boreholes. Table 2.2B presents the treatability analytical results from the bulk ash sample from boring 57294. IHSS 133.2 Toxic characteristic leaching potential (TCLP) metal results from five composite subsamples from the bulk sample indicated only one result for lead at 18 mg/L greater than the Land Disposal Restrictions (LDRs) for metals.

Tables 2.3 through 2.5 presents summary statistics for subsurface soil samples obtained while investigating the TDEM anomalies at IHSS 133. Barium, beryllium, cadmium, cobalt, copper, lead

molybdenum selenium thallium, and zinc were detected in subsurface soil samples at concentrations which exceeded the ranges detected in background and pre TM15 data (Table 2 3) Typically the highest concentration detected was in sample BH00034AS from borehole 55994 drilled in TDEM 2 Concentrations of the remaining metals were within the ranges of either the background or pre TM15 data for subsurface soil samples

With the exception of plutonium 239/240 and uranium 233/234 activities of radionuclides in subsurface soil samples from boreholes within the TDEM anomalies were within the ranges of either the background or pre TM15 data (Table 2 4) The elevated activities of plutonium 239/240 and uranium 233/234 detected were of similar magnitude to the pre TM15 data.

Table 2 5 presents summary statistics for organic compounds that were detected in subsurface soil samples from TDEM anomalies in IHSS 133 The only organic compounds detected were the VOC/PCE and the SVOCs/benzoic acid bis(2 ethylhexyl)phthalate di n butyl phthalate and phenanthrene These five compounds were detected in only one sample at concentrations that were less than the maximum concentration detected in the pre TM15 samples

Groundwater Investigation Based on information from geologic logs of boreholes and monitoring wells in and around the IHSS 133 area, with regard to bedrock topography and degree of saturated soils there were several areas where insufficient data existed after completion of the FSP outlined in the OU 5 Work Plan (DOE 1992a) Consequently ten boreholes (55194 55394 55494 55594 55794 56294 56394 56494 56594 and 57894) were advanced and small-diameter piezometers installed at locations around IHSS 133 (Figure 2 12) Four (55494 55594 56294 and 56494) were installed downgradient of ash pits Five of these boreholes (55394 55794 56394 56594 and 57894) were located as close to the stream bed as possible Borehole 56394 could not be completed as a small-diameter piezometer therefore 71394 was drilled with an HSA drill rig and a well was installed These five locations were not installed as water quality monitoring wells rather they were piezometers whose only purpose is for collecting water levels Small diameter well 55194 was installed near TDEM 1 at the west end of IHSS 133 Subsurface soil samples (core) were collected continuously with a Kansas sampler (with the exception of 71394 which was a twin of borehole 56394) retained in core boxes and logged (see Appendix B) Because these locations were outside the IHSS boundaries core was only screened by field instruments No above background readings were obtained on any field instruments

Water levels were measured in all the monitoring wells wellpoints and piezometers that are along or north of Woman Creek, south of the West Access Road, east of the west perimeter road and west of the eastern extent of the IHSS 133 area from September 1994 through August 1995. These water level measurements are summarized in Appendix C.

Groundwater samples were obtained from any monitoring wells small-diameter well and wellpoints that were adjacent to or downgradient of an IHSS or TDEM anomaly (except the piezometers along Woman Creek because they were not constructed for sampling) if water level measurements indicated presence of a sufficient quantity of water. Specifically wells 58793 59093 63093 63693 63793 55394 and 56594 were sampled. Table 2.6 presents a checklist of which locations were sampled and for which analytical groups they were analyzed. Tables 2.7 through 2.10 present summary statistics for the analytical data from these groundwater samples. The results of these analyses are discussed below.

Concentrations of total metals were within the ranges of either the background or pre TM15 data (Table 2.7). Only aluminum beryllium, iron potassium silicon and vanadium were detected exceeding the background range. These concentrations from samples of unfiltered groundwater were of similar magnitude to both the background and pre TM15 data. Mean concentrations of metals in these groundwater samples were similar to those for the pre TM15 data.

Concentrations of dissolved metals were within the ranges of either the background or pre TM15 data (Table 2.8). Concentrations of dissolved nickel exceeded the dissolved groundwater background range but were detected with similar frequency and concentrations. Selenium was detected in one groundwater sample at a concentration that exceeded the pre TM15 data, but the concentration detected was well within the range of background concentrations.

With the exception of radium 226 activities of radionuclides in samples of unfiltered groundwater for IHSS 133 were within the range of both the background and pre TM15 data (Table 2.9). Radium 226 had an activity that exceeded the background range but those activities were within the pre TM15 range.

With the exception of cesium 137 activities of dissolved radionuclides in the recent groundwater data for IHSS 133 were within the range of both the background and pre TM15 data (Table 2.9). Dissolved cesium 137 had an activity that exceeded the pre TM15 range but the activities were within the background range.

Volatile organic compounds methylene chloride and acetone were detected in two groundwater samples from IHSS 133 (Table 2 10) Acetone was detected at a concentration marginally above the detection limit in one sample SVOCs bis(2-ethylhexyl)phthalate butyl benzyl phthalate di n butyl phthalate and di n-octyl phthalate were detected in one groundwater sample from IHSS 133 These four constituents were detected at concentrations below the contract required reporting limits and are common field or laboratory contaminants Four TICs (cyclohexane (DOT) dodecanoic acid hexadecanoic acid and octadecanoic acid) were also detected in groundwater samples from IHSS 133 These four constituents were detected at concentrations below contract required reporting limits

A visual survey to characterize where bedrock crops out in the stream channel along the length of Woman Creek downgradient of the IHSS 133 series area was conducted on October 14 1994 This information was used to revise the bedrock topography map and provided input to the hydrogeologic model The survey did not identify any locations where bedrock crops out in the stream channel

A pumping test was performed at 58793 while water levels were monitored in 63593 63693 and 63793 The test was conducted on May 10 1994 Data are presented in Appendix D The results of this test were comparable to those from the previous test reported in TM15 (DOE 1994a) Both tests were unsuccessful in obtaining the hydrogeologic characteristics of the water producing strata at this location

Air Monitoring TM15 (DOE 1994a) described four air-quality investigations RAAMP special OU 5 ambient air samplers an investigation of the wind resuspension potential and an examination of the volatilization of soil gases Operation of the RAAMP and OU 5 samplers has continued as part of the routine air quality monitoring programs at the Site The potential for resuspension of contaminated soil was not directly addressed in the investigation of IHSS 133 To make this evaluation required an estimation of the corrected threshold friction velocity of the soil The phased investigation procedures to acquire corrected threshold friction velocity data for IHSS 115 are applicable to IHSS 133 and are discussed in Section 2 2 1 7

Because any VOCs would have been destroyed during the incineration process volatile chemical species were not a concern in IHSS 133 Therefore no field work to measure the emission rates of volatile species was conducted for IHSS 133

2 2 3 IHSS 142 10 and 142 11 (C Ponds)

Section 2 6 of Volume II of TM15 (DOE 1994a) provides a detailed discussion of the methodology for and results of the Phase I investigation conducted at IHSS 142 10 (C 1 Pond) and 142 11 (C 2 Pond) prior to implementation of work outlined in TM15. A summary of the information presented in Volume II of TM15 is provided below along with the results of implementation of activities proposed in TM15. Figure 1 2 shows the relation of these IHSSs to RFETS. Figure 2 13 is a larger scale map of the IHSS 142 area.

2 2 3 1 Stage 1

Stage 1 activities consisted of evaluating the existing data. The results of Stage 1 evaluations were used to develop surface water and sediment sampling activities as presented in TM1 (DOE 1993b). The results of this evaluation are discussed in Section 2 6 1 of Volume II of TM15 (DOE 1994a) and are also presented in detail in TM1 (DOE 1993b).

2 2 3 2 Stage 2

There were no Stage 2 activities.

2 2 3 3 Stage 3

Stage 3 investigation activities at Ponds C 1 and C 2 consisted of additional surface water and sediment sampling and the installation and monitoring of wellpoints along Woman Creek and its tributaries. These activities are discussed in detail in Section 2 6 2 of Volume II of TM15 (DOE 1994a) the Hydrogeologic Data Summary Report (Appendix A) and are summarized in the following paragraphs.

Surface Water and Sediment Sampling This section presents a summary of surface water and sediment sampling along the Woman Creek drainage including Woman Creek the South Intercept Ditch the C Series Ponds and the pond like depressions in IHSS 209. These various sampling locations are discussed together rather than with their associated IHSS because they are all part of a single system. Volume II of TM15 (DOE 1994a) presents detailed discussions of the result of each sampling event by IHSS. Also the

results of the surface water and sediment sampling activities at Ponds C 1 and C 2 are detailed in Appendix A

Twenty eight surface water samples were collected from various locations in the Woman Creek drainage. Water samples were obtained during two base flow sampling events (November 1992 and March 1993) and three high flow sampling events (March and May 1993 and April 1994). Water sampling activities conducted at the ponds consisted of two HydroLab surveys to develop depth profiles of the surface water sediment interface at both ponds. In addition, surface water samples were collected from the pond like depressions at IHSS 209.

Analyses of the data from the two base flow and first high flow sampling events indicated that only a few samples contained some analytes at concentrations greater than those of background. This indicated that, in general, constituents were not seeping into the creek and were not being washed into the creek at rates sufficient to be detected at elevated concentrations.

A general conclusion regarding the ponds was that both thermal and chemical stratification of the C ponds was very weak to nonexistent during all months of the year. No concentrations exceeding background Upper Tolerance Limit (BUTLs) were noted for radionuclides, metals, or organic constituents associated with the samples from the pond like depressions.

Stream sediment samples were also collected during a one time sampling event at various locations in the Woman Creek drainage. One time sediment samples were also collected from both ponds. Sediment samples were collected from the pond like depressions at IHSS 209 when no water was present in them during the surface soil sampling discussed in Section 2.2.4.3.

Several constituents were detected at concentrations exceeding background UTLs in stream sediment samples from various locations in Woman Creek. Based upon the pond sediment concentrations and comparisons with background UTLs, mercury, barium, calcium, and zinc were detected at concentrations exceeding background.

Well Point Installation and Monitoring Thirty six wellpoints were installed along Woman Creek, as outlined in TM1 (DOE 1993b). The wellpoints were located to coincide with the Woman Creek channel gain/loss sites previously used to measure streamflows in Woman Creek by CSU and EG&G. The results

of the well point and gain/loss measurements are summarized in Section 3.4 and discussed in detail in Section 2.6.2.2 of Volume II of TM15 (DOE 1994a) and Appendix A.

2.2.3.4 Stage 4

Stage 4 activities at IHSSs 142.10 (Pond C 1) and 142.11 (Pond C 2) consisted of the installation and sampling of groundwater monitoring wells. Section 2.6.4 of Volume II of TM15 (DOE 1994a) discusses the results of these activities and they are summarized in the following text.

Groundwater Investigation Two monitoring wells were installed immediately downgradient of each dam at Ponds C 1 and C 2 to monitor the saturated alluvium (Figure 2.13). Wells 50092 and 51193 below Pond C 1 have been sampled on a quarterly basis when sufficient groundwater is present. The wells below Pond C 2 (50192 and 50292) have not produced sufficient water for sampling.

None of the soil samples collected from the wells contained target analyte list (TAL) metal concentrations exceeding background. Plutonium 239/240 and americium 241 were detected in soil samples and in composite samples from drums of cuttings that represented the upper 15 feet. None of the soil samples collected from the wells contained pesticides or PCBs. No SVOCs were detected in soil samples collected from any of the wells; however, tentatively identified compounds (TICs) were detected in soil samples from all four of the groundwater monitoring well boreholes. VOCs (acetone, methylene chloride, and toluene) were detected in soil samples collected from all four monitoring well boreholes.

Three groundwater samples collected from the wells below Pond C 1 had metal concentrations exceeding background UTLs. Most of the results that exceeded background UTLs were from unfiltered samples. Samples from these same wells also had radium 226 (total) and gross beta (dissolved) activities that exceeded background UTLs and detectable concentrations of SVOCs. Samples from the wells have also contained elevated concentrations of chloride and total suspended solids. None of the groundwater samples collected from these wells contained pesticides, PCBs, or VOCs.

A multiple well aquifer pumping test was successfully completed on well 51193 located below Pond C 1. Water levels were monitored in small-diameter wells 63293, 63393, and 63493. The resulting transmissivities ranged from 0.021 to 0.030 square ft per minute (DOE 1994a).

2 2 3 5 Implementation of TM15

No additional work at IHSSs 142 10 and 142 11 was proposed in TM15 (DOE 1994a)

2 2 4 IHSS 209 and Other Surface Disturbances

Section 2 7 of Volume II of TM15 (DOE 1994a) provides a detailed discussion of the methodology for and results of the Phase I investigation conducted at IHSS 209 the Surface Disturbance West of IHSS 209 and the Surface Disturbance South of the Ash Pits prior to implementation of work outlined in Volume I of TM15 (DOE 1994a) A summary of the information presented in Volume II of TM15 (DOE 1994a) is provided in this section along with the results of implementation of activities proposed in TM15 (DOE 1994a) Figure 1 2 shows the relation of these areas to the Site Figures 2 14 and 2 15 are larger scale maps of these areas

2 2 4 1 Stage 1

Aerial photographs and oblique photographs covering IHSS 209 and the two other surface disturbance areas were reviewed to assess the location and history of the surface disturbances The results of the aerial photograph review are discussed in detail in Section 2 7 1 of Volume II of TM15 (DOE 1994a) and are summarized below

Aerial photographs indicate that the vegetation and upper sediments had been stripped from IHSS 209 prior to 1955 and that prior to 1964 several pits had been opened within the site The review of the photographs subsequently resulted in both an extension of the overall length of the IHSS as compared to the dimensions shown on Figure 2 7 of the OU 5 Work Plan, and some adjustments to the locations of the pits that were shown on Figure 2 7 of the OU 5 Work Plan Specifically Stage 1 aerial photo review resulted in relocating the eight pits in the Surface Disturbance West of IHSS 209 approximately 250 ft to the north (Figure 2 14) Three additional pits were identified as a result of Stage 1 activities and confirmed during the Stage 2 field reconnaissance

The Surface Disturbance South of the Ash Pits is shown on Figure 2 15 and consists of an area of disturbed ground as well as an area that contains two open and two reclaimed pits The locations of the

reclaimed pits shown on Figure 2 15 have been corrected as a result of Stage 1 activities according to scaled locations from the aerial photographs and do not agree with the locations shown on Figure 2 6 of the OU 5 Work Plan (DOE 1992a)

2 2 4 2 Stage 2

Stage 2 activities at IHSS 209 and the other surface disturbances consisted of a visual inspection of each site to confirm the information obtained in Stage 1 and to evaluate if any debris or staining indicative of waste disposal are present Stage 2 also involved the performance of surface radiological surveys over each site The results of these activities are discussed in detail in Section 2 7 2 of Volume II of TM15 (DOE 1994a) and summarized in this section

Visual Inspection A visual inspection/site reconnaissance of IHSS 209 and the other surface disturbances was conducted on September 24 1992 The following paragraphs summarize the results of this inspection for each site The features described in these paragraphs are shown on Figures 2 14 and 2 15

IHSS 209 The pond southwest of the road near the center of the site was found to be dry with a basin at least 10 ft in depth The pits shown throughout the area are small shallow excavations that are still open or partially backfilled There was no evidence that these pits were ever used for the disposal of waste materials The Stage 2 field reconnaissance confirmed that no significant debris or staining exist to indicate that waste disposal had occurred It appears that the largest disturbance on the northeast end of the area may have been used as a source of gravel prior to 1955

Surface Disturbance West of IHSS 209 Stage 2 field reconnaissance confirmed the locations of all eight pits identified on aerial photographs The largest pit is located near the center of the site and was found to be several feet deep The largest pit was dry at the time of the inspection but holds water during periods of wet weather or snow melt and is now the host to a fairly large cottonwood tree indicating that the site has been open for a long period of time The remaining pits are small and shallow appear to be capable of holding water during wet weather and are heavily revegetated There is no indication that any of these pits had ever been used as disposal sites It is unclear what use the pits may have served The OU 5 Work Plan speculated that these pits may have been part of a planned radio tower installation However the

configuration of these pits and the fact that the pits are located on a hillside rather than the top of the hill indicate that this may not be the case

Surface Disturbance South of the Ash Pits The field reconnaissance of the Surface Disturbance South of the Ash Pits confirmed the existence of the features noted in the OU 5 Work Plan and identified on the aerial photographs. The disturbed area located in the southwest half of the site consists of large cobbles and small boulders of the Rocky Flats Alluvium and appears to have been disturbed for a possible borrow area. However, there is no staining or debris associated with the site that would indicate disposal of any waste had occurred.

FIDLER Surveys Section 7.2.4 of the OU 5 Work Plan specified that IHSS 209 and the other surface disturbances be surveyed with a FIDLER. These surveys were performed on a grid as described in Section 2.7.2.2 of Volume II of TM15 (DOE 1994a). The FIDLER surveys of IHSS 209 and the other surface disturbances did not identify any areas of above background radiation. The random survey of the pond/seep area on the northeast side of IHSS 209 also did not indicate any above background levels of radiation.

2.2.4.3 Stage 3

Stage 3 activities at IHSS 209 and the other surface disturbances consisted of the collection of samples of surface water and sediments in the water filled pits. Surface and subsurface soil samples were also collected at IHSS 209 and the other surface disturbances under Stage 3. These activities are discussed in Section 2.7.3 of Volume II of TM15 (DOE 1994a) and summarized in this section.

Surface Water and Sediment Sampling Results of surface water and sediment sampling were discussed in Section 2.2.3.3.

Surface Soil Sampling The surface soil sampling program for IHSS 209 and the other surface disturbances is described in the OU 5 Work Plan and in TM10 (DOE 1993₁). Samples were collected at 19 locations as shown on Figures 2.14 and 2.15. None of the samples contained metals in concentrations that exceeded background UTLs and did not contain detectable concentrations of pesticides or PCBs. Approximately half of the 19 surface soil samples contained plutonium 239/240 activities exceeding the

background UTL and approximately half of these samples also contained americium 241 activities greater than the background UTL. The samples with above background activities of radionuclides were collected from all three of the surface-disturbance sites. The plutonium 239/240 activity (approximately 5 pCi/g) of one sample collected at the Surface Disturbance West of IHSS 209 was the highest detected in surface soil samples from any of the OU 5 IHSSs and consequently additional sampling was conducted under the implementation of TM15. Seven of the surface soil samples also contained detectable concentrations of SVOCs.

Subsurface Soil Sampling Section 2.7.3.3 of Volume II of TM15 (DOE 1994a) discusses the results of the borehole program as well as the rationale for the number of boreholes. One borehole (57693) was drilled in the Surface Disturbance West of IHSS 209 (Figure 2.14) and three boreholes (57793, 57893, and 57993) were drilled in the Surface Disturbance South of the Ash Pits (Figure 2.15).

None of the boreholes drilled at the surface disturbances encountered groundwater. The analyses of the subsurface soil samples identified one sample in which the concentration of chromium exceeded the background UTL. One sample contained a plutonium 239/240 activity greater than the background UTL. Pesticides and PCBs were not detected in any of the samples collected. Benzoic acid, a SVOC, was detected in at least one sample from each of the boreholes. Methylene chloride was also detected in several samples.

2.2.4.4 Implementation of TM15

Implementation of field work outlined in Section 3.4 of TM15 (DOE 1994a) for IHSS 209 and the Surface Disturbances began in September 1994. In summary the work consisted of

- Surface Radiological Surveys
- Surface Soil Sampling and
- Air Programs and Wind Resuspension Study

Surface Radiological Survey Because Stage 3 surface soil sampling and analysis indicated elevated levels of radionuclides (specifically plutonium 239/240), the following surface radiological surveys were conducted at IHSS 209 and the other surface disturbances:

- an HPGe survey and
- a FIDLER survey of HPGe anomalies

To provide full HPGe coverage of the areas of interest a grid spacing of 150 ft was used. In addition to providing full coverage this geometry also reduced the size of the areas that needed to be FIDLER surveyed to a manageable size. The HPGe survey indicated 24 anomalous areas with detectable americium 241 within IHSS 209: the Surface Disturbance West of IHSS 209 and the Surface Disturbance South of the Ash Pits (Figures 2-16 and 2-17). The HPGe detector is not capable of measuring plutonium 239/240. Therefore, americium 241, a daughter product of plutonium 239/240, was used as an indicator to identify those locations where plutonium 239/240 may be present in surface soils.

FIDLER surveys of the HPGe anomalous areas detected readings above background at six HPGe locations. These six HPGe anomalies and above background FIDLER areas are as follows:

IHSS 209

- **HPGe K 56** FIDLER K 56A (25 West/4 North) approximately 46 ft south of HPGe station K 56 was frisked with a Bicron B 50 beta/gamma probe with readings of 66 cpm, 35 cpm, 70 cpm, and 61 cpm above background.
- **HPGe K 57** FIDLER K 57A (10 West/90 North) approximately 60 ft northeast of HPGe station K 57 showed FIDLER counts of 350 cpm above background.
- **HPGe L 55** FIDLER L 55A (0 West/100 North) located at the NNE corner of L 55 grid showed elevated FIDLER counts of 500-600 cpm above background.
- **HPGe H-60** following are coordinates with FIDLER counts above background:
(0 West/10 North) 600 cpm (8 West/65 North) 750 cpm
(16 West/60 North) 600 cpm (28 West/55 North) 600 cpm
(28 West/96 North) 650 cpm (36 West/25 North) 625 cpm
- **HPGe I 62** following are coordinates with FIDLER counts above background:
(100 West/50 North) 350 cpm
(92 West/50 North) 600 cpm
(66 West/30 North) 600 cpm

Surface Disturbance West of IHSS 209

- No areas with activity above background

Surface Disturbance South of the Ash Pits

- **HPGe M 14 FIDLER M 14A** (90 West/90 North) located approximately 70 ft northwest of HPGe station M 14 showed elevated FIDLER counts of approximately 750 cpm above background

Surface Soil Sampling Surface soil samples were collected from locations with the greatest activity as identified by the surface radiological surveys. Samples were analyzed for americium 241 and plutonium 239/240. A total of six samples were collected from the five HPGe anomalies within IHSS 209 (Figure 2 16). One sample was collected at each of the FIDLER anomalies K 56A and L 55A (SS133194 and SS133294). Two samples were collected from each of the HPGe anomalies identified at stations H 60 (SS133594 and SS133694) and I 62 (SS133394 and SS133494). The relatively low activities detected with the FIDLER at these two stations did not warrant the collection of surface soil samples at the location of each FIDLER anomaly. Therefore, one sample was collected at the two FIDLER anomalies with the greatest number of counts. At HPGe anomaly H 60, one sample was collected at coordinates 8 West/65 North (SS133594) and one was collected at coordinates 28 West/96 North (SS133694). Similarly, samples were collected from the two FIDLER anomalies with the greatest number of counts within HPGe anomaly I 62 (coordinates 92 West/50 North SS133494 and 66 West/30 North SS133394). Due to the relatively low activities detected with the FIDLER at anomaly K 57A, the collection of surface soil samples was not warranted.

One sample (SS133894) was collected from FIDLER anomaly M 14A at the Surface Disturbance South of the Ash Pits (Figure 2 17). As discussed in Section 2 2 4 3, a relatively high activity of plutonium 239/240 was detected in a surface soil sample collected from the Surface Disturbance West of IHSS 209 (sample SS50075AS). The plutonium 239/240 activity detected at this location was the primary reason that additional radiological surveys and surface soil sampling were necessary at these sites. Although the HPGe survey did not detect americium 241 and plutonium 239/240 in the vicinity of this location, an additional surface soil sample was collected at this location (Figure 2 16) as a verification and quality control check.

Detected activities in these surface soil samples were within the range of activities of previous work (Section 2 2 4 3). However, both plutonium 239/240 and americium 241 activities typically exceeded all

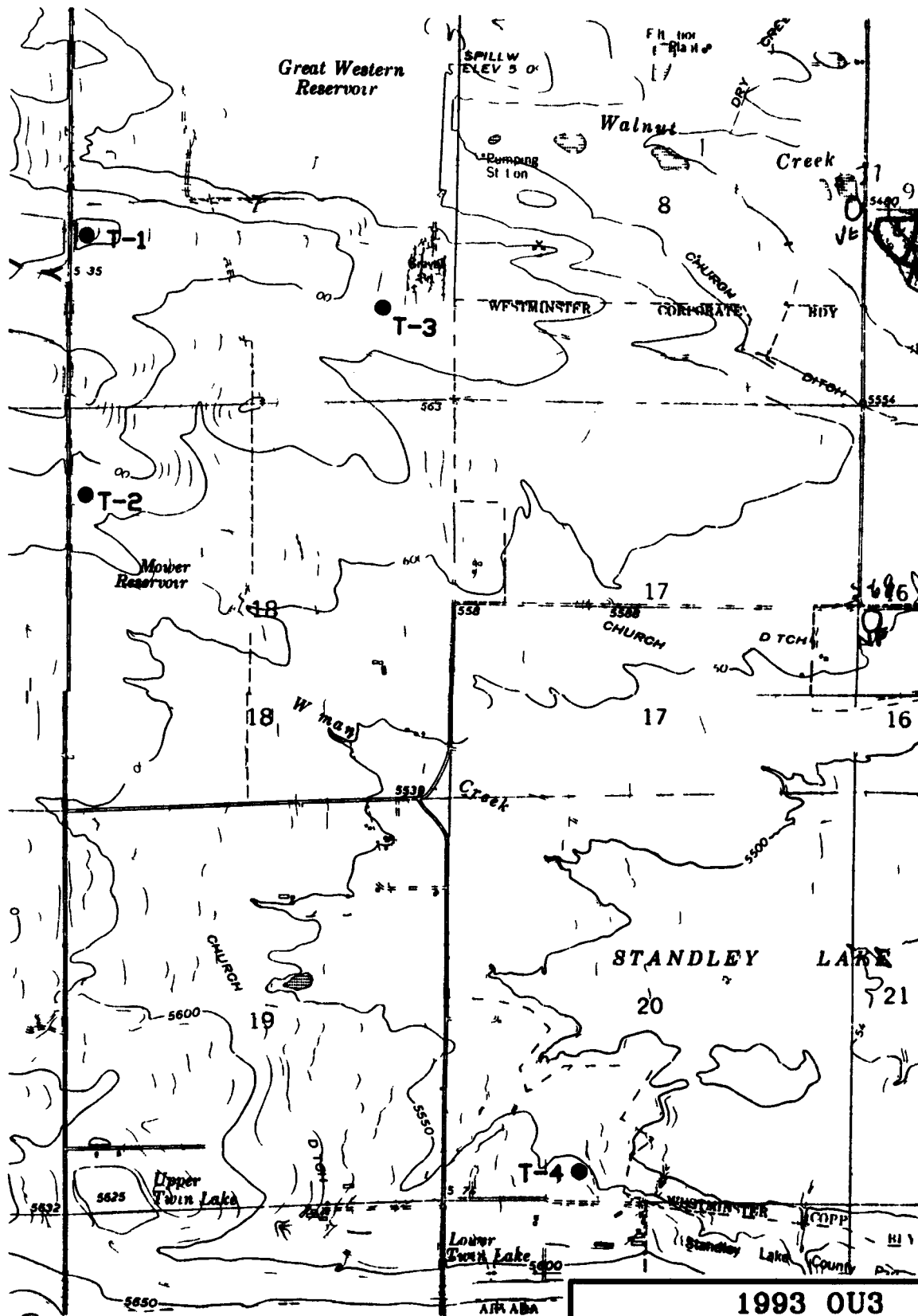
but the highest activity from previous soil samples (Table 2 13) None of these samples had activities that exceed the lognormal background UTL (7 66 pCi/g for americium 241 and 25 86 pCi/g for plutonium 239/240)

Air Monitoring TM15 (DOE 1994a) described an investigation for estimating the wind resuspension potential of surface soil However the potential for resuspension of contaminated soil was not directly addressed in the investigation of IHSS 209 and the surface disturbances To make this evaluation requires an estimation of the corrected threshold friction velocity of the soil The phased investigation procedures to acquire corrected threshold friction velocity data for IHSS 115 are applicable to IHSS 209 and the surface disturbances and are discussed in Section 2 2 1 7

2 2 5 Environmental Evaluation/Ecological Risk Assessment Investigation

Section 9 of the Work Plan Environmental Evaluation Plan was designed to describe the requirements for carrying out an ecological risk assessment, (ERA) The initial field sampling plan (FSP) was intended for screening purposes and baseline site characterization The overall ERA Work Plan Described an iterative approach with revisions planned after chemicals of concern receptors and contaminant pathways were identified The Work Plan Section 9 was modified in February 1993 The 1993 revised FSP was transmitted to the EPA and CDPHE by the DOE but approval of the document was not requested and the regulatory agencies did not provide a formal review or approval

In October of 1994 the approach to ERAs for the Site changed from an OU bases approach to a watershed approach for Woman Creek and Walnut Creek To accomplish this a sitewide ERA methodology was drafted and approved by the regulatory agencies As a result the scope of the Woman Creek ERA expand from OU 5 to include OU 1 part of OU 2 and part of OU 11 The modified field sampling plans for the OUs encompassed by the watershed ERAs are located in Appendix N and are not duplicated here



Drawn SAE 7/27/95 Date 7/27/95
 Checked 7/27/95 Date 7/27/95
 Approved _____ Date _____

FILE 0U5-2 5 DWG

**1993 0U3
 WIND TUNNEL STUDY
 TERRESTRIAL SAMPLING SITES**

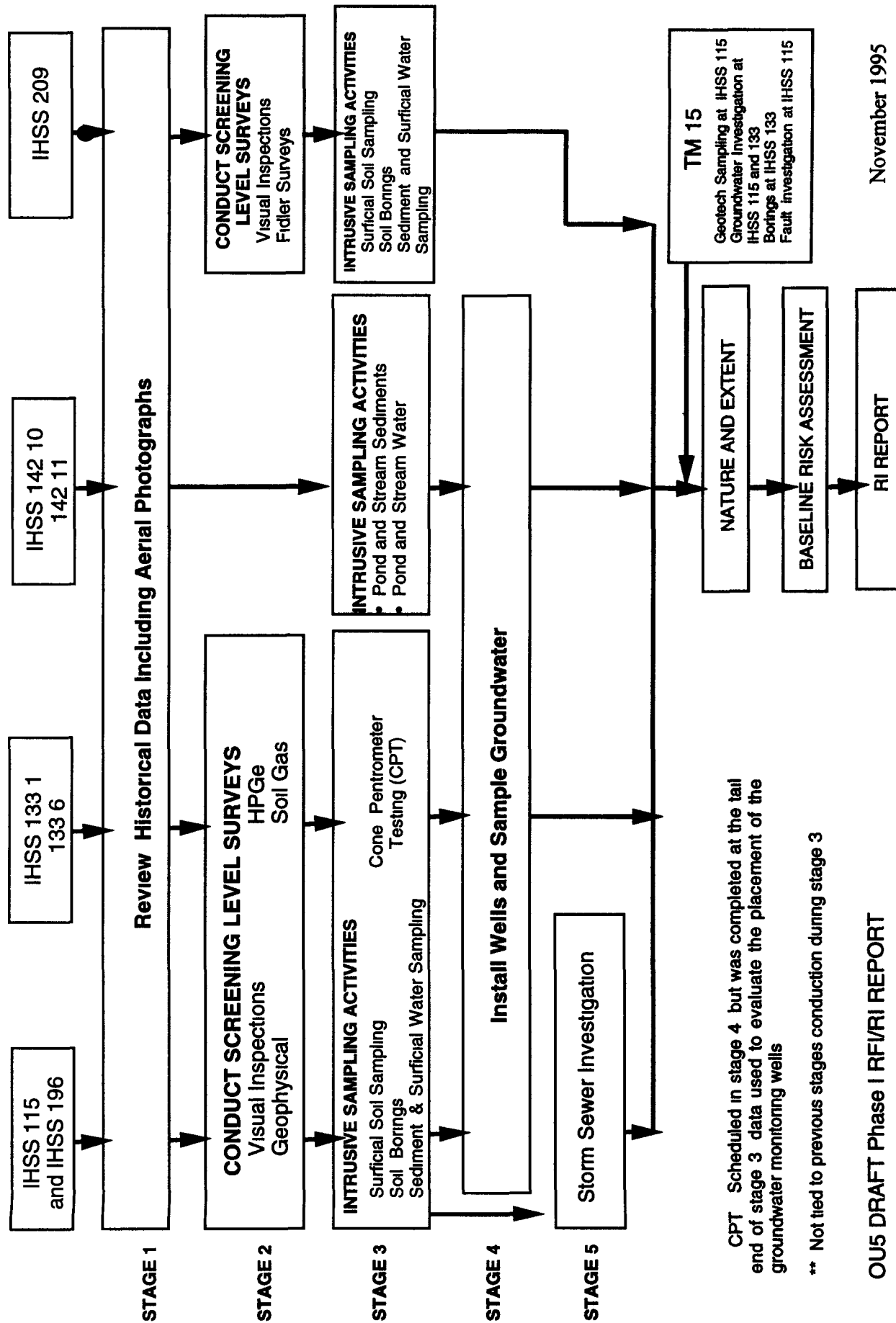
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

0U5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 2-5

FIGURE 2-18 - INVESTIGATIVE STAGES OF THE OU5 FIELD SAMPLING PLAN



CPT Scheduled in stage 4 but was completed at the tail end of stage 3 data used to evaluate the placement of the groundwater monitoring wells

** Not tied to previous stages conduction during stage 3

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Table 2 1
Evaluation of Intrinsic Air Permeability

SOIL BOREHOLES					SOIL GAS SURVEY RESULTS				
Location	Stat Pl n	Coordinates	Sampl No	Int v l	Soil Description	RHEDS	C	Soil G	Intrinsic Air
Code	North	East		Top	Bot	Loc tion	North	Sample	Permeability
						Code	ing	Number	k (d r y)
61293	747522 5	081148	BH50509AS	3 35	3 6 C v lly nd w/ lt	504093	747595 2081130	SC 50040 AS	0 03
			BH50510AS	5 25	5 5 Gravelly d w/ lt	503993	747595 2081170	SG 50039 AS	0 03
No associated borehole									
						501093	747595 2082250	SG 50010 AS	
						500993	747595 2082290	SG 50009 AS	
						500893	747595 2082330	SG 50008 AS	
						500893	747595 2082330	SG 50387 AS	
No associated borehole									
						543393	747595 2082110	SG 50433 AS	
						501393	747595 2082130	SG 50013 AS	
						501293	747595 2082170	SG 50012 AS	NA Manual p mp
59793	747552 6	2082128	BH50489AS	2 95	3 2 S ndy clay w/salt	543393	747595 2082110	SG 50433 AS	
			BH50490AS	6 25	6 5 Sandy lay w/salt	501393	747595 2082130	SG 50013 AS	NA Man al pur p
						501293	747595 2082170	SG 50012 AS	0 03
59993	747555	2081489	BH50466AS	2 75	3 Brok obbl to l y y and	515293	747530 2081450	SG 50152 AS	0 05
			BH50467AS	5 15	5 4 Cl yey sand	515193	747530 2081490	SG 50151 AS	0 12
						515093	747530 2081530	SG 50150 AS	0 12
No associated borehole									
						542993	747595 2082030	SG 50429 AS	
						542993	747595 2082030	SG 50457 AS	
						501593	747595 2082050	SG 50015 AS	NA Man al pump
59193	747569 2	2081261	BH50462AS	0 05	0 3 Clayey sand	503793	747595 2081250	SG 50037 AS	0 02
			BH50463AS	5 35	5 6 Cl yey siltstone	503693	747595 2081290	SG 50036 AS	NA Manual pur p
59593	747576 8	2081786	BH50541AS	4 75	5 Cl y y sand w/gravel	502293	747595 2081770	SG 50022 AS	NA Manual pur p
			BH50542AS	6 95	7 2 Cravelly sand w/clay	502193	747595 2081810	SG 50021 AS	NA Manual pump
59293	747583 9	2082143	BH50445AS	3 5	3 8 Sandy lay	501393	747595 2082130	SG 50013 AS	NA Manual pump
			BH50446AS	5	5 3 Clayey sand	501293	747595 2082170	SG 50012 AS	0 05
No associated borehole									
						503793	747595 2081750	SG 50037 AS	
						503693	747595 2081290	SG 50036 AS	NA Man al pur p

Table 2.1 (Continued)

SOIL BOREHOLES					SOIL GAS SURVEY RESULTS						
Location Code	State Plane Coordinates Northing Easting		Sample No.	Int rval Top Bot	Soil Description	RFEES Location Code	(Coordinates Northing Easting	Soil Gas Sample Number	Depth (ft)	Intrinsic Air Permeability P (darcy)	Corresponding Soil Type P - um R - port
No associated borehole						502093	747595 2081850	SG 50020 AS	5.0	NA	Manual pump
						501993	747595 2081890	SG 50019 AS	5.2	NA	Manual pump
						501993	747595 2081890	SG 50494 AS	5.7	NA	Duplicate
No associated borehole						508493	747664 2080970	SG 50084 AS	5.1		
No associated borehole						514093	747699 2080870	SG 50140 AS	5.0		
						514193	747699 2080910	SG 50141 AS	3.5		
63193	747696 8	2082542	BH50621AS	7 4	Sandy clay w/silt BH50622AS	518993	747695 2082550	SG 50189 AS	5.0	NA	Manual pump
61093	747764 3	2081952	BH50607AS	7 4	BH50608AS	532493	747770 2081900	SG 50324 AS	5.0	NA	Manual pump
				7 6		532393	747770 2082000	SG 50323 AS	5.0	NA	Manual pump
5109	747768 8	2081497	BH50159AS	3 6	Silty clay w/silt and gravel	527093	747770 2081550	SG 50270 AS	5.1	NA	Manual pump
(4) 747816 5	081948	BH50593AS	4 7	Clay silt	540593	747815 2081950	SG 50405 AS	5.0	NA	Manual pump	
		BH50594AS	6 7	Clay silt	540593	747815 2081950	SG 50434 AS	5.0	NA	Manual pump	
51413	747824 2	2081536	BH5054AS	0.75 1	Clay and	536693	747820 2081530	SG 50366 AS	3.0	0.05	Clay and
		BH50525AS	6.05 6.3	Gravelly sand w/silt	536693	747820 2081530	SG 50463 AS	3.0	NA	Duplicate	
					534793	747825 2081575	SG 50347 AS	5.0	NA	Manual pump	
50992	747842 8	2081536	BH50142AS	2 4.5	1 to 3 Sandy gravel w/cobbles	536893	747840 2081550	SG 50368 AS	5.0	0.05	Clay and
		BH50143AS	4.5 6	Silty sand w/gravel and clay	534893	747845 2081555	SG 50348 AS	5.0	NA	Manual pump	
					534893	747845 2081555	SG 50444 AS	5.0	NA	Manual pump	
					526693	747845 2081575	SG 50266 AS	5.1			
					526693	747845 2081575	SG 50373 AS	5.0			
					534693	747845 2081595	SG 50346 AS	5.0	NA	Manual pump	
50892	747882 4	2082279	BH50127AS	2 4	Sandy clay w/silt and trace of gravel	528493	747870 2082250	SG 50284 AS	5.1	0.12	Clay and
				4 6	Sandy clay w/silt and trace of gravel	522293	747895 2082250	SG 50222 AS	5.0	0.04	Clay and
						522393	747895 2082350	SG 50223 AS	5.0	0.01	Clay and
50792	747886 1	2082384	BH50110AS	2 4	Sandy gravel w/silt and trace of gravel	522393	747895 2082350	SG 50223 AS	5.0	0.01	Clay and
		BH50109AS	4 6	Sandy gravel w/silt and trace of gravel	522493	747895 2082450	SG 50224 AS	5.0	0.01	Clay and	

Table 2.1 (Continued)

SOIL GAS SURVEY RESULTS												
Location Cod	Stat Pl n Coordinates		Sample No	Int r l Top Bot	Soil Description	RFELDS Location Cod	C u rd nat s		Soil t Sample Numbe	Depth (ft)	Intrinsic Permeability (darcy)	Corresponding Soil Type
	Northing	Easting					Northing	Easting				
58693	747843.6	2081584	BH50373AS	2.8 3.1 6.7 7	G lly lly w/gra l	519793	747795	2081550	SG 50197 AS	5.7	0.0	(l y y
						525993	747795	2081575	SG 50259 AS	5.0	NA Manual pump	
						526093	747795	2081625	SG 50260 AS	3.4	NA Manual pump	
						537293	747800	2081600	SC 50372 AS	5.0	NA Manual pump	
						536493	747800	2081570	SG 50364 AS	5.0	NA Manual pump	
						536493	747820	2081570	SG 50437 AS	5.0	NA Manual pump	
						536793	747820	2081580	SG 50367 AS	5.0	NA Manual pump	
						526393	747820	2081600	SG 50263 AS	4.7	0.06	(l y y
						534793	747825	2081575	SC 50347 AS	5.0	NA Manual pump	
						537193	747840	2081600	SG 50371 AS	5.0	NA Manual pump	
						526693	747845	2081575	SG 50266 AS	5.1	0.07	(l y y
						526693	747845	2081575	SG 50373 AS	5.0	0.13	l
						534693	747845	2081595	SG 50346 AS	5.0	NA Manual pump	
534593	747865	2081575	SG 50345 AS	5.0	NA Manual pump							
534533	747865	2081575	SC 50466 AS	5.0	NA Duplicate							
58433	747875	081632	BH5043AS	3.15 3.4 5.15 5.4	Clly w/ly g aph t	540333	747875	2081630	SC 50403 AS	5.0	0.04	(l y y
						521693	747895	2081650	SG 50216 AS	5.0	0.06	(l y y
						521693	747895	2081650	SC 50480 AS	5.0	NA Duplicate	
						540393	747895	2081630	SG 50403 AS	5.0	0.04	(l y y
58533	747912.3	081632	BH50429AS	3.15 3.4 4.65 4.9	S ndy Cl y Sandy Cl y	521693	747895	2081650	SC 50216 AS	5.0	0.06	(l y y
						521693	747895	2081650	SG 50480 AS	5.0	NA Duplicate	
						535593	747915	2081610	SC 50355 AS	5.0	0.08	(l y y
						535593	747915	2081610	SG 50465 AS	5.0	NA Duplicate	
						534993	747915	2081630	SG 50349 AS	5.0	NA Manual pump	
						534993	747915	2081630	SG 50435 AS	5.0	NA Manual pump	
						540293	747915	2081650	SG 50402 AS	5.0	0.10	l n l
						50692	747914.4	2082505	BH50093AS	4 6	Clay y sand w/salt and gravel trace of cobbles	523993
524093	747995	2082550	SG 50240 AS	5.1	0.02							(lay y n l
522493	747895	2082450	SG 50224 AS	5.0	0.01							(l y y
522593	747895	2082550	SG 50225 AS	5.3	0.01							(l y y s

Table 2 1 (Continued)

SOIL BOREHOLES					SOIL GAS SURVEY RESULTS											
Location (Code)	State Plan (Coordinates Northing Easting)	Sample No.	Interval Top Bot	Soil Description	RFEIDS Location Code	Coordinates Northing Easting	Soil Gas Sample Number	Depth (ft)	Intrinsic Air Permeability (darcy)	Corresponding Soil Type from R report						
58393	747929 2	2081652	BH50418AS	0 15	Cl y y sand 1 0 wa te sand	533293	747920	2081650	SG 50332 AS	50	NA	Manual pump				
			BH50419AS	3 25	Waste sand metal	533293	747970	2081650	SG 50376 AS	50	0.17	1	sand			
			BH50420AS	6 45	waste dried paint	533193	747920	2081700	SG 50331 AS	50	NA	Manual pump				
					535093	747935	2081650	SG 50350 AS	48	NA	Manual pump					
					535093	747935	2081650	SG 50436 AS	50	NA	Manual pump					
					535793	747935	2081670	SG 50357 AS	50	NA	Manual pump					
					535793	747935	2081670	SG 50464 AS	50	NA	Manual pump					
					535693	747935	081630	SC 50356 AS	50	0.10	1	n				
					No associated borehole					522693	747895	2082650	SG 50226 AS	50		
									522793	747895	2082750	SG 50227 AS	51			
					524193	747995	2082650	SG 50241 AS	50							
					524193	747995	2082650	SG 50478 AS	50	NA	Dupl 1					
					524293	747995	2082750	SG 50242 AS	51							
										528993	748020	2082375	SC 50289 AS	46	NA	Manual p p
									528893	748020	2082400	SG 50288 AS	50	NA	Manual p i p	
5059	748051	2082358	BH50069AS	2 4	Sa dy g l w/ obbl nd lit	528693	748045	2082375	SG 50286 AS	45	0.06	(Cl y y n				
			BH50070AS	4 6	S ndy gra cl w/ obbl and s lit	528793	748045	2082400	SC 50287 AS	46	0.06	(Cl y y n				
						528593	748070	2082375	SC 50285 AS	50	0.07	(Cl y y n				
						524493	748095	2082450	SC 50244 AS	34	0.03	(Cl y y n				
50492	748077 2	2082461	BH50044AS	2 4	Gravelly sand w/cl y and lit	523993	747995	2082450	SG 50239 AS	50	0.13	1	sand			
			BH50045AS	4 6	Gravelly sand w/clay and lit	524093	747995	2082550	SG 50240 AS	51	0.07	(Clay y sand				
						524493	748095	2082450	SG 50244 AS	34	0.03	(Cl y y and				
						524593	748095	2082550	SG 50245 AS	36	0.06	(Cl y y sand				
50392	748088 3	2082630	BH50019AS	3 4 5	Sand nd silt	524093	747995	2082550	SG 50240 AS	51	0.0	(Cl y y sand				
			BH50020AS	4 5 5 8	Sand nd silt	524193	747995	2082650	SG 50478 AS	50	0.02	(Cl y y and				
						524593	748095	2082550	SG 50245 AS	36	0.06	(Cl y y				
						524693	748095	2082650	SG 50246 AS	50	0.05	(Cl y y s n				

Table 2 2A
Summary of Boreholes and Wells Installed Under TM 15

Location	TM15 Program	Type	Measuring Point (ft. MSL)	Ground Surface Elevation (ft. MSL)	Screen Interval (ft)	Total Depth (ft)	Depth to Bedrock (ft)	IHSS/Site	Bedrock Type
56794	Geotech	Borehole		5,995 20		25 14		115/196	Claystone with Some Silt
56894	Geotech	Borehole		5,994 20		33 7 5		115/196	Sandy Siltstone
56994	Geotech	Monitoring Well	6 021 63	6 019 80	14 5-24 5	29 24 45		115/196	Claystone
57094	Geotech	Monitoring Well	5 972 12	5 970 20	24 34	37 5 34		115/196	Claystone with Some Silt
57194	Geotech	Monitoring Well	6 000 02	5 998 10	119-129	150	5 3	115/196	Claystone with Some Silt
57394	Geotech	Borehole		5 938 20		23 7 4		115/196	Claystone with Trace Silt
57494	Geotech	Borehole		5,971 40		36 5 10 5		115/196	Claystone
57694	Geotech	Borehole		5,946 20		36 5 4		115/196	Claystone
57794	Geotech	Borehole		5,985 90		29 6 4		115/196	Claystone with Trace Silt
58394	Geotech	Monitoring Well	5,999 54	5,997 60	3 4 5 4	9 5	5 3	115/196	Claystone
58994	Geotech	Borehole		5 952 10		19 3 4 5		115/196	Claystone
59094	Geotech	Borehole		5 951 80		17 11 5		115/196	Claystone with Some Silt
59194	Geotech	Monitoring Well	6 039 74	6 037 70	24 34	46 33 4		115/196	Claystone
59294	Geotech	Monitoring Well	5 982 73	5,980 80	12 17	32 14		115/196	Sandy Claystone
59594	Geotech	Monitoring Well	6,048 91	6 046 70	27 6 37 6	41	37 5	115/196	Claystone
59694	Geotech	Monitoring Well	5 999 00	5 997 00	6-16	20 16 1		115/196	Claystone
59794	Geotech	Monitoring Well	6,008 88	6,006 40	11 21	25 2 15 5		115/196	Claystone with Trace Silt
71194	Geotech	Monitoring Well	6,008 67	6,006 20	87 5-97 5	150 16		115/196	Claystone
71294	Geotech	Borehole		5,934 40		34 3 7 2		115/196	Claystone
71494	Geotech	Monitoring Well	5,999 80	5,997 70	34-40	48 1	5 3	115/196	Claystone with Some Silt
55394	Groundwater	Small Diameter Well	6,023 55	6,021 60	3 5-8 5	12 6 8		Woman Creek	Claystone with Some Silt
56794	Groundwater	Small Diameter Well	6,010 56	6,007 80	3-8	8	Not Encountered	133 4	Not Encountered
56294	Groundwater	Small Diameter Well	6,018 49	6,017 30	6-16	16	8 9	133 3	Sandy Claystone
56394	Groundwater	Borehole		5,983 60		6	Not Encountered	Woman Creek	Not Encountered
56494	Groundwater	Small Diameter Well	6,012 69	6,011 70	4 14	14 10		133 2	Claystone with Some Silt
56594	Groundwater	Small Diameter Well	5 970 85	5,969 60	3-8	10 6 8		Woman Creek	Silty Claystone
56694	Groundwater	Borehole		5 982 90		150 7	14	115/196	Claystone with Trace Silt
57594	Groundwater	Monitoring Well	5 948 43	5,946 20	79 9-89 9	104 9	16 5	115/196	Claystone
57894	Groundwater	Small Diameter Well	5 950 01	5 949 90	5-10	10	Not Encountered	115/196	Not Encountered
57994	Groundwater	Small Diameter Well	5 941 27	5 939 80	2 7	11	7	115/196	Claystone

Table 2-2A (Continued)

Location	TM15 Program	Type	Measuring Point (ft. MSL)	Ground Surface Elevation (ft. MSL)	Screen Interval (ft)	Total Depth (ft)	Depth to Bedrock (ft)	IHSS/Soil	Bedrock Type
58094	Groundwater	Small Diameter Well	5,930 91	5,929 60	3-8	12 10		115/196	Claystone with Some Silt
58194	Groundwater	Small Diameter Well	5,930 63	5,928 60	3-8	8 6 6		115/196	Claystone with Trace Silt
58294	Groundwater	Small Diameter Well	5,948 81	5,947 10	2 5	9 3		115/196	Claystone
58494	Groundwater	Small Diameter Well	5,985 38	5,994 80	5-10	13		12 115/196	Claystone
58594	Groundwater	Small Diameter Well	5,920 14	5,917 90	1-6	8 5 4		115/196	Claystone with Some Silt
58694	Groundwater	Small Diameter Well	5,959 95	5,958 50	2 5	9 2 2		115/196	Claystone
58794	Groundwater	Small Diameter Well	5,958 91	5,957 60	2 5	9 1 95		115/196	Claystone
58894	Groundwater	Monitoring Well	5,966 96	5,965 30	77 5-87 5	88 3		14 115/196	Claystone
59494	Groundwater	Borehole		6 026 20		19 9		11 9 115/196	Sandy Siltstone
59894	Groundwater	Monitoring Well	6,028 34	6,025 70	105 1 120 1	132 5		11 9 115/196	Claystone with Some Silt
71394	Groundwater	Monitoring Well	5,985 89	5,983 80	5 6-10 6	13 6 10 5		Woman Creek	Claystone with Trace Silt
55194	TDEM	Small Diameter Well	6,048 69	6,046 10	9-19	19 16 1		TDEM 1	Claystone with Trace Silt
55294	TDEM	Borehole		6 045 30		20		15 25 TDEM 1	Claystone with Trace Silt
55494	TDEM	Small Diameter Well	6 026 88	6 026 00		14	Not Encountered	133 4	Not Encountered
55594	TDEM	Small Diameter Well	6 033 80	6 032 40	3-9	8 4		133 4	Claystone
55694	TDEM	Borehole		6 037 40		16 10 6		133 4	Claystone
55894	TDEM	Borehole		6 040 70		12 6 4		TDEM 2	Claystone
55994	TDEM	Borehole		6 040 30		16	Not Encountered	TDEM 2	Not Encountered
56094	TDEM	Borehole		6 038 70		22	Not Encountered	TDEM 2	Not Encountered
56194	TDEM	Borehole		6 074 70		30 28		Concrete Pad	Claystone with Some Silt
58894	TDEM	Borehole		6 044 00		8 2 7		TDEM W133	Claystone
59994	TDEM	Borehole		6 043 20		12	Not Encountered	TDEM 1	Not Encountered
60094	TDEM	Borehole		6 042 80		10	Not Encountered	TDEM 1	Not Encountered
57294	Treat	Borehole		6 027 20		8	Not Encountered	133 1	Not Encountered

Table 2 2B
TCLP Extraction Results IHSS 133 2 (Location 57294)

	Total (mg/Kg)	TCLP #1 (mg/L)	TCLP #2 (mg/L)	TCLP #3 (mg/L)	TCLP #4 (mg/L)	TCLP #5 (mg/L)
Aluminum	1 486 6B	0 35B	0 66B	0 3U	0 3U	0 3U
Antimony	29 3	0 3U	0 3U	0 3U	0 3U	0 3U
Arsenic	24 3	0 2U	0 2U	0 2U	0 2U	0 2U
Barium	337 9B	1 18B	1 36B	1 27B	1 52B	1 37B
Beryllium	82 4B	0 09B	0 12B	0 06B	0 13B	0 06B
Cadmium	64 8	0 68B	0 63B	0 67B	0 79B	0 82B
Calcium	1 438 7B	227 34B	309 97B	437 5B	387 61B	331 34B
Chromium	140 3	0 05U	0 05U	0 05U	0 05U	0 05U
Cobalt	16 7B	0 05U	0 07U	0 05U	0 05B	0 05U
Copper	1 394 3B	3 77B	9 07B	4 64B	4 67B	2 69B
Iron	62 263 7B	0 2U	0 28B	0 2U	0 2U	0 22B
Lead	825	0 22B	0 51B	0 26B	18 5	0 87B
Magnesium	3 376 3B	26 76B	30 9B	33 71B	35 04B	28 66B
Manganese	525 1B	1 63B	2 39B	1 68B	1 5B	1 17B
Molybdenum	14 3B	0 1U	0 1U	0 1U	0 1U	0 1U
Nickel	195B	0 29B	0 22B	0 27B	0 21B	0 22B
Phosphorus	974 6B	0 5U	0 5U	0 5U	0 5U	0 5U
Selenium	80 8	0 5U	0 5U	0 5U	0 5U	0 51B
Silver	89 9B	0 03U	0 03U	0 03U	0 03U	0 03U
Strontium	54 1B	0 97B	1 11B	1 29B	1 29B	1 08B
Thallium	29 U	0 3U	0 35B	0 31B	0 54B	0 3U
Titanium	282 7B	0 02U	0 02U	0 02U	0 02U	0 02U
Vanadium	61 3B	0 5U	0 5U	0 5U	0 5U	0 5U
Zinc	1 428 3B	7 34B	10 55B	7 7B	8 05B	8 21B

Qualifiers B=appears in blank
U=Contract detection limit

Table 2 3

Constituent	OU 5 or Background Data	Number of Samples	Range of Reporting Limits (mg/kg)	Percent Detection	Range of Concentrations (mg/kg)	Range of Concentrations (mg/kg)	Range of Concentrations (mg/kg)	Mean Concentration (mg/kg)	Deviation Standard
Aluminum	Background	98	504	98.98	7.690	279	102,000	12,712.80	11,334.96
	Geotech	26	200	100	N/A	5,710	12,400	8,514.04	1,699.63
	115-GW	25	40	100	N/A	2,350	20,700	9,779.40	4,640.47
	133-TDEM	22	636-200	100	N/A	4,660-28,600	11,776.82	5,738.99	5,630.95
	Pre-TM15	239	40	100	N/A	1,740-32,800	10,838.58	5,630.95	5,630.95
Antimony	Background	68	12	15.15	1.9	47	2.35-8.2	4.54	3.66
	Geotech	2	60	100	N/A	6.2	13.6	9.90	5.23
	115-GW	15	12	60	6	30	N/A	23.60	10.99
	133-TDEM	18	0.43	60	0.22	30	0.57	16.3	13.30
	Pre-TM15	223	12	12.11	12	22.1	6.7	14.9	8.49
Arsenic	Background	99	2	70.71	0.54	17.9	0.82-41.8	3.65	4.42
	Geotech	26	10	100	N/A	2.9	16.8	6.61	2.69
	115-GW	25	2	10	N/A	1.8	9.4	5.63	1.64
	133-TDEM	22	0.64-10	100	N/A	2.3	14.9	5.70	3.31
	Pre-TM15	239	2	99.58	2	0.47	18.9	3.91	2.40
Barium	Background	99	40	88.88	25.8	50.1	18.8-777	96.12	96.62
	Geotech	26	200	100	N/A	81.9	162	112.67	21.71
	115-GW	25	40	100	N/A	35.9	203	126.03	45.1
	133-TDEM	22	215	200	N/A	27.9	1,610	187.05	327.34
	Pre-TM15	239	40	100	N/A	28.6-683	130.30	92.10	92.10
Beryllium	Background	99	10-24	81.82	0.91	5.2	1.0	23.5	4.66
	Geotech	26	5	100	N/A	0.54	0.98	0.74	0.10
	115-GW	25	1	84	0.5	1.3	0.33	1.1	0.81
	133-TDEM	20	0.215-5	95	0.5	0.29	446	24.35	99.37
	Pre-TM15	239	1	69.46	1	1.25	0.23	131	8.46
Cadmium	Background	81	1	7.41	0.18	2.4	1.1-1.5	0.58	0.30
	Geotech	26	5	3.85	2.5	2.5	0.58	0.56	0.38
	115-GW	24	1	0	0.5	2.5	N/A	2.17	0.76
	133-TDEM	24	0.64-5	33	0.5	2.5	1.4-71	7.84	15.28
	Pre-TM15	239	1	11.3	1	1.32	0.62	58.9	1.45
Calcium	Background	99	110-2,420	96.99	1	160	1,170	157,000	7,052.58
	Geotech	26	5,000	100	N/A	3,240	20,400	7,821.92	3,901.68
	115-GW	25	1,000-5,000	100	N/A	1,730	14,000	6,580.00	2,993.72
	133-TDEM	23	4.89-5,000	100	N/A	1,140	18,900	4,153.48	3,841.19
	Pre-TM15	239	1,000	99.58	1,000	1,080	36,000	5,462.93	4,228.23
Ceium	Background	96	2.5	1.05	163.5	2,830	274	130.37	136.15
	Geotech	26	1,000	23.08	500	500	4.2	19.4	211.58
	115-GW	24	200-1,000	4	100	500	8.7	412.86	174.35
	133-TDEM	24	5.08	1,000	33	100	500	319.87	238.5
	Pre-TM15	212	200	2.36	200	1.9	12.6	97.80	14.17
Chromium	Background	99	2	84.85	4.1	17.8	5.6	17.6	24.66
	Geotech	26	10	100	N/A	5.3	163	24.94	32.88
	115-GW	25	2	10	N/A	3.8	48.8	14.60	9.01
	133-TDEM	22	0.64-10	100	N/A	7	434	37.54	89.42
	Pre-TM15	239	2	99.58	5.6	2.7	8.310	51.20	536.73
Cobalt	Background	99	10	22.22	3.8	93.9	4.5	18.4	6.45
	Geotech	26	50	100	N/A	3.9	12.6	8.32	2.10
	115-GW	25	10-50	100	N/A	3	13.2	7.76	2.45
	133-TDEM	24	1.29-50	96	5	2.3	70.1	38.55	141.60
	Pre-TM15	239	10	96.65	10	2.1	67.6	8.86	6.33
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean							45.12	22%

Table 2 3 (Continued)

Constituent (COCs are Bold/italic)	OU 5 or Background Data	Number of Samples	Range of Reporting Limits (mg/kg)	Percent Detection	Range of Non-detected Concentrations (mg/kg)	Range of Detected Concentrations (mg/kg)	Mean Concentration (mg/kg)	Standard Deviation
Copper	Background	99	5 12 1	94 95	5 11	2.2 123	12.59	12 77
	Geotech	26	25	100	N/A	13 9 31 2	21 92	3 95
	115-GW	25	5 25	80	12 5 17 45	8 8 42 4	19.25	6 83
	133-TDEM	24	0 43 25	96	7 1	5 6 8,850	801 83	1 843.23
	Pre-TM15	239	5	98 74	5 10 25	3 6 8,920	82 45	501 93
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							112 09	36%
Iron	Background	99	20 252	100	N/A	1 300 132 000	14 531 98	13,257.27
	Geotech	26	100	100	N/A	5 820 25 800	17 821 92	4 498 93
	115-GW	25	20 100	100	N/A	7 020 -- 24 000	16 833 00	4 856 74
	133-TDEM	24	1 47 100	100	N/A	6 480 108 000	23 430 42	25 540 08
	Pre-TM15	239	20	100	N/A	2,340 107,000	16 383 49	12 090 98
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							17,077 00	4
Lead	Background	99	1 6 1	98 99	4	2 6 39 8	10.85	7 07
	Geotech	26	3	100	N/A	6 5 21	18 82	3 47
	115-GW	25	0 6 3	100	N/A	5 3 22 3	15 20	4 67
	133-TDEM	22	0 43 3	100	N/A	3 9 5,200	316.50	1 106 69
	Pre-TM15	239	0 6 15	100	N/A	2 9 935	31 49	98 39
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							49 06	56%
Lithium	Background	99	2 1 26 1	61 62	2 9 26 1	3 7 83 2	9 99	8 51
	Geotech	26	100	100	N/A	3 6 10 9	7 41	1 88
	115-GW	25	20 100	92	10	2 45 -- 15 7	8 97	3 88
	133-TDEM	24	2 58 -- 100	96	10 10	2 8 17 9	8.57	4 44
	Pre-TM15	237	20	85 85	20	1 4 -- 29	8 55	4 79
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							8 49	1%
Magnesium	Background	99	110 2 420	95 96	713 -- 1 175 5	1 180 -- 32,500	2,852.83	3,248 35
	Geotech	26	5 000	100	N/A	1 450 5 480	3,289 42	1 024 00
	115-GW	25	1 000 5 000	100	N/A	882 5 335	3,243.08	1 193.54
	133-TDEM	24	7 52 5 000	100	N/A	828 -- 9 480	2 762.38	1 875.29
	Pre-TM15	239	1,000	100	N/A	392 -- 6,900	2,788.53	1,353.51
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							2,882.67	3%
Manganese	Background	99	3 7 3	100	N/A	37 3,330	217 84	341 98
	Geotech	26	15	100	N/A	41 7 488	281.99	120 80
	115-GW	25	3 15	100	N/A	102 488	250 48	118 97
	133-TDEM	22	0.245 15	100	N/A	42.2 2 150	300.08	450.27
	Pre-TM15	239	3	100	N/A	28 4 1,540	261 81	245 07
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							265.28	1%
Mercury	Background	86	0 08 0 3	25 58	0 05 5 9	0 1 0 64	0 19	0 34
	Geotech	26	0.2	42 31	0 1 0 1	0 064 0 1	0 09	0 01
	115-GW	24	0 1 0 2	33	0 05 0 1	0 06 0 11	0 09	0 02
	133 TDEM	18	0 1 -- 0 2	44	0 1	0 06 -- 0 36	0 11	0 08
	Pre-TM15	223	0 1	21 52	0 1 0 13	0 05 -- 1 4	0 09	0 18
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							0 09	1%
Molybdenum	Background	99	2 1 -- 40	50 51	2 28 9	2 5 67 6	10 90	8 61
	Geotech	26	200	30 77	100 100	1 2 3 5	68.84	48 13
	115-GW	24	40 200	25	20 100	1 3 7 1	65 73	45 49
	133-TDEM	24	3 44 -- 200	33	1 75 100	1 6 470	83.76	92 78
	Pre-TM15	238	40	8 4	40	0 9 190	20 19	13 73
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							32 72	62%
Nickel	Background	98	8 19 4	85 42	9 4 52 1	4 3 193	19.81	20.58
	Geotech	26	40	100	N/A	8 3 37	19.55	6 21
	115-GW	25	8 40	88	16 4 24 3	4 5 102	22.54	20 82
	133-TDEM	24	2 58 -- 40	100	N/A	6 6 355	50.99	82.86
	Pre-TM15	239	8	95 4	8 9 9	2 7 4 750	37.58	308.57
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							35.91	-4%
Potassium	Background	98	110 2 420	52 04	373 15 400	654 18 700	1 403.90	2 084.24
	Geotech	26	5 000	100	N/A	735 1 780	1,274.92	253 06
	115-GW	25	1 000 -- 5 000	84	500 2 140	473 3 750	1 437 38	665 78
	133-TDEM	24	78.2 5 000	96	500	470 -- 3 030	1,218 46	593 01
	Pre-TM15	239	1 000	88 7	000 558 5	327 7,040	1,341 99	748 86
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							1,334 59	1%

Table 2 3 (Continued)

Constituent	OCs are	Background	Number	Range of Reporting Limits (mg/kg)	Percent Detection	Range of N-detected Concentrations (mg/kg)	Range of Detected Concentrations (mg/kg)	Mean Concentration (mg/kg)	Standard Deviation
Selenium		Background	82	1.12-2.44	2.44	0.21-13.7	2.15-2.8	0.91	1.15
		Geotech	26	5	34.62	2.5-2.5	0.71-2.5	2.00	0.77
		115-GW	24	1.5	13	0.5-2.5	1.1-1.9	2.10	0.69
		133-TDEM	24	0.734-19.6	13	1.1-9.8	0.87-6.1	3.14	2.21
		Pre-TM15	233	1	9.44	1.14	0.24-0.78	0.49	0.06
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									
Silver		Background	83	1.48-39.76	39.76	0.54-6.8	1.45-40.9	5.57	9.46
		Geotech	26	10	30.77	3.15-5	1.31	3.93	1.57
		115-GW	25	2.10	16	1.5	1.3-2	3.77	1.73
		133-TDEM	20	0.644-10	65	1.5	0.59-20.9	20.48	47.01
		Pre-TM15	203	2	14.29	2	0.8-3.11	5.96	28.94
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									
Sodium		Background	99	110-2,420	17.17	126-2,720	161-3,680	303.62	421.97
		Geotech	26	5,000	80.77	2,500-2,500	74.5-677	675.06	917.81
		115-GW	25	1,000-5,000	100	N/A	28.2-1,140	281.36	287.33
		133-TDEM	24	5.63-5,000	92	500-2,500	54-3,380	594.98	796.52
		Pre-TM15	239	1,000	94.14	1,000	42-3,220	299.83	333.89
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									
Strontium		Background	99	21.6-484	36.36	20.3-484	25.1-226	52.02	48.27
		Geotech	26	200	100	N/A	21.3-119	65.42	24.78
		115-GW	25	40-200	100	N/A	13.7-111	61.10	27.32
		133-TDEM	22	0.245-200	100	N/A	9.9-92.6	30.50	22.19
		Pre-TM15	239	40-400	100	N/A	6.4-148	37.58	21.46
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									
Thallium		Background	75	2-20	4	0.18-4.9	0.22-0.4	0.50	0.54
		Geotech	26	10	19.23	2.91-5	0.39-0.78	4.07	1.79
		115-GW	24	2.10	0	1.5	N/A	4.33	1.52
		133-TDEM	24	0.734-10	17	1.5	0.5-6.3	4.08	1.77
		Pre-TM15	238	2	29.41	2	0.2-0.55	0.79	0.32
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									
Tin		Background	92	10-110	27.17	20.2-48.4	25.7-44.1	62.49	112.04
		Geotech	26	200	19.23	100-100	3.2-4.6	81.48	38.70
		115-GW	24	40-200	4	20-100	2.8	80.66	36.06
		133-TDEM	24	5.16-200	38	2.62-100	8.9-102	67.39	43.37
		Pre-TM15	239	40	4.6	40	2.4-5.79	23.10	37.16
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									
Vanadium		Background	99	24.2-97.98	97.98	8.45-11.6	11.1-28.3	31.49	28.50
		Geotech	26	50	100	N/A	13.9-36.3	22.63	4.22
		115-GW	25	10-50	100	N/A	8.1-38.7	26.36	9.59
		133-TDEM	24	0.644-50	100	N/A	12.2-60.4	31.28	12.52
		Pre-TM15	239	10	100	N/A	7.6-83.5	30.37	12.73
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									
Zinc		Background	98	4-97	92.86	9.7-25.9	0.52-48.6	36.31	51.36
		Geotech	26	20	100	N/A	18.3-87.1	65.04	15.58
		115-GW	25	4-20	100	N/A	13.8-121	58.78	22.27
		133-TDEM	24	0.488-20	100	N/A	8-6,920	441.26	1,414.47
		Pre-TM15	239	4	100	N/A	7.6-2,380	90.38	251.58
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean									

Geotech refers to samples collected from the geotechnical program at IHSS 115 as detailed in TM15
115-GW refers to samples collected from borholes used to investigate the TDEM anomalies at IHSS 115 as detailed in TM15
133-TDEM refers to samples collected from borholes used to investigate the TDEM anomalies at IHSS 133 as detailed in TM15
Pre-TM15 refers to samples collected within OJ 5 prior to January 1984
Mean and Standard Deviation are calculated assuming data are normally distributed. N/A not applicable
mg/kg milligrams per kilogram

Mean and Standard Deviation are calculated assuming data are normally distributed. mg/kg milligrams per kilogram. N/A not applicable

Table 2 4
Summary for Radionuclide Data from Subsurface-Soil Samples

Constituent (COCs are <i>Bold/italic</i>)	OU 5 or Background Data	Number of Samples	Range of Activities (pCi/g)	Mean Activity (pCi/g)	Standard Deviation
Total Activities					
Americium 241	Background	28	-0 015 -- 0 01	-0 002	0 007
	Geotech	24	-0 0119 0 2572	0 033	0 065
	115 GW	25	0 -- 0 08	0 01	0 02
	133 TDEM	21	0 0 2	0 05	0 06
	Pre-TM15	239	-0 016 0 61	0 014	0 053
Mean of OU 5 Data % Change from Pre-TM15 Mean --				0 02	26%
Plutonium 239/240	Background	99	-0 01 -- 0 03	0 004	0 007
	Geotech	24	-0 0019 0 0382	0 007	0 009
	115 GW	25	0 -- 0 08	0 01	0 02
	133 TDEM	25	0 5 16	0 31	1 03
	Pre-TM15	231	-0 03 -- 3 2	0 053	0 251
Mean of OU 5 Data % Change from Pre-TM15 Mean --				0 07	28%
Uranium-233/234	Background	99	0 2 -- 8 9	0 779	0 932
	Geotech	24	0 78915 1 578	1 157	0 212
	115 GW	29	0 58 -- 1 51	0 98	0 25
	133 TDEM	27	0 38 288 29	25 01	70 38
	Pre-TM15	244	0 35 126	3 95	15 811
Mean of OU 5 Data % Change from Pre-TM15 Mean --				5.23	32%
Uranium-235	Background	99	0 00 -- 0 2	0 02	0 048
	Geotech	24	-0 0031 0 1214	0 05	0 023
	115 GW	29	0 01 -- 0 13	0 04	0 02
	133-TDEM	27	0 01 -- 36 12	2 30	7 49
	Pre-TM15	245	-0 006 -- 37 88	0 49	3 017
Mean of OU 5 Data % Change from Pre-TM15 Mean --				0.57	16%
Uranium-238	Background	99	0 2 -- 3 2	0 733	0 378
	Geotech	24	0 8265 1 578	1 150	0 192
	115 GW	29	0 62 -- 1 45	0 97	0 23
	133-TDEM	27	0 37 -- 933 04	78 59	237 96
	Pre-TM15	245	0 43 -- 1 160	17.928	113 988
Mean of OU 5 Data % Change from Pre-TM15 Mean --				20.22	13%
Alpha	Background	99	5 -- 48	24 915	9 284
	Geotech	25	9 354 19 33	13 973	2 614
	115-GW	29	9 59 -- 29	15 00	5 33
	133-TDEM	28	5 8 -- 418 28	65 76	110 61
	Pre-TM15	221	5 59 -- 742	28 573	65 713
Mean of OU 5 Data % Change from Pre-TM15 Mean --				28.06	6%
Beta	Background	99	6 -- 44	24 717	6 061
	Geotech	25	22 86 37 81	27 188	2 915
	115-GW	29	19 78 38 42	27 03	4 09
	133 TDEM	28	13 64 898 92	115 97	216 25
	Pre-TM15	222	7 5 -- 1 580	45 759	125 611
Mean of OU 5 Data % Change from Pre-TM15 Mean --				48.91	7%

Notes OU 5 data where

Geotech refers to samples collected from the geotechnical program at IHSS 115 as detailed in TM15.

115 GW refers to samples collected from boreholes from the groundwater monitoring program at IHSS 115 as detailed in TM15

133 TDEM refers to samples collected from boreholes used to investigate the TDEM anomalies at IHSS 133 as detailed in TM15

Pre-TM15 refers to samples collected within OU5 prior to January 1994

Mean and Standard Deviation are calculated assuming data are normally distributed.

pCi/g picocuries per gram.

Table 2 5
Summary of Detected Organic Compounds in Subsurface-Soil Samples

TM15 Program*	Number	Range of Reporting Limits (ug/kg)	Percent of Samples Above Detection Limit	Range of Concentrations	Range of Concentrations	Range of Concentrations	Range of Concentrations	Maximum
(COCs are in Bold/Italics)				TM15	PDE-TM15	Non Detected	Detected	Con m atio
Geotech								PDE TM15 (ug/kg)
2-Butanone	27	10	7	5.1	11	31	3	40
Acetone	27	10	44	9.9	12	60	17	110
Chloroform	27	5	11	0	2.5	13	5.5	14
Methylene Chloride	27	5	41	14.4	2.5	31	3	13
Tetrachloroethane	27	5	19	13.3	2.5	16	2	12
Toluene	27	5	19	45.4	2.5	16	1	6
Trichloroethane	27	5	11	11.3	2.5	31	1	2
Semi-Volatile Organic Compounds								
Anthracene	25	330	4	23.2	350	1,000	212.5	46,000
Benz(a)Anthracene	25	330	20	28.8	360	1,000	43	88
Benz(a)Pyrene	25	330	52	25.6	368	400	40	320
Benz(b)Fluoranthene	25	330	20	28.8	360	1,000	75	125
Benz(k)Fluoranthene	25	330	8	24.4	350	1,000	40	44
Bis(2-Ethylhexyl)Phthalate	25	330	52	15.9	203.5	530	39	180
Bis(2-Ethylhexyl)Phthalate	25	330	92	<5	360	550	94	2,100
Chrysene	25	330	20	26.8	360	1,000	52	115
D-n-Butyl Phthalate	25	330	36	<5	350	1,000	43	215
Diethyl Phthalate	25	330	4	0	350	1,000	890	
Fluoranthene	25	330	28	30.5	370	1,000	60	260
Indeno(1,2,3-cd)Pyrene	25	330	8	21	350	1,000	47	54
Phenanthrene	25	330	20	31.7	365	1,000	70	205
Pyrene	25	330	28	31.7	370	1,000	46	215
Pesticides and PCBs								
Aroclor-1254	18	39	11	11.8	38.8	188	320	540
Volatile Organic Compounds								
2-Butanone	43	10	2	5.1	5	27	7	
Acetone	43	10	14	9.9	11	190	16	56
Bromoform	43	5	2	0	2.5	14	2	
Chloroform	43	5	14	0	2.5	7	2	
Methylene Chloride	43	5	9	14.4	2.5	29	4	150
Tetrachloroethane	43	5	21	13.3	2.5	14	3	30
Toluene	43	5	14	45.4	2.5	14	1	3
Trichloroethane	43	5	2	11.3	2.5	14	1	
Semi-Volatile Organic Compounds								
Benz(a)Pyrene	24	330	28	25.6	380	380	58	480
Benzic Acid	22	1,600	23	21.3	1,700	4,300	64	210
Bis(2-Ethylhexyl)Phthalate	24	330	46	15.9	350	390	42	540
Bis(2-Ethylhexyl)Phthalate	24	330	17	<5	350	1,135	170	1,400
D-n-Butyl Phthalate	24	330	8	<5	350	700	120	190
D-n-Octyl Phthalate	24	330	8	0	350	880	39	50
Diethyl Phthalate	24	330	8	0	350	880	63	305
Fluoranthene	24	330	4	30.5	350	880	39	
133-TDEM								
Tetrachloroethane	1	5	100	13.3	N/A		18	
Semi-Volatile Organic Compounds								
Benzic Acid	2	1,600	50	21.3	1,900		140	
Bis(2-Ethylhexyl)Phthalate	2	330	50	15.9	380		100	
D-n-Butyl Phthalate	2	330	50	2.4	380		190	
Phenanthrene	2	330	50	31.7	380		41	
Bis(2-Ethylhexyl)Phthalate	2	330	50	15.9	380		100	
D-n-Butyl Phthalate	2	330	50	2.4	380		190	
Phenanthrene	2	330	50	31.7	380		41	

Notes: OU 5 data where:

Geotech refers to samples collected from the geotechnical program at HSS 115 as detailed in TM15
 115-GW refers to samples collected from the groundwater monitoring program at HSS 115 as detailed in TM15
 133-TDEM refers to samples collected from boreholes used to investigate the TDEM anomalies at HSS 133 as detailed in TM15
 Mean and Standard Deviation are calculated assuming data are normally distributed.
 ug/kg micrograms per kilogram. N/A not applicable.

Table 2-6
TM15 Sampling Summary

Location	TM15 Program	Sample Number	QC Code	QC Partner	Sample Type	Completion Type	IHSS	Analyses Requested						
								Rate	Metals	VOA	SVOC	Pesticide	Water Qual	(note)
58793	GW	GW50123AS	REAL		GW	WELL	133	X	X	X	X	X	X	
58793	GW	GW50124AS	RNS	GW50123AS	GW	WELL	133	X		X			X	
59393	GW	GW50127AS	REAL		GW	WELL	115/196		X	X	X	X	X	
59393	GW	GW50134AS	TB	GW50127AS	GW	WELL	115/196			X				
59493	GW	GW50113AS	REAL		GW	WELL	115/196	X	X	X	X	X	X	
59493	GW	GW50113AS	REAL		GW	WELL	115/196	X	X	X	X	X	X	
59493	GW	GW50114AS	DUP	GW50113AS	GW	WELL	115/196	X	X	X	X	X	X	
59493	GW	GW50114AS	DUP	GW50113AS	GW	WELL	115/196	X	X	X	X	X	X	
59593	GW	GW50131AS	REAL		GW	WELL	115/196	X	X	X	X	X	X	
59793	GW	GW50133AS	REAL		GW	WP	115/196			X			X	
59793	GW	GW50136AS	RNS	GW50133AS	GW	WP	115/196	X	X	X	X	X	X	
59893	GW	GW50222AS	REAL		GW	WP	115/196						X	
59993	GW	GW50148AS	REAL		GW	WP	115/196			X			X	
59993	GW	GW50224AS	REAL		GW	WP	115/196		X				X	
60093	GW	GW50218AS	REAL		GW	WP	115/196	X	X	X	X		X	
60093	GW	GW50219AS	TB	GW50218AS	GW	WP	115/196			X				
60293	GW	GW50143AS	REAL		GW	WP	115/196	X	X	X	X	X	X	
60793	GW	GW50144AS	DUP	GW50143AS	GW	WP	115/196	X	X	X	X	X	X	
60293	GW	GW50170AS	REAL		GW	WP	115/196	X	X	X	X		X	
60293	GW	GW50171AS	DUP	GW50170AS	GW	WP	115/196	X	X	X	X		X	
60293	GW	GW50181AS	TB	GW50170-171A	GW	WP	115/196			X				
60393	GW	GW50220AS	REAL		GW	WP	115/196		X	X			X	
60393	GW	GW50221AS	TB	GW50220AS	GW	WP	115/196			X				
60493	GW	GW50156AS	REAL		GW	WP	115/196						X	
60493	GW	GW50226AS	REAL		GW	WP	115/196						X	
60593	GW	GW50155AS	REAL		GW	WP	115/196						X	
60593	GW	GW50212AS	REAL		GW	WP	115/196	X	X	X	X		X	
60593	GW	GW50213AS	TB	GW50212AS	GW	WP	115/196			X				
60693	GW	GW50160AS	REAL		GW	WP	115/196						X	
60693	GW	GW50214AS	REAL		GW	WP	115/196	X	X	X	X		X	
60693	GW	GW50215AS	TB	GW50214AS	GW	WP	115/196			X				
60893	GW	GW50157AS	REAL		GW	WP	115/196						X	
60893	GW	GW50158AS	RNS	GW50157AS	GW	WP	115/196		X		X		X	
60893	GW	GW50175AS	REAL		GW	WP	115/196	X	X	X	X		X	
60993	GW	GW50210AS	REAL		GW	MINI	115/196		X	X			X	
60993	GW	GW50211AS	TB	GW50210AS	GW	MINI	115/196			X				
61093	GW	GW50150AS	RNS	GW50151AS	GW	MINI	115/196	X	X	X	X	X	X	
61093	GW	GW50151AS	REAL		GW	MINI	115/196	X	X	X	X	X	X	
61093	GW	GW50154AS	DUP	GW50151AS	GW	MINI	115/196	X	X	X	X	X	X	
61093	GW	GW50164AS	TB	GW50151AS	GW	MINI	115/196			X				
61093	GW	GW50176AS	REAL		GW	MINI	115/196	X	X	X	X		X	
61093	GW	GW50177AS	DUP	GW50176AS	GW	MINI	115/196	X	X	X	X		X	
61093	GW	GW50194AS	TB	GW50176AS	GW	MINI	115/196			X				
61793	GW	GW50125AS	RNS	GW50126AS	GW	WELL	115/196	X	X	X	X	X	X	
61293	GW	GW50126AS	REAL		GW	WELL	115/196		X	X			X	
6593	GW	GW50216AS	REAL		GW	WP	133	X	X		X		X	
67693	GW	GW50217AS	REAL		GW	WP	133	X	X		X		X	
62793	GW	GW50147AS	REAL		GW	WP	115/196			X			X	
62793	GW	GW50149AS	DUP	GW50147AS	GW	WP	115/196			X			X	
62793	GW	GW50152AS	TB	GW50147AS	GW	WP	115/196			X				
62793	GW	GW50228AS	REAL		GW	WP	115/196		X	X			X	
62793	GW	GW50229AS	TB	GW50228AS	GW	WP	115/196			X				
62893	GW	GW50122AS	REAL		GW	WP	115/196	X	X	X	X	X	X	
62893	GW	GW50140AS	REAL		GW	WP	115/196						X	
62893	GW	GW50163AS	TB	GW50165AS	GW	WP	115/196			X				
62893	GW	GW50165AS	REAL		GW	WP	115/196						X	
62893	GW	GW50180AS	REAL		GW	WP	115/196	X	X	X	X		X	
62893	GW	GW50200AS	TB	GW50180AS	GW	WP	115/196			X				

Table 2-6 (Continued)

Location	TM15 Program	Sample Number	QC Code	QC Partner	Sample Type	Completion Type	IHSS	Analyses Requested						
								Rads	Metals	VOA	SVOA	Partic B	Water Qual	Crit tech
63093	GW	GW50129AS	RNS	GW50135AS	GW	WELL	133						X	
63093	GW	GW50135AS	REAL		GW	WELL	133	X	X	X	X	X	X	
63093	GW	GW50168AS	TB	GW50135AS	GW	WELL	133			X				
63193	GW	GW50178AS	REAL		GW	MINI	115/196	X	X	X	X	X	X	
63193	GW	GW50130AS	DUP	GW50128AS	GW	MINI	115/196	X	X	X	X	X	X	
63193	GW	GW50132AS	RNS	GW50128AS	GW	MINI	115/196	X	X	X	X	X	X	
63193	GW	GW50182AS	REAL		GW	MINI	115/196	X	X	X	X		X	
63193	GW	GW50183AS	DUP	GW50182AS	GW	MINI	115/196	X	X	X	X		X	
63193	GW	GW50184AS	RNS	GW50182 183A	GW	MINI	115/196	X	X	X	X		X	
63193	GW	GW50200AS	TB	GW50182 183A	GW	MINI	115/196			X				
63693	GW	GW50137AS	REAL		GW	WP	133			X			X	
63693	GW	GW50139AS	DUP	GW50137AS	GW	WP	133			X			X	
63693	GW	GW50166AS	REAL		GW	WP	133						X	
63693	GW	GW50167AS	TB	GW50166AS	GW	WP	133			X				
63693	GW	GW50207AS	REAL		GW	WP	133						X	
63793	GW	GW50115AS	REAL		GW	MINI	133	X	X	X	X	X	X	
63793	GW	GW50115AS	REAL		GW	WP	133	X	X	X	X	X	X	
63793	GW	GW50116AS	RNS	GW50115AS	GW	WP	133	X	X	X	X	X	X	
63793	GW	GW50117AS	TB	GW50115AS	GW	WP	133			X				
63793	GW	GW50206AS	REAL		GW	WP	133	X	X	X			X	
63893	GW	GW50120AS	REAL		GW	WP	115	X	X	X	X	X	X	
63893	GW	GW50121AS	REAL		GW	WP	115		X	X	X	X	X	
63893	GW	GW50187AS	REAL		GW	WP	115	X	X	X	X		X	
63893	GW	GW50196AS	TB	GW50187AS	GW	WP	115			X				
63993	GW	GW50119AS	REAL		GW	WP	115	X	X	X	X	X	X	
63993	GW	GW50188AS	REAL		GW	WP	115	X	X	X	X		X	
63993	GW	GW50197AS	TB	GW50188AS	GW	WP	115			X				
64093	GW	GW50118AS	REAL		GW	WP	115	X	X	X	X	X	X	
64093	GW	GW50189AS	REAL		GW	WP	115	X	X	X	X		X	
64093	GW	GW50198AS	TB	GW50189AS	GW	WP	115			X				
55194	TDEM	BH00028AS	REAL		BH	MINI	133	X	X					
55194	TDEM	BH00029AS	REAL		BH	MINI	133	X	X					
55194	TDEM	BH00030AS	REAL		BH	MINI	133	X	X					
55194	TDEM	BH00101AS	RNS		BH	MINI	133	X	X					
55294	TDEM	BH00031AS	REAL		BH	BH	133	X	X					
55294	TDEM	BH00032AS	REAL		BH	BH	133	X	X					
55294	TDEM	BH00033AS	REAL		BH	BH	133	X	X					
55394	GW	BH00055AS	REAL		GEOTECH	MINI	133							X
55394	GW	GW50106AS	REAL		GW	MINI	133	X	X	X	X	X	X	
55394	GW	GW50107AS	RNS		GW	MINI	133	X	X	X	X	X	X	
55394	GW	GW50111AS	TB		GW	MINI	133			X				
55494	TDEM	BH00023AS	REAL		GEOTECH	MINI	133							X
55494	TDEM	BH00024AS	REAL		GEOTECH	MINI	133							X
55594	TDEM	BH00025AS	REAL		GEOTECH	MINI	133							X
55594	TDEM	BH00100AS	RNS		BH	MINI	133	X	X					
55694	TDEM	BH00041AS	REAL		BH	BH	133	X	X					
55694	TDEM	BH00042AS	REAL		BH	BH	133	X	X					
55794	GW	BH00057AS	REAL		GEOTECH	MINI	133							X
55894	TDEM	BH00036AS	REAL		BH	BH	133	X	X					
55894	TDEM	BH00103AS	RNS		BH	BH	133	X	X					
55994	TDEM	BH00034AS	REAL		BH	BH	133	X	X					
55994	TDEM	BH00035AS	REAL		BH	BH	133	X	X					
55994	TDEM	BH00102AS	RNS		BH	BH	133	X	X					
56094	TDEM	BH00037AS	REAL		BH	BH	133	X	X					
56094	TDEM	BH00038AS	REAL		BH	BH	133	X	X					
56094	TDEM	BH00039AS	REAL		BH	BH	133	X	X					
56094	TDEM	BH00040AS	REAL		BH	BH	133	X	X					
56094	TDEM	BH00104AS	RNS		BH	BH	133	X	X					

Table 2-6 (Continued)

Location	TM15 Program	Sample Number	QC Code	QC Partner	Sample Type	Completion Type	IHSS	Analyses Requested						
								Radi	Metals	VOA	SVOA	Positiv B	Water Q	C or Tech
56194	TDEM	BH00043AS	REAL		BH	BH	133	X	X					
56194	TDEM	BH00072AS	REAL		BH	BH	133	X	X					
56194	TDEM	BH00073AS	REAL		BH	BH	133	X	X					
56194	TDEM	BH00074AS	REAL		BH	BH	133	X	X					
56194	TDEM	BH00075AS	REAL	BH00076AS	BH	BH	133	X	X					
56194	TDEM	BH00076AS	DUP	BH00075AS	BH	BH	133	X	X					
56194	TDEM	BH00077AS	REAL		BH	BH	133	X	X					
56194	TDEM	BH00105AS	RNS		BH	BH	133							
56194	TDEM	BH00107AS	RNS		BH	BH	133	X	X					
56294	GW	BH00026AS	REAL		GEOTECH	MINI	133							X
56294	GW	BH00027AS	REAL		GEOTECH	MINI	133							X
56394	GW	BH00056AS	REAL		GEOTECH	BH	133							X
56494	GW	BH00021AS	REAL		GEOTECH	MINI	133							X
56494	GW	BH00022AS	REAL		GEOTECH	MINI	133							X
56594	GW	BH00058AS	REAL		GEOTECH	MINI	133							X
56594	GW	GW50105AS	REAL		GW	MINI	133	X	X	X	X	X	X	
56594	GW	GW50110AS	TB		GW	MINI	133			X				
56694	GW	BH00092AS	REAL		BH	BH	115/196			X				
56694	GW	BH00093AS	REAL		BH	BH	115/196			X				
56694	GW	BH00094AS	REAL		BH	BH	115/196			X				
56694	GW	BH00095AS	REAL	BH00096AS	BH	BH	115/196	X	X		X	X		
56694	GW	BH00096AS	DUP	BH00095AS	BH	BH	115/196	X	X		X	X		
56694	GW	BH00097AS	REAL		BH	BH	115/196			X				
56694	GW	BH00098AS	REAL		BH	BH	115/196	X	X		X	X		
56694	GW	BH00099AS	REAL		BH	BH	115/196			X				
56694	GW	BH00109AS	RNS		BH	BH	115/196	X	X	X	X	X		
56694	GW	BH00110AS	RNS		BH	BH	115/196	X	X	X	X	X		
56694	GW	BH00111AS	REAL		DRUM	BH	115/196	X	X	X	X	X		
56694	GW	BH00112AS	REAL		DRUM	BH	115/196	X	X	X	X	X		
56694	GW	BH00113AS	REAL		DRUM	BH	115/196	X	X	X	X	X		
56694	GW	BH00115AS	RNS		DRUM	BH	115/196	X	X	X	X	X		
56694	GW	BH00116AS	FB		BH	BH	115/196			X				
56694	GW	BH00122AS	REAL		DRUM	BH	115/196	X	X	X	X	X		
56694	GW	BH00134AS	REAL		GEOTECH	BH	115/196							X
56794	GEOTECH	BH00228AS	REAL		GEOTECH	BH	115/196							X
56794	GEOTECH	BH00229AS	REAL		GEOTECH	BH	115/196							X
56794	GEOTECH	BH00230AS	REAL		GEOTECH	BH	115/196							X
56794	GEOTECH	BH00231AS	REAL		GEOTECH	BH	115/196							X
56794	GEOTECH	BH00232AS	REAL		GEOTECH	BH	115/196							X
56794	GEOTECH	BH00233AS	REAL		GEOTECH	BH	115/196							X
56794	GEOTECH	BP00034AS	REAL	BP00035AS	DRUM	BH	115/196	X	X	X	X	X		
56794	GEOTECH	BP00035AS	DUP	BP00034AS	DRUM	BH	115/196	X	X	X	X	X		
56794	GEOTECH	BP00036AS	RNS		DRUM	BH	115/196	X	X	X	X	X		
56894	GEOTECH	BH00216AS	REAL		GEOTECH	BH	115/196							X
56894	GEOTECH	BH00217AS	REAL		GEOTECH	BH	115/196							X
56894	GEOTECH	BH00218AS	REAL		GEOTECH	BH	115/196							X
56894	GEOTECH	BH00219AS	REAL		GEOTECH	BH	115/196							X
56894	GEOTECH	BH00220AS	REAL		GEOTECH	BH	115/196							X
56894	GEOTECH	BH00221AS	REAL		GEOTECH	BH	115/196							X
56894	GEOTECH	BH00222AS	REAL		GEOTECH	BH	115/196							X
56894	GEOTECH	BH00244AS	TB		BH	BH	115/196			X				
56894	GEOTECH	BP00032AS	REAL		DRUM	BH	115/196	X	X	X	X	X		
56894	GEOTECH	BP00033AS	RNS		DRUM	BH	115/196	X	X	X	X	X		
56994	GEOTECH	BH00185AS	REAL		GEOTECH	WELL	115/196							X
56994	GEOTECH	BH00186AS	REAL		CFOTECH	WELL	115/196							X
56994	GEOTECH	BH00187AS	REAL		CEOTECH	WELL	115/196							X
56994	GEOTECH	BH00188AS	REAL		CEOTECH	WELL	115/196							X
56994	GEOTECH	BH00189AS	REAL		CFOTECH	WELL	115/196							X

Table 2-6 (Continued)

Location	TM15 Program	Sample Number	QC Code	QC Partner	Sample Type	Completion Type	IHSS	Analyses Requested					
								Rads	Metals	VDA	SVDA	PC-MCB	Water Qual
56994	GEOTECH	BH00190AS	REAL		GEOTECH	WELL	115/196						X
56994	GEOTECH	BH00191AS	REAL		GEOTECH	WELL	115/196						X
56994	GEOTECH	BP00013AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57094	GEOTECH	BH00138AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00139AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00140AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00141AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00142AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00143AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00144AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00145AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00146AS	REAL		GEOTECH	WELL	115/196						X
57094	GEOTECH	BH00147AS	REAL	BH00148AS	DRUM	WELL	115/196	X	X	X	X	X	
57094	GEOTECH	BH00148AS	DUP	BH00147AS	DRUM	WELL	115/196	X	X	X	X	X	
57194	GEOTECH	BH00192AS	REAL		GEOTECH	WELL	115/196						X
57194	GEOTECH	BH00193AS	REAL		GEOTECH	WELL	115/196						X
57194	GEOTECH	BH00194AS	REAL		GEOTECH	WELL	115/196						X
57194	GEOTECH	BH00195AS	REAL		GEOTECH	WELL	115/196						X
57194	GEOTECH	BH00196AS	REAL		GEOTECH	WELL	115/196						X
57194	GEOTECH	BP00014AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57194	GEOTECH	BP00015AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57194	GEOTECH	BP00016AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57194	GEOTECH	BP00017AS	RNS		DRUM	WELL	115/196	X	X	X	X	X	
57194	GEOTECH	BP00018AS	RNS		DRUM	WELL	115/196	X	X	X	X	X	
57194	GEOTECH	BP00029AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57294	TREAT	BH00090AS	REAL		BH	BH	133						
57294	TREAT	BH00091AS	REAL		DRUM	BH	133	X	X				
57394	GEOTECH	BH00123AS	REAL		GEOTECH	BH	115/196						X
57394	GEOTECH	BH00124AS	REAL		GEOTECH	BH	115/196						X
57394	GEOTECH	BH00125AS	REAL		GEOTECH	BH	115/196						X
57494	GEOTECH	BH00175AS	REAL		GEOTECH	BH	115/196						X
57494	GEOTECH	BH00176AS	REAL		GEOTECH	BH	115/196						X
57494	GEOTECH	BH00177AS	REAL		GEOTECH	BH	115/196						X
57494	GEOTECH	BP00004AS	REAL		DRUM	BH	115/196	X	X	X	X	X	
57594	GW	BH00078AS	REAL		BH	WELL	115/196	X	X		X	X	
57594	GW	BH00079AS	REAL		BH	WELL	115/196			X			
57594	GW	BH00080AS	REAL		BH	WELL	115/196			X			
57594	GW	BH00081AS	REAL		BH	WELL	115/196			X			
57594	GW	BH00082AS	REAL		BH	WELL	115/196	X	X		X	X	
57594	GW	BH00083AS	REAL		BH	WELL	115/196			X			
57594	GW	BH00084AS	REAL		BH	WELL	115/196			X			
57594	GW	BH00085AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57594	GW	BH00086AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57594	GW	BH00087AS	REAL		BH	WELL	115/196	X	X	X	X	X	
57594	GW	BH00108AS	RNS		BH	WELL	115/196	X	X				
57594	GW	BH00117AS	RNS		DRUM	WELL	115/196	X	X	X			
57594	GW	BH00121AS	REAL		DRUM	WELL	115/196	X	X	X	X	X	
57694	GEOTECH	BH00197AS	REAL		GEOTECH	BH	115/196						X
57694	GEOTECH	BH00198AS	REAL		GEOTECH	BH	115/196						X
57694	GEOTECH	BH00199AS	REAL		GEOTECH	BH	115/196						X
57694	GEOTECH	BH00200AS	REAL		GEOTECH	BH	115/196						X
57694	GEOTECH	BH00201AS	REAL		GEOTECH	BH	115/196						X
57694	GEOTECH	BP00019AS	REAL		DRUM	BH	115/196	X	X	X	X	X	
57694	GEOTECH	BP00022AS	RNS		DRUM	BH	115/196	X	X	X	X	X	
57794	GEOTECH	BH00128AS	REAL		GEOTECH	BH	115/196						X
57794	GEOTECH	BH00129AS	REAL		GEOTECH	BH	115/196						X
57794	GEOTECH	BH00130AS	REAL		GEOTECH	BH	115/196						X
57794	GEOTECH	BH00131AS	REAL		GEOTECH	BH	115/196						X

Table 2-6 (Continued)

Location	TM15 Program	Sample Number	QC Code	QC Partner	Sample Type	Completion Type	IHSS	Analyses Requested						
								Radon	Metals	VOCs	SVOCs	PCBs	Water Qual	Geotech
57894	GW	GW50141AS	DUP	GW50161AS	GW	MINI	115/196	X	X	X	X	X	X	
57894	GW	GW50142AS	RNS		GW	MINI	115/196	X	X	X	X	X	X	
57894	GW	GW50145AS	TB		GW	MINI	115/196			X				
57894	GW	GW50161AS	REAL	GW50141AS	GW	MINI	115/196	X	X	X	X	X	X	
57894	GW	GW50162AS	TB		GW	MINI	115/196							
57994	GW	BH00044AS	REAL		BH	MINI	115/196			X				
57994	GW	BH00045AS	REAL		BH	MINI	115/196			X				
57994	GW	BH00046AS	REAL		BH	MINI	115/196			X				
57994	GW	BH00047AS	REAL		BH	MINI	115/196	X	X		X	X		
58094	GW	BH00061AS	REAL		GEOTECH	MINI	115/196							X
58094	GW	GW50101AS	RNS		GW	MINI	115/196	X	X	X	X	X	X	
58094	GW	GW50102AS	REAL	GW50103AS	GW	MINI	115/196	X	X	X	X	X	X	
58094	GW	GW50103AS	DUP	GW50102AS	GW	MINI	115/196	X	X	X	X	X	X	
58094	GW	GW50108AS	TB		GW	MINI	115/196			X				
58194	GW	BH00062AS	REAL		GEOTECH	MINI	115/196							X
58294	GW	BH00048AS	REAL		BH	MINI	115/196			X				
58294	GW	BH00049AS	REAL		BH	MINI	115/196			X				
58294	GW	BH00050AS	REAL		BH	MINI	115/196	X	X		X	X		
58394	GEOTECH	BH00223AS	REAL		GEOTECH	WELL	115/196							X
58394	GEOTECH	BH00224AS	REAL		GEOTECH	WELL	115/196							X
58394	GEOTECH	BH00225AS	REAL		GEOTECH	WELL	115/196							X
58394	GEOTECH	BH00226AS	REAL		GEOTECH	WELL	115/196							X
58394	GEOTECH	BH00227AS	REAL		GEOTECH	WELL	115/196							X
58394	GEOTECH	BP00046AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
58494	GW	BH00065AS	REAL		BH	MINI	115/196			X				
58494	GW	BH00066AS	REAL		BH	MINI	115/196			X				
58494	GW	BH00067AS	REAL		BH	MINI	115/196			X				
58494	GW	BH00068AS	REAL		BH	MINI	115/196	X	X		X	X		
58494	GW	BH00069AS	REAL		BH	MINI	115/196			X				
58494	GW	BH00070AS	REAL		BH	MINI	115/196			X				
58494	GW	BH00071AS	REAL		BH	MINI	115/196	X	X		X	X		
58594	GW	BH00063AS	REAL		GEOTECH	MINI	115/196							X
58594	GW	GW50104AS	REAL		GW	MINI	115/196	X	X	X	X	X	X	
58594	GW	GW50109AS	TB		GW	MINI	115/196			X				
58694	GW	BH00051AS	REAL		BH	MINI	115/196			X				
58694	GW	BH00052AS	REAL		BH	MINI	115/196	X	X		X	X		
58794	GW	BH00053AS	REAL		BH	MINI	115/196			X				
58794	GW	BH00054AS	REAL		BH	MINI	115/196	X	X		X	X		
58794	GW	BH00106AS	RNS		BH	MINI	115/196	X	X	X	X	X		
58894	TDEM	BH00064AS	REAL		BH	BH	133	X	X		X	X		
58994	GEOTECH	BH00126AS	REAL		GEOTECH	BH	115/196							X
58994	GEOTECH	BH00127AS	REAL		GEOTECH	BH	115/196							X
59094	GEOTECH	BH00202AS	REAL		GEOTECH	BH	115/196							X
59094	GEOTECH	BH00203AS	REAL		GEOTECH	BH	115/196							X
59094	GEOTECH	BP00023AS	REAL		DRUM	BH	115/196	X	X	X	X	X		
59094	GEOTECH	BP00024AS	RNS		DRUM	BH	115/196	X	X	X	X	X		
59094	GEOTECH	BP00030AS	TB		DRUM	BH	115/196			X				
59194	GEOTECH	BH00238AS	REAL		GEOTECH	WELL	115/196							X
59194	GEOTECH	BH00239AS	REAL		GEOTECH	WELL	115/196							X
59194	GEOTECH	BH00240AS	REAL		GEOTECH	WELL	115/196							X
59194	GEOTECH	BH00241AS	REAL		GEOTECH	WELL	115/196							X
59194	GEOTECH	BH00242AS	REAL		GEOTECH	WELL	115/196							X
59194	GEOTECH	BP00039AS	REAL	BP00040AS	DRUM	WELL	115/196	X	X	X	X	X		
59194	GEOTECH	BP00040AS	DUP	BP00039AS	DRUM	WELL	115/196	X	X	X	X	X		
59194	GEOTECH	BP00041AS	RNS		DRUM	WELL	115/196	X	X	X	X	X		
59194	GEOTECH	BP00052AS	TB		DRUM	WELL	115/196							
59194	GEOTECH	BH00170AS	REAL		GEOTECH	WELL	115/196							X
59194	GEOTECH	BH00171AS	REAL		GEOTECH	WELL	115/196							X

Table 2-8 (Continued)

Location	TM15 Program	Sample Number	QC Code	QC Partner	Sample Type	Completion Type	IHSS	Analyses Requested						
								Rads	Metals	VQA	SVQA	Leach/B	Water Qual	(see tech)
59 94	GEOTECH	BH00172AS	REAL		GEOTECH	WELL	115/196							X
59294	GEOTECH	BH00173AS	REAL		GEOTECH	WELL	115/196							X
59294	GEOTECH	BP00003AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
59494	GW	BH00149AS	RNS		BH	BH	115/196	X	X	X	X	X		
59494	GW	BH00150AS	REAL		BH	BH	115/196			X				
59494	GW	BH00151AS	REAL		BH	BH	115/196			X				
59494	GW	BH00152AS	REAL		BH	BH	115/196	X	X		X	X		
59494	GW	BH00153AS	REAL		BH	BH	115/196			X				
59494	GW	BH00154AS	REAL		BH	BH	115/196			X				
59494	GW	BH00155AS	REAL		BH	BH	115/196	X	X		X	X		
59494	GW	BH00156AS	REAL		BH	BH	115/196			X				
59494	GW	BH00157AS	REAL		BH	BH	115/196			X				
59494	GW	BH00158AS	REAL		BH	BH	115/196			X				
59494	GW	BH00159AS	REAL	BH00160AS	BH	BH	115/196	X	X		X	X		
59494	GW	BH00160AS	DUP	BH00159AS	BH	BH	115/196	X	X		X	X		
59494	GW	BH00165AS	TB		BH	BH	115/196			X				
59594	GEOTECH	BH00132AS	REAL		GEOTECH	WELL	115/196							X
59594	GEOTECH	BH00133AS	REAL		GEOTECH	WELL	115/196							X
59594	GEOTECH	BH00135AS	REAL		GEOTECH	WELL	115/196							X
59594	GEOTECH	BH00136AS	REAL		GEOTECH	WELL	115/196							X
59594	GEOTECH	BH00137AS	REAL		GEOTECH	WELL	115/196							X
59594	GEOTECH	BP00001AS	REAL		DRUM	WELL	115/196			X				
59594	GEOTECH	BP00002AS	REAL		DRUM	WELL	115/196			X				
59594	GEOTECH	BP00006AS	REAL		DRUM	WELL	115/196		X					
59594	GEOTECH	BP00037AS	REAL		DRUM	WELL	115/196		X					
59594	GEOTECH	BP00038AS	RNS		DRUM	WELL	115/196		X					
59694	GEOTECH	BH00211AS	REAL		GEOTECH	WELL	115/196							X
59694	GEOTECH	BH00212AS	REAL		GEOTECH	WELL	115/196							X
59694	GEOTECH	BH00213AS	REAL		GEOTECH	WELL	115/196							X
59694	GEOTECH	BH00214AS	REAL		GEOTECH	WELL	115/196							X
59694	GEOTECH	BH00215AS	REAL		GEOTECH	WELL	115/196							X
59694	GEOTECH	BP00028AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
59694	GEOTECH	BP00031AS	RNS		DRUM	WELL	115/196	X	X					
59794	GEOTECH	BH00178AS	REAL		GEOTECH	WELL	115/196							X
59794	GEOTECH	BH00179AS	REAL		GEOTECH	WELL	115/196							X
59794	GEOTECH	BH00180AS	REAL		GEOTECH	WELL	115/196							X
59794	GEOTECH	BP00005AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
59894	GW	BH00161AS	REAL		BH	WELL	115/196			X				
59894	GW	BH00162AS	REAL		BH	WELL	115/196	X	X		X	X		
59894	GW	BH00163AS	RNS		BH	WELL	115/196	X	X	X	X	X		
59894	GW	BH00164AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
59894	GW	BH00166AS	TB		BH	WELL	115/196			X				
59894	GW	BP00007AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
59894	GW	BP00010AS	FB		DRUM	WELL	115/196			X				
59894	GW	BP00011AS	REAL		DRUM	WELL	115/196	X	X	X				
59894	GW	BP00012AS	REAL		DRUM	WELL	115/196	X	X	X				
59894	GW	BP00020AS	TB		DRUM	WELL	115/196			X				
59994	IDEM	BH00088AS	REAL		BH	BH	133	X	X	X	X	X		
60094	IDEM	BH00089AS	REAL		BH	BH	133	X	X					
71194	GEOTECH	BH00182AS	REAL		GEOTECH	WELL	115/196							X
71194	GEOTECH	BH00183AS	REAL		GEOTECH	WELL	115/196							X
71194	GEOTECH	BH00184AS	REAL		GEOTECH	WELL	115/196							X
71194	GEOTECH	BP00008AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
71194	GEOTECH	BP00009AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
71194	GEOTECH	BP00071AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
71194	GEOTECH	BP00025AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
71294	GEOTECH	BH00204AS	REAL		GEOTECH	BH	115/196							X
71 94	GEOTECH	BH00205AS	REAL		GEOTECH	BH	115/196							X

Table 2-6 (Continued)

Location	TM15 Program	Sample Number	QC Code	QC Partner	Sample Type	Completion Type	IHSS	Analyses Requested						
								Rads	Metals	VQA	SVQA	Positiv B	W ter Qual	Cor tech
71 94	GEOTECH	BH00206AS	REAL		GEOTECH	BH	115/196							X
71794	GEOTECH	BH00207AS	REAL		GEOTECH	BH	115/196							X
71794	GEOTECH	BH00208AS	REAL		GEOTECH	BH	115/196							X
71294	GEOTECH	BH00209AS	REAL		GEOTECH	BH	115/196							X
71294	GEOTECH	BH00210AS	REAL		GEOTECH	BH	115/196							X
71294	GEOTECH	BP00026AS	REAL		DRUM	BH	115/196	X	X	X	X	X		
71794	GEOTECH	BP00027AS	RNS		DRUM	BH	115/196	X	X	X	X	X		
71394	GW	BH00245AS	REAL		GEOTECH	BH	133							X
71494	GEOTECH	BH00243AS	REAL		GEOTECH	WELL	115/196							X
71494	GEOTECH	BP00042AS	REAL	BP00043AS	DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00043AS	DUP	BP00042AS	DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00044AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00045AS	REAL		DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00047AS	RNS		DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00048AS	REAL	BP00049AS	DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00049AS	DUP	BP00048AS	DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00050AS	RNS		DRUM	WELL	115/196	X	X	X	X	X		
71494	GEOTECH	BP00051AS	TB		DRUM	WELL	115/196			X				
SS133194	SS	SS00001AS	REAL		SS	SS	115/196	X						
SS133294	SS	SS00002AS	REAL		SS	SS	115/196	X						
SS133394	SS	SS00003AS	REAL		SS	SS	115/196	X						
SS133494	SS	SS00004AS	REAL		SS	SS	115/196	X						
SS133594	SS	SS00005AS	REAL		SS	SS	115/196	X						
SS133694	SS	SS00006AS	REAL		SS	SS	115/196	X						
SS133794	SS	SS00007AS	REAL		SS	SS	115/196	X						
SS133894	SS	SS00008AS	REAL	SS00009AS	SS	SS	115/196	X						
SS133894	SS	SS00009AS	DUP	SS00008AS	SS	SS	115/196	X						
SS133894	SS	SS00010AS	RNS		SS	SS	115/196	X						

Table 2 7

Constituent (COCs are <i>Bold/Italic</i>)	OU 5 or Background Data	Number of Samples	Range of Reporting Limits (ug/l)	Percent Detection	Range of Non-detected Concentrations (ug/l)	Range of Detected Concentrations (ug/l)	Mean** Concentration (ug/l)	Standard Deviation**
Total Concentrations								
Aluminum	Background	149	18 -- 200	91 28	22 6 -- 200	26 8 -- 63 900	3 495 55	7 758 70
	IHSS 115	11	11 -- 200	100	N/A	129 75 -- 42 800	12 623 35	17 019 88
	IHSS 133	4	11 -- 26	100	N/A	47 -- 103 000	45 786 75	42733 07
	Pre-TM15	17	18 -- 200	88 24	200	1,100 -- 357,000	66 186 18	99 719 80
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							45,224 03	-32%
Antimony	Background	141	17 -- 60	16 31	7 -- 70	7 1 -- 86 6	16 37	11 19
	IHSS 115	13	2 -- 60	15	1 -- 30	13 5 -- 13 7	20 22	11 71
	IHSS 133	4	2 13	0	1 -- 6 5	N/A	4 90	2 63
	Pre-TM15	16	17 60	12 5	27 60	39 2 -- 40 8	25 44	8 69
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							20 89	16%
Arsenic	Background	138	0 7 -- 10 000	11 59	0 7 10	0 8 -- 3 0	1 83	1 76
	IHSS 115	13	1 10	38	1 5 -- 27 3	2 3 -- 12	8 32	7 25
	IHSS 133	3	1 3	33	0 7 -- 4 7	2 6	2 67	2
	Pre-TM15	17	2 -- 10	64 71	3 10	1 1 -- 13 3	5 60	2 98
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							6 41	14%
Barium	Background	149	2 1 -- 200	81 21	100 -- 200	25 9 -- 752	106 13	69 40
	IHSS 115	13	0 4 -- 200	100	N/A	37 1 -- 645	322 93	220 95
	IHSS 133	4	0 4 -- 12	100	N/A	137 -- 619	364 50	197 6
	Pre-TM15	17	16 -- 200	100	N/A	23 7 -- 3,040	873 95	872 28
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							603.33	-31%
Beryllium	Background	148	0 6 -- 5	7 43	0 8 -- 5	0 7 -- 4 8	1 05	0 87
	IHSS 115	13	0 2 -- 5	46	0 5 -- 2 5	0 21 -- 2 6	2 01	0 79
	IHSS 133	3	0 2 -- 1	100	N/A	2 2 -- 6 7	4 07	2 35
	Pre-TM15	17	1 -- 5	64 71	1 -- 5	1 55 -- 29 4	6 38	8 01
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							4 48	30%
Cadmium	Background	148	2 3 -- 5	11 49	1 -- 11 1	1 1 -- 7 8	1 52	1 07
	IHSS 115	13	1 6 -- 5	15	0 8 -- 2 5	2 1 -- 4 9	2 33	0 94
	IHSS 133	4	1 6 -- 3	0	0 8 -- 1 5	N/A	1 20	0 36
	Pre-TM15	17	2 -- 5	17 65	2 5	4 2 -- 8 2	2 71	1 98
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							2.39	12%
Calcium	Background	149	17 4 -- 5 000	100	N/A	15 950 -- 186 000	55 030 23	31 667 78
	IHSS 115	13	3 4 -- 5 000	100	N/A	43 800 -- 237 500	100 915 38	56 451 10
	IHSS 133	4	3 4 -- 20	100	N/A	48 100 -- 61 500	53 825 00	6148 92
	Pre-TM15	17	149 -- 5,000	100	N/A	53,200 -- 413,000	117,244 10	84 416 57
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							103,539 70	12%
Cesium	Background	142	500 -- 1 000	10 56	2 -- 1 000	30 -- 90	151 81	200 34
	IHSS 115	13	20 -- 1 000	0	10 -- 500	N/A	287 29	239 61
	IHSS 133	4	22 -- 79	0	21 5 -- 39 5	N/A	31 83	7 54
	Pre-TM15	17	13 -- 1,000	17 65	32 -- 1 000	13 -- 40	285 71	215 93
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							266 45	10%
Chromium	Background	145	2 -- 10	41 38	2 14 9	2 1 -- 729	12 30	60 77
	IHSS 115	13	1 8 -- 10	31	0 9 -- 35 5	28 -- 52 1	18 82	17 25
	IHSS 133	4	1 8 -- 3	75	1 5	38 6 -- 110	47 63	45 28
	Pre-TM15	17	3 -- 10	70 59	5 10	9 3 -- 442	84 34	128 03
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							54 97	35%
Cobalt	Background	148	2 7 -- 50	13 51	2 50	3 2 -- 39 4	7 56	9 69
	IHSS 115	12	1 4 -- 50	58	4 -- 25	5 4 -- 24 5	18 63	7 56
	IHSS 133	4	1 4 -- 7	75	3 5	15 4 -- 34 8	17 67	12 91
	Pre-TM15	17	4 -- 50	70 59	6 50	5 6 -- 161	42 13	41 17
Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							30 62	27%

Table 2 7 (Continued)

Constituent (COCs are <i>Bold/Italic</i>)	OU 5 or Background Data	Number of Samples	Range of Reporting Limits (ug/l)	Percent Detection	Range of Non-detected Concentrations (ug/l)	Range of Detected Concentrations (ug/l)	Mean** Concentration (ug/l)	Standard Deviation**
Copper	Background	148	2 25	54 05	2 77 5	1 105	9 43	11 12
	IHSS 115	13	1 1 25	46	7 2 44 6	2 5 -- 124	41 20	40 53
	IHSS 133	4	1 1 3	75	5 4	26 3 -- 75	34 43	29 25
	Pre-TM15	17	2 25	82 35	25	11 15 420	101 11	128 86
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							70 36
Iron	Background	149	4 7 100	93 29	11 8 -- 449	6 5 -- 97 000	3 906 27	9 681 12
	IHSS 115	13	2 100	100	N/A	276 8 -- 71 800	25 207 33	27 234 94
	IHSS 133	4	2 -- 7 3	75	141	36 200 -- 110 000	47 435 25	45802 5
	Pre-TM15	17	5 -- 100	88 24	100	3,190 -- 418,000	90,870 00	114 363 70
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							80,663 71
Lead	Background	141	0 8 -- 3 000	63 12	1 5	1 -- 52 50	3 57	5 53
	IHSS 115	13	0 9 -- 3	62	1 5	1 3 -- 74 7	24 04	27 88
	IHSS 133	4	0 9 -- 2	50	0 45 -- 1	13 5 -- 34 1	12 26	15 76
	P e-TM15	17	1 -- 5	88 24	5	1 2 -- 240	54 72	69 08
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							37 99
Lithium	Background	149	2 100	77 18	3 15 -- 100	1 1 -- 266	33 25	48 46
	IHSS 115	12	1 100	58	5 5 -- 50	15 2 -- 181 5	55 22	48 71
	IHSS 133	4	1 -- 14	100	N/A	23 7 -- 75 8	42 23	23 15
	Pre-TM15	17	2 100	82 35	17 -- 30	5 -- 306	73 72	96 52
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							63 18
Magnesium	Background	149	29 6 -- 5 000	97 99	5 000	2 465 -- 47 900	10 330 61	7 943 20
	IHSS 115	13	12 -- 5 000	100	N/A	9 505 -- 68 800	23 708 08	15 766 02
	IHSS 133	4	12 -- 37	100	N/A	14 500 -- 26 800	18 675 00	5517 47
	Pre-TM15	17	45 -- 5,000	100	N/A	14,200 -- 113,000	34,694 12	27,169 76
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							28,808 97
Manganese	Background	149	1 -- 15	90 6	1 15	1 8 -- 1 950	92 17	187 34
	IHSS 115	13	0 5 -- 15	100	N/A	18 45 -- 3 280	1 325 64	1 224 08
	IHSS 133	4	0 5 -- 1	75	5 7	417 -- 1 120	604 18	493 99
	Pre-TM15	17	1 -- 15	100	N/A	14 -- 13,700	2,847 89	3 232 99
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							2,001 89
Mercury	Background	148	0 2	2 03	0 2 -- 0 22	0 21 -- 0 27	0 10	0 02
	IHSS 115	13	0 2	23	0 1	0 2 -- 0 82	0 17	0 20
	IHSS 133	4	0 2	0	0 1	N/A	0 10	0
	Pre-TM15	17	0 2	29 41	0 2	0 24 -- 3	0 42	0 74
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							0 29
Molybdenum	Background	150	3 5 -- 200	28	2 200	2 2 -- 80 5	23 84	39 57
	IHSS 115	13	2 5 -- 200	8	6 -- 100	5 2	56 98	48 37
	IHSS 133	3	2 5 -- 3	33	5 -- 8 8	3 5	5 77	2 73
	Pre-TM15	17	7 -- 200	17 65	11 -- 200	11 1 -- 18	46 35	46 38
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							46 85
Nickel	Background	146	11 -- 40	28 08	2 -- 40	2 1 -- 334	12 49	28 44
	IHSS 115	13	3 7 -- 40	54	1 85 -- 20	20 5 41	23 75	11 17
	IHSS 133	4	3 7 -- 12	75	6	25 7 -- 75 5	34 06	29 44
	Pre-TM15	17	10 -- 40	82 35	11 -- 40	13 6 -- 313 0	82 17	92 59
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							54 17
Potass um	Background	150	675 -- 5 000	78 67	289 -- 5 000	243 -- 8 370	1 730 24	1 177 83
	IHSS 115	13	360 -- 5 000	62	2 500	1 190 -- 11 500	4 912 31	3 679 45
	IHSS 133	4	360 -- 680	100	N/A	1 450 -- 13 700	6 800 00	5086 98
	Pre-TM15	17	640 -- 5,000	82 35	5 000	3 670 -- 49,700	11 681 76	13 052 86
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							8,619 12
Selenium	Background	145	1 4 -- 5	23 45	1 5	1 05 -- 456	7 64	41 84
	IHSS 115	13	2 5	8	1 6 8	8 3	3 25	2 27
	IHSS 133	4	2 -- 3	0	1 4 3	N/A	1 90	1 61
	Pre-TM15	16	2 -- 5	25	2 5	4 7 -- 126	10 63	30 87
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							6 66

Table 2 7 (Continued)

Constituent (COCs are <i>Bold/Italic</i>)	OU 5 or Background Data	Number of Samples	Range of Reporting Limits (ug/l)	Percent Detection	Range of Non-detected Concentrations (ug/l)	Range of Detected Concentrations (ug/l)	Mean** Concentration (ug/l)	Standard Deviation**
Silicon	Background	84	1 4 1 000	100	N/A	1 31 -- 116 000	16 575 34	15 401 00
	IHSS 115	13	9 100	100	N/A	4 770 -- 87 500	32 034 23	28 048 25
	IHSS 133	4	9 120	100	N/A	8 050 -- 140 000	80 287 50	54614 05
	Pre-TM15	17	13 100	100	N/A	7 130 -- 354 000	79,041 47	87 784 49
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							61,214 71
Silver	Background	147	2 1 -- 10	6 8	2 -- 10	2 1 -- 4 8	2 15	1 62
	IHSS 115	12	2 10	17	1 5	8 2 -- 11 2	4 70	2 87
	IHSS 133	4	2 4	0	1 2	N/A	1 25	0 5
	Pre-TM15	17	3 10	23 53	3 -- 10	3 6 -- 53 2	7 35	12 27
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							5 68
Sodium	Background	149	28 3 5 000	98 66	5 000	4 300 -- 194 000	30 081 85	40 019 71
	IHSS 115	13	10 5 000	100	N/A	9 780 -- 184 000	42 593 08	50 373 11
	IHSS 133	4	10 23	100	N/A	34 900 -- 47 100	39 725 00	5251 27
	Pre-TM15	17	55 5 000	100	N/A	13,600 -- 120 000	38 650 00	25 878 98
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							40,284 12
Strontium	Background	146	0 8 200	89 73	200	58 1 -- 1 770	313 02	270 75
	IHSS 115	12	0 2 200	100	N/A	232 -- 1 485	585 17	370 58
	IHSS 133	4	0 2 -- 1	100	N/A	367 -- 478	420 75	54 05
	Pre-TM15	17	1 200	100	N/A	344 -- 2 575	789 97	521 38
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							670 74
Thallium	Background	146	0 1 -- 10	8 22	0 9 -- 10	1 -- 1 3	1 58	1 79
	IHSS 115	13	1 -- 100	8	0 5 -- 27 5	3 8	5 59	6 80
	IHSS 133	4	1 4 2	0	0 5 -- 2 1	N/A	1 28	0 68
	Pre-TM15	17	2 -- 10	5 88	3 10	1 3	3 05	1 70
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							3 81
Tin	Background	149	5 -- 200	8 05	9 4 200	14 5 -- 53 1	30 68	36 52
	IHSS 115	12	8 9 -- 200	8	4 45 100	40 3	66 10	42 96
	IHSS 133	4	8 9 -- 24	75	4 45	15 -- 29 7	18 34	11 07
	Pre-TM15	17	18 -- 200	35 29	28 -- 200	36 4 -- 300	88 91	64 34
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							72.06
Vanadium	Background	149	3 -- 50	71 14	2 -- 50	2 2 -- 167	14 46	18 72
	IHSS 115	13	1 5 -- 50	62	25	3 6 -- 93 9	43 58	29 95
	IHSS 133	4	1 5 -- 3	75	1 5	60 4 -- 183	80 48	75 64
	Pre-TM15	17	3 -- 50	76 47	4 50	19 85 -- 674	150 03	201 57
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							101 15
Zinc	Background	149	1 7 -- 20	77 18	4 2 -- 36 6	5 9 -- 498	35 85	50 33
	IHSS 115	12	1 -- 20	92	19 8	12 75 -- 261	81 83	84 93
	IHSS 133	4	1 -- 2	75	18 1	75 4 -- 180	87 43	67 45
	Pre-TM15	17	3 -- 20	82 35	20	37 8 -- 982	248 77	288 25
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							188 61

Notes OU 5 data where

IHSS 115 refers to groundwater samples obtained at IHSS 115 for the groundwater monitoring program as detailed in TM15

IHSS 133 refers to groundwater samples obtained at IHSS 133 for the groundwater monitoring program as detailed in TM15

Pre-TM15 refers to samples collected within OU 5 prior to January 1994

Mean and Standard Deviation are calculated assuming data are normally distributed

ug/l micrograms per liter N/A = not applicable

Table 2-8
Summary Statistics for Dissolved Data from Groundwater Samples

Constituent (COCs are Bold/italic)	CU 5 or Background Data	Number of Samples	Range of Reporting Limits (ug/l)	Percent Detection	Range of N -detected Concentrations (ug/l)	Range of Detected Concentrations (ug/l)	Mean Concentration (ug/l)	Standard Deviation
Dissolved Concentrations								
Aluminum	Background	248	10 - 200	68.15	5 - 200	5.1 - 8.610	105.38	595.50
	IHSS 115	25	8.6 - 200	24	4.3 - 291.5	26.4 - 900	437.86	1,231.98
	IHSS 133	9	8.6 - 200	0	4.3 - 100	N/A	57.79	50.08
	Pre-TM15	14	18 - 200	21.43	24 - 200	24.2 - 37.7	43.24	37.78
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							251.50 482%
Antimony	Background	248	0.05 - 60	28.23	6 - 60	7.8 - 54.1	15.00	9.95
	IHSS 115	25	2 - 60	12	5.5 - 30	3.8 - 71.9	27.48	13.11
	IHSS 133	9	11 - 60	0	5.5 - 30	N/A	19.33	12.65
	Pre-TM15	14	17 - 60	7.4	27 - 60	39.4	23.17	8.08
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							24.69 7%
Arsenic	Background	220	0.8 - 10	5	0.8 - 10	1 - 15	1.61	1.84
	IHSS 115	27	1 - 10	25.9	0.7 - 5	1.3 - 9.3	3.99	1.96
	IHSS 133	8	1 - 10	13	0.7 - 5	1	2.93	2.22
	Pre-TM15	14	2 - 10	42.86	2 - 10	2.8 - 8.05	3.98	2.55
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							3.81 -4%
Barium	Background	256	0.02 - 200	84.38	40 - 200	23.6 - 203	83.30	33.43
	IHSS 115	25	0.6 - 200	100	N/A	16.75 - 457	198.49	121.28
	IHSS 133	8	0.6 - 200	100	N/A	61.5 - 145	113.80	31.37
	Pre-TM15	14	16 - 200	100	N/A	108 - 647	242.18	150.33
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							198.03 19%
Beryllium	Background	212	0.2 - 5	2.36	0.3 - 5	0.8 - 4	0.95	0.82
	IHSS 115	26	0.2 - 5	7.7	0.1 - 2.5	0.49 - 0.56	1.79	0.99
	IHSS 133	8	0.2 - 5	0	0.1 - 2.5	N/A	1.40	1.19
	Pre-TM15	14	1 - 5	0	1 - 5	N/A	N/A	N/A
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							1.21 N/A
Cadmium	Background	240	0.1 - 5	13.33	1 - 5	1 - 8.6	1.55	0.99
	IHSS 115	25	2 - 5	4	1 - 2.5	3.1	2.30	0.51
	IHSS 133	8	2 - 5	0	1 - 2.5	N/A	1.81	0.75
	Pre-TM15	14	2 - 5	0	2 - 5	N/A	N/A	N/A
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							1.53 N/A
Calcium	Background	257	15.7 - 5,000	100	N/A	1,700 - 184,000	55,205.54	32,672.70
	IHSS 115	25	7 - 5,000	100	N/A	31,000 - 235,500	98,824.00	54,032.61
	IHSS 133	8	6 - 5,000	100	N/A	25,500 - 72,900	43,850.00	14,476.38
	Pre-TM15	14	29 - 5,000	100	N/A	43,300 - 156,000	79,292.86	35,514.55
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							83,848.94 3%
Cesium	Background	212	5 - 2,500	8.96	2 - 2,500	30 - 400	185.41	239.92
	IHSS 115	26	20 - 1,000	0	10 - 500	N/A	393.42	198.81
	IHSS 133	9	43 - 1,000	0	21.5 - 500	N/A	291.73	247.02
	Pre-TM15	14	13 - 1,000	7.14	13 - 1,000	14	272.25	213.82
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							348.12 25%
Chromium	Background	250	2 - 10	24	1 - 13.6	2.2 - 23.2	4.40	3.57
	IHSS 115	26	2 - 10	0	1 - 11.3	N/A	4.65	2.47
	IHSS 133	8	2 - 10	0	1 - 5	N/A	3.00	2.14
	Pre-TM15	14	3 - 10	0	3 - 10	N/A	N/A	N/A
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							3.02 N/A
Cobalt	Background	231	0.02 - 50	9.52	2 - 50	2 - 9.5	8.08	8.53
	IHSS 115	25	2 - 50	28	3 - 25	3.4 - 13.3	17.17	9.98
	IHSS 133	9	2 - 50	11	1 - 25	5.1	12.18	12.23
	Pre-TM15	14	4 - 50	14.29	5 - 50	5.7 - 11.1	11.45	10.72
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							14.57 27%
Copper	Background	250	2 - 25	28.4	1 - 68.5	1.3 - 175	5.74	12.68
	IHSS 115	26	1.6 - 25	11.5	1 - 42.8	3.1 - 12.9	10.75	8.50
	IHSS 133	9	1.6 - 25	11	0.8 - 44.7	2.3	11.09	13.8
	Pre-TM15	14	2 - 25	0	2 - 25	N/A	N/A	N/A
	Mean of CU 5 Data and Percent Change from Pre-TM15 Mean --							7.74 N/A

Table 2-8 (Continued)

Constituent (COCs are <i>Bold/Italic</i>)	OU 5 or Background Data	Number of Samples	Range of Reporting Limits (ug/l)	Percent Detection	Range of Non-detected Concentrations (g/l)	Range of Detected Concentrations (ug/l)	Mean Concentration (ug/l)	Standard Deviation
Iro	Background	256	4.7 100	62.5	2 1106.5	2.8 8790	86.61	554.79
	IHSS 115	27	1.8 100	85.2	3 167	32.7 29000	6924.68	10872.10
	IHSS 133	9	1.8 100	78	0.9 6.8	2.1 628	181.23	208.91
	Pre-TM15	14	5 100	78.57	5 45.7	24.7 34,900	8,636.80	10489.84
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							8186.65
Lead	Background	251	0.8 20	14.74	0.4 5.7	0.8 64	1.54	4.76
	IHSS 115	26	0.9 -- 5	7.7	0.45 2.5	4.6 -- 5.7	1.89	1.15
	IHSS 133	8	0.9 -- 5	13	0.45 2.5	0.92	1.35	0.97
	Pre-TM15	14	1 3	0	1 3	N/A	N/A	N/A
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean							1.25
Lithium	Background	250	2 100	70.4	1 100	1.2 250	33.44	54.22
	IHSS 115	24	1 100	20.8	1 50	12.5 172	47.28	34.04
	IHSS 133	8	1 100	50	50	10.6 20	31.54	19.97
	Pre-TM15	14	2 100	35.71	17 100	4.2 30	14.96	11.90
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean							34.71
Magnesium	Background	254	0.1 5000	96.08	28.5 5000	2355 46300	10015.78	8302.90
	IHSS 115	25	12 5000	100	N/A	8680 -- 68900	20942.80	13316.92
	IHSS 133	9	12 5000	89	2500	8080 -- 17000	9887.78	3903.61
	Pre-TM15	14	45 5000	100	N/A	10,100 -- 22200	15307.14	4005.23
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean							17228.25
Manganese	Background	256	1 15	60.16	1 24.35	1 934	30.94	87.98
	IHSS 115	24	0.6 -- 15	100	N/A	7.4 3,530	1122.75	1286.52
	IHSS 133	8	0.6 -- 15	100	N/A	1.3 843	231.93	356.63
	Pre-TM15	14	1 15	92.86	2	286 10500	2370.71	2,750.95
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							1,347.64
Mercury	Background	207	0.02 0.2	2.42	0.1 0.24	0.2 0.69	0.11	0.06
	IHSS 115	24	0.2	0	0.1	N/A	0.10	0.00
	IHSS 133	9	0.2	0	0.1	N/A	0.10	0
	Pre-TM15	14	0.2	0	0.2	N/A	N/A	N/A
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean							0.07
Molybde um	Background	241	3.5 200	28.63	2 200	2 114	19.18	34.02
	IHSS 115	25	3 200	4	3.2 100	4.6	77.49	40.89
	IHSS 133	9	3 200	11	1.5 100	12.2	57.81	50.12
	Pre-TM15	14	7 200	0	11 200	N/A	N/A	N/A
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean							51.20
Nickel	Background	238	0.02 40	22.03	2 40	2 35.8	6.48	6.89
	IHSS 115	26	4.1 40	30.8	2.5 20	5.9 64.6	17.95	11.82
	IHSS 133	8	4.1 -- 40	25	2.05 20	48 87.7	23.16	30.54
	Pre-TM15	14	10 -- 40	0	10 40	N/A	N/A	N/A
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --							13.89
Potassium	Background	253	0.02 5000	77.87	20 5000	170 -- 8110	1346.50	1078.02
	IHSS 115	26	363 -- 5000	50	2500 7810	783 -- 6550	3724.73	2202.46
	IHSS 133	8	381 -- 5000	50	2500	992 -- 1540	1879.00	679.89
	Pre-TM15	14	640 -- 5000	92.86	776	813 -- 6,110	2,397.07	1698.68
	Mean of OU 5 Data and Percent Cha ge from Pre-TM15 Mean --							3,028.87
Selenium	Background	220	1.2 10	28.64	1 5	1 607	8.29	44.80
	IHSS 115	27	2 5	11.1	1 655	3.2 -- 5.2	2.19	1.31
	IHSS 133	8	2 5	13	1 2.5	3.2	2.08	0.84
	Pre-TM15	14	2 5	14.29	2 5	1.5 -- 2.3	1.52	0.64
	Mean of OU 5 D ata and Percent Change from Pre-TM15 Mean --							1.88
Silver	Background	236	2 25	19.92	2 10	2.4 13600	60.29	885.11
	IHSS 115	24	2 10	4.2	1 5	3.8	4.11	1.45
	IHSS 133	8	2 10	0	1 5	N/A	3.08	2.07
	Pre-TM15	14	3 10	0	3 0	N/A	N/A	N/A
	Mean of OU 5 ata and Perce t Change from Pre-TM15 Mean --							2.68

Table 2-8 (Continued)

Constituent (COCs are <i>Bold/italic</i>)	U 5 or Background Data	Number of Samples	Range of Reporting Limits (ug/l)	Percent Detection	Range of Non-detected Concentrations (ug/l)	Range of Detected Concentrations (ug/l)	Mean Concentration (g/l)	Standard Deviation
Sodium	Background	255	10 5 000	98 82	10 5 000	4 060 252 000	31 887 46	43 627 69
	IHSS 115	26	10 5 000	96 2	2 500	7 440 192 000	34 492 31	41 256 34
	IHSS 133	8	10 5 000	100	N/A	18 000 71 900	36,975 00	16874 13
	Pre-TM15	14	55 5,000	100	N/A	12 400 44 000	28,057 14	10 540 03
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --						33 028 17	18%
Strontium	Background	253	0 7 200	92 89	100 1 000	51 05 7 930	351 76	564 63
	IHSS 115	24	0 3 200	100	N/A	225.5 1 480	600 35	340 45
	IHSS 133	8	0 3 200	100	N/A	175 -- 419	297 88	87 69
	Pre-TM15	14	1 200	100	N/A	280 -- 754	475.29	157 06
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --						508 68	7%
Thallium	Background	214	0 1 200	5 14	0 6 10	1 328	3 50	23 34
	IHSS 115	26	1 10	7 7	0 5 7 15	3 9 -- 4 1	4 11	1 60
	IHSS 133	9	1 10	0	0 5 5	N/A	3 41	1 95
	Pre-TM15	14	2 10	0	3 10	N/A	N/A	N/A
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --						2 80	N/A
Tin	Background	236	0 1 1 000	28 81	2 200	10 7 8 830	68.55	574 12
	IHSS 115	25	7 3 200	4	3 65 100	26.2	79 21	37 94
	IHSS 133	9	7 3 200	0	3 65 100	N/A	57 78	50 1
	Pre-TM15	13	18 200	7 69	28 200	29 7	48 60	42 49
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean						68 64	37%
Vanadium	Background	249	1 2 50	53 82	1 50	2 05 19 6	7 32	8 00
	IHSS 115	27	1 4 -- 50	11 1	1 25	1 9 12 9	17 65	10 79
	IHSS 133	9	1 4 -- 50	11	0 7 25	2	14 41	12.56
	Pre-TM15	14	3 50	7 14	4 50	6 6	10 76	11 07
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean						15 14	41%
Zinc	Background	256	1 7 20	67 19	1 1 48 7	1 3 137	13 33	17 85
	IHSS 115	26	1 20	73 1	1 10	3 4 89 7	18 64	16 14
	IHSS 133	9	1 20	78	4 4 14	4 1 23 8	12 44	7 16
	Pre-TM15	14	3 20	42 86	3 20	2 9 46 8	8.36	11 56
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean						14 87	74%

Notes OU 5 data where

IHSS 115 refers to groundwater samples obtained at IHSS 115 for the groundwater monitoring program as detailed in TM15

IHSS 133 refers to groundwater samples obtained at IHSS 133 for the groundwater monitoring program as detailed in TM15

Pre-TM15 refers to samples collected within OU 5 prior to January 1994

Mean and Standard Deviation are calculated assuming data are normally distributed

ug/l micrograms per liter N/A not applicable.

Table 2 9
Summary Statistics for Radionuclide Data from Groundwater Samples

Constituent (COCs are <i>Bold/Italic</i>)	OU 5 or Background Data	Number of Samples	Range of Activities (pCi/l)	Mean Activity (pCi/l)	Standard Deviation
Total Activities					
Americium 241	Background	183	0 007 -- 0 1	0 006	0 01
	IHSS 115	27	0 -- 0 06	0 01	0 01
	IHSS 133	6	0 -- 0 01	0 00	0
	Pre-TM15	15	0 007 -- 0 2	0 03	0 05
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean --			0 02	-50%
Plutonium 238	Background	15	0 001 -- 0 03	0 003	0 01
	IHSS 115	20	0 01 -- 0 03	0 00	0 01
	IHSS 133	5	0	0 00	0
	Pre-TM15	2	0 005 -- 0 01	0 007	0
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 001	-93%
Plutonium 239/240	Background	194	0 006 -- 0 22	0 004	0 02
	IHSS 115	26	0 -- 0 34	0 03	0 07
	IHSS 133	6	0 -- 0 02	0 00	0 01
	Pre-TM15	15	0 003 -- 1 04	0 098	0 26
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 05	-51%
Uranium 233/234	Background	35	0 -- 164	15 618	38 75
	IHSS 115	15	0 -- 28 72	7 33	7 91
	IHSS 133	4	0 69 -- 1 5	1 14	0 38
	Pre-TM15	14	0 506 -- 49	9 667	12 25
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			7.57	22%
Uranium 235	Background	35	0 02 -- 6 29	0 617	1 38
	IHSS 115	15	0 02 -- 1 57	0 34	0 41
	IHSS 133	4	0 01 -- 0 07	0 04	0 04
	Pre-TM15	14	0 055 -- 4	0 628	0 99
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 43	-32%
Uranium 238	Background	22	0 -- 108	10 84	27 73
	IHSS 115	15	0 -- 30 74	7 53	9 79
	IHSS 133	4	0 38 -- 1 5	1 07	0 51
	Pre-TM15	14	0 399 -- 44	8 553	10 979
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			7 18	16%
Alpha	Background	23	0 351 362	43 497	94 28
	IHSS 115	10	1 51 -- 73	24 52	23 18
	IHSS 133	3	29 -- 40	34 37	5 5
	Pre-TM15	14	8 1 1 600	213 275	408 8
	Mean of OU 5 Data and Percent Change from Pre TM15 Mean			123 49	-42%
Beta	Background	23	0 2 -- 220	24 945	53 34
	IHSS 115	10	1 25 -- 65	20 70	19 42
	IHSS 133	3	24 -- 45 04	32 35	11 18
	Pre-TM15	14	5 5 -- 1 300	158 102	332 38
	Mean of OU 5 Data and Percent Change from Pre TM15 Mean			93.24	-41%
Cesium 137	Background	156	0 594 -- 1 16	0 12	0 33
	IHSS 115	1	0 6 0 6	0 60	N/A
	Pre-TM15	1	0 38	0 38	N/A
	Mean of OU 5 Data and Percent Change from Pre TM15 Mean			0 49	29%

Table 2 9 (Continued)

Constituent (COCs are <i>Bold/italic</i>)	OU 5 or Background Data	Number of Samples	Range of Activities (pCi/l)	Mean Activity (pCi/l)	Standard Deviation
Radium 226	Background	6	0 182 -- 0 52	0 355	0 13
	IHSS 115	3	1 62 -- 4 4	2 74	1 47
	IHSS 133	3	0 58 1 7	1 13	0 56
	Pre TM15	14	0 46 -- 4 4	2 462	1 63
	Mean of OU 5 Data and Percent Change from Pre TM15 Mean			2.30	-6%
Strontium 89/90	Background	32	0 286 -- 1 12	0 215	0 28
	IHSS 115	5	0 356 -- 1 2	0 819	0 40
	IHSS 133	3	0 02 -- 0 47	0 30	0 25
	Pre TM15	8	0 48 -- 1 5	0 567	0 62
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 60	5%
Tritium	Background	84	240 39 030	624 852	4 246 75
	IHSS 115	9	39 3 322 2	162 869	89 60
	IHSS 133	5	56 4 -- 270 6	134 08	131 65
	Pre-TM15	5	240 -- 557 69	2 062	328 26
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			111 89	5526%
Dissolved Activities					
Americium 241	Background	2	0 003 -- 0 02	0 011	0 011
	IHSS 115	3	0 0024	0 002	0 004
	IHSS 133	3	0 -- 0 01	0 00	0
	Pre-TM15	9	0 004 -- 0 02	0 004	0 006
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 002	-48%
Plutonium 239/240	Background	1	0 011 0 01	0 011	N/A
	IHSS 115	5	0 0093	0 002	0 004
	IHSS 133	3	0	0 00	0
	Pre-TM15	9	0 004 -- 0	0	0 002
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 001	N/A
Uranium 233/234	Background	207	0 024 -- 199 5	6 914	25 439
	IHSS 115	30	0 015 -- 15 055	3 131	3 703
	IHSS 133	8	0 19 -- 1 39	0 60	0 47
	Pre-TM15	19	0 188 -- 11 5	2 701	2 928
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			2 63	3%
Uranium 235	Background	207	0 037 -- 4 8	0 195	0 635
	IHSS 115	30	0 0038 -- 0 846	0 151	0 177
	IHSS 133	8	0 02 0 28	0 08	0 11
	Pre-TM15	19	0 006 -- 0 53	0 162	0 162
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 14	11%
Uranium 238	Background	177	0 038 135 6	4 832	17 673
	IHSS 115	30	0 011 27 575	2 810	5 145
	IHSS 133	8	0 16 -- 3 59	1 04	1 14
	Pre-TM15	19	0 1412 8 8	2 1087	2 154
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			2 33	10%
Alpha	Background	213	0 65 -- 312 7	8 354	32 315
	IHSS 115	25	0 061 45 8	5 182	8 774
	IHSS 133	8	0 22 1 36	0 87	0 44
	Pre-TM15	19	0 27	5 162	6 023
	Mean of OU 5 Data and Percent Change from Pre TM15 Mean			4 51	13%

Table 2 9 (Continued)

Constituent (COCs are <i>Bold/italic</i>)	OU 5 or Background Data	Number of Samples	Range of Activities (pCi/l)	Mean Activity (pCi/l)	Standard Deviation
Beta	Background	196	1 5 -- 135 9	4 892	12 23
	IHSS 115	25	0 0096 -- 19 45	4 972	3 99
	IHSS 133	8	0 35 -- 2 69	1 62	0 86
	Pre TM15	19	1 41 230	17 661	51 529
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			9 09	-49%
Cesium 137	Background	38	0 19 -- 2 6	0 42	0 525
	IHSS 115	15	1 52 -- 0 95	0 11	0 58
	IHSS 133	4	0 -- 0 71	0 26	0 32
	Pre TM15	2	0 -- 0 08	0 04	0 057
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 13	230%
Radium 226	Background	36	0 055 -- 0 53	0 258	0 111
	IHSS 115	2	0 0245 -- 0 889	0 457	0 612
	Pre-TM15	7	0 2 -- 1 03	0 5	0 279
	Mean of OU 5 Data and Percent Change from Pre TM15 Mean			0 49	2%
Strontium 89/90	Background	180	0 396 -- 1 8	0 338	0 306
	IHSS 115	21	0 1131 -- 2 2	0 717	0 491
	IHSS 133	8	0 1 -- 0 55	0 21	0 22
	Pre-TM15	12	0 201 -- 1 83	0 603	0 497
	Mean of OU 5 Data and Percent Change from Pre-TM15 Mean			0 58	-3%

Notes = OU 5 data where

IHSS 115 refers to groundwater samples obtained at IHSS 115 for the groundwater monitoring program as detailed in TM15

IHSS 133 refers to groundwater samples obtained at IHSS 133 for the groundwater monitoring program as detailed in TM15

Pre-TM15 refers to samples collected within OU 5 prior to January 1994

= Mean and Standard Deviation are calculated assuming data are normally distributed

pCi/l = picocuries per liter N/A = not applicable

Table 2 10
Summary of Detected Organic Compounds in Groundwater Samples

TM15 Program Chemical (COCs are in <i>Bold/Italics</i>)	Number of Samples	Range of Reporting Limits (ug/kg)	Percent of Samples Above Detection Limit		Range of Nondetected Concentrations (ug/kg)	Range of Detected Concentrations (ug/kg)	Maximum Concentration Pre-TM15 (ug/kg)
			TM15	Pre-TM15			
115GW Volatile Organic Compounds							
1 1 1 Trichloroethane	31	0.5 – 10	6	5	0.25 – 5	0.3 – 9	40
1 1 2 2 Tetrachloroethane	31	0.5 – 10	3	0	0.25 – 5	4	10
1 1 2 Trichloroethane	31	0.5 – 10	3	0	0.25 – 5	2	10
1 1 Dichloroethane1	31	0.5 – 10	6	0	0.25 – 5	0.4 – 1	10
1 1 Dichloroethane1	31	0.5 – 10	10	5	0.25 – 5	2 – 5	32.5
1 2 Dichloroethane1	26	5 – 10	12	5	2.5 – 5	1 – 3	4
Acetone	25	10	4	5	5	8	4.5
Carbon Disulfide	26	5 – 10	4	0	2.5 – 5	1	10
cis-1 2 Dichloroethene	5	0.5	40	0	0.25	3	0.2
Methylene Chloride	31	0.5 – 10	16	5	0.25 – 5	2 – 4	6
Tetrachloroethene	31	0.5 – 10	16	0	0.25 – 5	0.78 – 24	10
Toluene	31	0.5 – 10	3	0	0.25 – 5	0.3	<10
Trichloroethene	31	0.5 – 10	16	5	0.25 – 5	2 – 50.5	150
Semi-Volatile Organic Compounds							
1 2 3-Trichlorobenzene	5	0.5	20	0	0.25	0.2	0.2
2 4-Dimethylphenol	26	10 – 14	4	0	5 – 100	2	10
2 Methylphenol	26	10 – 14	4	0	5 – 100	1	10
4-Isopropyltoluene	5	0.5	20	0	0.25	0.2	0.2
4-Methylphenol	26	10 – 14	3.8	0	5 – 100	3	10
Acenaphthene	26	10 – 14	11.5	20	5 – 100	2 – 4	5
Anthracene	26	10 – 14	3.8	0	5 – 100	0.5	10
Bis(2 Ethylhexyl)Phthalate	26	10 – 14	34.6	20	5 – 100	1 – 6	3
Butyl Benzyl Phthalate	26	10 – 14	3.8	0	5 – 100	3	10
Carbazole	22	10 – 14	4.5	0	5 – 100	4	10
Di-n-Butyl Phthalate	26	10 – 14	15.4	6.7	5 – 100	0.5 – 3	2
Dibenzofuran	26	10 – 14	3.8	0	5 – 100	2	10
Diethyl Phthalate	26	10 – 14	23.1	6.7	5 – 100	0.7 – 5	6
Fluoranthene	26	10 – 14	11.5	20	5 – 100	1 – 4	4
Fluorene	26	10 – 14	7.7	20	5 – 100	2 – 3	4
Naphthalene	32	0.5 – 14	9.4	11.8	0.25 – 100	0.6 – 16	13
Phenanthrene	26	10 – 25	11.5	20	5 – 100	1 – 4	6
Pyrene	26	10 – 14	11.5	20	5 – 100	1 – 3	6.5
133GW Volatile Organic Compounds							
Methylene Chloride	13	5 – 10	15	5	2.5 – 5	2 – 4	6
Acetone	10	10	10	0	5	27	4.5
Semi-Volatile Organic Compounds							
Bis(2 Ethylhexyl)Phthalate	7	10	14	20	5	2	3
Butyl Benzyl Phthalate	7	10	14	0	5 – 18	4	10
Di-n Butyl Phthalate	7	10	14	6.7	5	2	2
Di-n-Octyl Phthalate	7	10	14	0	5	3	10

Notes OU 5 data where;

115GW refers to groundwater samples obtained at IHSS 115 for the groundwater monitoring program as detailed in TM15

133GW refers to groundwater samples obtained at IHSS 133 for the groundwater monitoring program as detailed in TM15

Mean and Standard Deviation are calculated assuming data are normally distributed

ug/l micrograms per liter N/A not applicable.

Table 2 11
OU 5 Wind Resuspension Potential Study Results

Location	Aggregate Size	Velocity u t	Bare Soil (m 2) (2)	Vegetation	Other Nonerodible	Vertical
	Mode Estimate	Uncorrected (cm/s)		Coverage	Coverage	Fraction
	(mm)	(Figure 3-4) (1)		(m 2) (2 3)	(m 2) (2 3)	Embedded
115AQ1	4 00	115	0 30	0 35	0 65	0 35
115AQ2	3 00	100	0 60	0 15	0 25	0 50
115AQ3	4 00	155	0 40	0 35	0 25	0 50
115AQ4	4 00	115	0 20	0 05	0 80	0 50
115AQ5	1 50	75	0 15	0 80	0 25	0 50
115AQ6	0 50	50	0 10	0 90	0 10	0 75
115AQ7	0 75	58	0 55	0 40	0 15	0 50
115AQ8	4 00	115	0 10	0 90	0 65	0 50
115AQ9	1 50	75	0 05	0 95	0 15	0 50
115AQ10	0 75	58	0 05	0 95	0 03	0 80
115AQ11	3 00	100	0 05	0 95	0 25	0 50
115AQ12	1 50	75	0 00	1 00	0 05	0 50
115AQ13	1 00	65	0 25	0 75	0 10	0 50
115AQ14	4 00	115	0 00	1 00	0 70	0 50
115AQ15	0 75	58	0 00	1 00	0 30	0 80
SASH AQ16	0 75	58	0 20	0 80	0 30	0 50
SASH AQ17	0 30	40	0 03	0 97	0 30	0 50
209AQ18	4 00	115	0 25	0 40	0 40	0 50
209AQ19	4 00	115	0 20	0 30	0 50	0 50
209AQ20	4 00	115	0 10	0 50	0 85	0 80
W209AQ21	0 50	50	0 10	0 90	0 15	0 50
W209AQ22	0 75	58	0 10	0 90	0 03	0 50
OU3T 1AQ23	0 30	40	0 25	0 70	0 05	0 25
OU3T 2AQ25	0 50	50	0 35	0 60	0 15	0 20
OU3T 3AQ24	2 00	88	0 05	0 25	0 70	0 50
OU3T-4AQ26	0 50	50	0 85	0 10	0 10	0 50

Table 2 11 (Continued)

Location	Equivalent Frontal Area of Nonerodible Elements (m ²) (Coverage [1-emb frac])	Lc (Eq Front Area/Area of Bare Soil)	Correction Ratio (Figure 3 5) (1 4)	Threshold Friction Velocity u _t Corrected (cm/s) ([u _t] [Ratio])	Equivalent 10-m Wind Speed (mph) (5)
115AQ1	4225	1 4	10	1150	418
115AQ2	125	2	10	1000	364
115AQ3	125	3	10	1150	418
115AQ4	4	2	10	1150	418
115AQ5	125	8	10	750	273
115AQ6	025	3	10	50	182
115AQ7	075	1	7	406	148
115AQ8	325	3 3	10	1150	418
115AQ9	075	1 5	10	750	273
115AQ10	015	3	10	580	211
115AQ11	0625	1 3	10	1000	364
115AQ12	025	#Div/01	infinite	infinite	infinite
115AQ13	05	2	10	650	236
115AQ14	35	#Div/01	infinite	infinite	infinite
115AQ15	06	#Div/01	infinite	infinite	infinite
SASH-AQ16	15	8	10	580	211
SASH-AQ17	15	5	10	400	145
209AQ18	2	8	10	1150	418
209AQ19	25	1 3	10	1150	418
209AQ20	13	1 3	10	1150	418
W209AQ21	075	8	10	500	182
W209AQ22	0125	1	7	406	148
OU3T 1AQ23	0375	2	10	400	145
OU3T 2AQ25	12	3	10	500	182
OU3T 3AQ24	35	7	10	880	320
OU3T-4AQ26	05	1	7	350	127

Table 2 12
Comparison of Results of 1993 Wind Tunnel Study
and 1995 Rapid Assessment Method

OU 3 Location	Threshold Friction Velocity (cm/s)	
	1993 Wind Tunnel Study (1)	1995 Rapid Assessment Method
T 1	>280	400
T 2	>170	500
T 3	>180	880
T 4	>160	350

Note (1) Source DOE 1994c

Table 2 13**Summary of Radionuclide Data for Surface Soils
from IHSS 209 and Other Surface Disturbances**

Location	Sample Number	Chemical	Results	Units	Error	Qualifier	Validation
SS133194	SS00001AS	Americium 241	0 182	PCI/G	0 061		V
SS133794	SS00002AS	Americium 242	0 042	PCI/G	0 020		V
SS133394	SS00003AS	Americium 243	0 619	PCI/G	0 098		V
SS133494	SS00004AS	Americium 244	0 582	PCI/G	0 107		V
SS133594	SS00005AS	Americium 245	0 432	PCI/G	0 088		V
SS133694	SS00006AS	Americium 246	0 456	PCI/G	0 091		V
SS133794	SS00007AS	Americium 247	0 071	PCI/G	0 032		V
SS133894	SS00008AS	Americium 248	0 045	PCI/G	0 032		V
SS133894	SS00009AS	Americium 249	0 018	PCI/G	0 018		V
SS133194	SS00001AS	Plutonium 239/240	0 771	PCI/G	0 141		V
SS133794	SS00002AS	Plutonium 239/241	0 206	PCI/G	0 052		V
SS133394	SS00003AS	Plutonium 239/242	3 252	PCI/G	0 376		V
SS133494	SS00004AS	Plutonium 239/243	3 253	PCI/G	0 390		V
SS133594	SS00005AS	Plutonium 239/244	2 119	PCI/G	0 413		V
SS133694	SS00006AS	Plutonium 239/245	2 452	PCI/G	0 307		V
SS133794	SS00007AS	Plutonium 239/246	0 199	PCI/G	0 050		V
SS133894	SS00008AS	Plutonium 239/247	0 064	PCI/G	0 042		V
SS133894	SS00009AS	Plutonium 239/248	0 052	PCI/G	0 028		V

SS00009AS is a field duplicate of SS00008AS
Refer to Figures 2 16 and 2 17 for sample locations

Table 2 14
Comparison of Concentrations of Organic Chemicals in TM15 Subsurface-Soil Samples
with Risk Based Concentrations (RBCs)

Chemical	Residential Soil RBC (mg/kg)	Maximum Detected Concentration (mg/kg)	Maximum Detect Concentration Exceeds RBC?	Maximum Nondetected Concentration (mg/kg)	Maximum Nondetected Concentration Exceeds RBC?
Bis(2-ethylhexyl)phthalate	4.57E+01	5.4E-01	No	5.3E-01	No
Bromofom	8.11E+01	2.0E-03	No	1.4E-02	No
Butylbenzyl phthalate	5.4E+04	2.1E+00	No	1.14E+00	No
Cholorform	1.05E+02	3.6E-02	No	1.3E-02	No
Diethyl phthalate	2.2E+05	8.9E-01	No	1.0E+00	No
Di-n-octyl phthalate	5.49E+03	5.0E-02	No	8.9E-01	No
Methylene chloride	8.54E+01	1.5E-01	No	3.0E-02	No

Source: DOE (1995d)

Table 2 15
Comparison of Concentrations of Organic Chemicals in TM15
Groundwater with Risk Based Concentrations (RBCs)

Chemical	Residential Groundwater RBC (mg/l)	Maximum Detected Concentration (mg/l)	Maximum Detect Concentration Exceeds RBC?	Maximum Nondetected Concentration (mg/l)	Maximum Nondetected Concentration Exceeds RBC?
Compounds Not Detected in Samples Prior to TM15					
Anthracene	1.9E+01	5.0E-04	No	0.1	No
Butyl benzyl phthalate	7.3E+00	4.0E-03	No	1.0E-01	No
C. ribazole	NA	4.0E-03	NA	1.0E-01	NA
Carbon Disulfide	2.7E-02	1.0E-03	No	5.0E-03	No
Dibenzofuran	NA	2.0E-03	NA	1.0E-01	NA
1,1-Dichloroethane	1.01E+00	1.0E-03	No	5.0E-03	No
Cis 1,2-dichloroethane	3.2E-01	3.0E-03	No	2.5E-04	No
2,4-Dimethylphenol	7.3E-01	2.0E-03	No	1.0E-01	No
4-Isopropyltoluene	NA	2.0E-04	NA	2.5E-04	NA
2-Methylphenol	1.83E+00	1.0E-03	No	1.0E-01	No
Di-n-octyl phthalate	7.3E-01	3.0E-03	No	5.0E-03	No
1,1,2,2-Tetrachloroethane	8.95E-05	4.0E-03	Yes**	5.0E-03	Yes**
Tetrachloroethane	1.43E-03	2.4E-02	Yes**	5.0E-03	Yes*
Toluene	9.85E-01	3.0E-04	No	5.0E-03	No
1,2,3-Trichlorobenzene	NA	2.0E-04	NA	2.5E-04	NA
1,1,2-Trichloroethane	3.18E-04	2.0E-03	Yes**	5.0E-03	Yes*
Compounds Detected at Lower Concentrations in Samples Collected Prior to TM15					
Acetone	3.65E+00	2.7E-02	NO	5.0E-03	No
Bis(2-ethylhexyl)phthalate	6.07E-03	6.0E-03	NO	1.0E-01	Yes*
Di-n-butyl phthalate	3.65E+00	3.0E-03	NO	1.0E-01	No
Naphthalene	1.4E+00	1.6E-02	NO	1.0E-01	No

Source: DOE (1995d)

**

These concentrations are less than 1,000
times the RBC

3 0 PHYSICAL CHARACTERISTICS OF OU 5

This section provides a broad picture of the physical setting of and around OU 5. More specifically, this section discusses the physiographic features within and surrounding OU 5, the demography and land use of both OU 5 and the surrounding areas, as well as the climate, hydrology, geology, and hydrogeology of the area encompassing OU 5 (Figure 3.1).

3 1 PHYSIOGRAPHIC FEATURES

3 1 1 Regional

The Site is located on the western margin of the Colorado Piedmont section of the Great Plains Physiographic Province at an elevation of approximately 6,000 feet above mean sea level (MSL) on a broad eastward sloping plain of coalescing alluvial fans. The Colorado Piedmont terminates abruptly on the west at the Front Range section of the Southern Rocky Mountain Province (EG&G, 1995a).

The Colorado Piedmont is characterized as an area of dissected topography and denudation representing an old erosional surface along the eastern margin of the Rocky Mountains. The piedmont surface is broadly rolling and slopes gently to the east with a topographic relief of only several hundred feet. Drainages have been incised and portions of the alluvial cover have been removed by more recent erosional processes (Scott, 1963). The Site occupies an area on the eastern edge of the piedmont. In the eastern portions of the Rocky Flats Alluvium pediment, the nearly flat lying surface gives way to lower, gently rolling terrain of the High Plains section of the Great Plains Physiographic Province (EG&G, 1995a).

The eastern margin of the Front Range, from approximately four miles west of the Site, is characterized by a narrow zone of hogback ridges formed by steeply east dipping Paleozoic and Mesozoic aged strata (the Fountain formation and the Dakota Group, respectively). Less resistant sedimentary strata were removed by erosion. Approximately fifteen miles west of the Site, the Front Range reaches elevations of 12,000 to 14,000 feet about MSL. A Precambrian age basement comprised of igneous and metamorphic rock assemblages make up the core of the Front Range.

Several pediments were developed across both hard and soft bedrock in the area of the Site during the Quaternary period (Scott 1963). The Rocky Flats pediment is the most extensive of these, forming a broad flat surface east of Coal Creek. The broad pediments and narrow terraces are covered by thin alluvial deposits of ancient streams that once drained eastward into the Great Plains. The sequence of pediments reflects repetitive physical processes associated with cyclic changes in climate. Each erosional surface and stratigraphic sequence deposited on it probably represents a single glacial cycle. The oldest and highest pediment, the Subsummit Surface (Scott 1960), truncates the hogback ridges of the Front Range. Three successively younger pediments, veneered by alluvial gravels (including the Rocky Flats Alluvium), extend eastward from the mountain front. Erosion of valleys into the pediments followed each depositional cycle so that near the mountain fronts, stratigraphically younger geologic units occur at topographically lower elevations as narrow terrace deposits along the streams. These alluvial deposits in the OU 5 area are described in Section 3.6.1.

The industrial area of the Site is located on a relatively flat surface of Rocky Flats Alluvium (Figure 3.1). The pediment surface has been eroded by Walnut Creek on the north and Woman Creek on the south; subsequently, terraces along these streams range in height from 50 feet to 150 feet. The grade of the gently eastward sloping surface of the Rocky Flats Alluvium varies from 0.7 percent in the industrial area of the Site to approximately 2 percent just east of the industrial area.

Surface water that flows from the northern portion of the Site is drained by Rock Creek, which is a northeast trending tributary of Coal Creek. The central and southern portions of the site are drained by Walnut Creek, South Walnut Creek, and Woman Creek. These drainages are all ephemeral tributaries of Big Dry Creek that flow eastward. Coal Creek separates all of the streams on the Rocky Flats Alluvium pediment from the Front Range foothills. Small drainage basins and low recharge from snowmelt or rainfall at higher elevations account for the ephemeral nature of the creeks (EG&G 1995a).

3.1.2 OU 5 Area

The OU 5 study area consists of 11 IHSSs located along the Woman Creek Drainage including the Original Landfill (IHSS 115), the Water Treatment Plant Filter Backwash Pond (IHSS 196), the Ash Pits (IHSSs 133.1 through 133.4 and two previously unidentified ash pits), the Incinerator (IHSS 133.5), the Concrete Wash Pad (IHSS 133.6), Detention Ponds C.1 and C.2 (IHSSs 142.10 and 142.11, respectively).

and Surface Disturbance (IHSS 209) Also included are two additional areas of surface disturbances the Surface Disturbance South of the Ash Pits and the Surface Disturbance West of IHSS 209 (Figure 3 1)

The near surface geologic materials at OU 5 consist of alluvium colluvium valley fill alluvium and artificial fill that unconformably overlay bedrock Artificial fill and disturbed ground occur in localized areas including the landfill the ash pits and the C 1 and C 2 dams

3 2 DEMOGRAPHY AND LAND USE

Based on information provided by the Population Economic and Land Use Database for the Site (DOE 1995c) there are no residents within two miles of the industrial area of the Site and there are no predicted changes in population density through the year 2015 Exact numbers concerning current and future population trends of the plant site are not available The Site was the largest manufacturing employer in the Denver Metro Area in 1994 employing approximately 6 500 people However as the mission changed from production to environmental restoration employment numbers may continue to decrease until environmental work is complete (DOE 1995c)

Land use in the vicinity of the Site consists of residential and limited commercial development parks open space agricultural land and vacant land Increased residential development has occurred within five miles of the Site within the last five years Within five miles of Rocky Flats most residential land use including changes from other land use categories to residential land use occurs immediately north east, and south of Standley Lake Small parcels of unincorporated residential land are located to the west, northwest and north of Rocky Flats (DOE 1995c)

There is limited commercial development within five miles of the plant The primary exception is the commercial activity servicing the Jefferson County Airport Industrial land uses within five miles of Rocky Flats are limited to quarrying and mining operations (DOE 1995c) Other land uses within approximately five miles of the Site include parks and open space agricultural land and vacant land (DOE 1995c) Land uses more specific to OU 5 are discussed below

Current activities within OU 5 consist of environmental investigations monitoring cleanup and routine security surveillance Site operations and maintenance activities are not conducted within OU 5 according

to TM12 Exposure Assessment HHRA (DOE 1995b) OU 5 is currently occupied for the most part by wildlife and will most likely be preserved as open space or as an ecological reserve

Ecological surveys of the buffer zone performed in compliance with the Threatened and Endangered Species Act, have identified the presence of several listed species at the Site. Because the Site buffer zone including OU 5 has not been impacted by commercial development for many years thus allowing progressive re establishment of quality native habitats the future use of this area as an ecological reserve is reasonable. The Jefferson County Board of Commissioners has also adopted a resolution stating its support of maintaining in perpetuity the undeveloped buffer zone of open space around the Site for environmental safety and health reasons (DOE 1995b). However portions of OU 5 with suitable topography will be evaluated further for construction of and subsequent use as an office complex (DOE 1995b).

3.3 METEOROLOGY AND CLIMATOLOGY

Meteorology at the Site is influenced by its proximity to the Front Range. The Site is four miles east of the Front Range and the ground elevation rises along the Front Range from 6 000 feet to more than 10 000 feet at a distance of only 20 miles to the west. The Site operates a 200 foot meteorological tower that is positioned approximately 1.2 miles northwest of OU 5. This tower provides meteorological data that are representative of the general conditions at the Site. It gives the nearest and therefore the most useful meteorological information applicable to OU 5.

The predominant wind direction at the Site is from the west and northwest. These winds tend to have greater speeds than winds out of the east and south (EG&G 1991b). The average annual wind speed in 1991 was 8.7 mph (EG&G 1991b). Wind speeds greater than 20 mph occur between 500 and 600 hours per year at the Site (DOE 1980). During the winter and spring months these strong winds called chinooks are associated with continental air masses moving over the Rocky Mountains. These winds have been recorded exceeding 120 mph at the Site (DOE 1980). During the summer months localized thunderstorms account for strong wind conditions which are typically less intense than winter wind phenomena. However the more characteristic if not so dramatic airflow pattern at the Site is the daily cycle of mountain and valley breezes. During the night relatively cooler air flows off the east slope of the mountains and displaces warmer air at lower elevations. The wind rose for night hours in Figure 3.2

shows this strong westerly component (EG&G 1991b). Canyons, creek drainages, and ridges tend to channel these downslope winds as they move onto the plains. The downslope flows converge with the South Platte River Valley air flow moving to the north northeast. During the daytime hours, solar insolation heats up the air along the slopes of the mountains more quickly than the air over the plains and valleys. This warming causes breezes to move upslope out of the valleys toward the mountains. Upslope conditions tend to be less pronounced and less channelized than downslope conditions (EG&G 1991b). There are spatial and temporal distinctions in the shift from downslope to upslope conditions along the Front Range. The change typically occurs an hour or two earlier in the morning in the vicinity of the Site than at locations on the east side of the Denver Basin (DOE 1980).

According to the Pasquill classification, atmospheric stability is most frequently neutral (Class D) at the Site. During 1991, Class D cases occurred 46.2 percent of the time. Stable conditions, Pasquill Classes E and F, occurred 42.6 percent of the time. Unstable cases, Classes A, B, and C, occurred only 11.2 percent (EG&G 1991b). Unstable atmospheric conditions enhance vertical pollutant mixing. Stable conditions oppose atmospheric turbulence.

The climate at the Site is characterized as semi-arid. Annual climate summaries during 1993 indicated that the 1993 mean temperature of 45.7 F was more than 2 F below the average annual temperature. The annual temperature extremes ranged from a high of 91 F on July 10 and 29 to a low of 10 F on February 16 and November 25. The 1993 peak wind gust of 82 mph occurred on December 31. Precipitation during the year was more than 3 inches below normal, totaling 12.07 inches. The largest daily precipitation fell on June 7, when 1.15 inches of rain was recorded. The largest 15-minute rainfall of 0.15 inches was recorded on March 28. Monthly precipitation ranged from 1.79 inches in June to 0.13 inches in January (EG&G 1993b). Approximately 40 percent of the annual precipitation falls during the spring season, much of it as snow. Thunderstorms during the summer months provide another 30 percent of the annual precipitation (EG&G 1993b). These thunderstorm events can be intense. On August 6, 1991, for example, 1.15 inches of rain fell within two hours (EG&G 1991b).

3.4 SOILS

Soils within the OU 5 area have been classified by the Soil Conservation Service Department of Agriculture (Price and Amen 1980). The location and lateral extent of these soil types within the OU 5

area were digitized from Digital Line Graph (DLG) data from the Soil Conservation Service (Digital ARC/INFO Coverage provided by EG&G RFETSSOIL Coverage) and are presented in Figure 3-6. Table 3-1 lists the major soil units within the OU 5 area with their classifications and properties.

Most of the soil series shown on Table 3-4-1 are classified within the Argiustoll great group. Argiustolls are generally characterized as well-drained with dark-colored humus-rich surface A horizons, argillic B horizons, and calcic C horizons. They exist in aridic and ustic (limited moisture) regimes, which are adequate for plant growth during the growing season. The two predominant subgroups are Torretic and Aridic. Torretic Argiustolls typically have a higher shrink-swell potential than Aridic Argiustolls (Price and Amen, 1980).

The predominant soil type within OU 5 are clay loams of the Denver, Kutch, Midway group (Price and Amen, 1980). These soils occur along the Woman Creek drainage (Figure 3-6). Slope gradients for these soils range from 9 to 25 percent, with the Denver and Kutch soils typically located on the hillslopes of the drainages, while the Midway soils are found on the ridge crests. The Denver clay loams consist of deep, well-drained, calcareous clay, silty clay, and sandy clay material derived primarily from claystones, siltstones, and sandstones. The Kutch soils are moderately deep, well-drained, calcareous clayey alluvium and colluvium derived from claystones, siltstones, and sandstones, and from Rocky Flats Alluvium and terrace alluviums. The Midway clay loams are shallow, well-drained, calcareous clayey material derived from Rocky Flats Alluvium. These soils have low permeability and infiltration rates, which result in a severe water erosion hazard.

The Woman Creek drainage is covered by the Haverson loam (0-3 percent slopes) (Figure 3-6). This soil type is also present downgradient of Antelope Spring and at IHSS 209. The Haverson loam is a deep, well-drained, stratified alluvium derived from Rocky Flats Alluvium and terrace alluviums, and bedrock, claystones, siltstones, and sandstones (Price and Amen, 1980). The infiltration rate and permeability for this soil is slow and moderate/slow, respectively. This soil type is associated with slight water erosion hazards and low shrink-swell potential.

The Leyden, Primen, Standley cobbly clay loams (15 to 50 percent slopes) have limited areal extent east of Pond C-2 and north of the Woman Creek Drainage (Figure 3-6). The Leyden, Primen, Standley series is derived from the Rocky Flats Alluvium, terrace alluvium, and bedrock, claystones. The soil consists of clayey, gravelly, stony, and cobbly material, which constitute clayey, montmorillonitic, mesic, Aridic.

Argiustolls This series displays a slow infiltration and a slow permeability severe water erosion hazard and moderate to high potential for shrinkage swelling. **Leyden** soils are moderately deep and well drained consisting of calcareous cobbly and clayey material. The **Primen** soils are shallow and well drained. **Standley** soils are deep and well drained (Price and Amen 1980).

The **Flatirons** very cobbly sandy loams (0 to 3 percent slopes) are only found on ridge tops that consist predominately of Rocky Flats Alluvium. The Surface Disturbance South of the Ash Pits IHSS 133 5 and the north side of IHSS 115 are all characterized by this soil type (Figure 3 6). The **Flatirons** soil is deep and well drained and is formed in noncalcareous cobbly stony gravelly and loamy material of the Rocky Flats Alluvium. Slow infiltration rate slow permeability slight water erosion hazard and a moderate shrink swell potential are associated with this soil type (Price and Amen 1980).

The **Nederland** soil skirts the **Flatiron** soils along the ridges and hillsides of the OU 5 area and consists of very cobbly sandy loam which forms slopes of 15 to 50 percent (Figure 3 6). This soil is deep and well drained and formed in cobbly gravelly and loam alluvium derived from the Rocky Flats Alluvium and terrace alluviums. This soil has moderate permeability and infiltration rate a severe water erosion hazard and low shrink swell potential (Price and Amen 1980).

3 5 HYDROLOGY

Appendix A (Hydrologic Data Summary Report) provides detailed information regarding the hydrology of OU 5. OU 5 is located within the Woman Creek drainage basin (Figure 3 1) in which water generally flows from west to east. The Woman Creek drainage basin extends eastward from the base of the foothills near the mouth of Coal Creek Canyon to Standley Lake. The portion of the basin that lies within the study area (headwaters to Indiana Street) consists of approximately 2 884 acres. The long term average annual yield generated by this basin is 32 1 acre feet, with significant average storms producing surface flows of 4 to 7 cubic feet per second (cfs). During extreme precipitation events (greater than 15 year return occurrence based on precipitation) surface flows up to 40 cfs have been generated. Although seasonal flows can be low, Woman Creek receives continuous flow from Antelope Springs Creek. Woman Creek drains OU 5 and discharges via Mower Ditch into Mower Reservoir and Standley Lake. During periods of high flow, Woman Creek may discharge directly to Standley Lake (DOE 1994b).

Detention Ponds C 1 and C 2 are located within the eastern reach of the Woman Creek basin. Pond C 1 is located on the Woman Creek channel. Pond C 2 is located off the Woman Creek channel. Pond C 2 receives relatively minor local flow from its surrounding drainage basin while receiving the bulk of its flow from the South Interceptor Ditch which lies on the northern flank of the Woman Creek basin (Figure 3-1) and crosses under the Woman Creek Diversion Ditch before emptying into the pond. The South Interceptor Ditch collects runoff from the southern side of industrial area and diverts it to Pond C 2. Pond C 2 water is not discharged to Woman Creek, but is pumped to the Broomfield Diversion Ditch (around Great Western Reservoir) approximately semi annually (DOE 1994b).

The morphology of both Ponds C 1 and C 2 is related to sediment accumulations which have reduced their storage capacity (DOE 1993b). Pond C 1 had an estimated storage capacity at the spillway/outlet crest of approximately 6.1 acre feet at the time of construction. By 1992 this spillway/outlet-crest storage capacity had decreased to approximately 5.2 acre feet, or a volume reduction of approximately 15 percent (EG&G 1992e). At the time of construction Pond C 2 had a principal spillway storage capacity of approximately 7.1 acre feet. By 1992 this capacity had decreased to 7.0 acre feet, or a reduction of approximately 1.4 percent (Merrick Engineering 1992). The relatively small storage reduction from sedimentation in Pond C 2 appears reasonable because the pond is off-channel and only 15 years old.

It is anticipated that these alterations to pond morphology will continue into the future especially if additional development takes place onsite or in the upper Woman Creek drainage basin (Appendix A). Minor impacts on pond morphology (primarily affecting Pond C 1 but perhaps also Pond C 2 during larger storms) also could occur if development takes place in the Coal Creek basin and irrigation water continues to discharge into Woman Creek from the Kinnear and Smart 2 Ditches. This would mean that additional sediment might enter either of these ponds. Water/sediment interactions occur as precipitation and runoff erode surface soils as the water flows in open channels, streams, and within ponds (Appendix A).

The Woman Creek drainage basin has several artificial water controls including the SID which intercepts runoff and routes this runoff to Pond C 2. This runoff would normally flow into Woman Creek or would percolate into the underlying subsurface materials of the basin. Ponds C 1 and C 2 themselves are artificial water control structures that temporarily store water and in the case of Pond C 2 may export water from the Woman Creek basin to the Walnut Creek basin. The Woman Creek diversion dam routes all Woman Creek flows less than about the 100 year flood peak around Pond C 2. Irrigation inputs to

Woman Creek from the Kinnear Ditch and Smart 2 Ditch are artificial water controls that divert water from the Coal Creek basin into the Woman Creek basin (ASI 1990). The French drain on the 881 Hillside also may be classified as an artificial water control structure that changes the groundwater flow from the 881 Hillside to Woman Creek (Appendix A).

Stream reach gain/loss studies along Woman Creek, Mower Ditch and selected tributaries have been done by Colorado State University (Fedors and Warner 1993) and interim study results were discussed in Section 4.1 of TM1 (DOE 1993b). In addition, EG&G has continued the gain/loss measurements since December 1991. In March 1993, 36 well points were installed along Woman Creek, as described in TM1 (DOE 1993b). These well points were installed to assess which reaches of Woman Creek are gaining water (flowing from the shallow groundwater system into Woman Creek) and which reaches of Woman Creek are losing water (flowing from Woman Creek into the shallow groundwater system). Locations of these well points are shown on Figure 3.3.

For the well point/stream water surface elevation monitoring, a reach was assumed to be gaining if the upstream and downstream difference between the average groundwater elevation and surface water elevation was positive (that is, flow was from the shallow groundwater system into Woman Creek). Conversely, a reach was assumed to be losing if the upstream and downstream difference between the average groundwater elevation and surface water elevation was negative (flow was from Woman Creek into the shallow groundwater system). For the stream gain/loss study, a reach was assumed to be gaining if the difference between the downstream flow and the upstream flow was positive. Reaches were considered to be losing if the downstream flow and upstream flow difference was negative.

In general, four reaches of Woman Creek and its tributaries can be identified as generally gaining water from the shallow groundwater system on nearly a year-round basis. These include reaches 7.6 and 6.5 on the southwestern tributary flowing into Woman Creek, and reaches 9.10 and 18.19 on Woman Creek (Figure 3.3) (Appendix A). Gaining reach 9.10 is adjacent to IHSS 115 (Figure 3.3); however, this gain is more likely due to inflows from the south bank (i.e., the opposite bank from the Original Landfill location) due to seepage input from an old orchard area (Appendix A). (Reach 18.19 lies downgradient from the Old Firing Range.)

Other reaches downstream from Pond C.1 (reach C.1.18) and both upstream and downstream from Pond C.2 (reach 20.24) have been identified based upon existing data, as losing year-round (Appendix A). It is

uncertain why the reach downstream from Pond C 1 is losing year round. The reach in the vicinity of Pond C 2 most likely loses year round because it is a man made channel that is part of the Woman Creek diversion around Pond C 2.

The other Woman Creek reaches range from gaining during the winter and spring months and losing during the rest of the year (reaches 1 2 2 3 3-4 4+5 8 8 9 11 12 17 C1 and 19 20 (Figure 3 3) to gaining for two months or less and losing the rest of the year (reaches 10 11 12+13 16 16 17 (Figure 3 3). The gain/loss data is based upon historical data collected by Fedors and others 1993. The data presented herein generally support the conclusions of Fedors and others 1993 as supported by additional EG&G gain/loss data on Woman Creek (Appendix A).

3 6 GEOLOGY AND HYDROGEOLOGY

A comprehensive geologic and hydrogeologic framework for the Site is presented in the Geologic Characterization Report for the Site (EG&G 1995a) and the Hydrogeologic Characterization Report (EG&G 1995b). The Section 3 6 1 summarizes the geologic history setting and deposits. Section 3 6 2 presents a discussion of the inferred faults within the OU 5 area. Section 3 6 3 summarizes the OU 5 hydrogeologic setting.

3 6 1 Geologic History Setting and Deposits

During the late Cretaceous period, sediments east of the Front Range underwent initial orogenic uplift. As the Cretaceous sea gradually regressed from the west to the east, the Fox Hills beach front sands, the Laramie delta plain deposits, and the Arapahoe fluvial deposits prograded eastward over the Pierre Shale prodelta muds. This marine regression was occasionally interrupted by small scale marine transgressions which may have been caused by variations in the rate of uplift along the Front Range. During transgressive pulses, thin intervals of Pierre Shale prodelta muds were deposited above the Fox Hills Sandstone. As a result, the Fox Hills Sandstone intertongues with the underlying Pierre Shale (DOE 1991). During the Pleistocene age, the Rocky Flats Alluvium was deposited as an alluvial fan at the base of Coal Creek Canyon. Holocene age uplift has dissected the Rocky Flats Alluvium and deposited the unconsolidated terrace and valley fill sediments along the drainages. Geologic units observed in OU 5 are the Laramie Formation, the Arapahoe Formation, Rocky Flats Alluvium, valley fill alluvium, colluvium.

land slide and artificial fill or man made deposits Piney Creek Alluvium and valley fill alluvium are one in the same as presented herein The following paragraphs summarize the characteristics of each of the geologic units present in the OU 5 area.

The bedrock that is present in the OU 5 area is predominantly the Laramie Formation (Figure 3 4) Figure 3 5 shows the most recent interpretation of the bedrock elevation in the OU 5 area. The Upper Cretaceous aged Laramie Formation is approximately 600 to 800 feet thick It has been informally subdivided into lower and upper members The Upper Laramie Formation is generally distinguished from the Lower Laramie Formation where the Upper Laramie Formation becomes dominantly composed of fine grained sedimentary rocks (primarily claystone with no thick sandstone beds) The upper part of the Laramie Formation is approximately 300 to 500 feet thick and consists primarily of olive gray and yellowish orange claystones with large ironstone nodules A few thin coal beds occur in the Upper Laramie Formation but they are discontinuous Lenticular beds of platy laminated or friable calcareous fine grained light olive gray sandstones are also present and occur with greater frequency at higher levels in the section

The Upper Cretaceous aged Arapahoe Formation lies stratigraphically above the Laramie Formation was deposited by a fluvial system and is absent or as much as 50 feet thick within the vicinity of the Site (EG&G 1995a) The Arapahoe Formation is composed primarily of sandstones and claystones that are very similar to those in the underlying Laramie Formation This similarity between the upper Laramie and Arapahoe Formations has resulted in confusion distinguishing these two units (EG&G 1992f and 1995a) Previous works (Van Horn 1957 and EG&G 1992f) have described the base of the Arapahoe Formation as a thick discontinuous conglomerate with clasts composed principally of chert with some granite gneiss and schist As shown on Figure 3 4 only a small amount of Arapahoe Formation is present within the OU 5 area, with most of it located in the southeast portion of the OU and very little in the area of IHSS 133 or IHSS 115

The sandstone units appear to be composed of channel point bar and overbank deposits from meandering and braided streams (Figure 3 7) It has been a point of controversy as to whether these sandstone units are part of the Laramie Formation or part of the Arapahoe Formation Arapahoe Formation sandstones were previously classified as the No 1 through No 5 sandstones (DOE 1991) However the most recent study indicates that the No 1 Sandstone belongs to the Arapahoe Formation and Sandstones Nos 2 through 5 belong to the Laramie Formation (EG&G 1995a) More data have been collected from the

No 1 Sandstone than any of the other sandstone intervals because of its shallow subsurface depth and its hydraulic connection with other units of the UHSU in the eastern portion of the industrialized area, underlying OU 2

In this report sandstones and siltstones encountered in drill core collected during the OU 5 investigation are classified as undifferentiated Laramie Formation/Arapahoe Formation due to the inability to differentiate between the Laramie Formation or Arapahoe Formations at the Site (Figure 3 8) According to Plate 5 9 of the Geologic Characterization Report (EG&G 1995a) the Arapahoe Formation No 1 sandstone or equivalent sandstones are interpreted to be present in OU 5 on the east side of IHSS 133 on the northeast side of IHSS 115 and in an area east of the Surface Disturbance South of the Ash Pits (Figure 3 7)

On the basis of the OU 5 investigation the bedrock encountered in the area of IHSS 115 and IHSS 133 are comprised predominantly of claystone with some thin interbeds and laminae of siltstone and sandstone (Appendix B) The claystone was observed to be massive to-thinly laminated containing trace ironstone nodules trace to some organics in the form of leaf imprints disseminated carbon and trace lignite interbeds with some thin interbeds and laminae of siltstone and sandstone Sandstone and siltstone interbeds from 0 5 to 10 feet in thickness (Figure 3 8) consisted of very fine to fine grained clayey to silty sandstones and sandy to clayey siltstones slightly friable to well cemented trace ironstone nodules cross bedded to laminated with some soft sediment deformation structures and trace fossils with trace to some disseminated carbon The environment of deposition appears to be a low energy fluvial environment

Unconsolidated material within OU 5 consists predominantly of landslide deposits and Rocky Flats Alluvium Lesser amounts of artificial fill including waste fill Piney Creek Alluvium colluvium, and terrace alluvium exist within the OU 5 boundaries (Figures 3 9 and 3 10) The overall thickness of the unconsolidated material throughout OU 5 ranges from about 2 to approximately 30 feet.

Rocky Flats Alluvium The Rocky Flats Alluvium was deposited by a system of coalescing alluvial fans aggraded by debris flows and braided streams along the base of the Front Range at the mouth of Coal Creek Canyon (EG&G 1995a) This unit forms a large (approximately 10 square miles) fan shaped deposit with bar and channel morphology on the Rocky Flats pediment Eastward flowing streams have

dissected the pediment in several locations and have exposed Cretaceous age bedrock in some areas (EG&G 1995a)

According to the Preliminary Surficial Geologic Map of the Rocky Flats Plant and Vicinity (Shroba and Carrera, 1994) the Rocky Flats Alluvium commonly consists of beds and lenses of poorly sorted clast and matrix supported white to pink sandy cobbly gravel gravelly sand and silty sand. Clasts are commonly subangular quartzite that were derived from Coal Creek Canyon. Clasts of claystone and sandstone are locally present in the lower 20 inches of the unit. Generally the thickness of this unit is about three to 30 feet where pediment deposits overlie Upper Cretaceous aged bedrock, and about 30 to greater than 100 feet where these deposits overlie valley fill deposits (Shroba and Carrera 1994)

Terrace alluvium as described in the Geologic Characterization Report (EG&G 1995a) consists predominantly of a slightly cobbly gravelly light grayish brown to light reddish brown silty sand to clayey silt. Clasts are mostly subangular quartzite. The unit forms small terraces and terrace remnants about 8 to 33 feet above current stream levels that lack bar and channel morphology and are locally mantled by a thin layer of colluvium. The terrace deposits within OU 5 are probably composed mostly of Broadway and Louviers Alluviums. The thickness of these deposits ranges from about 10 to 20 feet.

Piney Creek Alluvium The Piney Creek Alluvium and post Piney Creek Alluvium undifferentiated are commonly referred to as valley fill alluvium in this report. These units consist of channel and terrace deposits in and along most of the ephemeral streams across the Site. Areas in which Piney Creek Alluvium has been identified (Figure 3 10) consist of materials that are commonly slightly cobbly grayish brown silty sand to sandy clayey silt in the upper part and poorly sorted clast supported slightly cobbly gravel in a light yellowish brown clayey silty sand matrix in the lower part. Clasts are mostly subangular quartzite with a minor amount of subrounded sandstone that was derived from older Quaternary aged deposits. Thickness of this unit is about 3 to 15 feet with an average of about 10 feet (Shroba and Carrera, 1994). The Piney Creek Alluvium contains stage I (Gile and others 1966) carbonate veinlets and locally one or more buried soil A horizons about 2 to 3 inches thick and also may contain expansive clays. The Piney Creek Alluvium forms low terraces approximately 3 to 6 feet above stream level that locally have poorly preserved bar and-channel morphology.

Colluvium The colluvial deposits at the Site are middle Pleistocene to Recent in age and occur along Valley Slopes. The colluvial material commonly consists of dark gray to light reddish brown silty sand, sandy silt, clayey silt, and silty clay that contain minor amounts of boulders and cobbles. The unit locally includes clast- and matrix-supported boulders and cobbles to coarse to fine to cobbly gravel in a silty-clay matrix. These materials are typically wellgraded to poorly graded and unstratified to poorly stratified. Clasts are typically subangular to subrounded; their sedimentologic composition reflects that of the bedrock and surficial deposits from which they were derived. The thickness of these deposits is probably about 3 to 15 feet (Shroba and Carrera, 1994). The colluvium occurs as thin, discontinuous deposits in the western portion of the Site and as more broad and laterally extensive deposits in the eastern portion of the Site (EG&G 1995a).

Landslide Deposits Landslide deposits include a wide variety of mass movement deposits resulting from the downslope transport of unconsolidated surficial and bedrock material along slip planes. Landslide deposits are common along modern drainage slopes throughout the site and can occur as laterally extensive deposits (EG&G 1995a) (Figure 3-9). These deposits consist of materials that are commonly a dark gray to light reddish brown, heterogeneous mixture of unsorted and unstratified surficial material and rock fragments in a wide range of sizes (including clasts that are of the same composition of the bedrock from which they were derived). Generally, the thickness of these units is probably 10 to 30 feet (Shroba and Carrera, 1994).

Artificial Fill According to the Surficial Geologic Map of the Rocky Flats Environmental Technology Site and Vicinity (EG&G 1995a), the artificial fill consists of compacted and uncompact fill material composed of varying amounts of sand and finer material, heterogeneous cobbles and boulders, and refuse. Artificial fill which contains refuse will be referred to as waste fill herein. The unit locally includes small areas of Rocky Flats Alluvium, claystone, and other unconsolidated deposits. Generally, the thickness of this unit is less than 10 feet; however, some of the earthen dams are greater than 30 feet thick.

3.6.2 Inferred Faulting

Inferred bedrock structures within the OU 5 area predominantly consist of three faults. These inferred faults trend north-northeast and are assumed to be high angle reverse faults in conformance with the regional structural framework (Figure 3-11) (EG&G 1995a). The dip of the fault planes is not known.

The longest inferred fault, referred to as Fault 2 in the Geologic Characterization Report (EG&G 1995a) is northeast trending reverse fault that extends from Woman Creek to Colorado Highway 128 across the western part of the industrial area and the Landfill Pond (Figure 3 1) It is assumed that the fault plane dips to the west This fault was confirmed during the past year by a series of boreholes drilled to the north of the Landfill Pond as part of the Systematic Evaluation Program (SEP) (EG&G 1995d) and by boreholes drilled in OU 5 This data provided the best control for both the location and displacement of the fault Displacement of the A claystone was determined to be about 60 feet at both locations

Fault 4 as referred to in the Geologic Characterization Report (EG&G 1995a) is an inferred northeast trending fault that extends from Woman Creek to South Walnut Creek across OU 2 and into OU 5 (Figure 3 11) It is assumed that the Fault 4 is a reverse fault that dips to the northwest Displacement in the A claystone has been observed to be approximately 70 feet within OU 2 (EG&G 1995a) The location of this fault is similar to that of the OU 2 bedrock step which was identified using shallow seismic reflection and borehole data (EG&G 1995a)

Inferred Fault 5 as referred to in the Geologic Characterization Report (EG&G 1995a) also extends through OU 5 and is located along the southeastern edge of the Industrial Area (Figure 3 11) Displacement of the A claystone across this fault is estimated to be approximately 30 feet (EG&G 1995a)

Evaluation of geologic and topographic features indicates a lack of recent movement along faults at the Site This lack of movement was recently confirmed in the Systematic Evaluation Program (SEP) trench where extensive fracturing was exposed in the bedrock across Fault 2 but was not present in the alluvium and did not offset the unconformity between the Laramie Formation and the overlying Rocky Flats Alluvium (EG&G 1995a and 1995d) The fault is reported as not capable according to Nuclear Regulatory Commission guidelines and therefore does not pose a seismic risk for the site (EG&G 1995d)

3 6 3 Hydrogeology

The regional hydrogeology and OU 5 hydrogeology are summarized in the following sections

3 6 3 1 Regional Hydrogeology

The Denver Groundwater Basin underlies a 6 700 square mile area in Colorado extending from the Front Range on the west to near Limon on the east and from Greeley on the north to Colorado Springs on the south. The center of the basin is located south of Bennett, Colorado, in western Arapahoe and Elbert Counties. Alluvial aquifers, 20 to 100 feet in thickness, commonly occur in the valleys of large streams in the basin.

The four major bedrock aquifers occurring in the Denver Basin, from deepest to shallowest, are the Laramie, Fox Hills, Arapahoe, Denver, and Dawson Aquifers. The Pierre Shale underlies these units and, due to its great thickness (up to 8 000 feet) and low permeability (Robson et al., 1981a and 1981b), is considered to be the base of the four bedrock aquifers listed above. Descriptions of the Denver Basin bedrock aquifers that exist beneath the Site, the Laramie, Fox Hills, Arapahoe, and Denver Aquifers, are presented below. The Dawson Aquifer does not underlie the Site.

Laramie Fox Hills Aquifer The Laramie Fox Hills Aquifer is composed of the sandstone and siltstone units of the Fox Hills Formation and the lower sandstone units of the Laramie Formation (Figure 3-3). The thickness of the aquifer ranges from 200 to 300 feet near the center of the Denver Basin (Robson et al., 1981b). The Site is located near the western boundary of the aquifer. The base of the aquifer dips steeply to the east in the area west of the Site and then 2 to 3 degrees to the east beneath the Site. The upper Laramie Formation, which separates the unconsolidated water-bearing Upper Hydrostratigraphic Unit (UHSU) in OU 5 (Section 3-6-3-2) from the underlying Laramie Fox Hills Aquifer, consists of several hundred feet of claystones, siltstones, and some clayey or silty sandstones with occasional coal layers (EG&G, 1995a and b).

In outcrop and shallow subcrop areas, recharge to the Laramie Fox Hills Aquifer occurs as infiltration of incident precipitation and as infiltration of groundwater from shallow alluvial aquifers, respectively. Outcrops of the Laramie and Fox Hills Formations in clay pits west of the Site are believed to be recharge areas for the aquifer (Rockwell, 1987). Toward the interior of the basin, downward leakage may also occur through the upper Laramie Formation from the overlying Arapahoe Aquifer (Robson et al., 1981b). Recharge to the Laramie Fox Hills Aquifer from vertical leakage through the upper Laramie Formation is

expected to be minimal at the Site due to the substantial thickness of claystones and siltstones of the upper Laramie Formation

On a regional scale groundwater in the Laramie Fox Hills Aquifer flows from outcrop recharge areas toward the center of the basin. In the vicinity of the Site groundwater flow is generally from west to east (Hurr 1976)

Arapahoe Aquifer In the central part of the Denver groundwater basin the Arapahoe Formation consists of a 400 to 700 foot thick sequence of interbedded claystones siltstones sandstones and conglomerates with claystones and shale being more prominent in the northern third of the basin (Robson et al 1981a). Individual sandstone beds are commonly lenticular and range from a few inches to 30 to 40 feet in thickness (Robson et al 1981a). Beneath the Site the majority of groundwater flow in the Arapahoe Formation occurs in the lenticular sandstones within the claystones. The portion of Arapahoe Aquifer present beneath the Site at OU 5 is not significant from a regional aquifer perspective because it is truncated by drainages on the Site and does not extend laterally from the Site to offsite areas.

Recharge to the Arapahoe Aquifer occurs by the same mechanisms described for the Laramie Fox Hills Aquifer. In outcrop and subcrop areas recharge occurs from infiltration of incident precipitation and as infiltration of groundwater from shallow alluvial aquifers respectively. At the Site the Arapahoe Formation sandstones are recharged from infiltration of groundwater from overlying unconsolidated surface deposits. On a regional scale the primary recharge mechanism for the Arapahoe Aquifer occurs through leakage from the overlying Denver Aquifer (Robson et al 1981a).

Groundwater in the Arapahoe Aquifer flows from recharge areas at the edge of the basin toward discharge areas along incised stream valleys. Groundwater also discharges from pumping wells (Robson et al 1981a).

3.6.3.2 OU 5 Hydrogeology

Saturated unconsolidated surface deposits and weathered bedrock units of the Arapahoe and/or upper Laramie Formations (Figures 3.4.3.9 and 3.10) are considered the UHSU. The UHSU is the hydrogeologic unit of concern at the Site because of the potential for contamination and contaminant

migration. The vast majority of site impact has occurred in the UHSU. The unweathered undifferentiated Arapahoe Formation and Laramie Formation are considered the LHSU at the Site. Contaminant concentrations in the unweathered upper Laramie Formation at the Site are typically very low, and the Laramie Fox Hills Aquifer exists at a substantial depth below the Site with a substantial thickness of unweathered intervening claystones and siltstones separating it from the shallow UHSU (EG&G 1995b). Therefore, the Laramie Formation and the Laramie Fox Hills Aquifer are not addressed in the context of OU 5 hydrogeology because the potential for contamination of these units from site-related activities appears to be minimal.

Hydrogeologic conditions in the shallow surface units at OU 5 are influenced by local conditions, local recharge, and interactions with the SID, the 881 Hillside French Drain, and Woman Creek. The earthen dams of Ponds C 1 and C 2 also influence groundwater flow. The SID and Ponds C 1 and C 2 were constructed to contain surface water. The French Drain was constructed south of OU 1 to intercept groundwater flow.

In general, groundwater in the shallow unconsolidated geologic units of OU 5 flows from topographically higher pediment areas (recharge) toward the drainages (creeks) (discharge) that divide the pediment areas. Groundwater is then transmitted into and through the valley fill alluvium that underlies the creeks, ultimately discharging to the creeks. The shape of the top of bedrock surface strongly influences groundwater flow by concentrating flow within erosional lows on the bedrock surface. Groundwater recharge to the shallow unconsolidated units occurs primarily as a result of local infiltration of snowmelt, rainfall, and surface water within the OU 5 area. Groundwater recharge also occurs as inflow to OU 5 from upgradient areas to the west and from the industrial area to the north. Artificial sources of recharge from the industrial area occur from building footing drains, storm drains, and storm surface water diversion ditches. Standing surface water with marsh-type vegetation observed along the SID suggests that the SID captures surface and groundwater and locally affects the recharge to the groundwater system. Antelope Springs, located on the southwest corner of OU 5, receives recharge from Rocky Flats Lake (Figure 3-1).

Upper Hydrostratigraphic Unit The shallow, saturated hydrogeologic units at OU 5 comprise the UHSU, which consists of unconsolidated surface deposits (Rocky Flats Alluvium, valley fill alluvium, landslide, artificial fill, and colluvium) and weathered bedrock (claystone, sandstone, siltstone) of the Arapahoe/Laramie Formations that are in hydraulic communication with the saturated surface materials.

The Arapahoe/Laramie Formation sandstones where they appear to be in hydraulic communication with saturated surface materials are also considered to be part of the UHSU. The UHSU within OU 5 is believed to exist predominantly under unconfined conditions; however, partially confining conditions may exist in the bedrock sandstones that are part of the UHSU.

Groundwater in the UHSU flows generally eastward with secondary flow patterns along slopes toward drainages. Groundwater flow in OU 5 is strongly affected by the topographic relief, the thin, relatively permeable surficial deposits, and the underlying impermeable claystone bedrock surface topography. Site-wide, the geometric means of the hydraulic conductivities are 2.54×10^{-3} centimeters per second (cm/sec) for the valley fill alluvium, 2.1×10^{-4} cm/sec for the Rocky Flats Alluvium, and 9.33×10^{-5} cm/sec for the colluvium, 3.89×10^{-5} cm/sec for the weathered sandstone, 2.88×10^{-5} cm/sec for the weathered siltstone, and 8.82×10^{-7} cm/sec for the weathered claystone (EG&G 1995b). The colluvium and landslide deposits are similar in textural and hydraulic properties (Schroba and Carrera, 1994). Hydraulic characteristics of the artificial fill vary depending on the purpose of the fill. Generally, the fill ranges from low hydraulic conductivity, such as the Pond C-2 dam, to relatively high hydraulic conductivity associated with waste fill materials. Many areas of artificial fill are superficial (road base) and the base of the fill is above the water table.

Groundwater elevations in the UHSU vary seasonally, with the highest elevations recorded during the late winter/spring time period and the lowest elevations recorded during the late summer/fall time period. Seasonal variations in groundwater elevations ranged from less than 1 foot to over 6 feet. The OU 5 area exhibits localized flow from seeps and springs on the slopes of the Woman Creek drainage (EG&G 1995b). Some of the groundwater emerging at seeps and springs is lost to evaporation; however, some flows along the surface and discharges into Woman Creek. Woman Creek is both a gaining and a losing stream. In the western half of the drainage, Woman Creek is generally gaining, whereas in the eastern half it is generally losing. The extent of gaining and losing reaches varies seasonally (Fedors and Warner 1993) as described previously in Section 3.5.

Groundwater level data used for the evaluation of the UHSU were collected from historical and Phase I monitoring wells within the OU 5 area. These data were obtained from RFEDS and are presented in detail in Section 5.8 for the individual IHSSs. Groundwater level data were used to create UHSU groundwater hydrographs (Section 5.8) and the UHSU potentiometric maps (Section 5.7, Figures 3.24, 3.25, 3.35, and 3.36). The potentiometric surface maps were prepared using all available groundwater elevation data.

Physical parameter data, used for the evaluation of the hydraulic properties of the UHSU (Appendices A and C) were obtained from aquifer test results [Appendix D]). Descriptions of alluvial and bedrock materials were obtained from lithologic logs (Appendix B)

Lower Hydrostratigraphic Unit The LHSU underlies the UHSU and is composed of unweathered upper Laramie Formation or Arapahoe Formation clayey to silty sandstones, claystones, and clayey to sandy siltstones. Unweathered bedrock sandstone, siltstone, and claystone geometric mean hydraulic conductivities are 5.77×10^{-7} cm/sec, 1.59×10^{-7} cm/sec, and 2.48×10^{-7} cm/sec, respectively (EG&G 1995b). The relatively low hydraulic conductivity of the unweathered bedrock suggests that the unweathered bedrock acts as a barrier to downward groundwater flow and effectively minimizes groundwater interaction between units above and below the base of weathering. Hydrograph data indicate unweathered bedrock and UHSU deposits are not hydraulically connected (EG&G 1995b). Six bedrock wells were installed as part of the scope of TM15 to evaluate possible hydraulic interaction between the UHSU and the LHSU in OU 5, specifically in and around the Original Landfill (IHSS 115/196). Because of the lack of hydraulic connection between the UHSU and the LHSU, the vast majority of contamination occurs in the UHSU. A discussion of the LHSU in the area of the Original Landfill is presented in Section 3.8.1.

3.7 ECOLOGY

3.7.1 Terrestrial Ecosystems

The Site is located just below the elevation at which plains grasslands grade abruptly into lower montane (foothills) forests (Marr 1964). The vegetation of the Site and adjacent areas is dominated by mixed grass prairie interspersed with various upland and lowland community types.

Wildlife communities at the Site have been greatly influenced by the increase in human use and disturbance over the past 100 years. Most notable has been the reduction in the number and diversity of ungulates and predators. The relative isolation and habitat diversity of the Site have resulted in a rich animal community when compared to nearby rangeland, cropland, and commercial or industrial development. The absence of domestic livestock and the proximity to large areas of open space have contributed significantly to the ecological resources at the Site.

More information on ecological receptors and potential ecological risk in OU 5 can be found in the ecological risk assessment for the Woman Creek watershed presented in Section 7.0

3.7.1.1 Vegetation

Plant communities within OU 5 are influenced primarily by moisture and prior disturbance. Topographic position is the major factor influencing soil moisture. Areas along Woman Creek are persistently moist (mesic) because of subsurface flows within the valley floor alluvium, in addition to runoff and interflow from adjacent hillsides. The stream channel is wet (hydric) for much of the year, although duration of surface flow is variable. North-facing slopes within the drainage are relatively mesic because of the low angle of insolation and the retention of snow. South-facing slopes and ridgetops are not as dry (xeric) as might be expected, probably because of shallow subsurface flow through the Rocky Flats Alluvium that caps the drainage divides.

A complete list of plant species documented at the Site is supplied in Appendix B of the *Baseline Biological Characterization of Terrestrial and Aquatic Habitats at the Rocky Flats Plant* (DOE 1992c).

Mesic mixed grassland is the predominant habitat type associated with OU 5, occurring both as large communities and small inclusions in other habitats. It dominates the north-facing and south-facing hillsides along the upper reaches of Woman Creek and the broad valley floor south and east of the OU 5 IHSSs (Figure 3.12). This habitat tends to be dominated by sod-forming (rhizomatous) grasses. Western wheatgrass (*Agropyron smithii*) is typically the dominant species. Other prevalent graminoids include blue grama (*Bouteloua gracilis*), side-oats grama (*Bouteloua curtipendula*), prairie junegrass (*Koeleria pyramidata*), big bluestem (*Adropogon gerardii*), little bluestem (*A. scoparium*), Canada bluegrass (*Poa compressa*), Kentucky bluegrass (*Poa pratensis*), needle and thread (*Stipa comata*), green needlegrass (*Stipa viridula*), sleepygrass (*Stipa robusta*), switchgrass (*Panicum virgatum*), and narrowleaf sedge (*Carex stenophylla*). Fringed sagebrush (*Artemisia frigida*), prairie sage (*A. ludoviciana*), and broom snakeweed (*Gutierrezia sarothrae*) are common throughout this habitat. Nonnative species such as knapweed (*Centaurea diffusa*), cheatgrass (*Bromus tectorum*), smooth brome (*Bromus inermis*), and Russian thistle (*Salsola iberica*) also exist. The prevalence of taller and more sod-forming grasses, a generally higher diversity of native forbs, and an increased abundance of low shrubs or subshrubs influences the use by small birds and mammals.

Xeric mixed grassland occupies the broad uplands both north of the OU 5 IHSSs and south of Woman Creek (Figure 3 12) This habitat is relatively dry as a result of greater exposure to sun and wind and well drained soils but persistent moisture is available at relatively shallow depths in the Rocky Flats Alluvium capping the ridges As a result some mesophytic species such as big bluestem and little bluestem are present Prevalent native species include prairie junegrass red three awn (*Aristida purpurea*) and mountain muhly (*Muhlenbergia montana*) with varying amounts of blue grama side-oats grama, and sand dropseed (*Sporobolus cryptandrus*) Other common species include needle and thread Canada bluegrass bottlebrush squirreltail (*Sitanion hystrix*) and narrowleaf sedge Yucca and cacti are locally common in areas of shallow soil

Annual grass/forb habitat is located in the surface disturbance south east of Pond C 1 and is dominated by weedy species (Figure 3 12) Prevalent species are usually aggressive nonnative annual or biennial plants Weedy mustards weedy composites field bindweed (*Convolvulus arvensis*) and great mullein (*Verbascum thapsus*) dominate these areas along with cheatgrass and Japanese brome (*Bromus japonicus*) Cover height and seed production may support some wildlife use but relatively low diversity extreme seasonality and short lived productivity are limiting factors

Reclaimed grassland generally occurs as distinct plantings north of Woman Creek up to and including patches in the industrial area of the Site (Figure 3 12) This habitat consists of introduced range or pasture grasses particularly smooth brome (*Bromopsis inermis*) and intermediate wheatgrass (*Agropyron intermedium*) with minor amounts of crested wheatgrass (*A cristatum*) Many of the stands are nearly a monoculture of the planted species The low plant diversity and structure of these coarse grasses are important limiting factors on wildlife use

Riparian woodland habitats are associated with the hydric soils located along a narrow corridor on either side of Woman Creek and along the margins of Ponds C 1 and C 2 (Figure 3 12) This habitat consists of mature plains cottonwoods (*Populus deltoides*) and peachleaf willows (*Salix amygdaloides*) occurring either as small clumps or individual trees along the drainages ponds and seeps Associated species often include those listed below for riparian shrubland as well as wild rose (*Rosa* spp) golden currant (*Ribes aureum*) snowberry (*Symphoricarpos* spp) and a variety of grasses and forbs The presence of large trees and seasonal availability of surface water attract wildlife not otherwise associated with the prairie ecosystems that dominate the Site

Riparian shrubland also occurs along the Woman Creek corridor often in association with riparian woodland. Dominant species include coyote willows (*Salix exigua*), peachleaf willows, and leadplant (*Amorpha fruticosa*). The shrubby species that dominate this habitat support use by some wetland or riparian wildlife species, but diversity and density are typically lower.

Short marsh habitats occur along Woman Creek and the SID and in groundwater seep areas to the south. It requires seasonally wet (saturated) sites such as hillside seeps (Figure 3-13). They are dominated by sedges, rushes, and hydrophytic forbs. Low plant height, low plant species diversity, dense cover, and wet soil limit the variety of wildlife using this habitat type.

Ponderosa pine woodland occurs as sparse stands on rocky uplands, such as those found in the surface disturbance located south of the south fork of Woman Creek (Figure 3-12). The understory beneath the open pine canopy is typically dominated by native species characteristic of the foothills a few miles west of the Site. Shrubs in the understory include wax currant (*Ribes cereum*), skunkbrush (*Rhus trilobata*), and snowberry. Ponderosa pine (*Pinus ponderosa*) attracts wildlife not otherwise present in prairie ecosystems, including a number of species that are eastward extensions of the nearby foothills fauna.

Disturbed communities and/or barren lands occur as small inclusions of other habitat types usually associated with IHSSs. Some IHSSs, such as the old landfill, are essentially devoid of vegetation. Most of the disturbed land has been invaded by annual weeds, such as tumble mustard (*Sisymbrium altissimum*), tansy mustard (*Descurainia pinnata*), alyssum (*Alyssum minus*), prickly lettuce (*Lactuca serriola*), diffuse knapweed (*Centaria diffusa*), Russian thistle (*Salsola iberica*), kochia (*Kochia scoparia*), and bracted vervain (*Verbena bracteata*). The lack of cover and food limits wildlife use of this habitat.

3.7.1.2 Wildlife

Large Mammals Wildlife species within OU 5 are typical of the Site and similar habitats throughout the Front Range foothills. This semblance is due to a lack of barriers within the Site and between the western plains and the surrounding foothills. Larger mammals observed within OU 5 include the coyote (*Canis latrans*) and mule deer (*Odocoileus hemionus*). Both of these species are wide-ranging, and the mosaic of habitats within OU 5 is suitable for their use. Raccoons (*Procyon lotor*), long-tailed weasels (*Mustela*

frenata) striped skunks (*Mephitis mephitis*) and red foxes (*Vulpes vulpes*) also occur at the Site in habitats such as those in OU 5

Small Mammals The most common and widespread small mammal within OU 5 is the deer mouse (*Peromyscus maniculatus*) which has been captured in nearly every habitat type. Additional small mammal captures include the meadow vole (*Microtus pennsylvanicus*), prairie vole (*M. ochrogaster*), plains harvest mouse (*Reithrodontomys montanus*), western harvest mouse (*R. megalotus*) and hispid pocket mouse (*Chaetodipus hispidus*). Less widely distributed species include the silky pocket mouse (*Perognathus flavus*), plains pocket mouse (*P. flavescens*), olive backed pocket mouse (*P. fasciatus*) and meadow jumping mouse (*Zapus hudsonius*).

The meadow jumping mouse is of special interest because the subspecies that occurs at the Site, Preble's meadow jumping mouse (*Z. h. preblei*), is a candidate for federal listing as threatened or endangered (Figure 3-14). Preble's meadow jumping mouse has been captured at OU 5 and a significant amount of suitable habitat occurs there (Figure 3-14). Animals were captured in riparian areas with well-developed shrub canopies and a relatively lush understory of grasses and forbs. This is typical of habitats occupied by the subspecies throughout its range. Quantitative descriptions of small mammal distribution and abundance can be found in the Ecological Monitoring Program 1995 Annual Report (EG&G 1995f pending clearance).

Birds A variety of birds of prey occur at the Site. The most common species are the red-tailed hawk (*Buteo jamaicensis*) and great horned owl (*Bubo virginianus*), both of which are present on the site throughout the year and nest in mature cottonwoods or conifers such as those found in the Woman Creek valley. Other species that breed onsite include the Swainson's hawk (*Buteo swainsonii*), American kestrel (*Falco sparverius*) and long-eared owl (*Asio otus*).

The C ponds constructed at the Site for control of surface water runoff support seasonal use by a number of wading birds, shorebirds, waterfowl and related species. The largest water bird observed at the site is the great blue heron (*Ardea herodias*) which preys on fish, amphibians and large macroinvertebrates. Herons are prevalent at Pond C-2 because of its abundant fathead minnow population. The smaller black-crowned night heron (*Nycticorax nycticorax*) also feeds along the ponds although less commonly. Neither of these species is known to nest in OU 5 although they use the site during the breeding season.

The most common waterfowl on Ponds C 1 and C 2 are the Canada goose (*Branta canadensis*) mallard (*Anas platyrhynchos*) gadwall (*A. strepera*) green winged teal (*A. crecca*) blue winged teal (*A. discors*) and pied billed grebe (*Podilymbus podiceps*). All of the species listed above nest in wetland vegetation along the margins of the ponds.

The most extensive small bird communities in OU 5 are dominated by ground nesting species typical of prairie ecosystems in the region. Ridgetops and hillsides support species such as western meadowlark (*Sturnella neglecta*) vesper sparrow (*Pooecetes gramineus*) and grasshopper sparrow (*Ammodramus savannarum*) plus the horned lark (*Eremophila alpestris*) in more xeric habitats.

The presence of mature deciduous trees along Woman Creek riparian corridors attract arboreal (tree nesting) species such as the northern flicker (*Colaptes auratus*) eastern and western kingbirds (*Tyrannus tyrannus* and *T. verticalis*) black billed magpie (*Pica pica*) American robin (*Turdus migratorius*) warbling vireo (*Vireo gilvus*) yellow warbler (*Dendroica petechia*) northern oriole (*Icterus galbula*) blue grosbeak (*Guiraca cyanea*) and American and lesser goldfinches (*Carduelis tristis* and *C. psaltria*).

Wetland shrubs and cattails support a songbird community dominated by the red winged blackbird (*Agelaius phoeniceus*) common yellowthroat (*Geothlypis trichas*) song sparrow (*Melospiza melodia*) and less commonly the yellow headed blackbird (*Xanthocephalus xanthocephalus*).

Reptiles and Amphibians As is typical for the region, reptile and amphibian species are not as numerous as other invertebrates in OU 5. The most common species are the bullsnake (*Pituophis melanoleucus*) yellow bellied racer (*Coluber constrictor*) garter snakes (*Thamnophis* spp.) and prairie rattlesnake (*Crotalus viridis*). All of these species occur in the open grassland habitats that dominate OU 5, although the garter snakes are frequently found in or near water.

By far the most abundant and widespread amphibian at the Site and within OU 5 is the boreal chorus frog (*Pseudacris triseriata*). This small wetland dwelling member of the tree frog family occurs in virtually every stream, pond, ditch, or other area where surface water persists through the spring and early summer. A true frog, the northern leopard frog (*Rana pipiens*) is completely aquatic and requires permanent water such as is found in the C ponds.

The Woodhouse s toad (*Bufo woodhousei*) breeds in ponds and streams at the site but may wander considerable distances from water in search of insect prey. The plains spadefoot (*Scaphiopus bombifrons*) requires the least persistent water of any of the amphibians at the site. Like true toads such as the Woodhouse s toad, spadefoots spend most of the year in the mud beneath seasonally wet sites.

Arthropods Four classes of arthropods have been captured during sweep netting, pitfall trapping, or opportunistic netting of invertebrates within OU 5: the millipedes (Diplopoda), isopods or pill bugs (Crustacea), spiders and allies (Arachnida), and insects (Insecta) (DOE 1992c). Of these, the insects were the most abundant and taxonomically diverse group.

The arthropod community in OU 5 provides a prey base for insectivores. Grasshoppers and leafhoppers are probably the most important prey groups because of their abundance, size, and tendency to occur on the foliage of plants where they are easily detected and captured. Large grasshoppers are also consumed by predators such as kestrels and coyotes.

3.7.2 Aquatic Ecosystems

Aquatic habitats within OU 5 are restricted to the head waters of Woman Creek and its tributaries. Intermittent stream flow with areas of persistent flow typifies Woman Creek in OU 5. Intermittent segments contain isolated pools that provide important habitat for many aquatic species during the late summer and early fall when flow ceases. Persistent flows originate from seeps and springs around SW104, a surface water sampling site south of the OU 5 area, from Rocky Flats Lake, an abandoned gravel pit southwest of the Site, and dispersed groundwater seeps along Woman Creek. Pond C1 is the only impoundment of Woman Creek on the Site, as Pond C2 receives flow from the SID.

OU 5 IHSSs do not appear to impact Woman Creek's water quality. Water quality throughout the upper reaches of Woman Creek is good, and heterogeneous substrate in the stream channels provides habitat for species adaptable to variable flow (DOE 1992a, 1992c).

Benthic Communities The benthic macroinvertebrate community within Woman Creek is relatively rich and diverse (DOE 1992c). The most abundant and widespread groups overall in stream communities are the larvae of true flies (Diptera) and mayflies (Ephemeroptera). The most common dipteran taxa are

blackflies (Simuliidae) and midges (Chironomidae). Both caenid and baetid mayflies are also common. Other aquatic invertebrates include caddisflies (Trichoptera), crane flies (Diptera: Tipulidae), predatory damselfly larvae (Odonata), and two non-insect taxa, the amphipod (sideswimmer) (*Hyaella arteca*) and the snail (*Physella* sp.). Species richness for mayflies and caddisflies increases from headwater segments to SW026 (east of Pond C 2) where flow in Woman Creek decreases, apparently due to loss to groundwater (DOE 1992c).

The OU 5 pond habitats provide a more reliable water source than the intermittent stream channels. However, as is typical of lentic (pond) water bodies, the more homogenous substrate and lack of flow limits the macroinvertebrate communities. Most of the communities are strongly dominated by midges and aquatic earthworms (Oligochaeta). Pond C 1, with a more developed aquatic plant community along the edges, supports a more diverse assemblage of nektonic forms, including water striders (Hemiptera: Gerridae) and water boatmen (Hemiptera: Corixidae). Predatory dragonfly nymphs (Odonata) are present in the C ponds, as are crayfish (Astacidae).

Fish As with macroinvertebrates, low and intermittent flow along most stream reaches within OU 5 greatly limits the ichthyofauna of the site. Species captured in the streams include the creek chub (*Semotilus atromaculatus*), stoneroller (*Camptostoma anomalum*), fathead minnow (*Pimephales promelas*), and green sunfish (*Lepomis cyanellus*). Of these species, the creek chub is the most tolerant of poor water conditions. McClane (1978) reported that within its range, the creek chub may be found in almost any stream capable of supporting fish life.

Fish communities in the C ponds are highly influenced by the presence of suitable substrates, aquatic vegetation, and persistence of water. The most common species include the golden shiner (*Notemigonus crysoleucas*), white sucker (*Catostomus commersoni*), and largemouth bass (*Micropterus salmoides*). Golden shiners feed on a variety of small prey and algae and may themselves be important prey for larger fish or piscivorous birds because of the large populations they attain and their relatively large size. White suckers are tolerant of large amounts of pollution, siltation, and turbidity and are able to survive in waters low in oxygen (McClane 1978). This widespread species feeds on insect larvae and algae. Largemouth bass caught in Pond C 1 include large individuals that undoubtedly are at the top of the aquatic food web, aside from large terrestrial piscivores such as cormorants or great blue herons.

3 7 3 Species and Habitats of Special Concern

Candidate endangered animal species of interest include the Preble's meadow jumping mouse and ferruginous hawk (*Buteo regalis*). Both have been documented at the Site during field investigations in 1991 and 1992. Specimens of Preble's meadow jumping mouse were collected in moist habitats along Woman Creek in both 1991 and 1992 (EG&G 1992g). Swainson's hawks nest at the Site and the tall cottonwoods along Woman Creek represent suitable nest sites. Ferruginous hawks are present in the region primarily during the winter, but an unmated juvenile male spent considerable time in the Woman Creek drainage during the summer of 1991.

Only one endangered plant species, the Ute (or Diluvium) ladies' tresses orchid, is potentially on or near the Site. It has been observed on Boulder County open space 10 miles to the north and along Clear Creek to the south. However, it has not been observed during intensive field investigations in OU 5 and other reaches of Woman Creek in 1991 or during a sitewide endangered species survey in 1992 (EG&G 1992h).

3 8 PHYSICAL CHARACTERISTICS OF EACH IHSS

This section provides discussions of physical characteristics as they pertain specifically to the geology and hydrogeology of each IHSS within OU 5. The physical setting of each IHSS is also described within each of the following sections.

3 8 1 IHSS 115 (Original Landfill) and IHSS 196 (Filter Backwash Pond)

This section discusses the geology, hydrogeology, and physical setting of IHSSs 115 and 196. Because IHSS 196 is located within the boundaries of IHSS 115, these IHSSs are discussed together.

The Original Landfill (IHSS 115) and the Filter Backwash Pond (IHSS 196) are located within the south buffer zone just south of the Site industrial area (Figure 3-15). IHSS 115/196 are located north of Woman Creek on a moderately to steeply sloping south-facing hillside (DOE 1994a, Appendix C Photos 39, 40, and 42). The northern portion of the Original Landfill lies just south of the buffer zone access road and forms a flat bench that drops off to the south (DOE 1994a, Appendix C Photo 14). In the western section of the Original Landfill (DOE 1994a, Appendix C Photo 47), an erosional swale exists. The original

landfill extends beneath the SID and the SID road and along the south sloping hillside down to Woman Creek. Three seeps have been identified along the eastern edge of the surface disturbance east of the Original Landfill (Figure 3-15). A sewer outfall pipe daylights in the top central portion of the original landfill (DOE 1994a Appendix C Photos 51 and 54). Waste debris can be found along the surface of the original landfill and sticking out of sloped areas (DOE 1994a Appendix C Photos 19, 20, 44, 52, and 53).

IHSS 196 lies near the bottom of the above mentioned swale north of the SID within IHSS 115 (Figure 3-15). IHSS 196 lies within a flat section of the swale and is surrounded by steeping sloping sidewalls to the north, west, and east. Two seeps have also been identified in the area of and west of IHSS 196 (Figure 3-15).

The physical characteristics of the IHSS 115/196 area were based on information from the Phase I and TM15 field investigations (DOE 1992a and 1994a), the Geologic Characterization Report (EG&G 1995a), the Hydrogeologic Characterization Report (EG&G 1995b), and the Preliminary RFETS OU 5 Geotechnical Investigation (EG&G 1995e).

3.8.1.1 Geology IHSS 115/196

Geologic deposits present in IHSS 115/196 consist of unconsolidated artificial fill, waste fill, landslide colluvium, valley fill, alluvium (Piney Creek Alluvium), Rocky Flats Alluvium, and consolidated bedrock of the undifferentiated Arapahoe/Laramie Formations, and are discussed below. Borehole and monitoring well locations are presented in Figures 2-4 and 3-16. The preliminary geotechnical map of the area shows the surficial geology and is presented in Figure 3-16. Geologic cross sections through the area are presented in Figures 3-17 through 3-20B. Figure 3-21 presents the thickness of unconsolidated materials in IHSS 115/196 which range from 2 feet up to approximately 37 feet. The thickest sections of unconsolidated material is apparently Rocky Flats Alluvium in the northwest (boring 59594), waste fill in the central (boring 58693), and artificial fill and landslide material in the southeast center (57094) of the Original Landfill.

Artificial Fill Artificial fill was encountered along the eastern portion of IHSS 115 and consisted primarily of sandy, gravelly clay and lacked plant production waste. The artificial fill was placed along the

south side of the SID during its construction and consisted of excavated material and clean imported road base/fill

Waste Fill Waste fill encountered in IHSS 115/196 consisted predominantly of sandy clayey gravels and cobbles derived from the Rocky Flats Alluvium mixed with varying amounts and types of waste from previous production at the site. Types of waste observed during this investigation included sheet metal, wood, broken glass, glass bottles, plastic, rubber, metal shavings, ceramic, shingles, nails, solid blocks of graphite, fine graphite silt and sand, concrete, asphalt, and 55 gallon steel drums. The consistency of the waste fill ranged from loose and unconsolidated to moderately dense and consolidated. The thickest deposits of the waste fill ranged from 9 feet (boring 56994), 12 feet (59194), and 15.5 feet (boring 56893) in the central area of IHSS 115/196 to approximately 12 to 20 feet on the west side of IHSS 115 (Figure 3-17).

Landslide Landslide deposits were not differentiated from the other geologic deposits presented in Figure 3-16 because the other geologic units were incorporated into the landslides during the landsliding. Figures 3-18 through 3-20B show a symbol for landslide deposits; however, this unit may contain material from several discrete units and possibly different landslide events. A discussion of the landsliding in IHSS 115/196 is presented in Section 3-8.1.2.

Colluvium Colluvium is exposed in small undisturbed areas south of the Rocky Flats pediment terrace (Figure 3-16) where the deposit was developed on the gently sloping bedrock surface. Colluvium consisted primarily of sandy clayey gravel and cobbles and sandy clay. In cross section, the colluvium appears to be mixed with and apparently mobilized into the landslide deposits. The thickness of colluvium ranged from 1 foot up to 13 feet.

Valley Fill Alluvium/ Piney Creek Alluvium Valley fill alluvium (Piney Creek Alluvium of Figure 3-9) was encountered along Woman Creek and consisted primarily of sandy to silty-clayey gravel with cobbles. The maximum thickness of valley fill alluvium was 5 to 7 feet.

Rocky Flats Alluvium Rocky Flats Alluvium was encountered on the north side of IHSS 115/196 and consisted primarily of gravelly sand with some clay to sandy clay and clayey sand with some to trace gravel. In addition, there was a paleo-stream channel encountered in boring 59594 where a medium to

fine grained sand was observed from 32 feet to 37 45 feet immediately above the underlying bedrock. Thickness of the Rocky Flats Alluvium ranged from approximately 15 feet (boring 56994 where 9 feet of overlying waste fill was observed) to 37 45 feet (boring 59594).

Arapahoe/Laramie Formations The undifferentiated Arapahoe/Laramie Formation in IHSS 115/196 consisted predominantly of claystone with some thin interbeds and laminae of siltstone and sandstone. The claystone was observed to be massive to thinly laminated containing trace ironstone nodules trace to some organics in the form of leaf imprints disseminated carbon and trace lignite interbeds with some thin interbeds and laminae of siltstone and sandstone. Sandstone and siltstone interbeds from 0 5 to 10 feet in thickness consisted of very fine to fine grained clayey to silty sandstones and sandy to clayey siltstones slightly friable to well cemented trace ironstone nodules cross bedded to laminated with some soft sediment deformation structures and trace fossils with trace to some disseminated carbon.

As part of the groundwater investigation to evaluate possible hydraulic interaction between the UHSU and the LHSU and to evaluate the inferred Fault 2 (Figure 3 11) five bedrock boreholes (56694 57194 57594 59894 and 71194) were drilled in and around the IHSS 115/196 area (Figures 2 4 and 3 16). Monitoring wells were installed in the borehole and screened where potential water bearing sandstones or siltstones (Figure 3 8) were encountered on the basis of the geologic and geophysical logs (Appendix B). Boring 56694 was abandoned due to borehole collapse during well installation and boring/well 59394 was installed as an offset. A sixth well (71494) was located on the basis of the upper siltstone interval observed at location 57194. The inferred Fault 2 apparently intersects the Old Landfill between locations 71194 and 57194 striking north northeast. Vertical displacement of the A claystone along Fault 2 was estimated at 60 feet.

As part of the geotechnical investigation of the Original Landfill (EG&G 1995e) the claystone bedrock presented in cross sections A A through D D (Figures 3 17 through 3 20b) was differentiated based on the degree of weathering. Classifications are severely weathered claystone moderately weathered claystone and fresh claystone. Severely weathered claystone ranged in thickness from 0 5 feet to 4 feet and is weathered to the extent that little to no original rock texture or structure are recognizable. Moderately weathered claystone ranged in thickness from 2 feet to 23 feet and is highly weathered (showing some discernible bedding structure with heavy iron oxide staining of both the groundmass and fractures and/or bedding planes) to moderately weathered (easily discernible bedding structures with

variable amounts of iron oxide staining) to slightly weathered (occasional iron oxide staining along fractures and bedding) Fresh unweathered bedrock is characterized by the absence of iron-oxide staining

3 8 1 2 Landsliding IHSS 115/196

As shown on Figure 3 16 several discrete landslides as well as general areas of land sliding within the IHSS 115/196 area were defined during the geotechnical investigation Other areas of land sliding may possibly exist within the study area, although these areas are not readily evident due to their lack of indicative surface morphology Such areas would involve slides that are obscured by fill and that are not apparent on pre landfill airphotos or that are very old with completely eroded surface features (EG&G 1995e)

Three types of slope failure were noted within the IHSS 115/196 area during this geotechnical study These failure types involve different geologic materials underlying the landfill slope and are presented below

The first type of slope failure involved waste fill land sliding on severely weathered claystone Evidence for this type of failure was encountered in borehole 57194 which was located approximately 20 feet downslope of the upper concave landslide scarp in the central portion of the upper landfill slope (Figure 3 21) (EG&G 1995e) Approximately 3 feet of waste fill on disturbed moderately weathered claystone overlies in place severely weathered claystone The contact of disturbed and in place claystone at 4 feet lies along a nearly horizontal (10 degree) slick slide surface The disturbed material from 3 2 to 4 feet may represent a block of claystone worked in with the waste during fill placement, or bedrock incorporated within the sliding fill (EG&G 1995e)

The second type of slope failure involved colluvium sliding on severely weathered claystone Evidence of this type of land sliding was found in borehole 71294 located within the recent slide mass at the southeast corner of the study area The colluvium at this location appears to have failed on or with underlying severely weathered claystone (EG&G 1995e)

The third type of slope failure involved landsliding within moderately weathered claystone Direct evidence of this type of slope failure was found in boring 57694 and in deep bedrock monitoring well

57594 These boreholes were drilled in the lower slope south of the SID in the east portion of IHSS 115 (Figure 3 21) (EG&G 1995e) At borehole 57694 (drilled into a relatively recent land slide) 3 feet of colluvium and 11 5 feet of underlying moderately to severely weathered claystone overlies in place severely weathered claystone at 14 5 feet At borehole 57594 a similar sequence with 6 feet of colluvium and about 10 5 feet of claystone overlies in place moderately weathered claystone at a depth of 16 5 feet (EG&G 1995e) The landslide encountered in borehole 57694 is shown on section C C

The occurrence of colluvium or landslide debris underlain by moderately weathered claystone without an intermediate zone of severely weathered bedrock, presents indirect evidence of sliding within the moderately weathered claystone This relation was encountered in several boreholes including 59694 58693 57094 and possibly 56994 (EG&G 1995e) The land slides as interpreted in these boreholes located along the slope above the SID are shown in sections A A and B B and Figure 3 21

Based on a 1951 airphoto boreholes 59794 71194 58693 59294 and 59094 are located within the limits of what appears to be a large landslide (Figure 3 21) No apparent slide debris was encountered in borings 59794/71194 however the alluvial bedrock contact is approximately 14 feet deeper than the elevation of the contact observed in borings 43392 and 59194 suggesting some movement downslope at this location has occurred At 58693 roughly 12 feet of wet colluvium/slide material underlies approximately 15 feet of waste fill and overlies fresh claystone at about 27 feet Boreholes 59294 and 59094 are located on the lower slope south of the SID 59294 shows landslide materials that overlie severely weathered claystone and 59094 shows similar landslide debris overlying valley fill alluvium along Woman Creek (EG&G 1995e)

The geologic interpretation presented on Section B B (Figure 3 18) suggests a thick landslide deposit or complex of land slides through borehole 57094 This interpretation is based on the appearance of colluvium/slide material in the deeper portion of the core from 57094 the low top of bedrock elevation the relatively thin moderately weathered zone underlying colluvium/slide and the base elevation of the nearby land slide evidenced in core from borehole 57594 Along the upper portion of Section B B sliding at the location of grouped boreholes 57194 58394 and 71494 (located between prominent scarps on the upper landfill slope) involves waste fill slipping on weathered claystone The conceptual landslide model presented on Section B B shows waste fill below the lower scarp failing on the older slide material encountered in 57094 The actual depth of this upper waste fill slide below the lower scarp is uncertain (EG&G 1995e)

No compelling evidence for deep seated sliding within the fresh claystone was encountered during the geotechnical investigation (EG&G 1995e)

3 8 1 3 Hydrogeology IHSS 115/196

The UHSU hydrogeology of the IHSS 115/196 area is characterized by the southerly slope toward Woman Creek man made drainages (the SID and building drains) and groundwater flow through the unconsolidated surface deposits (artificial fill waste fill landslide deposits colluvium, and valley fill alluvium) and the weathered bedrock of the Arapahoe/Laramie Formations) As described in Section 3 6 3 2 the LHSU consists of unweathered bedrock of the Arapahoe/Laramie Formations A total of sixty one wells or piezometers (well points using teflon tubing mini wells using 1 inch PVC pipe and monitoring wells using 2 inch PVC pipe) were installed in the IHSS 115/196 area as part of the OU 5 RFI/RI investigation The UHSU potentiometric surface for September 1994 and May 1995 are presented in Figures 3 24 and 3 25 which represent the lowest and highest water level elevations respectively recorded during the period August 1994 to July 1995 Only four UHSU wells were dry during the May 1995 water level monitoring event and these locations were south of the SID on bedrock topographic highs Well 62893 which was constructed in an area of a seep was observed to be flowing at the surface during May 1995

Groundwater generally flows from the upgradient Rocky Flats Alluvium through the laterally continuous and intertonguing unconsolidated surficial materials in a south southeasterly direction until reaching the apex of Woman Creek (Figures 3 17 to 3 19) Along Woman Creek the groundwater flow direction changes to an easterly direction parallel to surface water flow The average groundwater gradient is 0 13 foot/foot during September 1994 and 0 16 foot/foot during May 1995 Groundwater flow is downgradient along the contact between the overlying unconsolidated deposits and the low permeability claystone bedrock

Recharge of the IHSS 115/196 area is primarily from upgradient precipitation infiltration (ground surface and along the SID) and possibly from building drains Groundwater discharges to the surface in places of shallow bedrock as diffuse flow (seeps) and concentrated flow (springs) (Figures 3 15 and 3 16) Below the SID Woman Creek is a losing stream for most of the year except for the wettest months Seasonal variations in recharge strongly affect the UHSU potentiometric surface (Figures 3 24 and 3 25) Figures

3 22 and 3 23 present hydrographs of wells located in the IHSS 115/196 area. Note the cyclic nature of the hydrographs for wells 59493 and 59593 which were monitored over a two year period (Figure 3 22). Seasonal fluctuations of six feet were observed in the wells located in IHSS 196 (wells 59493 63893 63993 and 64093) and over nine feet in well 60593 southwest of IHSS 115/196.

Hydraulic characteristics of the waste fill in IHSS 115/196 were estimated during aquifer tests performed in 1993 (DOE 1994a). Results of the test on Well 59493 revealed hydraulic conductivities ranged from 1.37×10^{-3} to 1.73×10^{-2} cm/sec. Hydraulic conductivities in this range are indicative of permeable well sorted sands and gravels. The log of 59493 indicates the waste fill is underlain by approximately 1 foot of colluvium which is underlain by fresh to moderately weathered claystone bedrock.

Hydraulic conductivities of the valley fill alluvium/Piney Creek Alluvium in IHSS 115/196 were estimated in well 7086 during aquifer test evaluations for the RFETS Hydrogeologic Characterization Report which ranged from 1.5×10^{-4} to 6.8×10^{-4} cm/sec (EG&G 1995b).

Hydraulic characteristics of the Rocky Flats Alluvium in IHSS 115/196 were estimated during aquifer tests performed in 1995 by the Aquifer Testing Program (EG&G 1995i). Hydraulic conductivities in well 56994 ranged from 1.0×10^{-5} to 1.2×10^{-6} cm/sec using the falling head and rising head methods respectively and well 59594 was estimated at 7.7×10^{-3} cm/sec using both the rising and falling head methods.

Hydraulic characteristics of the colluvium/landslide material in IHSS 115/196 were estimated during aquifer tests performed in 1995 by the Aquifer Testing Program (EG&G 1995i). Hydraulic conductivities in well 59694 were estimated at 6.8×10^{-7} cm/sec using the rising head method.

As described in Section 3 5 3 2 the LHSU consists of unweathered bedrock of the Arapahoe/Laramie Formations. To evaluate the potential for hydraulic interaction between the UHSU and LHSU six bedrock monitoring wells were installed during the implementation of TM15 (DOE 1994a). One of the six monitoring wells (well 57594) displayed artesian conditions (a water level elevation higher than the top of the confined aquifer it is screened in) during May 1995. Well 57594 had a hydraulic head measured at 5940.5 feet above MSL and two adjacent UHSU wells with lower water table elevations wells 59993 and 57994 at 5937 feet and 5936 feet above MSL respectively. Thus the vertical gradient in this area near Woman Creek is upward at 1.0 foot/foot.

Of the six LHSU wells three developed sufficient groundwater to be sampled for water quality parameters (57594 59894 and 71494) the remaining three wells have developed very slowly and have not been fully developed or sampled (57194 59394 and 71194). Water level measurements from wells 57194 59394 and 71194 have not stabilized since installation which is consistent with the textural properties and low permeabilities of the LHSU. Water level measurements in wells 57194 59394 59894 71194 and 71494 indicate downward vertical gradients reflecting areas of recharge.

Hydraulic characteristics of the LHSU in IHSS 115/196 were estimated during aquifer tests performed in 1995 by the Aquifer Testing Program (EG&G 1995i). Hydraulic conductivities of the upward fining clayey sandstone to sandy claystone in well 57594 ranged from 1.1×10^{-6} to 7.0×10^{-7} cm/s. Hydraulic conductivities of the sandy siltstone in well 59894 ranged from 2.5×10^{-6} to 9.7×10^{-7} . Hydraulic conductivities of the siltstone in well 71494 ranged from 3.8×10^{-6} to 6.2×10^{-6} . The hydraulic conductivities of the LHSU lithologies screened in IHSS 115/196 are comparable to the geometric means for unweathered bedrock sandstone siltstone and claystone (5.7×10^{-7} cm/s, 1.5×10^{-7} cm/s, and 2.4×10^{-7} cm/s respectively [EG&G 1995b]) reported in Section 3.5.3.2.

In summary on the basis of the contrasts in hydraulic conductivities observed in IHSS 115/196 the UHSU groundwater flow is along the contact between the fresh to moderately weathered bedrock and the overlying unconsolidated surficial materials. Due to the downward vertical gradient created by the two to three orders of magnitude difference in hydraulic conductivities between waste fill/Rocky Flats Alluvium and the bedrock in IHSS 115/196 very little possibility exists for downwind migration of contaminants.

3.8.2 IHSS 133 (Ash Pits Incinerator and Concrete Wash Pad)

This section discusses the geology hydrogeology and physical setting of IHSS 133. The IHSS incorporates four original ash pits and two new ash pits (TDEM 1 and TDEM 2) that were used to dispose of incinerator ashes the former incinerator area and a concrete wash pad. The concrete wash pad was used to wash out cement trucks that were being used to construct the Site facilities.

The IHSS 133 area is located within the south buffer zone just southwest of the Site industrial area south of the west access road and north of Woman Creek (Figure 3.15). Six IHSSs one pit, and a disturbed area east of the IHSSs were identified. Two additional ash pits (TDEM 1 and TDEM 2) were identified from

aerial photographs results of the TDEM survey and the soil boring investigation IHSSs 133 1 through 133 4 (the four original ash pits) IHSS 133 6 (concrete wash and disposal area) and the two TDEM anomalies lie south of a steep south facing slope on a fairly flat lying surface that slopes gently toward Woman Creek (DOE 1994a, Appendix C Photos 31 and 32) Photographs 18 and 36 in TM15 Appendix C show IHSS 133 2 (an ash pit delineated by two signs shown at the right side of photo 18) located just below the above mentioned steep slope The terrain is hummocky (DOE 1994a, Appendix C Photos 31 and 32) and the individual ash pits can to some extent be identified as a hump on the ground surface IHSS 133 5 (shown on DOE 1994a, Appendix C Photo 17) occupies a portion of the above mentioned steep south facing slope and a portion of a flat bench above the sloped area IHSS 133 5 is the where the old incinerator was located and an area that was subsequently used for washing concrete trucks It was common practice for concrete trucks with unused partial loads of concrete to have their remaining loads poured and their interiors washed prior to being returned to their respective concrete plants

The overall area is predominantly covered with prairie grasses and cacti A dirt access road, an underground abandoned gasline and an overhead powerline pass east to west through the IHSS 133 area

The physical characteristics of the IHSS 133 area were based on information from the Phase I and TM15 field investigations (DOE 1992a and 1994a) the Geologic Characterization Report (EG&G 1995a) and the Hydrogeologic Characterization Report (EG&G 1995b)

3 8 2 1 Geology IHSS 133

Geologic deposits present in IHSS 133 consist of unconsolidated artificial fill waste fill landslide colluvium valley fill alluvium (Piney Creek Alluvium) Rocky Flats Alluvium, and consolidated bedrock of the Arapahoe/Laramie Formations are discussed below The surficial geology and bedrock geologic map are presented in Figures 3 4 and 3 9 Borehole and monitoring well locations are presented in Figures 2 12 and 3 26 Geologic cross sections through the area are presented in Figures 3 27 through 3 32 Figure 3 33 presents the thickness of unconsolidated materials in IHSS 133 which range from 2 5 feet up to approximately 34 feet The thickest sections of unconsolidated material appears to be the Rocky Flats Alluvium along the north side (55493) of IHSS 133 5 and the colluvium/landslide material in the east side (57093) in IHSS 133 2 A moderately thick section of colluvium/landslide material is present

along the west side of IHSS 133 4 The thick sections of unconsolidated material on the east side of IHSS 133 2 and west side of IHSS 133 4 may represent paleo-landslide deposits

Artificial Fill Artificial fill encountered along the west central portion of IHSS 133 consisted primarily of gravelly to clayey sand and clay concrete and lacks incinerated waste ash The artificial fill was placed in and around IHSS 133 5 the former incinerator area and IHSS 133 6 the concrete washout area (Figure 3 9) Artificial fill was also placed as thin lifts for daily cover during disposal of the incinerator ash

Waste Fill Waste fill encountered in IHSS 133 consisted predominantly of incinerated types of waste from previous production at the Site mixed with sandy silt Types of waste observed during this investigation included small pieces of rusted metal sand to silt size metal broken glass asbestos ceramic and nails The consistency of the waste fill was loose with some evidence of differential compaction which created void spaces above the ash and the overlying cover of artificial fill Waste fill from the incinerator was apparently placed into the ash pits in thin lifts which ranged in thickness from less than 0 5 foot up to approximately 3 feet (Appendix B) Waste fill was encountered to depths of up to 18 feet (boring 56094) but predominantly limited to depths less than 8 feet Waste fill/ash material was encountered in IHSSs 133 1 133 2 (northern half was confirmed to be an ash pit) 133 4 and in the two previously unidentified ash pits TDEM 1 and TDEM 2 (Figures 3 26 3 27 3 29 and 3 30) Waste ash material was also encountered in borehole 58093 between IHSSs 133 1 and 133 4 (Figure 3 26) The lateral extent of waste fill correlates well with the TDEM anomaly map in Figure 2 11

Landslide Landslide deposits were differentiated from the other geologic deposits presented in Figure 3 9 on the basis of the hummocky topography present. Because the colluvium was incorporated into the landslide deposits during the landsliding and colluvium closely resembles the textural characteristics observed in IHSS 115/196 landslide deposits will be referred to as colluvium.

Colluvium Colluvium is exposed south of the Rocky Flats pediment terrace (Figure 3 9) where the deposit was developed on the gently sloping bedrock surface Colluvium consisted primarily of sandy clayey gravel and cobbles and sandy clay The colluvium appears to mixed with and apparently mobilized into the landslide deposits on the eastern portion of IHSS 133 The thickness of colluvium ranged from 2 5 up to 34 feet

Valley Fill Alluvium/ Piney Creek Alluvium Valley fill alluvium (Piney Creek Alluvium of Figure 3 9) was encountered along Woman Creek and consisted primarily of sandy to silty-clayey gravel with cobbles. The maximum thickness of valley fill alluvium was 5 to 10 feet.

Rocky Flats Alluvium Rocky Flats Alluvium was encountered on the north side of IHSS 133 and consisted primarily of gravelly sand with some clay to sandy clay and clayey sand with some to trace gravel. Thickness of the Rocky Flats Alluvium ranged from 27 feet (boring 55393) to 32.8 feet (boring 55493).

Arapahoe/Laramie Formations The undifferentiated Arapahoe/Laramie Formation in IHSS 133 is assumed to be the same as the bedrock encountered in IHSS 115/196. Bedrock lithology observed in boring 59894 northeast of IHSS 133.2 consisted predominantly of claystone with some thin interbeds and laminae of siltstone and sandstone. The claystone was observed to be massive to thinly laminated containing trace ironstone nodules, trace to some organics in the form of leaf imprints, disseminated carbon and trace lignite interbeds with some thin interbeds and laminae of siltstone and sandstone. Sandstone and siltstone interbeds (Figure 3 8) from 0.5 to 10 feet in thickness consisted of very fine to fine grained clayey to silty sandstones and sandy to clayey siltstones, slightly friable to well cemented, trace ironstone nodules, cross bedded to laminated with some soft sediment deformation structures and trace fossils with trace to some disseminated carbon.

Sandy claystone and clayey sandstone was encountered in boreholes east of IHSS 733.2 (boreholes 57493, 57593, and 59494/59894) on the east side of IHSS 133.2 (boreholes 57093 and 57393). Sandy claystone was also encountered between IHSSs 133.3 and 133.4 (borehole 63093) and clayey siltstone was encountered on the west side of the north ash pit in IHSS 133.4 (55893).

3 8 2 2 Hydrogeology IHSS 133

The UHSU hydrogeology of the IHSS 133 area is characterized by the southerly slope toward Woman Creek and groundwater flow through saturated unconsolidated surface deposits (artificial fill, waste fill, colluvium/landslide deposits, and valley fill alluvium) and the weathered bedrock of the Arapahoe/Laramie Formations. As described in Section 3 6 3 2, the LHSU consists of unweathered bedrock of the Arapahoe/Laramie Formations. A total of twenty-nine wells or piezometers (well points using teflon tubing, mini wells using 1 inch PVC pipe, and monitoring wells using 2 inch PVC pipe) were

installed in the IHSS 133 area as part of the OU 5 RFI/RI investigation. The UHSU potentiometric surface for October 1994 and May 1995 are presented in Figures 3-34 and 3-35 which represent the lowest and highest water level elevations respectively recorded during the period August 1994 to July 1995. Only two UHSU wells were dry during the May 1995 water level monitoring event and these wells were 51593 and 55794. Well 51593 is south of IHSS 133-3 and well 55794 is southwest of IHSS 133-3. These wells are dry and do not fully penetrate the surficial materials due to refusal during drilling. Well 62693 which was constructed in an area of a seep was observed to be flowing at the surface during May 1995.

Groundwater generally flows from the upgradient Rocky Flats Alluvium through the laterally continuous and intertonguing unconsolidated surficial materials in a south southeasterly direction until reaching the apex of Woman Creek (Figures 3-34 and 3-35). Along Woman Creek the groundwater flow direction changes to an easterly direction parallel to surface water flow. The groundwater gradient appears to be strongly affected by seasonal fluctuations and from west to east across IHSS 133. For October 1994 the gradient is 0.09 foot/foot on the west side, zero or unsaturated through the center, and 0.07 foot/foot on the east side. For May 1995 the gradient is 0.1 foot/foot on the west side, 0.18 foot/foot through the center, and 0.1 foot/foot on the east side. Groundwater flow is downgradient along the contact between the overlying unconsolidated deposits and the low permeability claystone bedrock where there appears to be bedrock topographic lows.

Recharge of the IHSS 115/196 area is primarily from upgradient precipitation infiltration. Groundwater discharges to the surface in places of shallow bedrock as diffuse flow (seeps) and concentrated flow (springs) (Figures 3-15 and 3-16). Woman Creek is a losing stream for most of the year except for the wettest spring months (December, March, or April). Seasonal variations in recharge strongly affect the UHSU potentiometric surface (Figures 3-34 and 3-35). Figure 3-36 presents hydrographs of wells located in the IHSS 133 area. Note the cyclic nature of the hydrographs for wells 58793 and 63093 which were monitored over a two year and one period respectively. Seasonal fluctuations of 9 feet were observed in several of the wells located in IHSS 133 (wells 58793, 63593, 63693, and 56494) and over 15 feet in well 56294 southwest of IHSS 133-3.

Hydraulic characteristics of the colluvium/landslide material in well 58793 in IHSS 133 were estimated during aquifer tests performed in 1993 (DOE 1994a). However, the results of the test on well 58793 were inconclusive. The well dewatered at a low pumping rate and no drawdown was observed in the observation wells (DOE 1994a).

Hydraulic conductivities of the valley fill alluvium/Piney Creek Alluvium in IHSS 133 were estimated in well 5686 during aquifer test evaluations for the RFETS Hydrogeologic Characterization Report which ranged from 1.0×10^{-4} to 5.0×10^{-5} cm/s (EG&G 1995b)

3.8.3 IHSS 142 (C Series Ponds)

This section discusses the physical setting, geology, and hydrogeology of IHSSs 142.10 and 142.11. Also, because these IHSSs are actually ponds, a section describing their hydrology is included.

Ponds C.1 (IHSS 142.10) (DOE 1994a, Appendix C Photo 68) and C.2 (IHSS 142.11) (DOE 1994a, Appendix C Photo 74) are located along Woman Creek within the southeast section of the south buffer zone on the eastern reach of Woman Creek (Figure 3.15). These ponds are approximately 2,000 feet apart, with Pond C.1 to the west or upstream of Pond C.2 along Woman Creek. According to Merrick Engineering (1992), the maximum storage capacity of Pond C.1 is 5.2 acre feet and Pond C.2 is 69.4 acre feet. The estimated average retention in Pond C.1 is 29 percent or 1.5 acre feet and Pond C.2 is 20 percent or 14 acre feet (Patton 1995). Sediment from erosional processes has been deposited into these ponds since their construction, thereby decreasing their storage capacities (see Section 3.4).

3.8.3.1 Geology IHSS 142

The geology of IHSSs 142.10 and 142.11 has been characterized from information obtained from monitoring well boreholes and the Geologic Characterization Report for The Rocky Flats Environmental Technology Site (EG&G 1995a). The surficial geology within the area of IHSSs 142.10 and 142.11 is for the most part nonexistent because these IHSSs primarily encompass Ponds C.1 and C.2. However, the surficial material surrounding the ponds consists mainly of artificial fill. Small areas along the north and west shores of both ponds and a larger area east of Pond C.1 and north of Pond C.2 consist of Piney Creek Alluvium (Figure 3.10) (EG&G 1995a). Descriptions of these units, as well as an IHSS-specific description of the alluvial thickness, are provided in the following paragraphs.

Other surficial materials surrounding these IHSSs are primarily landslide deposits and colluvium (Figure 3.10), both of which have been described in previous sections of this report.

The valley filled alluvium that was encountered in the wells east of IHSSs 142 10 and 142 11 ranged in thickness from 4 to 10 feet. The thickness of the valley fill alluvium encountered in wells 50092 and 50192 (east of IHSS 142 10) and 50292 (east of IHSS 142 11) was approximately 10 feet and consisted predominantly of a sandy or silty gravel and silty sands overlain with a silty clay/clayey silt (Figures 3 37 and 3 38). The thickness of the valley fill alluvium encountered in well 51193 (east of IHSS 142 10) was approximately 7 1 feet (Figure 3 38) and the thickness of the valley fill alluvium in the small diameter wells (drilled for aquifer testing) surrounding well 51193 was 5 5 feet in well 63293, 4 feet in well 63393 and 9 5 feet in borehole 63493. The valley fill alluvium encountered at these locations is assumed to be the same as described above.

Valley fill alluvium may not be present beneath the detention ponds because the top 5 to 10 feet of the surficial materials was removed during construction. The base of the C 2 pond is keyed into the bedrock of the Laramie Formation but C 1 Pond is not keyed into bedrock. The sediment that has been deposited in the ponds since their construction is unconsolidated and consists of fine grained organic silts and clays (DOE 1992a).

Based on borehole data, the bedrock underlying the areas adjacent to IHSSs 142 10 and 142 11 consists of claystone. Claystone bedrock provides a relatively impermeable layer. As shown on the Geologic Map of the Rocky Flats Environmental Technology Site and Vicinity (Plate 2 1 EG&G 1995a) the bedrock beneath these ponds appears to be the Laramie Formation (Figure 3 4).

3 8 3 2 Hydrogeology IHSS 142

The hydrogeology of the C 1 and C 2 Ponds is controlled primarily by surface water as both ponds are located along Woman Creek (Figure 1 2). Both ponds were created by dams. The C 1 Pond is within the channel of Woman Creek and is recharged by stream flow and possibly by groundwater inflow during the wetter months. Woman Creek upgradient of the C 1 pond is gaining during the wet months of December through March or April but losing the rest of the year. Immediately downgradient of the C 1 pond Woman Creek is losing year round. During the drier months the C 1 pond may act as a source of recharge to the groundwater system. The water level in the C 1 pond is controlled by a gate. Two wells (50092 and 51193) located at the base and east of the C 1 dam perennially contain groundwater (Figure 2 13). The

C 1 dam is not keyed to bedrock and groundwater appears to flow beneath the dam. Dam C 1 has a hydraulic height of 15 feet and is classified as a small size dam (Army Corps of Engineers 1984).

The C 2 Pond is located farther east along a losing reach of the original Woman Creek stream channel. Woman Creek has been diverted around the C 2 pond and surface water from Woman Creek flows into the pond only during periods of high flow. The SID drains into the C 2 Pond and therefore accepts surface water drainage from the industrialized area upgradient of the SID. The dam at C 2 Pond is keyed into bedrock and effectively stops groundwater flow from moving out of the pond and cutting off flow to the natural stream channel east of the dam (Figure 2 13). This is evidenced by wells 50192 and 50292 east of the base of the dam which are perennially dry. Dam C 2 has a hydraulic height of 35.5 feet and is classified as a small size dam (Army Corp of Engineers 1984). The C 2 Pond is a terminal pond and the water level in the pond is controlled by pumping and transferring the water to the Broomfield Diversion Ditch.

3 8 4 IHSS 209 and Other Surface Disturbances

This section discusses the physical setting, geology, and hydrogeology specific to IHSS 209, the Surface Disturbance West of IHSS 209, and the Surface Disturbance South of the Ash Pits.

Three separate surface disturbances are described in this section. These areas include IHSS 209, the Surface Disturbance West of IHSS 209, and the Surface Disturbance South of the Ash Pits. IHSS 209 is located approximately 1,000 feet southeast of Pond C 1 (Figure 3 15). This area was included as an IHSS because unknown activities took place in this area of shallow excavations and surface disturbances. This IHSS covers approximately 5.2 acres and is located along a long narrow plateau bounded to the north, east, and south by a uniform slope leading into the Woman Creek drainage. A dirt road transects this IHSS and circles near the eastern boundary of the IHSS. Three excavations are located within the boundary of this IHSS (Figure 1 5). Two depressions, which periodically retain water, are present near the northern and southwestern boundary of this unit (Figure 1 5) (DOE 1992a). Photo 82 in TM15 Appendix C shows the depression at the southwestern end of the IHSS. The depth of this depression is about five feet.

A second surface disturbance, the Surface Disturbance West of IHSS 209, is located approximately 1,500 feet west of IHSS 209 (Figures 1 5 and 3 15) and consists of several small disturbed areas. This

disturbance covers an area of about 62 500 square feet (DOE 1992a) and is located on a fairly shallow slope that faces north toward Woman Creek

A third surface disturbance area, the Surface Disturbance South of the Ash Pits is located approximately 1 200 feet south of the IHSS 133 area and south of Woman Creek (Figure 3 15) This area consists of four excavations and a disturbed area that is covered with boulders (DOE 1994a, Appendix C Photo 89) on the western side of the disturbed area (Figure 1 6) Two excavations trend along northeast southwest axes each approximately 30 feet wide and 400 feet long Photos 83 and 84 in TM15 Appendix C show one of the excavated trenches looking southwest and northeast respectively These photos show this trench to be approximately 5 to 8 feet wide and about 2 feet deep A horseshoe shaped area is located northeast of the parallel excavations and a third excavation is located to the southwest (DOE 1992a) This surface disturbance is located on top of a high plateau that is situated along the southern portion of the OU It is sloped on the north and southeast Two ephemeral streams drain this area These streams flow into Woman Creek from the north and southeast sides of the disturbed area

3 8 4 1 Geology

The geology of IHSS 209 and the other surface disturbances have been characterized from information obtained from boreholes and the Geologic Characterization Report (EG&G 1995a) There are a number of geologic units present at IHSS 209 and the other surface disturbances including artificial fill landslide deposits Rocky Flats Alluvium colluvium and the Arapahoe/Laramie Formations Descriptions of these units as well as an IHSS specific description of the alluvial thickness are provided in the following paragraphs

IHSS 209 The surficial geology of IHSS 209 consists primarily of Rocky Flats Alluvium with three small pockets of artificial fill (Figure 3 10) The surface materials surrounding the IHSS have been identified as landslide deposits (EG&G 1995a) (Figure 3 10)

Artificial fill landslide deposits colluvium and the Rocky Flats Alluvium present in IHSS 209 have been described in previous sections The only subsurface data available are from borehole 41191 (Figure 3 36) These data indicate that the alluvial material is approximately 31 feet thick on top of this knoll Also based on data from borehole 41191 the bedrock underlying IHSS 209 consists of claystone This

claystone most likely belongs to the Arapahoe Formation as inferred from Plate 2 1 of the Geologic Characterization Report (EG&G 1995a) (Figure 3 3) A discussion of the Arapahoe Formation is provided in Section 3 6

Surface Disturbance West of IHSS 209 The surficial geology of the Surface Disturbance West of IHSS 209 has recently been mapped According to the Surficial Geologic Map of the Rocky Flats Environmental Technology Site and Vicinity (EG&G 1995a) the area is covered with landslide deposits (Figure 3 10) A description of landslide deposits was previously provided in Section 3 6 According to data from borehole 57693 there is no alluvial material at this location The geological material encountered in borehole 57693 consisted of highly to slightly weathered claystone to a depth of 6 feet Figure 3-4 (Plate 2 1 EG&G 1995a) shows that both the Arapahoe and Laramie Formations underlie this IHSS Descriptions of these two formations were presented in Section 3 6

Surface Disturbance South of the Ash Pits Surficial geology of the Surface Disturbance South of the Ash Pits consists mostly of Rocky Flats Alluvium with about one third of the area covered with colluvium (Figure 3 9) The surface materials surrounding the IHSS have been identified as landslide deposits (EG&G 1995a) (Figure 3 9) Summary descriptions of these landslide deposits were provided in Section 3 6

Based on borehole data, the Rocky Flats Alluvium on top of the knoll is approximately 30 feet thick and, off to the side of the knoll the thickness decreases to approximately 24 feet in borehole 57893 (Figure 3 39) The Rocky Flats Alluvium consisted predominantly of a gravelly sand with some interbedded silty or clayey sands (Figure 3 39)

Bedrock data from the IHSS are from boreholes 57793 and 57893 (borehole 57993 did not reach bedrock) The bedrock encountered in borehole 57793 consisted of claystone However the bedrock encountered in borehole 57893 consisted of clayey sandstone at 24 4 feet and grading to a sandstone at 30 4 feet Two other boreholes that are nearest to the surface disturbance include borehole 41391 and well 0590/borehole 590 and borehole 5386 Borehole 41391 and well 0590 encountered a claystone and borehole 5386 was not logged Borehole 41391 southeast of the IHSS encountered 38 feet of rocky Flats Alluvium four feet silty claystone 4 5 feet of silty sandstone to clayey siltstone claystone to a depth of 130 feet, 0 5 feet of siltstone 14 feet of claystone one foot of silty sandstone then claystone to a total depth of 202 feet.

Three boreholes located in the area of the Surface Disturbance South of the Ash Pits encountered sandstone. Two sandstone units were encountered in borehole B402189 at depths of 6 feet and 20.5 feet below top of bedrock. Because each of these three boreholes encountered sandstone at depths of 24.4, 28, and 33 feet, it may be possible that they have penetrated the same lithologic unit. According to Plate 5.9 of the Geologic Characterization Report (EG&G 1995a), these boreholes are all interpreted to have penetrated the Arapahoe No. 1 sandstone. The thickness of these sandstones ranges from 5.5 (borehole 57893) to 16 feet (second sandstone encountered in borehole B402189). Both boreholes B402189 and B405889 encountered a sandstone that was 12 feet thick.

3.8.4.2 Hydrogeology

The hydrogeology of IHSS 209 and the other surface disturbances on the south side of Woman Creek were not characterized for hydrogeology with the installation of wells during RFI/RI activities. Generally, groundwater flows into these areas from areas upgradient and then downslope toward the north to the apex of Woman Creek. All are located on or at the edge of the Rocky Flats Alluvium pediment. The UHSU water table south of Woman Creek was not included in the potentiometric map of OU 5 (Figure 5.15) but is sufficiently described and presented in the Geological and Hydrogeologic Characterization Reports (EG&G 1995a and b).

IHSS 209 was dry when investigated during the summer of 1992. It is located on the Rocky Flats Alluvium pediment, and contains small areas of artificial fill (Figure 3.10). Recharge is from infiltration of precipitation. Since the site is on the drainage divide between Woman Creek and Smart Ditch, groundwater is expected to flow north, east, and south toward both drainage basins. No seeps were observed in this area (EG&G 1994a).

The Surface Disturbance West of IHSS 209 occurs on the top of the slope adjacent to the Rocky Flats Alluvium pediment outcrop within landslide material (EG&G 1992e). Bedrock is essentially at the surface, and the area was dry when drilled during the summer months of 1992. The area is within the Woman Creek drainage basin, and when saturated conditions exist, groundwater flows to the east and north. Recharge is from infiltration of precipitation. Discharge is through evapotranspiration and downgradient groundwater and surface water flow. Figure 3.15 shows the location of an ephemeral seep present to the west of the IHSS (EG&G 1994a).

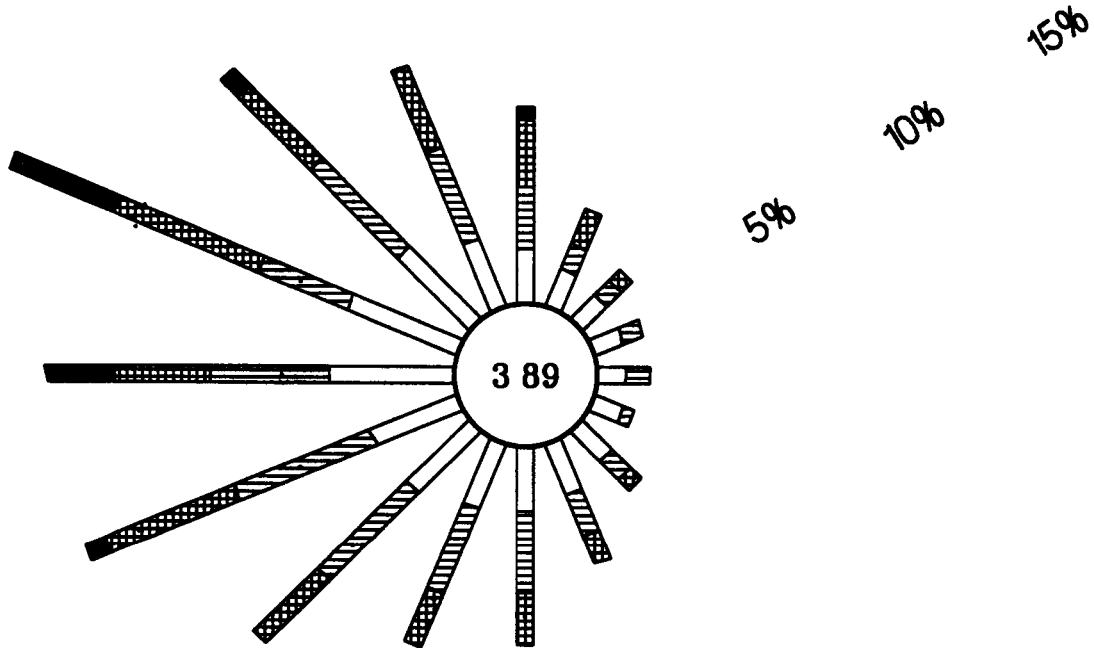
The Surface Disturbance South of the Ash Pits is located on the Rocky Flats Alluvium pediment with some colluvium (EG&G 1992e). It lies on a minor groundwater divide within the Woman Creek drainage basin. Groundwater recharge is primarily from precipitation infiltration. A small tributary of Woman Creek bounds the southeastern edge of the disturbance, and a number of perennial and ephemeral seeps bound the northwestern edge (EG&G 1994a). Groundwater discharges to the seeps and the tributary to the southeast, and flows to the north through unconsolidated surficial materials toward Woman Creek. Discharge also occurs through evapotranspiration.

NIGHT 1991

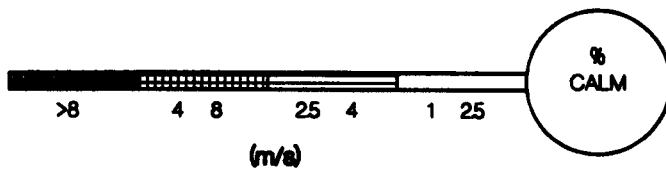
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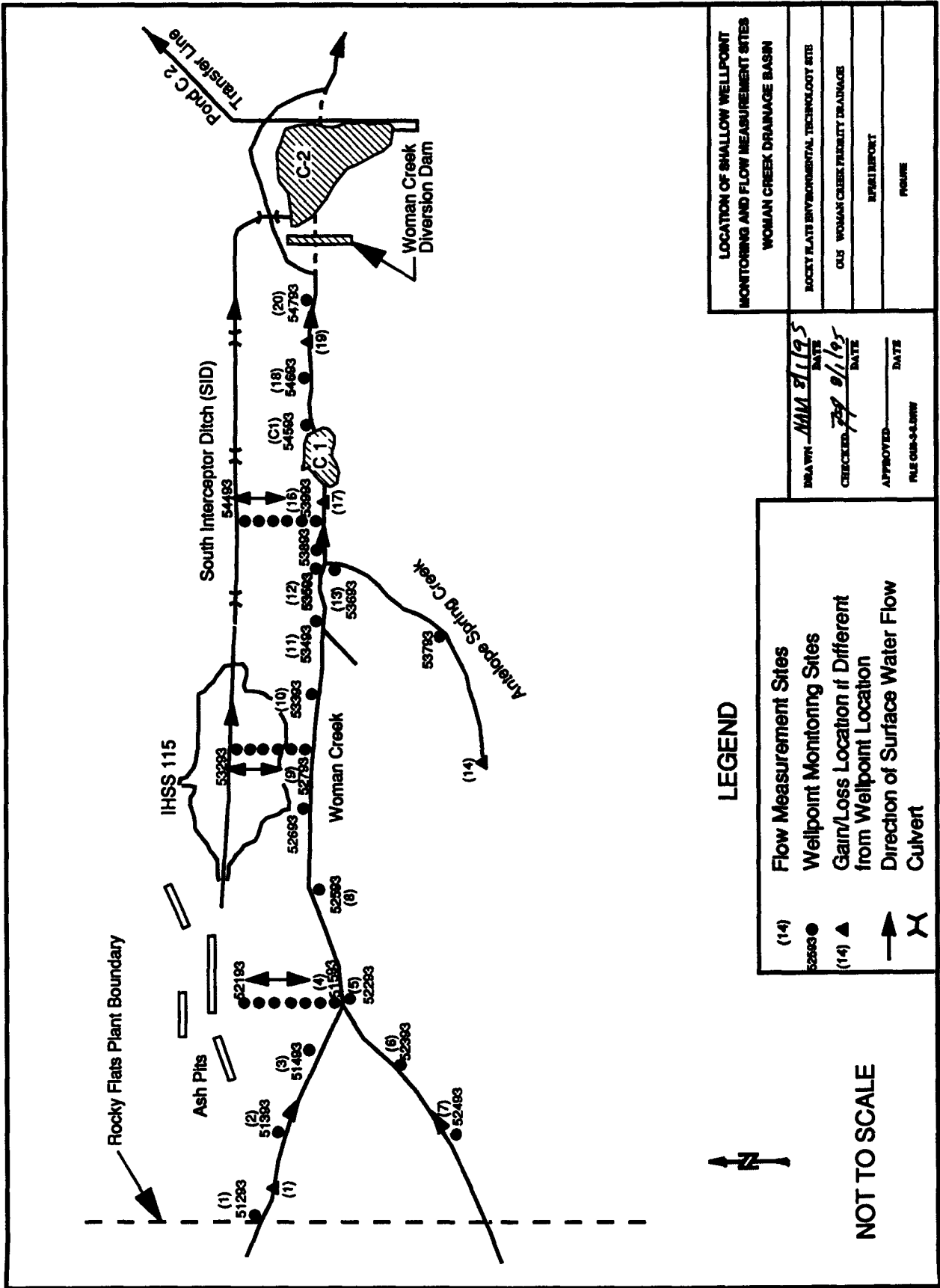


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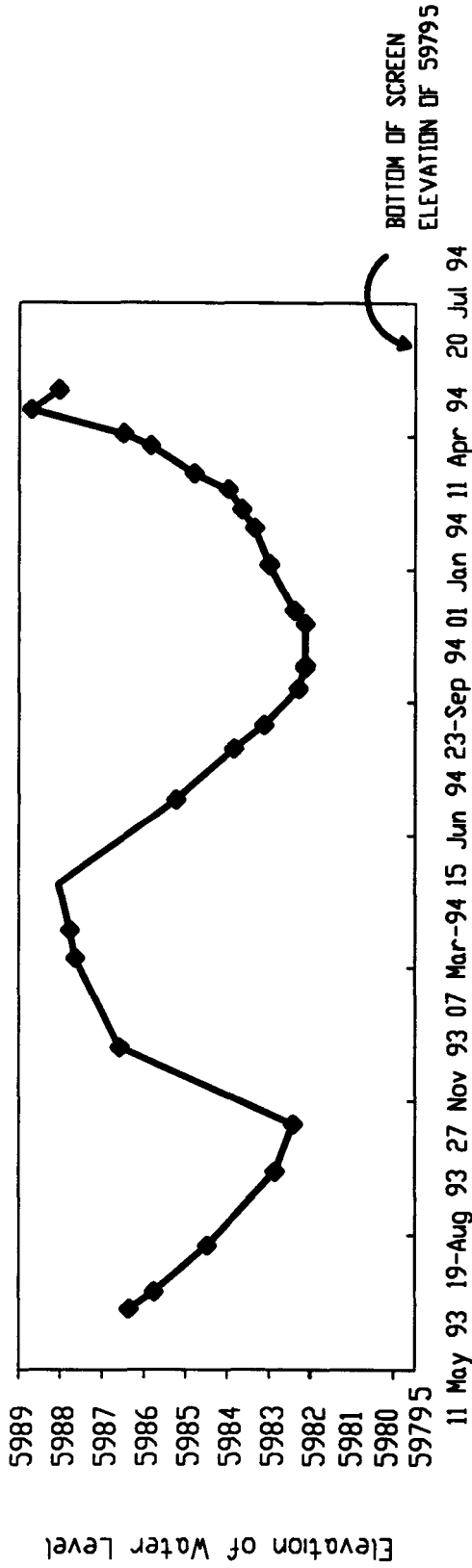


Source EG&G Rocky Flats n d Crocker pers comm 1993

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Checked	<u>7/2/95</u>	Date
Approved		Date
FILE OUS-3 2.DWG		
WIND ROSE FOR THE ROCKY FLATS PLANT (NIGHT 1991)		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUS-WOMAN CREEK PRIORITY DRAINAGE		
RFI/RI REPORT		
FIGURE 3-2		

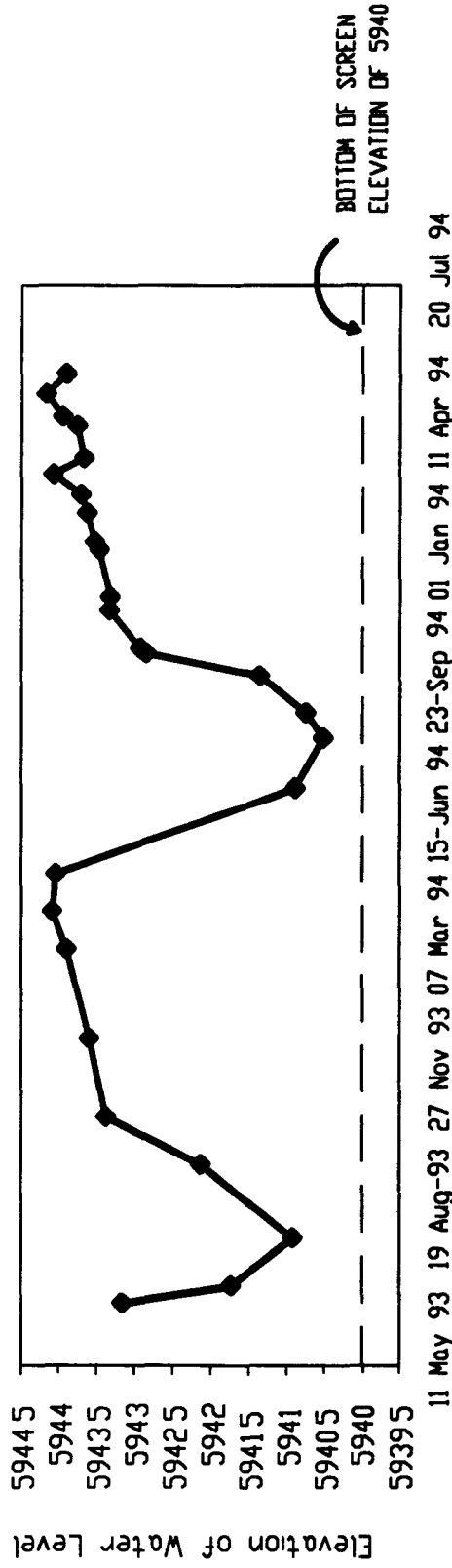


WELL 59493 - HYDROGRAPH



Date of Measurement

WELL 59593 - HYDROGRAPH

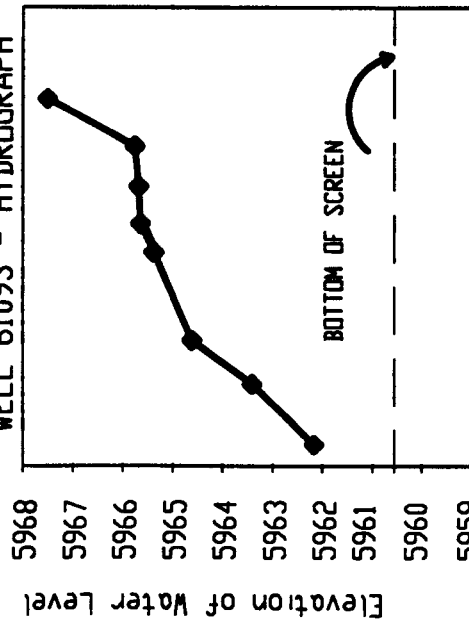


Date of Measurement

HYDROGRAPHS OF WELLS 59493 & 59593
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OU5 - WOMAN CREEK PRIORITY DRAINAGE
RPT/RI REPORT
FIGURE 3-22

Drawn	NAM	8/9/95
Checked	RMN	8/9/95
Approved		
FILE	OU5 3 22 DWG	

WELL 61093 - HYDROGRAPH

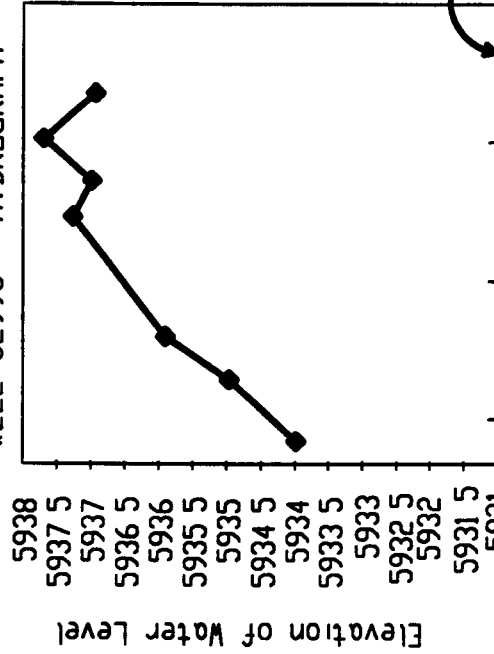


ELEVATION OF 5960.6

23 Sep 94 01 Jan 95 11-Apr 95 20-Jul-95

Date of Measurement

WELL 52993 - HYDROGRAPH



BOTTOM OF SCREEN
ELEVATION OF 5931

23 Sep-94 01 Jan-95 11-Apr 95 20 Jul 95

Date of Measurement

HYDROGRAPHS OF WELLS 52993 & 61093

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 3-23

Drawn NAAH 9/22/95

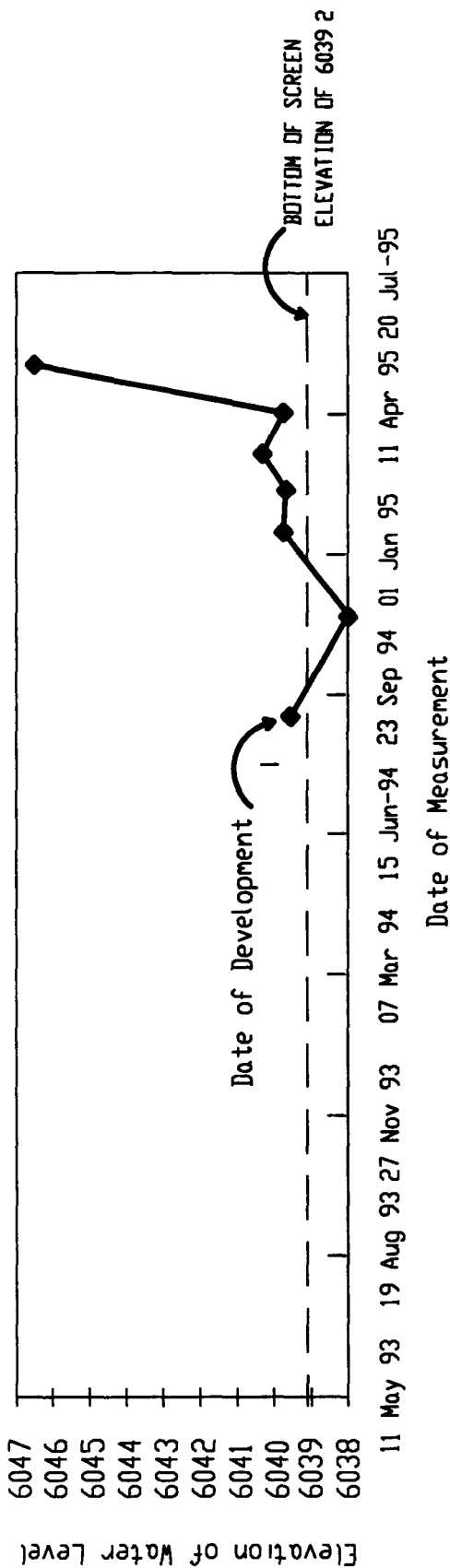
Checked FEP 9/28/95

Approved M.W. 9/29/95

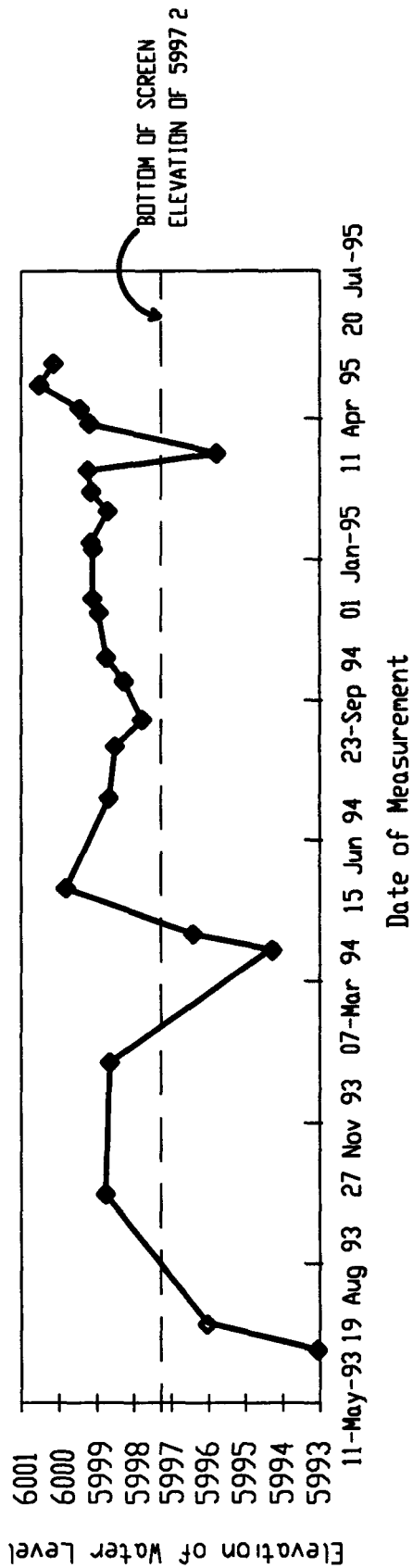
FILE OU5 3 23.DWG

Source of Data RFEDS

WELL 62593 - HYDROGRAPH



WELL 63093 - HYDROGRAPH



HYDROGRAPHS OF WELLS 62593 & 63093

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OJUS - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 3-36

Drawn NAM Date 10/2/95
 Checked TEP Date 10/2/95
 Approved MRW Date 10/10/95

FILE OJUS 3-36 DWG

Source of Data RFEDS

Table 3-1
Soil Units Within the OU 5 Area

Series	Family	Phase	Minimum Maximum Slope (%)	Location (to hillside ridge etc.)	Infiltration Rate	Permeability	Water Capacity	Water Erosion Hazard	Shrink Swell Potential
Denver Kutch Midway	Torretic Argiustolls	clay loam	9-25	hillsides ridge	slow	slow	high/low	severe	high
Flatirons	Aridic Paleustolls	very cobbly sandy loam	0-3	ridges	slow	slow	low	slight	moderate
Denver	Torretic Argiustolls	clay loam	5-9	hillside	slow	slow	high	severe	high
Nederland	Aridic Argiustolls	very cobbly sandy loam	15-50	ridges hillsides	moderate	moderate	moderate	severe	low
Haverson	Ustic Torrifluvents	loam	0-3	flood plain	slow	moderate/slow	high	slight	low
Leyden Pnmen Standley	Aridic Argiustolls	cobbly clay loam	15-50	hillsides	slow	slow	low/high	severe	moderate to high

Source Department of Agriculture (1980)

4 0 NATURE AND EXTENT OF CONTAMINATION

The nature and extent of COCs within OU 5 were evaluated for various media, including surface soil subsurface soil groundwater surface water seep water pond sediment seep sediment and stream sediment. These evaluations were performed in accordance with Section 3.4.1.3 of *Guidance for Conducting Remedial Investigations and Feasibility Studies Under CERCLA* (EPA 1988c). Section 4.1 presents a discussion of data used in the evaluation of the nature and extent of contamination, as well as an assessment of the quality of those data. Section 4.2 presents a summary of the comparison of these data to background values. The distributions of those analytes identified as COCs—based on the methodology described in Section 4.2—are discussed in Section 4.3. Section 4.4 presents a summary of the contaminant assessment.

4 1 DESCRIPTION OF DATA USED FOR CONTAMINANT ASSESSMENT

4 1 1 Description of Data

Data used for preparation of this report were collected during the OU 5 Phase I field program, which was conducted in two stages. The first stage began in August 1992 and continued through November 1993. The second stage began in August 1994, after TM15 was finalized, and ended in June 1995. First stage data, which were used for identifying constituents as COC, are documented in TM15 (DOE 1994a). Data from both stages have been used to evaluate the nature and extent of contamination. All data were obtained from the Rocky Flats Environmental Database System (RFEDS).

Data obtained from RFEDS were carefully reviewed, and unusable data were removed from the working data sets prior to being used in any analysis. These steps are documented in Appendix A of DOE (1995a).

4 1 2 Evaluation of Data Usability

The OU 5 Work Plan (DOE 1992a) established the data quality objectives (DQOs) for each analyte group and medium sampled. DQOs are expressed in quantitative and qualitative terms of precision, accuracy, representativeness, completeness, and comparability. These parameters are routinely referred to as the PARCC parameters.

Appendix O presents a data quality and usability summary for the OU 5 RFI/RI. The data usability summary evaluates how data quality supports or limits the achievement of the prescribed DQOs and how it affects data usability for the RFI/RI. The discussion presented in Appendix O indicates that the data collected for the OU 5 RFI/RI generally meet or exceed the DQOs established in the OU 5 Work Plan (DOE 1992a).

4.2 COMPARISON TO THE SITE BACKGROUND DATA

Data collected prior to implementation of TM15 (DOE 1994a) were compared quantitatively to background data. As described in TM15, constituents found in samples of surface soil, subsurface soil, groundwater, surface water, and stream sediments were compared to the corresponding UTL_{99/99} as provided in the 1993 Background Geochemical Characterization Report (DOE 1993a). For those analytes where a UTL_{99/99} was not provided by the Background Geochemical Characterization Report, the maximum background concentration was used for this comparison. Because the background concentrations of organic compounds are assumed to be zero, therefore, any detected organic compound was considered to be an indication of possible contamination. The data documented in TM15 provided initial indications of contamination based on data from field investigations completed in August 1993 and groundwater samples collected through November 1993.

In Section 2.0, Tables 2.7 through 2.9 show a comparison of concentrations from the combined stage one and stage two data sets to both background data and the OU 5 data collected prior to implementation of TM15. These comparisons show the statistical effects to the data set after integrating the data collected during the implementation of TM15.

The COCs described in TM11 (DOE 1995a) were derived from the same data set reported in TM15 (DOE 1994a). The COCs were selected based on the results of statistical comparison to background concentrations, assessments of toxicity, evaluation of detection frequencies, and review of the spatial/temporal distribution of analyte concentrations. The resulting COCs are listed in Table 6.25. During selection of COCs, the concentrations of each analyte were compared to those of the same analyte in the corresponding background medium. However, data for pond sediment in OU 5 were compared to background data for seep sediments due to the lack of background pond data, and because flow conditions for ponds and seeps are similar (both have relatively long residence time) (DOE 1995a). Background comparisons for inorganic analytes were performed according to the procedures given in the Guidance Document, Statistical Comparisons of Site Background Data in Support of RFI/RI Investigations (EG&G 1994b), which was primarily based on the methodology proposed by

Gilbert (1993) The formal statistical tests include the Gehan test, Slippage test, Quantile test, and t test. Comparisons of the analytical results to the background UTL_{99/99} for each analyte in each medium were performed to ensure that isolated areas of contamination (i.e., hot spots) were not overlooked. Appendix A of the COC TM11 (DOE 1995a) presents a detailed description of the conditions for applying each of these tests.

4.3 THE EXTENT OF COCs IN AND AROUND OU 5 IHSSs

The nature of the wastes in the OU 5 IHSSs has been discussed in Section 1.0 and in TM15 (DOE 1994a) for the field investigation outlined in the OU 5 Work Plan (DOE 1992a). Section 6.2 discusses the identification of COCs for each medium. These COCs are summarized in Table 6.25 and listed below.

- Surface Soils: Aroclor 1254, benzo(a)anthracene, benzo(a)pyrene, benzo(b)fluoranthene, copper, dibenzo(a,h)anthracene, fluoranthene, indeno(1,2,3-cd)pyrene, mercury, pyrene, silver, uranium 233/234, uranium 235, and uranium 238.
- Subsurface Soils: antimony, Aroclor 1254, benzo(a)anthracene, benzo(a)pyrene, benzo(b)fluoranthene, beryllium, cadmium, copper, molybdenum, nickel, silver, uranium 233/234, uranium 235, and uranium 238.
- Groundwater: aluminum, barium, beryllium, manganese, vanadium, americium 241, plutonium 239/240, radium 226, uranium 233/234, uranium 235, and uranium 238.
- Surface Water: barium, lithium, strontium, americium 24, uranium 233/234, and uranium 238.
- Seep Water: acetone, 1,1-dichloroethene (1,1-DCE), 1,2-dichloroethene (1,2-DCE), PCE, and TCE.
- Pond Sediment: mercury, zinc, americium 241, plutonium 239/240, uranium 233/234, uranium 235, and uranium 238.
- Seep Sediment: antimony, beryllium, zinc, uranium 233/234, uranium 235, and uranium 238.
- Stream Sediment: copper, mercury, zinc, americium 241, and plutonium 239/240.

The extent and variation of concentration of the COCs are graphically displayed as symbols on Figures 4.1A through 4.12. Data used to develop these figures represent a combined data set that includes the pre-TM15 data and data collected during implementation of activities specified in TM15 (DOE 1994a).

For metal and radionuclide COCs, the following concentration intervals (levels) were used to characterize and display concentrations:

- Level 5 concentrations/activities that are less than or equal to the arithmetic mean background concentration/activity
- Level 4 concentrations/activities that exceed the background mean but are less than or equal to the background mean plus one standard deviation
- Level 3 concentrations/activities that exceed the background mean plus one standard deviation but are less than or equal to the background mean plus two standard deviations
- Level 2 concentrations/activities that exceed the background mean plus two standard deviations but are less than or equal to the background mean plus three standard deviations and
- Level 1 concentrations/activities that exceed the background mean plus three standard deviations

As part of the COC selection process as discussed in the COCTM (DOE 1995a) and in Chapter 6 0 concentrations/activities were compared to the corresponding background UTLs_{99/99}. The UTL_{99/99} in most cases is comparable to the background mean plus three standard deviations. Therefore four of the five symbols on Figures 4 1 through 4 12 indicate concentrations that are not above the UTLs_{99/99} for metals and radionuclides.

For organic COCs the following concentration intervals (levels) were used to characterize concentrations

- Level 4 concentrations that were detected at levels less than the reporting limit
- Level 3 concentrations that exceed the reporting limit but are less than or equal to ten times the reporting limit
- Level 2 concentrations that exceed ten times the reporting limit but are less than or equal to 100 times the reporting limit and
- Level 1 concentrations that exceed 100 times the reporting limit.

The symbol at each sample location in Figures 4 1A through 4 12 indicates the greatest concentration level for one or more COCs. The symbols show the general distribution of the COCs and the general deviation from background mean concentrations. Boxes associated with the symbols list the individual COCs that show concentrations greater than the background mean. The upper panel in each box corresponds to the level 1 concentration intervals described above; that is, the box contains a list of inorganic COCs found at concentrations/activities exceeding three standard deviations above the background mean. For organic chemicals the box contains a list of those compounds found at concentrations exceeding 100 times the reporting limit. The lower panel lists COCs in the level 2 concentration interval. All metal and radionuclide COCs not listed anywhere in the box are less than two standard deviations above the background mean. All organic COCs not listed

anywhere in the box were found only at levels less than ten times the reporting limit. Tables 4 1 through 4 11 present data used to create Figures 4 1A through 4 12

The following subsections describe the nature and extent of contamination associated with each IHSS in OU 5. However, all surface water and sediment data are presented under IHSS 142 in order to be consistent with the AOCs presented in Section 6 0 of this RFI/RI report.

4 3 1 IHSS 115 (Original Landfill) and IHSS 196 (Filter Backwash Pond)

4 3 1 1 Surface Soil

Data used to determine the extent of metal COCs for IHSS 115/196 surface soil (copper, mercury, and silver) are presented in Table 4 1. Figures 4 1A, B, C, D show the extent of these COCs. The central area of IHSS 115 contains the greatest number of locations that have COCs at level 1 concentrations. Copper, mercury, and silver are all found at level 1 concentrations in this area. Construction of the outfall pipe (Section 1 2 2 1) and slumping of surficial materials may have brought contaminated landfill material to the surface in the central area of IHSS 115. Three sampling locations (Figure 4 1C) are just south of this area and outside the IHSS boundary. Of these, location SS509693 is the only one that has a COC concentration at level 1 (mercury: 0.26 mg/kg).

Data used to plot the extent of radionuclide COCs for surface soil (the three isotopes of uranium) are presented in Table 4 2. These data are illustrated on Figures 4 2A, B, C, D. The center of IHSS 115 contains the greatest number of locations that have radionuclide COCs that exceed the background mean plus three standard deviations (level 1). All three uranium isotopes are found in the level 1 concentration interval there. As indicated above, construction of the outfall pipe and slumping of surficial materials may have brought contaminated landfill material to the surface in this area. Three locations (SS509693, SS510293, and SS505893, Figure 4 2D) containing uranium isotopes at level 1 concentrations are located south of this area, just outside of the IHSS boundary.

Data used to plot the extent of organic COCs for surface soil are presented in Table 4 3. These data are shown on Figures 4 3A, B, C. All of the locations where organic COCs were detected are in the IHSS 115/196 area. Locations of detected organic COCs correspond with the location of the soil gas anomalies (Section 2 2 1 2). The highest concentrations were detected at location SS510593 (Figure 4 3C) where all of the organic COCs were

found at concentrations greater than 10 times the reporting limit. No concentrations greater than the reporting limit were found outside the boundary of IHSS 115 although two locations immediately south of IHSS 115 showed detected concentrations that were greater than the instrument detection limit but less than the contract required detection limit.

4.3.1.2 Subsurface Soil

Data used to plot the extent of metal COCs for IHSS 115/196 subsurface soil (antimony, beryllium, cadmium, copper, molybdenum, nickel, and silver) are presented in Table 4.4. Figures 4-4A, B, C, D show the general extent of these COCs. The location symbols in this figure show the maximum concentration level of any metal COC in each borehole without regard to the depth sampled. As discussed previously, the boxes show metal COCs that were detected at level 1 and level 2 concentrations. A metal may appear in both panels of a box because of its depth-related variability in concentration.

In IHSS 115, copper and nickel were found at several locations in level 1 concentrations. Antimony, cadmium, molybdenum, and silver were also detected at this concentration level. All but one of these samples with metals in the highest concentration interval were from depths of less than 13 feet in an area where waste was identified in boreholes. Moreover, with only one exception, those boreholes in which waste was not identified contained lower concentrations of metals. The exception was the nickel concentration at location 63193 (Figure 4-4C) where the composited interval from 12 to 20 ft contained 84.9 mg/kg nickel. However, this concentration only marginally exceeds the background mean plus three standard deviations. Although waste was not identified in this borehole, the borehole is in an area where landfill materials were relocated during construction of the SID. Cadmium, copper, and nickel were also detected at level 2 concentrations within the area where boreholes did not contain the waste material. One borehole (57994, Figure 4-4C) south of the central area of the landfill and the IHSS boundary contains copper and nickel in the upper six feet at level 2 concentrations. These observations indicate that the greatest concentrations of metal COCs are within IHSS 115 and have about the same vertical distribution as the wastes. Downslope from the IHSS, metal COCs were detected at lower concentrations.

Data used to plot the extent of radionuclide COCs for subsurface soil (the three isotopes of uranium) are presented in Table 4.5. These data are summarized on Figure 4.5A, B.

The distribution of radionuclides in subsurface soil at IHSS 115/196 is similar to that of metal COCs. Samples containing radionuclide COCs at level 1 and level 2 activities were collected within the IHSS boundary from the upper 13 feet of subsurface soil (Table 4-5). An exception to this observation on the vertical distribution is for a sample collected from below 19.5 feet in borehole 58693 (Figure 4-5D) that contained uranium 238 at 1.7 pCi/g (level 2). The radionuclides tend to be associated with waste material, and more than 15 ft of waste was identified in borehole 58693. Waste material was identified in all IHSS 115/196 boreholes with level 1 and level 2 activities, with the exception of samples BH50087AS from borehole 50692 and BH50603AS from borehole 61093 (Figure 4-5D). These two boreholes contained no identified waste. Borehole 50692 is located in the surface disturbance at the east end of IHSS 115. Sample BH50087AS was collected from a composited interval from 0 to 6 feet and may therefore be influenced by surface soil contamination. Borehole 61093 is located in the central portion of the landfill within a slump that is surrounded by waste. Therefore, the radionuclides in the sample from 61093 are likely to be associated with waste. The only borehole outside the IHSS boundary that contained a radionuclide COC at an activity exceeding the background mean plus two standard deviations was 61293 (Figure 4-5C), where uranium 238 was detected with an activity of 0.3395 pCi/g in the sample collected from 6 to 10.6 feet deep. These observations indicate that elevated activities of radionuclide COCs are essentially contained within the waste material area, although the occurrence of uranium 325 at an elevated concentration in borehole 61293 is unexplained.

Data used to plot the extent of organic COCs in subsurface soil are presented in Table 4-6. These data are summarized on Figures 4-6A-B. The greatest number of locations that have organic COCs are located in the vicinity of IHSS 196, where the thickest section of waste was penetrated. Organic COCs were also detected at the soil gas anomaly in the central portion of IHSS 115 (Section 2.2.1.2.2). The two level 3 concentrations of COCs at locations 56694 and 57594 (Figure 4-6A) outside of IHSS 115 are composited samples of drilling mud from deep boreholes. These samples contained benzo(a)pyrene. Evaluation of the spatial distribution of these COC concentrations indicates that organic COCs are restricted to areas within the waste material of IHSS 115/196.

4.3.1.3 Groundwater

Data used to plot the extent of metal COCs (aluminum, barium, beryllium, manganese, and vanadium) dissolved in IHSS 115/196 groundwater are presented in Table 4-7. These data are summarized on Figure 4-7A-B. The extent of dissolved metals, rather than total metals, is presented to provide a meaningful interpretation of groundwater chemistry (EG&G 1995c). The concentrations of total metals includes those metals contained in or absorbed onto

suspended sediments which may be affected by factors unrelated to the extent or degree of groundwater contamination. Dissolved manganese and barium are present at level 1 and level 2 concentrations within the landfill. Only two sampling locations downgradient from IHSS 115 (61293 and 58094, Figure 4.7A) yielded samples with concentrations of dissolved metals at level 1 or level 2. Dissolved barium and manganese were detected at levels 1 and 2 in the sample obtained in January 1995 from monitoring well 61293 (Figure 4.7A). In addition, dissolved manganese was detected at a level 3 concentration at location 59594 upgradient from the landfill (Figure 4.7A). These observations indicate that manganese and barium are the dominant metal COCs associated with IHSS 115, although their distribution does not seem to be well correlated with waste materials.

Data used to plot radionuclide COCs (americium 241, plutonium 239/240, radium 226, and the three isotopes of uranium) in groundwater are presented in Table 4.8. These data are summarized on Figure 4.8A. Dissolved radium 226 was detected with level 1 or level 2 activities at three locations in IHSS 115. No level 1 or level 2 activities of dissolved radium 226 have been detected downgradient of IHSS 115. Radium 226 seems to be the only radionuclide present at elevated activities in the groundwater of IHSS 115.

4.3.1.4 Surface Water

Distribution of COCs in IHSS 115/196 surface water is discussed in Section 4.3.3.1.

4.3.1.5 Seep Water

Seep water was only sampled at two locations (62793 and 62893) in IHSS 115/196. Only location 62893 at the northeast edge of the landfill contained any of the COCs. All detected values were trace detections of organic compounds.

4.3.1.6 Seep Sediments

Seep sediment samples were only collected at the two IHSS 115/196 locations where seeps occur (Figure 2.12). TM15 (DOE 1994a) contains a detailed discussion of results for these samples. The sediment sample collected adjacent to seep water sampling location 62893 contained antimony at a concentration exceeding the UTL_{99/99}. Neither of the two sediment samples contained radionuclide COCs exceeding the corresponding UTLs.

4 3 2 IHSS 133 (Ash Pits)

4 3 2 1 Surface Soil

Data used to plot metal COCs in IHSS 133 surface soil (copper mercury and silver) are presented in Table 4 1 Figure 4 1D summarizes the extent of these COCs Two locations (SS513693 and SS514493 Figure 4 1A) contain copper at level 2 concentrations One location (SS513893) contains copper at a level 1 concentration (26 8 mg/kg) but its concentration is only 0 73 mg/kg above the base of the level 1 concentration interval Metal COCs in surface soils are not greatly elevated in the IHSS 133 area

Data used to plot radionuclide COCs in surface soil (the three isotopes of uranium) are presented in Table 4 2 Figure 4 2D summarizes the extent of these COCs Fifteen surface soil sampling locations contain radionuclide COCs at level 1 activities Results from one location (SS515493 Figure 4 2D) are the only ones that exceed the UTLs_{99/99} listed in TM11 (DOE 1995a) This location was sampled at the position of an elevated HPGe measurement (Section 2 2 2 3) With the exception of this sample data indicate that these constituents are fairly evenly distributed throughout the surface soil in the vicinity of IHSS 133

No organic COCs were detected in surface soils in the IHSS 133 area

4 3 2 2 Subsurface Soil

Data used to plot metal COCs in IHSS 133 subsurface soil (antimony beryllium cadmium copper molybdenum nickel and silver) are presented in Table 4 4 These data are summarized on Figure 4-4D which shows the location of the boreholes Most boreholes that contain metals at level 1 concentrations contain waste materials as may be seen by inspection of borehole logs in Appendix B or they are near locations with waste materials in the subsurface Exceptions are boreholes 55193 58793 59093 and 55294 (Figure 4-4C) The presence of level 1 concentrations of metals at these locations is unexplained In borehole 55193 the concentration of copper exceeds level 1 in a sample taken at 6 to 8 feet in claystone just below the top of bedrock Borehole 58793 is near the southern trench of IHSS 133 2 where no waste was found in the subsurface This borehole contained a level 1 concentration of antimony in gravelly sand just above bedrock at 18 to 24 feet Borehole 59093 contained antimony at a level 1 concentration in a sample from 0 to 6 feet in clayey sand Borehole 55294 is located at the position designated as TDEM 1 approximately 25 feet north of IHSS 133 6 A sample from gravelly sand at 12 to

15 to 2 feet immediately above bedrock contained a level 1 concentration of nickel. Except for these four unexplained occurrences, it appears that the lateral extent of level 1 concentrations of COC metal detects is consistent with the extent of waste materials.

The vertical extent of explained occurrences of level 1 concentrations in IHSS 133 are consistent with the depth of waste materials. However, cadmium and copper were detected in borehole 56094 at 18 to 22 feet. This borehole contained waste material, but the depth of the waste was not recorded due to radioactivity hazard. A sample from borehole 58093 contained cadmium at a level 1 concentration from a depth of 10 to 12 feet, which was in the top of bedrock immediately beneath a waste interval. All other occurrences of level 1 metals concentrations were from sample intervals that extended to shallower depths, consistent with known depths of waste materials.

Data used to plot radionuclide COCs in subsurface soil are presented in Table 4.5 and are summarized on Figure 4.5D. These data indicate lateral and vertical extent similar to that of the metal COCs. One difference is the level 1 activity of uranium 235 detected in borehole 64493, which lies within the magnetic anomaly west of IHSS 133 (Section 2.2.2.2). The presence of a level 1 activity of uranium 235 at this location is unexplained.

Data used to plot organic COCs in subsurface soil are summarized in Table 4.6. These data are shown on Figure 4.6A. No organic COCs were detected at IHSS 133, although only a very limited number of subsurface soil samples were collected for analysis of organic chemicals at IHSS 133.

4.3.2.3 Groundwater

Data used to plot metal COCs (aluminum, barium, beryllium, manganese, and vanadium) dissolved in IHSS 133 groundwater are presented in Table 4.7 and are summarized on Figure 4.7A. As shown on Figure 4.7A, only manganese was detected at level 1 concentrations in the IHSS 133 area. Wells 58793 and 63793 are downgradient from the IHSS 133 ash pit. If the manganese in these wells is from waste in the ash pit to the north, sampling data are insufficient to define the downgradient and lateral extent of the possible plume, because no monitoring wells are located in downgradient and lateral positions; however, a plume may not exist. Manganese in the IHSS 133 area is not closely associated with subsurface occurrences of waste, and its occurrence at level 1 concentrations is unexplained. It is noteworthy that manganese staining is described in samples from several

boreholes in OU 5 including those in the IHSS 133 area, and manganese will coprecipitate with barium (Hem 1985). Results throughout OU 5 as summarized in Figure 4.7A suggest that barium is associated with manganese.

Data used to plot radionuclide COCs dissolved in groundwater are presented in Table 4.8 and are summarized on Figure 4.8A. No level 1 activities of radionuclides were detected in the IHSS 133 area. Radium was detected at a level 2 activity in well 58793 and may come from the IHSS 133.2 ash pit to the north.

4.3.2.4 Surface Water

Distribution of COCs in IHSS 133 surface water is discussed in Section 4.3.3.1.

4.3.2.5 Seep Water

Seep water was only sampled at two locations (wellpoints 62593 and 62693) in IHSS 133 (Figure 2.12). Neither location contained any of the COCs for seep water. TM15 (DOE 1994a) contains a detailed discussion of results of these samples.

4.3.2.6 Seep Sediments

Seep sediment samples were only sampled at the two IHSS 133 seep locations where seeps occur (Figure 2.12). TM15 (DOE 1994a) contains a detailed discussion of results of these samples. Both locations contained zinc at a concentration exceeding the background $UTL_{99/99}$. Antimony exceeded the background $UTL_{99/99}$ in the sample from the seep near wellpoint 62693 (Figure 2.12). The sample from the sampling location near wellpoint 62593 (Figure 2.12) contained uranium 238 exceeding the background $UTL_{99/99}$.

4.3.2.7 Stream Sediments

Distribution of COCs in IHSS 133 stream sediments is discussed in Section 4.3.3.3.

4 3 3 IHSS 142 (C Series Ponds)

4 3 3 1 Surface Water

No water samples were collected from the C Series ponds as part of the OU 5 RFI/RI. Appendix A presents a discussion of historical surface water data for the ponds.

Figure 4 9 shows that metal COCs for surface water (barium, lithium, and strontium) were not detected within OU 5 at concentrations exceeding the background mean; however, statistical analyses indicated that the distribution of these metals was sufficiently different from background to warrant their inclusion as COCs (DOE 1995a).

Data used to plot radionuclide COCs (americium 241, uranium 233/234, and uranium 238) in surface water are presented in Table 4 9 and are summarized on Figure 4 10. Americium 241 and uranium 238 were detected at a level 1 activities in the SID at SW027 north of Pond C 2.

The sample from location SW50293 (Figure 4 10) flowing seep water contained americium 241, uranium 233/234, and uranium 238 at level 1 activities. Americium 241, uranium 233/234, and uranium 238 were also detected at level 1 activities in the SID (SW507).

4 3 3 2 Pond Sediments

The nature and extent of COCs in C Series pond sediments are discussed in Appendix A and TM15 (DOE 1994a). A summary for each pond is presented below.

IHSS 142.10 (Pond C 1) Mercury was detected in samples from the three locations (inlet, mid point, and deepest) at concentrations exceeding the background $UTL_{99/99}$. One sample had an activity of uranium 238 that exceeded the background $UTL_{99/99}$. This sample was obtained from the midpoint of Pond C 1.

IHSS 142.11 (Pond C 2) Zinc was detected at concentrations exceeding the background $UTL_{99/99}$ in the samples from the midpoint and the deepest portion of Pond C 2. Radionuclide COCs were not detected at activities exceeding the background $UTL_{99/99}$.

4 3 3 3 Stream Sediments

Data used to plot metal COCs (copper mercury and zinc) in stream sediments from Woman Creek and the SID are presented in Table 4 10 These data are summarized on Figure 4 11 No metal COCs were detected at level 1 or level 2 concentrations for samples collected along Woman Creek or its tributaries

Copper mercury and zinc were detected at level 1 concentrations in the sediment sample from the location in the SID at the southeast corner of IHSS 115

Data used to plot radionuclide COCs (americium 241 and plutonium 239/240) in stream sediments are presented in Table 4 11 and are summarized on Figure 4 12 There are no radionuclide COCs that were detected at activities exceeding even the background mean for samples collected along Woman Creek or its tributaries There are no radionuclide COCs that were detected at activities exceeding the background mean plus one standard deviation

4 3 3 4 Subsurface Soil

IHSS 142.10 (Pond C 1) In subsurface soils downgradient of Pond C 1 COCs were not detected at concentrations exceeding the background mean plus one standard deviation (Figure 4 4B)

IHSS 142.11 (Pond C 2) Cadmium was detected at a level 1 concentration in borehole 50292 east of Pond C 2 (Figure 4 4B) No other metal COCs were detected at concentrations exceeding level-4 for samples collected near Pond C 2 Radionuclide COCs were not detected at activities exceeding level 4 Organic COCs were not detected in subsurface soil samples at Pond C 2

4 3 3 5 Groundwater

Data used to plot metal COCs (aluminum barium, beryllium manganese and vanadium) dissolved in groundwater from Woman Creek are presented in Table 4 7 and are summarized on Figure 4 7B Data used to plot radionuclide COCs (americium 241 plutonium 239/240 radium 226 and the three isotopes of uranium) in groundwater from Woman Creek are presented in Table 4-8 and summarized on Figure 4 8B

Pond C 1 Downgradient of Pond C 1 no metal COCs dissolved were detected in groundwater at level 1 concentrations (Figure 4 7B) Dissolved barium and manganese were found at level 2 concentrations

Dissolved radium 226 in groundwater is the only radionuclide COC that has been detected exceeding level 3 activities in the wells downgradient of Pond C 1 No radionuclides were detected at level 1 activities

Pond C 2 Both wells below Pond C 2 have been dry since they were constructed therefore no groundwater samples have been collected from these wells

4 3 4 IHSS 209 and Other Surface Disturbances

Data used to plot COCs for the various media for IHSS 209 and the other surface disturbances are presented in Tables 4 1 through 4 6 and summarized on Figures 4 1A through 4 6B

Of the media sampled at IHSS 209 and the other surface disturbances (surface soil and subsurface soil) the following is a short list of the COCs detected at level 1 and level 2 concentrations

- A surface soil sample from location SS512493 in IHSS 209 (Figure 4 1B) contained mercury at level 1 concentration
- A subsurface soil sample obtained from 24 to 28 9 feet in borehole 57793 (Figure 4-4A) in the Surface Disturbance South of the Ash Pits contained a level 2 concentration of antimony
- A subsurface soil sample obtained from the surface to 2 feet in borehole 57793 (Figure 4 5A) contained a level 2 activity of uranium 235

These data suggest that COCs exceeding background are not present within IHSS 209 and the other surface disturbances with the possible exception of mercury in one surface soil sample at IHSS 209

4 3 5 Summary of COCs In and Around OU 5 IHSSs

4 3 5 1 Summary of IHSS 115/196

At IHSS 155/196 elevated concentrations of the COCs in all media (surface soils subsurface soils and groundwater) tend to be located in areas where buried wastes are present and elevated concentrations in the

subsurface soil tend to be limited to the same depths as waste materials. However, one surface soil sample located outside of the IHSS 115 boundary south of the central part of the landfill contained elevated mercury which was also detected at elevated concentrations in surface soil within IHSS 115 directly upslope. Elevated activities of uranium in surface soil follow the same pattern with downslope occurrences between the IHSS boundary and Woman Creek. The distribution of organic chemicals in surface soils is also similar but more restricted areally with all of the detects greater than the contract required reporting limits occurring within the boundary of the IHSS where concentrations are generally less than 100 times these reporting limits.

The greatest concentrations of COCs in subsurface soil are within the IHSS 115 boundary and most of the greater concentrations are near IHSS 196 where much waste is buried. A few occurrences of nickel and uranium 238 and 235 that are not closely associated with the wastes may be related to construction of the SID and other unknown causes.

The metal COCs dissolved in groundwater are primarily manganese and barium which may be naturally occurring because considerable manganese staining is found on subsurface materials and barium tends to be associated with manganese. No elevated metal COCs are unequivocally associated with the wastes. However, radium 226 dissolved in groundwater does appear to be associated with the waste in the central part of the landfill and to have migrated downgradient at low activities toward Woman Creek.

4.3.5.2 Summary of IHSS 133

The occurrence of COCs in the IHSS 133 area is similar to that in IHSS 155/196 in that elevated concentrations tend to be in areas where buried wastes are present and tend to be limited to depths of wastes. Metals in the surface soils are at lower concentrations than in IHSS 115 with copper dominating. Again the uranium COCs in the surface soils tend to be elevated near waste sites and downslope from them. No organic COCs were detected in the IHSS 133 area. Elevated levels of metal and radionuclide COCs in subsurface soils are closely associated with the buried wastes. However, as in IHSS 115, copper and nickel in addition to uranium isotopes are more widely distributed than the waste. Also in IHSS 115, manganese and barium are at elevated concentrations in groundwater though these two metals may be naturally occurring. Radium 226 was detected at greater than two standard deviations above the background mean in a well downgradient from the ash pit in IHSS 133.2 suggesting the presence of a plume containing low activities of radium 226.

4 3 5 3 Summary of IHSS 142

Elevated levels of COCs in the Pond C 1 and Pond C 2 appear to be confined to the pond sediments. Mercury and uranium 238 concentrations were detected in Pond C 1 sediments and zinc concentrations exceeding the UTL_{99/99} were found in Pond C 2. Dissolved radium 226 was detected in a monitoring well downgradient from Pond C 1 at levels greater than two standard deviations above the background mean. Wells immediately downslope from Pond C 2 are dry.

Elevated levels of COCs have been detected in surface water and sediments at a few locations in OU 5. In a sediment sample from the SID at the southeast corner of IHSS 115, copper, mercury, and zinc were detected at concentrations greater than three standard deviations above the background mean. In Woman Creek north of Pond C 2, americium 241 and uranium 238 were detected at greater than three standard deviations above the background mean. Other measurable concentrations/activities of COCs in surface water and stream sediments have been at relatively low levels.

4 3 5 4 Summary of IHSS 209 and Surface Disturbances

The only detect of a COC at a concentration greater than three standard deviations above the background mean is for mercury in surface soil at a location in IHSS 209.

Table 4-1
Summary of Metal COCs Exceeding Background Mean in Surface Soil

Sequence		Sample		Result		Reporting		Mean (X STD DEV) of background				
IHSS	ID	Locatio	No.	Constituen	in mg/kg	Qualifier	Limit	Valid	Mean	X 1	X=2	X=3
Exceeds the Background Mean but is less than Background Mean plus one Standard Deviation												
115/196	2161124	SS510593	SS50056AS	COPPER	16.1		5	V	13.41	17.63	21.85	26.07
	2206001	SS507993	SS50030AS	COPPER	15.75		5	V	13.41	17.63	21.85	26.07
	2160900	SS507293	SS50023AS	COPPER	15.7		5	V	13.41	17.63	21.85	26.07
	2224988	SS510393	SS50054AS	COPPER	15.6		5	JA	13.41	17.63	21.85	26.07
	2160984	SS507593	SS50026AS	COPPER	15.5		5	V	13.41	17.63	21.85	26.07
	2161208	SS510893	SS50059AS	COPPER	15.5		5	V	13.41	17.63	21.85	26.07
	2223606	SS509293	SS50043AS	COPPER	15.4		5	V	13.41	17.63	21.85	26.07
	2075525	SS506893	SS50019AS	COPPER	14.9		5	V	13.41	17.63	21.85	26.07
	2227179	SS508093	SS50031AS	COPPER	14.7		5	JA	13.41	17.63	21.85	26.07
	2160872	SS507193	SS50022AS	COPPER	14.5		5	V	13.41	17.63	21.85	26.07
	2161096	SS510193	SS50052AS	COPPER	14.5		5	V	13.41	17.63	21.85	26.07
	2160816	SS506993	SS50020AS	COPPER	14.1		5	V	13.41	17.63	21.85	26.07
	2224966	SS509793	SS50048AS	COPPER	13.8		5	JA	13.41	17.63	21.85	26.07
	2225309	SS509793	SS50048AS	MERCURY	0.1	B	0.1	V	0.08	0.11	0.14	0.17
	2225315	SS510393	SS50054AS	MERCURY	0.1	B	0.1	V	0.08	0.11	0.14	0.17
	2223807	SS509993	SS50050AS	MERCURY	0.09	B	0.1	V	0.08	0.11	0.14	0.17
	2123597	SS506493	SS50015ASU5	SILVER	3.3		2	V	2.8	4.84	6.88	8.92
133.2	2746484	SS514993	SS50112AS	COPPER	15.6		5	V	13.41	17.63	21.85	26.07
	2650897	SS514893	SS50111AS	COPPER	14.75		5	V	13.41	17.63	21.85	26.07
	2746462	SS515193	SS50114AS	COPPER	14.3		5	V	13.41	17.63	21.85	26.07
	2746073	SS514993	SS50112AS	MERCURY	0.1	B	0.1	V	0.08	0.11	0.14	0.17
133.4	2746116	SS514093	SS50102AS	COPPER	15.9		5	V	13.41	17.63	21.85	26.07
133.5	2744014	SS513493	SS50096AS	COPPER	13.8		5	V	13.41	17.63	21.85	26.07
	2746204	SS514393	SS50106AS	COPPER	13.6		5	V	13.41	17.63	21.85	26.07
209	2666874	SS512493	SS50083AS	COPPER	14.2		5	V	13.41	17.63	21.85	26.07
S133	2569821	SS513393	SS50092AS	MERCURY	0.1	B	0.1	V	0.08	0.11	0.14	0.17
W209	2569263	SS511793	SS50076AS	COPPER	17.3		5	V	13.41	17.63	21.85	26.07
	2569329	SS512193	SS50080AS	COPPER	17		5	V	13.41	17.63	21.85	26.07
	2569307	SS511993	SS50078AS	COPPER	16.4		5	V	13.41	17.63	21.85	26.07
	2569219	SS511593	SS50074AS	COPPER	16.2		5	V	13.41	17.63	21.85	26.07
	2569285	SS511893	SS50077AS	COPPER	16		5	V	13.41	17.63	21.85	26.07
	2569241	SS511693	SS50075AS	COPPER	14.9		5	V	13.41	17.63	21.85	26.07
	2666818	SS512293	SS50081AS	COPPER	13.7		5	V	13.41	17.63	21.85	26.07
	2569743	SS512193	SS50080AS	MERCURY	0.09	B	0.1	V	0.08	0.11	0.14	0.17
Exceeds the Background Mean plus one Standard Deviation but is less than Background Mean plus two Standard Deviations												
115/196	2160844	SS507093	SS50021AS	COPPER	20.3		5	V	13.41	17.63	21.85	26.07
	2223628	SS509893	SS50049AS	COPPER	20.3		5	V	13.41	17.63	21.85	26.07
	2161068	SS509593	SS50046AS	COPPER	20.1		5	V	13.41	17.63	21.85	26.07
	2703339	SS510293	SS50053AS	COPPER	19.1		5	V	13.41	17.63	21.85	26.07
	2206029	SS508293	SS50033AS	COPPER	18.3		5	V	13.41	17.63	21.85	26.07
	2206253	SS511293	SS50063AS	COPPER	17.7		5	V	13.41	17.63	21.85	26.07
	2225297	SS508693	SS50037AS	MERCURY	0.12		0.1	V	0.08	0.11	0.14	0.17
	2225303	SS509193	SS50042AS	MERCURY	0.12		0.1	V	0.08	0.11	0.14	0.17
	2703561	SS510293	SS50053AS	MERCURY	0.12	B	0.1	V	0.08	0.11	0.14	0.17
133.3	2746006	SS514493	SS50107AS	MERCURY	0.12		0.1	JA	0.08	0.11	0.14	0.17
	2746254	SS514493	SS50107AS	SILVER	6.3		2	JA	2.8	4.84	6.88	8.92
133.5	2744036	SS513793	SS50099AS	COPPER	18.1		5	V	13.41	17.63	21.85	26.07
W209	2666790	SS512093	SS50079AS	COPPER	18.1		5	V	13.41	17.63	21.85	26.07
Exceeds the Background Mean plus two Standard Deviations but is less than Background Mean plus three Standard Deviations												
115/196	2223825	SS509893	SS50049AS	MERCURY	0.17		0.1	V	0.08	0.11	0.14	0.17
	2161157	SS510693	SS50057AS	MERCURY	0.16		0.1	V	0.08	0.11	0.14	0.17
133.3	2746248	SS514493	SS50107AS	COPPER	24.4		5	V	13.41	17.63	21.85	26.07
	2743970	SS513693	SS50098AS	COPPER	23.9		5	V	13.41	17.63	21.85	26.07

Table 4-1 (Continued)

IHSS	Sequence		Sample		Result		Reporting		Mean (X STD DEV) of background			
	ID	Location	No.	Constitution	in mg/kg	Qualifier	Limit	Valid	Mean	X 1	X=2	X=3
Exceeds the Background Mean plus three Standard Deviations												
115/196	2224922	SS508693	SS50037AS	COPPER	184		5	JA	13 41	17 63	21 85	26 07
	2223562	SS509993	SS50050AS	COPPER	139		5	V	13 41	17 63	21 85	26 07
	2227223	SS510093	SS50051AS	COPPER	112		5	JA	13 41	17 63	21 85	26 07
	2161152	SS510693	SS50057AS	COPPER	78 2		5	V	13 41	17 63	21 85	26 07
	2223540	SS509393	SS50044AS	COPPER	71 9		5	V	13 41	17 63	21 85	26 07
	2205973	SS507893	SS50029AS	COPPER	68 3		5	V	13 41	17 63	21 85	26 07
	2227075	SS508993	SS50040AS	COPPER	60 45		5	JA	13 41	17 63	21 85	26 07
	2206113	SS508893	SS50039AS	COPPER	58 8		5	V	13 41	17 63	21 85	26 07
	2227201	SS509493	SS50045AS	COPPER	55 7		5	JA	13 41	17 63	21 85	26 07
	2206085	SS508493	SS50035AS	COPPER	45 2		5	V	13 41	17 63	21 85	26 07
	2224944	SS509193	SS50042AS	COPPER	35 4		5	JA	13 41	17 63	21 85	26 07
	2223584	SS508793	SS50038AS	COPPER	33 5		5	V	13 41	17 63	21 85	26 07
	2223650	SS510493	SS50055AS	COPPER	30 4		5	V	13 41	17 63	21 85	26 07
	2205945	SS507793	SS50028AS	COPPER	27 6		5	V	13 41	17 63	21 85	26 07
	2205978	SS507893	SS50029AS	MERCURY	0 38		0 1	V	0 08	0 11	0 14	0 17
	2227372	SS508093	SS50031AS	MERCURY	0 37		0 1	JA	0 08	0 11	0 14	0 17
	2227384	SS510093	SS50051AS	MERCURY	0 34		0 1	JA	0 08	0 11	0 14	0 17
	2227378	SS509493	SS50045AS	MERCURY	0 28		0 1	JA	0 08	0 11	0 14	0 17
	2703567	SS509693	SS50047AS	MERCURY	0 26		0 1	V	0 08	0 11	0 14	0 17
	2227342	SS508993	SS50040AS	MERCURY	0 255		0 1	JA	0 08	0 11	0 14	0 17
	2205950	SS507793	SS50028AS	MERCURY	0 23		0 1	V	0 08	0 11	0 14	0 17
	2206118	SS508893	SS50039AS	MERCURY	0 21		0 1	V	0 08	0 11	0 14	0 17
	2223801	SS509393	SS50044AS	MERCURY	0 21		0 1	V	0 08	0 11	0 14	0 17
	2223813	SS508793	SS50038AS	MERCURY	0 195		0 1	V	0 08	0 11	0 14	0 17
	2205982	SS507893	SS50029AS	SILVER	94 3	N	2	JA	2 8	4 84	6 88	8 92
	2206038	SS508293	SS50033AS	SILVER	12 6	N	2	JA	2 8	4 84	6 88	8 92
133.5	2744058	SS513893	SS50100AS	COPPER	26 8		5	V	13 41	17 63	21 85	26 07
209	2666879	SS512493	SS50083AS	MERCURY	0 66		0 1	V	0 08	0 11	0 14	0 17
These data are graphically displayed in Figures 4-7 and 7b.												

These data are graphically displayed Figures 4-7 and 7b.

Table 4 2 Summary of Radionuclide COCs Exceeding Background Mean in Surface Soil

Sequence		Sample		Result		Reporting		Mean (X STD DEV) of background				
IHSS	ID	Location	N	Constituent	PC/G	Qualifier	Limit	Valid	Mean	X 1	X-2	X+3
Exceeds the Background Mean by less than Background Mean plus one Standard Deviation												
5 96	367 442	SS505 93	SS50002AS	U233234			0364	Y	0.822	.202	.582	.962
	3670873	SS505593	SS50006AS	U233234	1 126		0.0287	Y	0.822	.202	.582	.962
	367144	SS505793	SS50008AS	U233234	1005		0.0247	Y	0.822	.202	.582	.962
	2269934	SS51089	SS50059AS	U233234	1 0919		0.0341		0.822	.202	.582	.962
	2269942	S 50989	SS50049AS	233234	0697		03 6		.822	1.202	.582	.962
	2330946	SS508593	SS50036AS	U233234	1 04		0.027	A	0.822	1.202	.582	.962
	2425847	SS506293	SS50013AS	U233234			1	A	0.822	1.202	.582	.962
	2425879	SS507393	SS50024AS	U233234	0.96		0.2	A	0.822	1.202	.582	.962
	2330938	SS508493	SS50035AS	U233234	94		0.0 6		0.822	1.202	.582	.962
	2405921	SS507093	SS50021AS	U233234	0.934		0.023	A	0.822	1.202	.582	.962
	24059 8	507593	SS50026AS	U233234	929			A	0.822	.202	.582	.962
	2330932	SS507993	SS50030AS	U233234	0. 14		0.019	A	0.822	1.202	.582	.962
	2330940	SS508293	SS50033AS	U233234	0.9 2		017	A	0.822	1.202	.582	.962
	367087	SS505693	SS50007AS	U233234	0.905		0.0178	Y	0.822	1.202	.582	.962
	2330930	SS508993	SS50040AS	U233234	0.896		0.032		0.822	1.202	.582	.962
	2425839	S506	SS500 2AS	U23 234	0.89		0.1		0.822	1.202	.582	.962
	2405909	S508693	SS50037AS	U233234	0.873		0.031	A	0.822	1.202	.582	.962
	2330944	SS509493	SS50045AS	U233234	0.856		019		0.822	1.202	.582	.962
	2425871	SS506893	SS50019AS	U233234	0.83		0.1	A	0.822	1.202	.582	.962
	25895	S 506993	50020AS	U23 234	0.83				.822	1.202	.582	.962
	3670894	SS510293	SS50053AS	U235	0.085		0251	Y	0.039	0.091	0.143	0.195
	670895	SS509693	SS50047AS	U235	0.0826		0.0265	Y	.039	0.091	0.143	0. 95
	2330909	SS508893	SS50039AS	U235	0.0759		0	A	0.039	0.091	0.143	0.195
	25856	SS506493	SS50015AS	U235	07	U	0.2		.039	0.09	.143	0.195
	2405868	SS507193	SS50022AS	U235	0.0739		0		0.039	0.091	0.143	0.195
	3671464	SS505893	SS50009AS	U235	0.0724		0.0205	Y	0.039	0.091	0. 43	.195
	2425888	SS507693	SS50027AS	U235	0.072	U	0.2	A	0.039	0.091	0.143	0.195
	2330900	SS509493	SS50045AS	U235	0.0652		0	A	0.039	0.091	0.143	0.195
	2269969	SS511393	SS50064AS	U235	0.0623		0.0459	A	0.039	0.091	0.143	0.195
	3670903	S 515293	SS50126AS	U235	0.0557		0.0273	Y	0.039	0.091	0.143	0.195
	2405884	SS507093	SS50021AS	U235	0.0556		0	A	0.039	0.091	0.143	0.195
	2269960	SS508793	SS50038AS	U235	0.0524		0.0379	A	0.039	0.091	0. 43	0.195
	2425872	SS506893	SS50019AS	U235	0.052	U	0.1	A	0.039	0.091	0.143	0.195
	2270050	SS50909	SS5004 AS	U235	0.0503		0618		0.039	.091	0. 43	0. 95
	2681789	SS509093	SS50041AS	U235	0.05		0.06	A	0.039	0.091	0.143	0.195
	2330903	50829	SS50033AS	U235	049				.039	.09	.43	.95
	2269958	SS509393	SS50044AS	U235	0.0482		0.0973	A	0.039	0.091	0.143	0.195
	2425880	SS507393	SS50024AS	U235	048	U	0.2	A	.039	0.091	0.143	0.195
	367 462	SS505993	SS50010AS	U235	0.04705		0297	Y	0.039	0.091	0.143	0. 95
	2425848	S 506293	SS50013AS	U235	0.047	U	0.2		0.039	0.091	0.143	0.195
	2330896	SS508993	SS50040AS	U235	0.0459		0.023	A	0.039	0.091	0.143	0.195
	2425832	S 50609	SS500 1AS	U235	0.045		0.1		0.039	0.091	0.143	0.195
	2330902	SS507993	SS50030AS	U235	0.0448		0	A	0.039	0.091	0.143	0.195
	2330905	SS508393	SS50034AS	U235	0.0442		0	A	0.039	0.091	0.143	0.195
	2405870	SS507493	SS50025AS	U235	0.0413		0	A	0.039	0.091	0.143	0.195
	2425840	SS506193	S50012AS	U235	04	U	0.2	A	0.039	0.091	0.143	0.195
	3670897	SS505593	SS50006AS	U235	0.0399		0.0196	Y	0.039	0.091	0.143	.195
	3670901	SS515293	SS50124AS	U235	0.0391		0.0222	Y	0.039	0.091	0.143	0.195
	3671479	SS505793	SS50008AS	U238	1 0632		0.0196	Y	0.733	1.146	1.559	1.972
	2330966	SS508593	SS50036AS	U238	1 02		0.027	A	0.733	1.146	1.559	1.972
3670922	SS505693	SS50007AS	U238	0.9608		0.0179	Y	0.733	1.146	1.559	1.972	
2330951	SS508393	SS50034AS	U238	0.954		0.018	A	0.733	1.146	1.559	1.972	
2405935	SS507593	SS50026AS	U238	0.95		0.021		0.733	1.146	1.559	.972	
2425889	SS507693	SS50027AS	U238	0.93		0.2	A	0.733	1.146	1.559	1.972	
2269978	SS5 0593	SS50056AS	U238	98		03 5		0.733	1.146	.559	.972	
2425857	SS506493	SS50015AS	U238	9		0.2	A	0.733	1.146	1.559	1.972	
2405937	SS509193	SS50042AS	U238	0.874		0.02	A	0. 33	1.146	.559	1.972	
2425849	SS506293	SS50013AS	U238	0.87		0.1	A	0.733	1.146	1.559	1.972	
226997	SS510893	SS50059AS	U238	0.8699		0.034		0.733	.46	1.559	.972	
2425873	SS506893	SS50019AS	U238	0.85		0.1		0.733	1.146	1.559	1.972	
2330954	SS507993	SS50030AS	U238	0.843		0	A	0.733	1.146	1.559	.972	
2425897	SS506993	SS50020AS	U238	0.84		0.1		0.733	1.146	1.559	1.972	
2330952	SS508293	SS50033AS	U238	0.821		0.017	A	733	1.146	1.559	.972	
2425841	SS506193	SS50012AS	U238	0.82		0.1	A	0.733	1.146	1.559	1.972	
2405936	509793	SS50048AS	U238	98		033		0.733	1.146	.559	1.972	
2425881	SS507393	SS50024AS	U238	0.79		0.2	A	0.733	1.146	1.559	1.972	
226998	SS5 04	SS50055AS	U238	7779		0425		733	.46	.559	.972	
2405922	SS507193	SS50022AS	U238	0.76		0.022		0.733	1.146	1.559	1.972	
24258	50609	SS500 AS	U238					733	.46	.559	.972	
2405925	SS510393	SS50054AS	U238	0. 49		0.019	A	0.733	1.146	1.559	.972	
2330955	5077	SS50028AS	U238	.44		022		73	.46	1.559	.972	
2269989	SS511293	SS50063AS	U238	402		0359		0.733	1.146	.559	1.972	
33	689692	5 3	S50 03AS	U235	0.062	BJ	0. 1		0.039	091	0.143	0.195
33.2	2689762	SS514993	S50112AS	U235	0.089	BJ	012		.039	091	1 3	0. 95
	3670899	SS 489	S50 AS	U235	04895		027	Y	0.039	091	3	0.195

Table 4-2 (Continued)

IRSS	Sequence ID	Location	Sample No.	Constituent	Result in PC/G	Qualifier	Reporting Limit	std.	Mean	(X STD DEV) of background	X=1	X=2	X=3
33.3	2689720	SS514493	SS50107AS	U235	0.087	BJ	0.025	A	0.039	0.091	0.143	0.195	
133.4	2642367	SS51399	SS50101AS	U235	0.045		13		0.039	0.091	0.143	0.195	
33.5	2642339	SS5 349	SS50096AS	U235	0.04		0.011		0.039	0.091	0.143	0.195	
	2642346	SS513793	SS50099AS	U235	0.048	J	0.038	A	0.039	0.091	0.143	0.195	
33.6	26423	SS5 3593	SS50097AS	U235	0.044		0.021		0.039	0.091	0.143	0.195	
289	2732828	SS512493	SS50083AS	U233234	1.07		0.037	A	0.822	1.202	1.582	1.962	
	2732799	SS512493	SS50083AS	U235	0.0494		0.3		0.039	0.091	0.143	0.195	
	2732851	SS512493	SS50083AS	U238	1.08		0.031	A	0.733	1.146	1.559	1.972	
S133	2725 84	SS5 309	50089AS	U233234	836		0.035		0.822	1.202	1.582	1.962	
	2725149	SS512993	SS50093AS	U235	0.05255		0.036	A	0.039	0.091	0.143	0.195	
	2725 98	SS5 3093	SS50089AS	U238	0.873		0.035		0.733	1.146	1.559	1.972	
W289	2732824	SS511993	SS50078AS	U233234	0.965		0.032	A	0.822	1.202	1.582	1.962	
	2725180	SS512193	SS50080AS	U233234	0.926		0.034	A	0.822	1.202	1.582	1.962	
	2732831	SS512093	SS50079AS	U233234	0.892		0.046	A	0.822	1.202	1.582	1.962	
	2732805	SS511993	SS50078AS	U235	0.0573		0.016	A	0.039	0.091	0.143	0.195	
	2732804	SS5 2093	SS50079AS	U235	0.063		0.07		0.039	0.091	0.143	0.195	
	2732794	SS511593	SS50074AS	U235	0.046		0.016	A	0.039	0.091	0.143	0.195	
	2732795	SS51169	SS50075AS	U235	0.046		0.05		0.039	0.091	0.143	0.195	
	2732841	SS511993	SS50078AS	U238	1.03		0.026	A	0.733	1.146	1.559	1.972	
	2732845	SS511593	SS50074AS	U238	3		0.013	A	0.733	1.146	1.559	1.972	
	2732842	SS511893	SS50077AS	U238	0.875		0.031	A	0.733	1.146	1.559	1.972	
	2725205	SS 2193	SS50080AS	U238	0.869		0.03		0.733	1.146	1.559	1.972	
	2732843	SS511 93	SS50076AS	U238	0.842		0.11		0.733	1.146	1.559	1.972	
	2732854	SS5 2093	SS50079AS	U238	0.827		0.04		0.733	1.146	1.559	1.972	
	2732853	SS512293	SS50081AS	U238	0.807		0.03	A	0.733	1.146	1.559	1.972	
Exceeds the Background Mean plus one Standard Deviation but less than Background Mean plus two Standard Deviations													
15/196	2330943	SS510093	SS50051AS	U233234	1.55		0.023	A	0.822	1.202	1.582	1.962	
	2330945	SS50809	SS5003 AS	U233234	46		0.026		0.822	1.202	1.582	1.962	
	3670878	SS515293	SS50125AS	U233234	1.3237		0.0302	Y	0.822	1.202	1.582	1.962	
	3670879	SS515293	SS50126AS	U233234	1.2839		0.04	Y	0.822	1.202	1.582	1.962	
	3670877	SS515293	SS50124AS	U233234	1.2634		0.0361	Y	0.822	1.202	1.582	1.962	
	3671443	SS509993	SS50010AS	U23 234	2.1295		0.042	Y	0.822	1.202	1.582	1.962	
	2330912	SS51009	SS50051AS	U235	0.124		0		0.039	0.091	0.143	0.195	
	2330904	SS508493	SS50035AS	U235	0.11		0.016	A	0.039	0.091	0.143	0.195	
	2425912	SS508193	SS50032AS	U235	0.11	U	0.2	A	0.039	0.091	0.143	0.195	
	3670925	29	SS50 24AS	U238	22		0.022		0.73	1.146	1.559	1.972	
	2330965	SS508093	SS50031AS	U238	54		0.019		0.733	1.146	1.559	1.972	
	2330964	SS508493	SS50035AS	U238	1.35		0.016		0.733	1.146	1.559	1.972	
	2405931	SS507493	SS50023AS	U238	1.31		0.029	A	0.733	1.146	1.559	1.972	
	367 481	SS509993	SS50010AS	U238	1.24775		0.0234	Y	0.733	1.146	1.559	1.972	
	3670927	SS515293	SS50126AS	U238	2.394		0.0273	Y	0.733	1.146	1.559	1.972	
	240594	SS507093	SS50021AS	U238	1.18		0	A	0.733	1.146	1.559	1.972	
	2269982	SS508293	SS50043AS	U238	1.1761		0.0323	A	0.733	1.146	1.559	1.972	
133.2	2689763	SS514993	SS50112AS	U233234	1.5	B	0.012	A	0.822	1.202	1.582	1.962	
	2689748	SS515093	SS50113AS	U235	0.13	BJ	0.023		0.039	0.091	0.143	0.195	
	2689755	SS515193	SS50114AS	U235	0.099	BJ	0.021	A	0.039	0.091	0.143	0.195	
33.3	2689742	SS5 4793	SS50110AS	U233234		B	0.049		0.822	1.202	1.582	1.962	
133.4	2642361	SS514093	SS50102AS	U233234	1.5	B	0.033	A	0.822	1.202	1.582	1.962	
	2642368	SS513993	SS50101AS	U233234	1.5	B	0.033		0.822	1.202	1.582	1.962	
133.5	2642353	SS513893	SS50100AS	U235	0.11	J	0.022	A	0.039	0.091	0.143	0.195	
	2642338	SS513493	SS50096AS	U238	1.3	B	0.03	A	0.733	1.146	1.559	1.972	
133.6	2642325	SS513693	SS50098AS	U235	0.11	J	0.031	A	0.039	0.091	0.143	0.195	
Exceeds the Background Mean plus two Standard Deviations but less than Background Mean plus three Standard Deviations													
115/196	2269937	SS509393	SS50044AS	U233234	1.7913		0.1149	A	0.822	1.202	1.582	1.962	
	2330963	SS508893	SS50039AS	U238	92		0.01		0.733	1.146	1.559	1.972	
	2330947	SS508993	SS50040AS	U238	1.77		0.02	A	0.733	1.146	1.559	1.972	
	3671480	SS505193	SS50002AS	U238	5753		0.0223	Y	0.733	1.146	1.559	1.972	
	3670926	SS515293	SS50125AS	U238	5.696		0.0302	Y	0.733	1.146	1.559	1.972	
33.1	2689728	SS514593	SS50108AS	U233234	1.8	B	0.019	A	0.822	1.202	1.582	1.962	
	2689693	SS5	SS50103AS	U233234		B	0		0.822	1.202	1.582	1.962	
	2689691	SS51 193	SS50103AS	U238	1.6	B	0.017	A	0.733	1.146	1.559	1.972	
33.2	3670875	SS514893	SS501 AS	U23 234	1.6469		0.073	Y	0.822	1.202	1.582	1.962	
	2689749	SS515093	SS50113AS	U233234	1.6	B	0.01	A	0.822	1.202	1.582	1.962	
	3670923	SS514893	SS50111AS	U238	1.96495		0.0274	Y	0.733	1.146	1.559	1.972	
33.3	2689735	SS514693	SS50109AS	U233234	1.6	B	0.036	A	0.822	1.202	1.582	1.962	
	26897	SS5147 3	SS50110AS	U235	0.9	BJ	0.027		0.039	0.091	0.143	0.195	
	2689734	SS514693	SS50109AS	U235	17	BJ	0.014		0.039	0.091	0.143	0.195	
	2689740	SS514793	SS50110AS	U238	1.8	B	0.049	A	0.733	1.146	1.559	1.972	
33	2642360	514093	SS50102AS	U235	0.15	J	0.021	A	0.039	0.091	0.143	0.195	
33.5	2642354	SS513893	SS50100AS	U233234	1.8	B	0.052	A	0.822	1.202	1.582	1.962	
	2689700	29	50 04AS	U23 234					822	1.202	1.582	1.962	
	2689706	439	50 06AS	U235	635	BJ			0.039	0.091	0.143	0.195	
	2689699	SS514293	SS50104AS	U235	5	BJ	0.011		0.039	0.091	0.143	0.195	

Table 4 2 (Continued)

IHSS	Sequence		Sample No.	Constituent	Result in PC/G	Qualifier	Reporting Limit		std.	Mean (X STD DEV) of background			
	ID	Location					Limit			Mean	X 1	X-2	X-3
33.6	2642326	SS513693	SS50098AS	U233234	16	B	0.041			0.822	1.202	1.582	1.962
Exceeds the Background Mean plus three Standard Deviations													
15/196	9245	SS505493	SS50005AS	U233234	2800		70	V		0.822	1.202	.582	1.962
	3419233	SS505093	SS50001AS	U233234	200		9	V		0.822	1.202	1.582	1.962
	34 9239	SS505293	SS50003AS	U233234	97		5	V		0.822	.202	.582	1.962
	3419251	SS515593	SS50127AS	U233234	94		6	V		0.822	1.202	1.582	1.962
	9257	SS515693	SS50128AS	U23 234			0.8	V		0.822	1.202	1.582	1.962
	3670870	SS510293	SS50053AS	U233234	3 637		0.0446	Y		0.822	1.202	1.582	1.962
	3670872	SS505393	SS50004AS	U233234	2.707		0.75	Y		0.822	1.202	.582	1.962
	2269938	SS509993	SS50050AS	U233234	2.6707		0.049			0.822	1.202	1.582	1.962
	367087	SS509693	SS50047AS	U23 234	392		0.0492	Y		0.822	.202	1.582	1.962
	3671445	SS505893	SS50009AS	U233234	2.3131		0.0258	Y		0.822	1.202	1.582	1.962
	2269939	SS508793	SS50038AS	U233234	2.26 5		0.0619	A		0.822	.202	1.582	1.962
	3419246	SS505493	SS50005AS	U235	670		30	V		0.099	0.091	0.143	0.195
	34 9234	SS505093	SS5000 AS	U235	46		6	V		0.099	0.091	0.143	0.195
	34 9240	SS505293	SS50003AS	U235	23		3	V		0.099	0.091	0.143	0.195
	34 9252	SS5 5593	SS50127AS	U235	9			V		0.099	0.091	0.43	0.195
	3419258	SS515693	SS50128AS	U235	2.1		0.5	V		0.099	0.091	0.143	0.195
	3670896	SS505393	SS50004AS	U235	0.2739		0.0176	Y		0.099	0.091	0.143	0.195
	2269959	SS509993	SS50050AS	U235	0.2283		0.0301	A		0.099	0.091	0.143	0.195
	9247	SS505493	SS50005AS	U238	38000		70	V		0.733	1.146	1.559	1.972
	3419235	SS505093	SS50001AS	U238	2000		9	V		0.733	1.146	1.559	1.972
	3 19241	SS505293	SS50003AS	U238	000			V		0.733	1.146	1.559	1.972
	9253	SS 5593	SS50127AS	U238	780		5	V		0.733	.146	1.559	1.972
	34 9259	SS515693	SS50128AS	U238	86					0.733	1.146	.559	1.972
	2269980	SS509993	SS50050AS	U238	1 7287		0.0576	A		0.733	1.146	1.559	1.972
	3670920	SS505393	SS50004AS	U238	10.0269		0.222	Y		0.733	1.146	.559	1.972
	2269979	SS509393	SS50044AS	U238	7.7302		0.0829	A		0.733	1.146	1.559	1.972
	2330957	SS5 0093	SS50051AS	U238	5.43		0	A		0.733	.46	1.559	1.972
	2269981	SS508793	SS50038AS	U238	3.6463		0.0379	A		0.733	1.146	1.559	1.972
	3670918	SS510293	SS50053AS	U238	3.3073		0.0251	Y		0.733	1.146	1.559	1.972
	2269984	SS509893	SS50049AS	U238	2.3629		0.0317	A		0.733	1.146	1.559	1.972
	36709 9	SS509693	SS50047AS	U238	2.2344		0.0265	Y		0.733	.146	1.559	1.972
	2330958	SS504493	SS50045AS	U238	2		0.019	A		0.733	1.146	1.559	1.972
	2269977	SS510693	SS50057AS	U238	2.037		0.0399	A		0.733	1.146	1.559	1.972
	3670921	SS505593	SS50006AS	U238	2.0258		0.0196	Y		0.733	1.146	1.559	1.972
	3671483	SS505893	SS50009AS	U238	1.98		0.0205			0.73	.46	.59	1.972
133	2689726	SS514593	SS50108AS	U238	2	B	0.05	A		0.733	1.146	1.559	1.972
133.2	2689756	SS515193	SS50114AS	U233234	2.2	B	0.021	A		0.822	1.202	1.582	1.962
	2689754	SS515193	SS50114AS	U238	2.6	B	0.021	A		0.733	1.146	1.559	1.972
	2689761	SS514993	SS50112AS	U238	2.3	B	0.021	A		0.733	1.146	1.559	1.972
	2689747	SS515093	SS50113AS	U238	2.1	B	0.023	A		0.733	1.146	1.559	1.972
133.3	2689721	SS514493	SS50107AS	U233234	3.3	B	0.015	A		0.822	.202	1.582	1.962
	2689719	SS514493	SS50107AS	U238	5.2	B	0.039	A		0.733	1.146	1.559	1.972
	2689733	SS514693	SS50109AS	U238	2.8	B	0.036	A		0.733	.146	1.559	1.972
133.4	3670881	SS5 5493	SS50121AS	U233234	47.4833		0.073	Y		0.822	.202	1.582	1.962
	3670882	SS515493	SS50122AS	U233234	44.9751		0.0933	Y		0.822	1.202	1.582	1.962
	3670883	SS515493	SS50123AS	U233234	3.2646		0.1066	Y		0.822	1.202	.582	1.962
	3670906	SS515493	SS50122AS	U235	2.8877		0.1366	Y		0.099	0.091	0.143	0.195
	3670905	SS515493	SS50121AS	U235	2.2385		0.073	Y		0.099	0.091	0.143	0.195
	3670907	SS515493	SS50123AS	U235	2.994		0.1066	Y		0.099	0.091	0.143	0.195
	3670929	SS515493	SS50121AS	U238	209.2773		0.0921	Y		0.733	1.146	1.559	1.972
	3670930	SS515493	SS50122AS	U238	203.0783		0.0933	Y		0.733	1.146	1.559	1.972
	367093	SS515493	SS50123AS	U238	90.3		0.066	Y		0.733	.46	1.559	1.972
	2642359	SS514093	SS50102AS	U238	2.6	B	0.038	A		0.733	1.146	1.559	1.972
	2642366	SS513993	SS50101AS	U238	2.2	B	0.033	A		0.733	1.146	.559	1.972
33.5	2689707	SS514393	SS50106AS	U233234	2.6	B	0.012			0.822	1.202	1.582	1.962
	2642347	SS513793	SS50099AS	U233234	2	B	0.014			0.822	1.202	1.582	1.962
	2689705	SS514393	SS50106AS	U238	1	B	0.012			0.733	1.146	1.559	1.972
	2642345	SS513793	SS50099AS	U238	3.5	B	0.014			0.733	1.146	.559	1.972
	2642352	SS513893	SS50100AS	U238	3	B	0.068			0.733	1.46	1.559	1.972
	2689698	SS514293	SS50104AS	U238	2.5	B	0.019			0.733	1.146	.559	1.972
133.6	2642333	SS513593	SS50097AS	U233234	2	B	0.021	A		0.822	1.202	1.582	1.962
	2642331	SS513593	SS50097AS	U238	2.5	B	0.039	A		0.733	1.146	1.559	1.972
	2642324	SS513693	SS50098AS	U238	2.3	B	0.06	A		0.733	1.146	1.559	1.972

These data are graphically displayed on Figures 4 2a and 2b

Table 4 3 Summary of Organic COCs in Surface Soil

DESS	Sequence ID	Location	Sample No.	Test Comp Code	Constituent	Result in ug/kg	Qualifier	Reporting Limit	Ed
Detected concentration below Reporting Limit									
15/196	22646	SS50999	SS50050A3	BNACLP	Benzo(a)anthracene	320		330	
	2203934	SS507993	SS50030A3	BNACLP	Benzo(a)anthracene	90		330	
	2265850	SS50999	SS50050A	NACLP	Benzo(a)anthracene	80		330	
	22 84	SS508693	SS500	ACLP	Benzo(a)anthracene	40		330	
	2266034	50929	50043A	BNACLP	Benzo(a)anthracene			330	
	224 60	5094	SS50045A3	ACLP	Benzo(a)anthracene	00		30	
	2247252	SS5 0093	SS50051A3	BNACLP	Benzo(a)anthracene	200		30	
	2 5867	SS508	SS50032A3	BNACLP	Benzo(a)anthracene	1		330	
	220408	5084	SS50035	BNACLP	Benzo(a)anthracene			330	
	2204473	SS5 39	SS50064A	BNACLP	Benzo(a)anthracene	60		30	
	22662 8	SS 04	SS50055A	BNACLP	Benzo(a)anthracene	60		30	
	5833	507 3	SS50022A3	BNCLP	Benzo(a)anthracene	50		30	
	2204326	51 093	SS50061A	BNACLP	Benzo(a)anthracene	0	JX	330	
	2204228	SS509093	SS50041A3	BNACLP	Benzo(a)anthracene	83		30	
	70164	50969	SS50047 3	BNACLP	Benzo(a)anthracene	66		330	
	2247068	SS508093	SS50031A3	BNACLP	Benzo(a)anthracene	64		330	
	224 66	SS509493	SS50045A	BNACLP	Benzo(a)Pyrene	240		330	
	2247258	0093	SS500 1A	BNACLP	Benzo(a)Pyrene	240		330	
	2266040	SS50929	SS50043A3	BNACLP	Benzo(a)Pyrene	240		330	
	58680	SS508 93	SS50032A	BNACLP	Benzo(a)Pyrene	80		30	
	223 85	SS508693	SS500 A	BNACLP	Benzo(a)Pyrene	60		330	
	2204479	39	SS50064A	BNACLP	Benzo(a)Pyrene	50		30	
	2266224	SS5 04	SS50055A3	BNACLP	Benzo(a)Pyrene	50		30	
	2246656	508993	SS50040A	BNACLP	Benzo()Pyrene	02		30	
	224707	SS50809	SS5003 A3	BNACLP	Benzo(a)Pyrene	7		30	
	58678	508	SS50032A	ACLP	Benzo(b)Fluoranthene	32		30	
	223 53	508693	SS5003	ACLP	Benzo(b)Fluoranthene			30	
	2247 64	5094	SS50045A	BNACLP	Benzo(b)Fluoranthene	32	J	30	
	2266222	SS 04	SS5005 A3	BNACLP	Benzo(b)Fluoranthene	300		330	
	2204477	SS5 39	SS50064 3	BNACLP	Benzo(b)Fluoranthene	220	JX	330	
	2204085	SS508493	SS50035A3	BNACLP	Benzo(b)Fluoranthene	200		330	
	2247256	0093	SS500 1A	BNACLP	Benzo(b)Fluoranthene	130		330	
	2247072	SS50809	SS50031A3	BNACLP	Benzo(b)Fluoranthene	110		330	
	2246654	SS508993	SS50040A3	BNACLP	Benzo(b)Fluoranthene	03.5	J	30	
	2 5843	SS507393	SS50024	BNACLP	Benzo(b)Fluoranthene	87		330	
	2265950	50879	SS50038A	BNACLP	Dibenz(a,h)anthracene	35		30	
	2265766	SS509393	SS50044A	BNACLP	Dibenz(a,h)anthracene	69		30	
	2265858	SS509993	SS50050A3	BNACLP	Dibenz(a,h)anthracene	60		330	
	2246646	SS508993	SS50040A	BNACLP	Fluoranthene	250		30	
	2204322	SS511093	SS50061A3	BNACLP	Fluoranthene	230	J	330	A
	2247064	SS50809	SS50031A	BNACLP	Fluoranthene	2 0	J	330	
	2204224	SS509093	SS5004 3	BNACLP	Fluoranthene	80		330	
	70 63	SS508693	SS5004	BNACLP	Fluoranthene	80		330	
	58278	SS507093	SS50021A3	BNCLP	Fluoranthene	50		30	
	2204	SS5 3	SS5006	NACLP	Fluoranthene	50		330	
	58180	SS506693	SS500	BNCLP	Fluoranthene	30		30	
	5822	SS506993	SS50020A	BNACLP	Fluoranthene	30	J	330	
	2 584	SS507393	SS50024A	BNACLP	Fluoranthene		J	330	
	2 546	S 02	SS50053A	BNACLP	Fluoranthene			30	
	5862	SS50769	SS50027	BNACLP	Fluoranthene			330	
	2246972	SS508593	SS50036A	BNACLP	Fluoranthene			30	
	58572	SS507593	SS50026A3	BNCLP	Fluoranthene	97		330	
	2232209	SS5 0393	SS50054A3	BNACLP	Fluoranthene	83		30	
	2122 70	SS506193	SS50012A3U	BNACLP	Fluoranthene	68	J	330	
	2265857	SS509993	SS50050A3	BNACLP	Indeno(2,3-cd)Pyrene	250	J	330	
	2265765	SS509393	SS50044A3	BNACLP	Indeno(1,2,3-cd)Pyrene	240		330	
	226461	509993	SS50050A	BNACLP	Indeno(2,3-cd)Pyrene	230		330	
	2266133	SS509893	SS50049A3	BNACLP	Indeno(2,3-cd)Pyrene	2	J	330	A
	122365	SS5064	SS500 5A3U	BNACLP	Indeno(2,3-cd)Pyrene	70		330	
	224 67	SS5094	SS50045A3	BNACLP	Indeno(2,3-cd)Pyrene	40	J	330	
	226604	SS509293	SS50043A	BNACLP	Indeno(2,3-cd)Pyrene	30		330	
	2247259	SS510093	SS50051A3	BNACLP	Indeno(1,2,3-cd)Pyrene	120	J	330	A
	2266225	04	SS50055A	BNACLP	Indeno(2,3-cd)Pyrene	82	J	330	
	224665	SS508993	SS50040A	BNACLP	Indeno(2,3-cd)Pyrene	59		30	A
	224 07	SS508093	SS50031A	BNACLP	Indeno(2,3-cd)Pyrene	52	J	330	A
	2 58328	507	SS50022A	BNCLP	Pyrene	280		30	A
	2 5872	509593	SS50046A	BNCLP	Pyrene	280	J	330	A
	220407	SS508493	SS50035A	BNACLP	Pyrene	270		30	
	2204323	SS511093	SS50061A3	BNACLP	Pyrene	00		330	A
	224664	SS508993	50040A3	BNACLP	Pyrene			30	
	2204225	SS509093	SS5004 3	BNACLP	Pyrene	70	J	30	
	638	50969	SS5004	BNACLP	Pyrene			30	
	58279	SS507093	SS50021A	NCLP	Pyrene	50	J	330	
	224706	SS508093	SS500 1A	BNACLP	Pyrene	40		30	A
	2204	SS 3	SS50065A3	BNACLP	Pyrene	30		330	A
	58230	506993	SS50020A	BNACLP	Pyrene			330	A
	58	SS50669	SS500	BNCLP	Pyrene			30	
	58573	SS50759	SS50026A	NCLP	Pyrene			30	
	22322	SS 39	SS50054A3	BNACLP	Pyrene	00		30	
	58622	SS507693	SS5002	BNACLP	Pyrene	90		330	
	54	02	SS500 3A	BNACLP	Pyrene			30	
	2 58426	SS507393	50024	NACLP	Pyrene		J	330	
	1221 1	506 93	SS50012A3U3	BNACLP	Pyrene		BJ	30	

Table 4 3 (Continued)

IRHS	Sequence ID	Location	Sample N	test resp Code	Contaminant	Result in ug/kg	Qualifier	Reporting Limit	add.
	2246973	508593	SS50036A.S	BNACLP	Pyrene	59		30	
			Exceeds Reporting Limit but less than ten times the Reporting Limit						
15/196	223 31	S509	SS50042A.S	BNACLP	Benzo(a)anthracene	3000		30	
	223 39	509 93	SS50042A.S	BNACLP	Benzo(a)anthracene	900		30	
	223212	509793	50048A	BNACLP	Benzo(a)anthracene	500		30	
	22 3836	S507793	SS50028A.S	NACLP	Benzo(a)anthracene	300		330	
	22 3885	S50789	SS50029	NACLP	Benzo(a)anthracene	800		30	
	22 5942	SS50879	SS50038A	BNACLP	Benzo(a)anthracene	800		330	V
	5887	0693	S50057	BNCLP	Benzo(a)anthracene	80		30	
	122358	5064 3	SS500 5A.SU5	ACLP	Benzo(a)anthracene	460		30	
	2204277	S5 099	S50060A.S	BNACLP	Benzo(a)anthracene	440		30	
	2265758	SS50939	SS50044	BNACLP	Benzo(a)anthracene	0		330	
	22 3983	50829	SS500 3A	ACLP	Benzo(a)anthracene	380		30	
	2266126	SS509893	SS50049 S	BNACLP	Benzo(a)anthracene	360		330	
	223203	SS509 93	SS50042A.S	BNACLP	Benzo(a)Pyrene	400	D	330	Z
	2203842	SS507793	S50028A	BNACLP	Benzo(a)Pyrene	300		330	
	22 94	509	SS50042A.S	BNACLP	Benzo(a)Pyrene	300		30	
	223212	S509793	SS50048A	ACLP	Benzo(a)Pyrene	1200		30	
	220389	S50789	SS50029A.S	BNACLP	Benzo(a)Pyrene	30		30	
	22 5948	SS50879	SS50038A.S	BNACLP	Benzo(a)Pyrene	840		330	
	5887	069	SS50057A.S	BNCLP	Benzo(a)Pyrene	790		330	
	2203940	SS50799	SS50030A	BNACLP	Benzo(a)Pyrene	5		330	
	22 3989	508293	SS50033A.S	BNACLP	Benzo(a)Pyrene			330	A
	22 5764	S509393	SS50044 S	BNACLP	Benzo(a)Pyrene	460		330	
	22364	5064	S500 5A.SU5	BNACLP	Benzo(a)Pyrene	400		30	
	22646	S50993	SS50050A	ACLP	Benzo(a)Pyrene	400		30	
	2266 32	S509893	SS5004	ACLP	Benzo(a)Pyrene	90		330	
	22 5856	SS50999	S50050A	BNACLP	Benzo(a)Pyrene			30	
	22 94	509	SS50042A.S	BNACLP	Benzo(b)Fluoranthene	600		30	
	2232 35	509 93	SS50042A.S	NACLP	Benzo(b)Fluoranthene	2500	D	30	Z
	2232125	S50793	SS50048A	ACLP	Benzo(b)Fluoranthene	2000		330	
	220384	S50779	SS50028A	BNACLP	Benzo(b)Fluoranthene	00		330	
	2203889	S50793	SS5002 AS	BNACLP	Benzo(b)Fluoranthene	700		330	V
	2265946	S50879	SS50038A.S	BNACLP	Benzo(b)Fluoranthene	350		30	
	5887	S5 0693	SS5005 S	BNCLP	Benzo(b)Fluoranthene	300		330	
	2266 30	SS509893	SS50049	BNACLP	Benzo(b)Fluoranthene	40		30	
	2265762	S50939	S50044A.S	BNACLP	Benzo(b)Fluoranthene	730		30	
	2203938	S50793	SS50030A	ACLP	Benzo(b)Fluoranthene	64		30	
	2264614	SS509993	SS50050A.S	BNACLP	Benzo(b)Fluoranthene	640		330	
	2203987	508293	SS50033A.S	BNACLP	Benzo(b)Fluoranthene	620	JX	30	
	122362	SS5064	SS50015A.SU5	BNACLP	Benzo(b)Fluoranthene	530		330	V
	2266038	S509293	SS50043A	BNACLP	Benzo(b)Fluoranthene	0		30	V
	2204 38	SS50889	SS50039	BNACLP	Dibenz(a,h)anthracene	00		30	
	2204 87	SS50889	50039	BNACLP	Dibenz(a,h)anthracene	960	D	330	
	2232 7	SS509793	SS50048A.S	BNACLP	Fluoranthene	2500		330	
	58866	0693	SS50057 S	BNCLP	Fluoranthene	2 00		330	
	220388	SS507893	SS50029A.S	BNACLP	Fluoranthene	2000		330	
	2265938	S508793	S50038A	ACLP	Fluoranthene	700		30	
	122354	SS506493	SS50015A.SU5	BNACLP	Fluoranthene	1000		330	V
	2265754	S509393	S50044A.S	BNACLP	Fluoranthene	940		330	
	2266122	S509893	SS5004	BNACLP	Fluoranthene			330	
	2264606	S50993	SS50050A.S	BNACLP	Fluoranthene	900		330	
	2203979	S508293	SS50033A	BNACLP	Fluoranthene	8 0		30	
	2265846	SS509993	SS50050A	BNACLP	Fluoranthene	60		330	
	22 3930	S50793	SS50030A	BNACLP	Fluoranthene	730		30	
	2266030	S50929	SS50043A.S	BNACLP	Fluoranthene	640		330	
	2247156	SS509493	SS50045A.S	BNACLP	Fluoranthene	580		330	V
	223 84	S508693	SS5003	BNACLP	Fluoranthene	570		30	
	2247248	SS510093	SS5005 AS	BNACLP	Fluoranthene	570		330	
	22662	0493	SS50055	BNACLP	Fluoranthene	520		330	
	2204273	S5 0993	SS50060A.S	BNACLP	Fluoranthene	505		330	
	5867	SS508	SS50032A.S	BNACLP	Fluoranthene	440		30	
	587	SS50959	SS50046A	BNCLP	Fluoranthene	380		30	
	5832	SS507 93	SS50022A.S	BNCLP	Fluoranthene	370	J	330	
	2204469	S5 1	S5064A.S	BNACLP	Fluoranthene	360	J	330	
	2204077	SS508493	SS50035A.S	BNACLP	Fluoranthene	50	J	30	
	2204 37	S508893	SS50039	BNACLP	Indeno(1,2,3-cd)Pyrene	00		330	JA
	2204 86	S508893	SS50039A.S	BNACLP	Indeno(2,3-cd)Pyrene	3100	D	330	
	220384	S507793	SS50028A.S	BNACLP	Indeno(1,2,3-cd)Pyrene	00		330	
	2232 38	509 93	SS50042A.S	BNACLP	Indeno(2,3-cd)Pyrene	600	DJ	330	Z
	226594	S50879	SS50038A.S	BNACLP	Indeno(2,3-cd)Pyrene			330	
	2232128	S509793	S50048A	BNACLP	Indeno(2,3-cd)Pyrene	42		330	
	223 946	509 93	SS50042A.S	BNACLP	Indeno(2,3-cd)Pyrene			30	
	2263773	SS509393	SS50044 S	PESTCLP	PCB 1254	00		60	
	22639	S5 04	SS50055A.S	PESTCLP	PCB 1254	00		60	
	2246200	SS508893	SS50040A.S	PESTCLP	PCB 254	065		60	
	22 5407	SS508893	SS50039	PESTCLP	PCB 1254	900	X	60	
	22 5245	SS507793	S50028A	PESTCLP	PCB 1254	50		60	
	226382	S50879	S50038A.S	PESTCLP	PCB 254	630		60	
	2205380	SS508493	SS50035A.S	PESTCLP	PCB 1254	560		60	
	2263885	SS508893	S50049	PESTCLP	PCB 1254	30		160	
	2263857	S50929	SS50043A	PESTCLP	PCB 1254	220		60	
	2203833	S507793	SS50028A.S	ACLP	Pyrene	2600		30	
	2232 8	SS509793	SS50048A.S	BNACLP	Pyrene	2600		330	

Table 4 3 (Continued)

IHSS	Sequence ID	Location	Sample N	Test Group Code	Constituent	Result in ug/kg	Qualifier	Reporting Limit	Alt.
	2203882	SS507893	50029 S	BNACLP	Pyrene	00		30	
	58867	SS 0693	SS50057	BNCLP	Pyrene	600		30	
	2263939	508793	50038A	ACLP	Pyrene	500		330	
	223	SS5064	50015ASU	BNACLP	Pyrene	000	EX	330	A
	2264607	SS09993	SS50050AS	BNACLP	Pyrene	730		330	
	22 5	509393	SS50044AS	BNACLP	Pyrene	30		330	
	22 584	SS50999	50050A	BNACLP	Pyrene			30	
	22 3980	5082	SS50033AS	ACLP	Pyrene	00	J	330	
	2266123	50989	5004	ACLP	Pyrene			330	
	220393	SS50799	SS50030A	B ACLP	Pyrene	35		330	V
	220427	099	SS50060A	BNACLP	Pyrene	90		330	
	226603	SS50929	SS50043AS	NACLP	Pyrene			330	V
	224724	SS5 0093	50051A	BNACLP	Pyrene	44		30	
	223 846	508693	SS50037 S	BNACLP	Pyrene	30		30	
	224 157	SS09493	SS50045A	BNACLP	Pyrene	30		30	
	2 5867	SS508 3	SS50032AS	BNACLP	Pyrene	0	J	330	
	220447	51	SS50064A	ACLP	Pyrene	340		30	
	226621	5 04	SS50055AS	BNACLP	Pyrene	340		330	A
Exceeds ten times the Reporting Limit but less than one hundred times the Reporting Limit									
15/196	2204 30	SS508893	SS50039	BNACLP	Benzo(a)anthracene	4400		330	
	2204 79	SS508893	SS50039AS	BNACLP	Benzo(a)anthracene	3500	D	330	
	2204 36	50889	SS50039	BNACLP	Benzo(a)Pyrene	500		330	
	2204 85	50889	SS50039	B ACLP	Benzo(a)Pyrene	3900	D	30	
	2204 34	SS50889	SS50039	ACLP	Benzo(b)Fluoranthene	500		30	
	2204 83	50889	SS50039	BNACLP	Benzo(b)Fluoranthene	600		330	
	5882	5 59	SS50056AS	ACLP	Dibenz(a,h)anthracene	9200	D	330	
	58780	SS 59	SS50056A	BNACLP	Dibenz(a,h)anthracene	000		30	
	2204 2	508893	SS50039 S	BNACLP	Fluoranthene	000		330	
	2204	SS508893	SS50039AS	NACLP	Fluoranthene	9900	D	330	
	223202	SS509 93	SS50042A	BNACLP	Fluoranthene	6200	D	330	
	223 3	509 93	SS50042A	BNACLP	Fluoranthene	00		330	Z
	2203832	SS507793	SS50028AS	BNACLP	Fluoranthene	3400		330	
	58828	SS5 099	SS50056AS	BNACLP	Indeno(1,2,3-cd)Pyrene	32000	D	330	JA
	2158779	SS510593	SS50056AS	BNACLP	Indeno(1,2,3-cd)Pyrene	28000	E	330	
	2246396	SS51009	SS50051AS	PESTCLP	PCB 1254	3900		160	
	2246368	SS5094	SS50045A	PESTCLP	PCB 1254	2400		60	
	226380	SS50999	SS50050AS	PESTCLP	PCB 1254	2300	C	160	
	2 60260	SS510693	SS50057 S	PESTCLP	PCB 1254	2200	X	60	
	2204127	SS508893	SS50039AS	BNACLP	Pyrene	9500		30	V
	2204 7	50889	SS50039	BNACLP	Pyrene	8400		30	
	2232028	509193	SS50042AS	BNACLP	Pyrene	00	D	330	
	2231936	509193	SS50042AS	BNACLP	Pyrene	5 00		330	Z
Exceeds one hundred times the Reporting Limit									
15/196	5882	SS51059	SS50056AS	BNACLP	Benzo(a)anthracene	5000	D	330	
	58772	SS510593	SS50056AS	BNACLP	Benzo(a)anthracene	0000	E	330	
	2158778	SS51 593	SS50056AS	BNACLP	Benzo(a)Pyrene	3000	E	330	
	58827	SS5 0593	SS50056A	BNACLP	Benzo(a)Pyrene	000	D	330	
	58825	SS5 0593	SS50056A	BNACLP	Benzo(b)Fluoranthene	9000	XD	30	
	5877	SS5 593	SS50056AS	BNACLP	Benzo(b)Fluoranthene	8000	E	30	
	588	SS5 059	50056A	BNACLP	Fluoranthene	0000	D	330	
	58768	SS5 59	SS50056AS	BNACLP	Fluoranthene	73000	E	30	
	588	SS510593	SS50056A	BNACLP	Pyrene	0000	D	30	
	2158769	S 1 593	SS50056A	BNACLP	Pyrene	59000	E	330	

These data are graphically displayed on Figures 4-3a and 3b.

Table 4-4
Summary of Metal COCs Exceeding Background Mean in Subsurface Soil

IHSS/Site	Sequence	Location	Sample	Depth	Constituent	Result	Qualifier	Reporting	Valid	Mean (X STD DEV) of background				
	ID		N	I		Interval		in mg/kg		Limit	Mean	X	1	X=2
Exceeds the Background Mean but is less than Background Mean plus one Standard Deviation														
115/196	3335198	59593	BH50540AS	0' 2	ANTIMONY	8.5	B	12	JA	6.56	9.4	12.24	15.08	
	3334952	59793	BH50488AS	0' 2'	ANTIMONY	7.1	B	12	JA	6.56	9.4	12.24	15.08	
	4981949	56694	BH00122AS	43 0-150 0	COPPER	25.2		25	JA	12.59	25.36	38.13	50.9	
	5105493	59894	BH00164AS	19 9-31 9	COPPER	23.3		25	V	12.59	25.36	38.13	50.9	
	2700368	59593	BH50552AS	0'-6'	COPPER	22.85		5	V	12.59	25.36	38.13	50.9	
	5009789	58794	BH00054AS	0 0-2 4	COPPER	22.6		5	JA	12.59	25.36	38.13	50.9	
	2633713	58593	BH50404AS	12.5' 18 1	COPPER	22.5		5	V	12.59	25.36	38.13	50.9	
	4929377	57594	BH00082AS	6 0-12 0	COPPER	22.4		25	V	12.59	25.36	38.13	50.9	
	5105437	59494	BH00160AS	11 9-17 9	COPPER	22.4		25	V	12.59	25.36	38.13	50.9	
	4929349	57594	BH00078AS	0 0-6 0	COPPER	22.2		25	V	12.59	25.36	38.13	50.9	
	2686964	59293	BH50441AS	12' 18 9'	COPPER	21.7		5	V	12.59	25.36	38.13	50.9	
	2700126	59793	BH50486AS	13.3 15.3	COPPER	21.6		5	V	12.59	25.36	38.13	50.9	
	2700434	59593	BH50554AS	14.4' 16 4	COPPER	21.3		5	V	12.59	25.36	38.13	50.9	
	4932915	57594	BH00085AS	18 0-23 0	COPPER	21		25	V	12.59	25.36	38.13	50.9	
	2700500	59493	BH50522AS	12 9' 17.8	COPPER	20.7		5	V	12.59	25.36	38.13	50.9	
	2091481	50792	BH50105AS	0' 10'	COPPER	20.5		5	V	12.59	25.36	38.13	50.9	
	4981921	56694	BH00113AS	43 0-150 0	COPPER	20.4		25	V	12.59	25.36	38.13	50.9	
	4880286	58494	BH00068AS	0 0-6 0	COPPER	20.3		25	V	12.59	25.36	38.13	50.9	
	5105297	57094	BH00147AS	0 0-40 0	COPPER	19.9		25	V	12.59	25.36	38.13	50.9	
	4961693	56694	BH00112AS	0 0-41 0	COPPER	19.6		25	V	12.59	25.36	38.13	50.9	
	4880314	58494	BH00071AS	6 0-9 5	COPPER	19.5		25	V	12.59	25.36	38.13	50.9	
	2133994	51092	BH50153AS	0'-6'	COPPER	19.1		5	V	12.59	25.36	38.13	50.9	
	4961553	56694	BH00096AS	0 0-6 0	COPPER	18.4		25	V	12.59	25.36	38.13	50.9	
	5105325	57094	BH00148AS	0 0-40 0	COPPER	17.9		25	V	12.59	25.36	38.13	50.9	
	5009761	58694	BH00052AS	0 0-2 9	COPPER	17.3		5	JA	12.59	25.36	38.13	50.9	
	2700802	63193	BH50616AS	0'-6'	COPPER	17.3		5	JA	12.59	25.36	38.13	50.9	
	2700044	59793	BH50484AS	0' 7.3	COPPER	17.2		5	V	12.59	25.36	38.13	50.9	
	2120433	50892	BH50121AS	0'-6'	COPPER	17.1		5	V	12.59	25.36	38.13	50.9	
	2686942	59293	BH50440AS	6' 12'	COPPER	16.9		5	V	12.59	25.36	38.13	50.9	
	2700692	61293	BH50505AS	6' 10.6'	COPPER	16.9		5	JA	12.59	25.36	38.13	50.9	
	2120477	50892	BH50123AS	8' 16'	COPPER	16.7		5	V	12.59	25.36	38.13	50.9	
	4961525	56694	BH00095AS	0 0-6 0	COPPER	16.7		25	V	12.59	25.36	38.13	50.9	
	2686882	59293	BH50439AS	0'-6'	COPPER	16.7		5	V	12.59	25.36	38.13	50.9	
	2700890	61093	BH50603AS	6' 13	COPPER	16.7		5	JA	12.59	25.36	38.13	50.9	
	2120389	50592	BH50064AS	12' 18'	COPPER	16.6		5	V	12.59	25.36	38.13	50.9	
	2700192	59193	BH50457AS	2'-8'	COPPER	16.55		5	V	12.59	25.36	38.13	50.9	
	3334959	59793	BH50488AS	0' 2'	COPPER	16.5		5	V	12.59	25.36	38.13	50.9	
	2060864	50692	BH50089AS	0' 14	COPPER	15.9		5	V	12.59	25.36	38.13	50.9	
	2005309	50392	BH50015AS	18' 24	COPPER	15.8		5	V	12.59	25.36	38.13	50.9	
	2746550	58693	BH50349AS	12' 19.5'	COPPER	15.55		5	V	12.59	25.36	38.13	50.9	
	2120455	50892	BH50122AS	6' 12'	COPPER	15.3		5	V	12.59	25.36	38.13	50.9	
	2700824	63193	BH50617AS	6' 12'	COPPER	15.3		5	JA	12.59	25.36	38.13	50.9	
	2005272	50392	BH50016AS	25' 30'	COPPER	14.8		5	V	12.59	25.36	38.13	50.9	
	2060820	50692	BH50087AS	0'-6'	COPPER	14.8		5	V	12.59	25.36	38.13	50.9	
	2650787	58693	BH50405AS	25.5' 29.5'	COPPER	14.7		5	V	12.59	25.36	38.13	50.9	
	3334995	59293	BH50444AS	0' 2'	COPPER	14.7		5	V	12.59	25.36	38.13	50.9	
	4961581	56694	BH00098AS	6 0-10 0	COPPER	14.5		25	V	12.59	25.36	38.13	50.9	
	5105353	59494	BH00152AS	0 0-5 9	COPPER	14.5		25	V	12.59	25.36	38.13	50.9	
	2037352	50492	BH50039AS	12' 18'	COPPER	13.9		5	V	12.59	25.36	38.13	50.9	
	2060842	50692	BH50088AS	6' 12'	COPPER	13.2		5	V	12.59	25.36	38.13	50.9	
2700632	61293	BH50504AS	0'-6'	COPPER	12.8		5	JA	12.59	25.36	38.13	50.9		
5105465	59894	BH00162AS	17 9-19 9	COPPER	12.7		25	V	12.59	25.36	38.13	50.9		
4880295	58494	BH00068AS	0 0-6 0	NICKEL	33.2		40	JA	19.81	40.37	60.93	81.49		
2633635	58593	BH50347AS	0'-6'	NICKEL	33.05		8	V	19.81	40.37	60.93	81.49		
2700872	60993	BH50588AS	0'-6'	NICKEL	28.6		8	V	19.81	40.37	60.93	81.49		
4961674	56694	BH00111AS	0 0-35 0	NICKEL	27.1		40	V	19.81	40.37	60.93	81.49		
2700438	59593	BH50554AS	14 4 16.4	NICKEL	25.5		8	V	19.81	40.37	60.93	81.49		
5105502	59894	BH00164AS	19 9-31 9	NICKEL	23.7		40	V	19.81	40.37	60.93	81.49		
2120393	50592	BH50064AS	12' 18'	NICKEL	23.6		8	V	19.81	40.37	60.93	81.49		
3335189	59593	BH50540AS	0' 2'	NICKEL	23.5		8	V	19.81	40.37	60.93	81.49		
2133976	50992	BH50140AS	0' 16'	NICKEL	23.4		8	V	19.81	40.37	60.93	81.49		
4981958	56694	BH00122AS	43 0-150 0	NICKEL	23.4		40	V	19.81	40.37	60.93	81.49		
5105306	57094	BH00147AS	0 0-40 0	NICKEL	22.6		40	V	19.81	40.37	60.93	81.49		

Table 4 4 (Continued)

IHSS/Site	Sequence		Sample N	Depth Interval	Constituent	Result in mg/kg	Qualifier	Reporting Limit	V M.L.	Mean (X STD DEV) of background			
	ID	Locatio								Mean	X 1	X 2	X=3
	5105334	57094	BH00148AS	0 0-40 0	NICKEL	22		40	V	19 81	40 37	60 93	81 49
	5105446	59494	BH00160AS	11 9-17 9	NICKEL	21 3		40	V	19 81	40 37	60 93	81 49
	2746340	58393	BH50343AS	0'-6'	NICKEL	21		8	V	19 81	40 37	60 93	81 49
	2133932	50992	BH50138AS	0'-6'	NICKEL	20 9		8	V	19 81	40 37	60 93	81 49
	2700048	59793	BH50484AS	0' 7.3	NICKEL	20 4		8	V	19 81	40 37	60 93	81 49
	2700372	59593	BH50552AS	0'-6'	NICKEL	20 15		8	V	19 81	40 37	60 93	81 49
	2746534	58493	BH50346AS	6' 12	SILVER	13 7		2	V	5 7	15 1	24.5	33 9
	2133934	50992	BH50138AS	0'-6'	SILVER	11 3		2	V	5 7	15 1	24.5	33 9
	2746512	58493	BH50345AS	0'-6'	SILVER	11 2		2	V	5 7	15 1	24.5	33 9
	3335055	59493	BH50524AS	4 2	SILVER	8 2		2	V	5 7	15 1	24.5	33 9
	2133978	50992	BH50140AS	0' 16'	SILVER	6 5		2	V	5 7	15 1	24.5	33 9
133.1	2700280	58893	BH50458AS	0'-6'	COPPER	23 1		5	V	12.59	25.36	38 13	50 9
	2453018	56493	BH50219AS	0'-6'	COPPER	21		5	V	12.59	25.36	38 13	50 9
	2700302	58893	BH50459AS	6' 12	COPPER	20 1		5	V	12.59	25.36	38 13	50 9
	2452294	56293	BH50206AS	0'-6'	COPPER	15 9		5	V	12.59	25.36	38 13	50 9
	3334885	58893	BH50646AS	0' 2'	COPPER	14 1		5	V	12.59	25.36	38 13	50 9
	2700284	58893	BH50458AS	0'-6'	NICKEL	23 1		8	V	19 81	40 37	60 93	81 49
	2743652	56393	BH50211AS	0' 2'	SILVER	9 8		2	V	5 7	15 1	24.5	33 9
133.2	2687052	58793	BH50409AS	18' 24	COPPER	24 7		5	V	12.59	25.36	38 13	50 9
	2453410	57593	BH50301AS	12' 14	COPPER	19 4		5	V	12.59	25.36	38 13	50 9
	2452630	57393	BH50256AS	0' 2	COPPER	19 3		5	V	12.59	25.36	38 13	50 9
	2452686	57393	BH50258AS	4 6' 12.1	COPPER	19 1		5	V	12.59	25.36	38 13	50 9
	2452658	57393	BH50257AS	0' 6 6'	COPPER	18 9		5	V	12.59	25.36	38 13	50 9
	2515255	57293	BH50252AS	0'-6'	COPPER	17 6		5	V	12.59	25.36	38 13	50 9
	2425182	56993	BH50202AS	8 1 14	COPPER	17 5		5	V	12.59	25.36	38 13	50 9
	2425322	57093	BH50241AS	0' 2	COPPER	17 5		5	V	12.59	25.36	38 13	50 9
	2452714	57393	BH50259AS	10.2' 18 1	COPPER	17 4		5	V	12.59	25.36	38 13	50 9
	2452546	57193	BH50246AS	0' 2'	COPPER	17 1		5	V	12.59	25.36	38 13	50 9
	2686986	58793	BH50406AS	0' 6 1	COPPER	16 9		5	V	12.59	25.36	38 13	50 9
	2425350	57093	BH50242AS	0'-6'	COPPER	16 1		5	V	12.59	25.36	38 13	50 9
	2452574	57193	BH50247AS	0' 5.5'	COPPER	15		5	V	12.59	25.36	38 13	50 9
	2462699	56993	BH50199AS	0'-4'	COPPER	14 5		5	V	12.59	25.36	38 13	50 9
	2453158	57493	BH50261AS	0' 2'	COPPER	14 5		5	V	12.59	25.36	38 13	50 9
	2425266	56893	BH50239AS	8.3 14.3	COPPER	14 3		5	V	12.59	25.36	38 13	50 9
	2453270	57493	BH50265AS	18' 20'	COPPER	14 3		5	V	12.59	25.36	38 13	50 9
	2425406	57093	BH50244AS	12.3 18.6'	COPPER	14		5	V	12.59	25.36	38 13	50 9
	2687008	58793	BH50407AS	6 1 12	COPPER	13 95		5	V	12.59	25.36	38 13	50 9
	2515284	57293	BH50253AS	6' 12'	COPPER	13 7		5	V	12.59	25.36	38 13	50 9
	2515422	57293	BH50292AS	26' 30'	COPPER	13 6		5	V	12.59	25.36	38 13	50 9
	2462677	56993	BH50198AS	0' 2	COPPER	13 1		5	V	12.59	25.36	38 13	50 9
	2515226	57293	BH50251AS	0' 2'	COPPER	12 9		5	V	12.59	25.36	38 13	50 9
	2515313	57293	BH50254AS	12' 18'	COPPER	12 7		5	V	12.59	25.36	38 13	50 9
	2452664	57393	BH50257AS	0'-6.6'	NICKEL	30 6		8	V	19 81	40 37	60 93	81 49
	2425356	57093	BH50242AS	0'-6'	NICKEL	27 7		8	V	19 81	40 37	60 93	81 49
	2687056	58793	BH50409AS	18' 24	NICKEL	25 7		8	V	19 81	40 37	60 93	81 49
	2515259	57293	BH50252AS	0'-6'	NICKEL	25 4		8	JA	19 81	40 37	60 93	81 49
	2687078	58793	BH50410AS	24 28 4	NICKEL	24 8		8	V	19 81	40 37	60 93	81 49
	2425412	57093	BH50244AS	12.3 18.6'	NICKEL	22 5		8	V	19 81	40 37	60 93	81 49
	2452636	57393	BH50256AS	0' 2'	NICKEL	20 8		8	V	19 81	40 37	60 93	81 49
133.3	3335136	61193	BH50649AS	0' 2'	ANTIMONY	6 7	B	12	JA	6 56	9 4	12.24	15.08
	2700588	61493	BH50585AS	8.5' 15 9'	COPPER	25 3		5	V	12.59	25.36	38 13	50 9
	2700736	61393	BH50570AS	0'-6'	COPPER	24 55		5	V	12.59	25.36	38 13	50 9
	2452462	56593	BH50224AS	13' 17'	COPPER	23 9		5	V	12.59	25.36	38 13	50 9
	2701000	63093	BH50559AS	15' 20'	COPPER	20 55		5	JA	12.59	25.36	38 13	50 9
	2700758	61393	BH50576AS	0' 10'	COPPER	20 1		5	V	12.59	25.36	38 13	50 9
	2452518	56693	BH50227AS	0'-6'	COPPER	20		5	V	12.59	25.36	38 13	50 9
	2700566	61493	BH50583AS	0' 8.5'	COPPER	19 8		5	JA	12.59	25.36	38 13	50 9
	2700978	59693	BH50558AS	12 15.5'	COPPER	18 15		5	V	12.59	25.36	38 13	50 9
	2453074	56793	BH50232AS	0'-6'	COPPER	18		5	V	12.59	25.36	38 13	50 9
	2452434	56593	BH50223AS	6' 12'	COPPER	17		5	V	12.59	25.36	38 13	50 9
	2700912	59693	BH50556AS	0'-6'	COPPER	16 5		5	JA	12.59	25.36	38 13	50 9
	3335123	61193	BH50649AS	0' 2	COPPER	15		5	V	12.59	25.36	38 13	50 9
	2452490	56693	BH50226AS	0' 2'	COPPER	14.5		5	V	12.59	25.36	38 13	50 9
	2453130	56793	BH50234AS	10' 12'	COPPER	14 5		5	V	12.59	25.36	38 13	50 9

Table 4 4 (Continued)

IHSS/Site	Sequence		Sample N	Depth Interval	Constituent	Result in mg/kg	Qualifier	Reporting		Valid	Mean (X STD DEV) of background			
	ID	Location						Limit	Mean		X	X-1	X-2	X-3
	2452378	56593	BH50221AS	0' 2'	COPPER	13.6		5	V		12.59	25.36	38.13	50.9
	2453102	56793	BH50233AS	6' 12'	COPPER	13.4		5	V		12.59	25.36	38.13	50.9
	2700610	61493	BH50584AS	5.5' 13.5'	COPPER	13.4		5	JA		12.59	25.36	38.13	50.9
	2453046	56793	BH50231AS	0' 2'	COPPER	13.3		5	V		12.59	25.36	38.13	50.9
	3334793	61493	BH50651AS	0' 2'	COPPER	13.3		5	V		12.59	25.36	38.13	50.9
	2452406	56593	BH50222AS	0'-6'	COPPER	13.1		5	V		12.59	25.36	38.13	50.9
	2700350	61193	BH50503AS	6' 10'	NICKEL	34.65		8	V		19.81	40.37	60.93	81.49
	2700916	59693	BH50556AS	0'-6'	NICKEL	21.3		8	V		19.81	40.37	60.93	81.49
	2700762	61393	BH50576AS	0' 10'	NICKEL	20.9		8	V		19.81	40.37	60.93	81.49
133.4	2519064	55793	BH50307AS	0'-6'	CADMIUM	0.76	B	1	JA		0.64	0.88	1.12	1.36
	2519068	55793	BH50307AS	0'-6'	COPPER	24.9		5	V		12.59	25.36	38.13	50.9
	2519090	55793	BH50308AS	6' 12'	COPPER	23.9		5	V		12.59	25.36	38.13	50.9
	3335051	58993	BH50647AS	0' 2'	COPPER	23.4		5	V		12.59	25.36	38.13	50.9
	2358212	55593	BH50082AS	18' 24'	COPPER	23.1		5	V		12.59	25.36	38.13	50.9
	2463001	55993	BH50187AS	9.3 15'	COPPER	22.7		5	V		12.59	25.36	38.13	50.9
	2519134	55793	BH50309AS	12.4 18.4	COPPER	21.7		5	V		12.59	25.36	38.13	50.9
	2358240	55593	BH50083AS	24' 26'	COPPER	21.1		5	V		12.59	25.36	38.13	50.9
	2358128	55593	BH50058AS	6' 12'	COPPER	20.4		5	V		12.59	25.36	38.13	50.9
2700214	59093	BH50411AS	0'-6'	COPPER	19.65		5	V		12.59	25.36	38.13	50.9	
	2743712	58093	BH50313AS	0' 2'	COPPER	19.5		5	V		12.59	25.36	38.13	50.9
	2358100	55593	BH50057AS	0'-6'	COPPER	19		5	V		12.59	25.36	38.13	50.9
	2703235	58993	BH50480AS	0'-6.4	COPPER	17.75		5	V		12.59	25.36	38.13	50.9
	2703317	58993	BH50482AS	6.4 12	COPPER	16.3		5	V		12.59	25.36	38.13	50.9
	2462891	56093	BH50271AS	2'-8'	COPPER	15.5		5	V		12.59	25.36	38.13	50.9
	2425126	55893	BH50141AS	0' 2'	COPPER	15.2		5	V		12.59	25.36	38.13	50.9
	2700236	59093	BH50412AS	6' 12'	COPPER	14.3		5	V		12.59	25.36	38.13	50.9
	3335105	59093	BH50648AS	0' 2'	COPPER	13.2		5	V		12.59	25.36	38.13	50.9
	2743744	58093	BH50314AS	0'-8'	MOLYBDENUM	19.6	B	40	V		15.39	24.4	33.41	42.42
	2358218	55593	BH50082AS	18' 24'	NICKEL	30.3		8	V		19.81	40.37	60.93	81.49
	2519072	55793	BH50307AS	0'-6'	NICKEL	26.1		8	V		19.81	40.37	60.93	81.49
	2519094	55793	BH50308AS	6' 12'	NICKEL	25.3		8	V		19.81	40.37	60.93	81.49
	2358134	55593	BH50058AS	6' 12'	NICKEL	20.3		8	V		19.81	40.37	60.93	81.49
	2743716	58093	BH50313AS	0' 2'	NICKEL	20.1		8	JA		19.81	40.37	60.93	81.49
3335037	58993	BH50647AS	0' 2'	SILVER	11.6		2	V		5.7	15.1	24.5	33.9	
133.5	2358012	55493	BH50033AS	6' 12.4'	CADMIUM	0.7	B	1	V		0.64	0.88	1.12	1.36
	2358352	55293	BH50107AS	6' 10'	COPPER	19.9		5	V		12.59	25.36	38.13	50.9
	2358016	55493	BH50033AS	6' 12.4	COPPER	19.9		5	V		12.59	25.36	38.13	50.9
	2358324	55293	BH50106AS	0'-6'	COPPER	18.2		5	V		12.59	25.36	38.13	50.9
	2357988	55493	BH50032AS	0'-6'	COPPER	17.6		5	V		12.59	25.36	38.13	50.9
	2331328	55493	BH50166AS	17.3 24.3	COPPER	13.9		5	V		12.59	25.36	38.13	50.9
	2331300	55393	BH50117AS	25.8' 33.3	COPPER	13.7		5	V		12.59	25.36	38.13	50.9
	2358268	55193	BH50090AS	0'-6'	COPPER	13.6		5	V		12.59	25.36	38.13	50.9
	2432354	55393	BH50165AS	12 17.2'	COPPER	13.35		5	V		12.59	25.36	38.13	50.9
2358330	55293	BH50106AS	0'-6'	NICKEL	22.2		8	V		19.81	40.37	60.93	81.49	
133.6	2357932	54893	BH50017AS	0'-6.5'	COPPER	24.1		5	V		12.59	25.36	38.13	50.9
	2358380	55093	BH50131AS	6' 13.2'	COPPER	19.5		5	V		12.59	25.36	38.13	50.9
	2358044	54993	BH50035AS	0'-6'	COPPER	19.4		5	V		12.59	25.36	38.13	50.9
	2358072	54993	BH50042AS	6' 10'	COPPER	15.1		5	V		12.59	25.36	38.13	50.9
	2358050	54993	BH50035AS	0'-6'	NICKEL	19.9		8	V		19.81	40.37	60.93	81.49
142.10	1882999	50092	BH50000AS	0' 14.8'	CADMIUM	0.82	B	1	V		0.64	0.88	1.12	1.36
	1883003	50092	BH50000AS	0' 14.8'	COPPER	20.5		5	V		12.59	25.36	38.13	50.9
	2075487	51193	BH50168AS	0' 10'	COPPER	16.8		5	V		12.59	25.36	38.13	50.9
142.11	1883227	50292	BH50008AS	0' 14.5'	COPPER	22.8		5	V		12.59	25.36	38.13	50.9
Magnetic Anomaly W f 133	2860046	64493	BH50632AS	12' 14'	ANTIMONY	7.7	B	12	JA		6.56	9.4	12.24	15.08
	2859958	64593	BH50636AS	12' 18'	ANTIMONY	6.9	B	12	JA		6.56	9.4	12.24	15.08
	2860031	64493	BH50631AS	6' 12'	COPPER	18.6		5	V		12.59	25.36	38.13	50.9
	2859817	64693	BH50638AS	0'-6'	COPPER	18.4		5	V		12.59	25.36	38.13	50.9
	2860009	64493	BH50630AS	0'-6'	COPPER	17.9		5	V		12.59	25.36	38.13	50.9
	2859921	64593	BH50634AS	0'-6'	COPPER	17		5	V		12.59	25.36	38.13	50.9
	2860053	64493	BH50632AS	12' 14'	COPPER	16.5		5	V		12.59	25.36	38.13	50.9
	2859943	64593	BH50635AS	6' 12'	COPPER	16		5	V		12.59	25.36	38.13	50.9
	2859877	64693	BH50639AS	6' 12'	COPPER	15.6		5	V		12.59	25.36	38.13	50.9
	2859899	64693	BH50640AS	12' 16'	COPPER	14.5		5	V		12.59	25.36	38.13	50.9
	2859969	64593	BH50636AS	12' 18'	NICKEL	27		8	V		19.81	40.37	60.93	81.49

Table 4 4 (Continued)

IHSS/Site	Sequence		Sample N	Depth Interval	Constituent	Result in mg/kg	Qualifier	Reporting		Mean (X STD DEV) of background			
	ID	Location						Limit	V Hd.	Mean	X 1	X=2	X=3
	2859821	64693	BH50638AS	0'-6"	NICKEL	24		8	V	19.81	40.37	60.93	81.49
	2860035	64493	BH50631AS	6' 12"	NICKEL	23.9		8	V	19.81	40.37	60.93	81.49
	2860013	64493	BH50630AS	0'-6"	NICKEL	23.3		8	V	19.81	40.37	60.93	81.49
	2859881	64693	BH50639AS	6' 12"	NICKEL	23		8	V	19.81	40.37	60.93	81.49
	2859947	64593	BH50635AS	6' 12"	NICKEL	22.5		8	V	19.81	40.37	60.93	81.49
	2859925	64593	BH50634AS	0'-6"	NICKEL	22.1		8	V	19.81	40.37	60.93	81.49
S133	2569395	57993	BH50316AS	4' 9" 8' 1"	COPPER	19.55		5	V	12.59	25.36	38.13	50.9
	2519398	57793	BH50338AS	24' 28' 9"	COPPER	16.8		5	V	12.59	25.36	38.13	50.9
	3348803	57893	BH50342AS	18' 7" 26.4"	COPPER	14.7		5	V	12.59	25.36	38.13	50.9
TDEM 1	4933027	60094	BH00089AS	0 0-5 0	COPPER	19.6		25	V	12.59	25.36	38.13	50.9
	5209091	55194	BH00029AS	6 0-12 0	COPPER	16.4		25	V	12.59	25.36	38.13	50.9
	5209203	55294	BH00033AS	12 0-15 2	COPPER	15		25	V	12.59	25.36	38.13	50.9
	5209175	55294	BH00032AS	6 0-12 0	COPPER	13.5		25	V	12.59	25.36	38.13	50.9
	5209147	55294	BH00031AS	0 0-6 0	COPPER	13.4		25	V	12.59	25.36	38.13	50.9
	5209156	55294	BH00031AS	0 0-6 0	NICKEL	29.3		40	JA	19.81	40.37	60.93	81.49
	4933008	59994	BH00088AS	0 0-5 3	NICKEL	26.5		40	V	19.81	40.37	60.93	81.49
TDEM 2	4880230	55894	BH00036AS	0 0-6 0	COPPER	23		25	V	12.59	25.36	38.13	50.9
	5284212	56094	BH00038AS	6 0-12 0	NICKEL	32.6		40	Y	19.81	40.37	60.93	81.49
	5284268	56094	BH00040AS	18 0-22 0	NICKEL	30.6		40	Y	19.81	40.37	60.93	81.49
	5284240	56094	BH00039AS	12 0-18 0	NICKEL	24.6		40	Y	19.81	40.37	60.93	81.49
	5284249	56094	BH00040AS	18 0-22 0	SILVER	8.5		10	Y	5.7	15.1	24.5	33.9
TDEM W133	4880258	58894	BH00064AS	0 0-2.7	COPPER	19.6		25	V	12.59	25.36	38.13	50.9
W209	2519178	57693	BH50319AS	0'-6"	COPPER	18.9		5	V	12.59	25.36	38.13	50.9
	3334903	57693	BH50642AS	0' 2"	COPPER	16.9		5	V	12.59	25.36	38.13	50.9
Exceeds the Background Mean plus one Standard Deviation but is less than Background Mean plus two Standard Deviations													
115/196	2746568	58693	BH50350AS	19.5' 25.5'	CADMIUM	1.1	B	1	V	0.64	0.88	1.12	1.36
	3335069	59493	BH50524AS	4' 2"	COPPER	37		5	V	12.59	25.36	38.13	50.9
	3335013	58693	BH50644AS	0' 2"	COPPER	34.5		5	V	12.59	25.36	38.13	50.9
	3335185	59593	BH50540AS	0' 2"	COPPER	30.9		5	V	12.59	25.36	38.13	50.9
	2650809	58693	BH50348AS	0'-6"	COPPER	29.8		5	V	12.59	25.36	38.13	50.9
	4961665	56694	BH00111AS	0 0-35 0	COPPER	29.7		25	V	12.59	25.36	38.13	50.9
	2037296	50492	BH50037AS	0'-6"	COPPER	26.6		5	V	12.59	25.36	38.13	50.9
	2700868	60993	BH50588AS	0'-6"	COPPER	26		5	V	12.59	25.36	38.13	50.9
	2700828	63193	BH50617AS	6' 12"	NICKEL	46.6		8	V	19.81	40.37	60.93	81.49
133 1	2743678	56393	BH50212AS	2'-6"	MOLYBDENUM	24.5	B	40	V	15.39	24.4	33.41	42.42
	4961506	57294	BH00091AS	0 0-4 0	NICKEL	58		40	V	19.81	40.37	60.93	81.49
	2743628	56393	BH50213AS	6'-8"	NICKEL	45.3		8	V	19.81	40.37	60.93	81.49
133 2	2452770	57393	BH50291AS	22 1 26.1	COPPER	34.2		5	V	12.59	25.36	38.13	50.9
	2687074	58793	BH50410AS	24 28.4	COPPER	27		5	V	12.59	25.36	38.13	50.9
	2462725	56993	BH50201AS		NICKEL	51		8	V	19.81	40.37	60.93	81.49
133.3	2700346	61193	BH50503AS	6' 10'	COPPER	29.8		5	V	12.59	25.36	38.13	50.9
	2700956	59693	BH50557AS	6' 12'	COPPER	28.2		5	V	12.59	25.36	38.13	50.9
	3334867	61393	BH50650AS	0' 2"	COPPER	27.3		5	V	12.59	25.36	38.13	50.9
	2452471	56593	BH50224AS	13' 17"	SILVER	15.6		2	V	5.7	15.1	24.5	33.9
133 4	2743729	58093	BH50314AS	0'-8"	BERYLLIUM	12.2		1	V	4.66	9.43	14.2	18.97
	2462935	55993	BH50162AS	0' 2"	COPPER	27.9		5	V	12.59	25.36	38.13	50.9
	2519046	55793	BH50306AS	0' 2"	COPPER	26.4		5	V	12.59	25.36	38.13	50.9
	2700258	59093	BH50413AS	12' 16.3"	COPPER	26.3		5	V	12.59	25.36	38.13	50.9
	5422816	55694	BH00041AS	0 0-6 0	NICKEL	59.6		2.58	Y	19.81	40.37	60.93	81.49
	2462961	55993	BH50151AS	0'-6"	NICKEL	54.8		8	V	19.81	40.37	60.93	81.49
	2463007	55993	BH50187AS	9.3 15'	SILVER	16.4		2	JA	5.7	15.1	24.5	33.9
Magnetic Anomaly W 133	2860002	64493	BH50630AS	0'-6"	ANTIMONY	11.1	B	12	JA	6.56	9.4	12.24	15.08
	2859914	64593	BH50634AS	0'-6"	ANTIMONY	9.5	B	12	JA	6.56	9.4	12.24	15.08
	2859810	64693	BH50638AS	0'-6"	ANTIMONY	9.5	B	12	JA	6.56	9.4	12.24	15.08
	2859991	64593	BH50637AS	18' 20"	NICKEL	58.8		8	V	19.81	40.37	60.93	81.49
	2859903	64693	BH50640AS	12' 16"	NICKEL	51.8		8	V	19.81	40.37	60.93	81.49
S133	2569391	57993	BH50316AS	4' 9" 8' 1"	CADMIUM	0.935		1	V	0.64	0.88	1.12	1.36
	2569399	57993	BH50316AS	4' 9"-8' 1"	NICKEL	45.4		8	V	19.81	40.37	60.93	81.49
TDEM-1	4932999	59994	BH00088AS	0 0-5 3	COPPER	37.9		25	V	12.59	25.36	38.13	50.9
TDEM-2	5284182	56094	BH00037AS	0 0-6 0	MOLYBDENUM	25		200	Y	15.39	24.4	33.41	42.42
	5372479	55994	BH00035AS	6 0-11 2	NICKEL	44.9	EN	2.94	Y	19.81	40.37	60.93	81.49
	5284193	56094	BH00038AS	6 0-12 0	SILVER	23.1		10	Y	5.7	15.1	24.5	33.9

Table 4 4 (Continued)

IHSS/Site	Sequence		Sample	Depth	Constituent	Result	Reporting			Mean (X STD DEV) of background				
	ID	Location	N	Interval		in mg/kg	Qualifier	Limit	Valid	Mean	X	1	X=2	X=3
Exceeds the Background Mean plus two Standard Deviations but is less than Background Mean plus three Standard Deviations														
115/196	2746354	58393	BH50344AS	6' 12.7	CADMIUM	13		1	V	0.64	0.88	1.12	1.36	
	2650805	58693	BH50348AS	0'-6'	CADMIUM	12		1	V	0.64	0.88	1.12	1.36	
	2633685	58593	BH50403AS	6' 12.5	COPPER	50.8		5	V	12.59	25.36	38.13	50.9	
	2633629	58593	BH50347AS	0'-6'	COPPER	49.85		5	V	12.59	25.36	38.13	50.9	
	5009655	57994	BH00047AS	0 0-6.3	COPPER	42.4		5	JA	12.59	25.36	38.13	50.9	
	2700894	61093	BH50603AS	6' 13	NICKEL	73.8		8	V	19.81	40.37	60.93	81.49	
	5009660	57994	BH00047AS	0 0-6.3	NICKEL	69.9		8	JA	19.81	40.37	60.93	81.49	
133 1	2743672	56393	BH50212AS	2'-6'	NICKEL	66.3		8	V	19.81	40.37	60.93	81.49	
	4961487	57294	BH00091AS	0 0-4.0	SILVER	26.9		10	V	5.7	15.1	24.5	33.9	
133 2	2687023	58793	BH50408AS	12' 18"	ANTIMONY	14.2		12	JA	6.56	9.4	12.24	15.08	
	2462670	56993	BH50198AS	0' 2'	ANTIMONY	14.1	B	12	JA	6.56	9.4	12.24	15.08	
	2515251	57293	BH50252AS	0'-6'	CADMIUM	13		1	JA	0.64	0.88	1.12	1.36	
	2462695	56993	BH50199AS	0'-4	CADMIUM	12		1	JA	0.64	0.88	1.12	1.36	
133 4	2462884	56093	BH50271AS	2'-8"	ANTIMONY	15		12	JA	6.56	9.4	12.24	15.08	
	2519042	55793	BH50306AS	0' 2'	CADMIUM	13		1	JA	0.64	0.88	1.12	1.36	
	2743690	58093	BH50315AS	10' 12	COPPER	40.2		5	V	12.59	25.36	38.13	50.9	
C ncrete Pad	5009822	56194	BH00043AS	0 0-6.0	NICKEL	75.9		8	JA	19.81	40.37	60.93	81.49	
Mag. An m.	2860057	64493	BH50632AS	12' 14	NICKEL	72		8	V	19.81	40.37	60.93	81.49	
S133	2519391	57793	BH50338AS	24 28 9'	ANTIMONY	13.5	B	12	JA	6.56	9.4	12.24	15.08	
Exceeds the Background Mean plus three Standard Deviations														
115/196	2700707	59493	BH50520AS	0'-6.3	ANTIMONY	19.5		12	V	6.56	9.4	12.24	15.08	
	2746351	58393	BH50344AS	6' 12.7	ANTIMONY	15.8		12	JA	6.56	9.4	12.24	15.08	
	2746521	58493	BH50346AS	6' 12'	ANTIMONY	15.6		12	JA	6.56	9.4	12.24	15.08	
	2746524	58493	BH50346AS	6' 12'	CADMIUM	2.3		1	V	0.64	0.88	1.12	1.36	
	2633625	58593	BH50347AS	0'-6'	CADMIUM	2.2		1	JA	0.64	0.88	1.12	1.36	
	2700714	59493	BH50520AS	0' 6.3	COPPER	6920		5	V	12.59	25.36	38.13	50.9	
	2746528	58493	BH50346AS	6' 12	COPPER	749		5	V	12.59	25.36	38.13	50.9	
	2746358	58393	BH50344AS	6' 12.7	COPPER	361		5	V	12.59	25.36	38.13	50.9	
	2700456	59493	BH50521AS	6 9 12.9'	COPPER	117.35		5	V	12.59	25.36	38.13	50.9	
	2650831	58693	BH50417AS	6' 12'	COPPER	92		5	V	12.59	25.36	38.13	50.9	
	2746336	58393	BH50343AS	0'-6'	COPPER	73.5		5	V	12.59	25.36	38.13	50.9	
	2133927	50992	BH50138AS	0'-6'	COPPER	65.7		5	V	12.59	25.36	38.13	50.9	
	2746506	58493	BH50345AS	0'-6'	COPPER	59.1		5	V	12.59	25.36	38.13	50.9	
	2133972	50992	BH50140AS	0' 16'	COPPER	58		5	V	12.59	25.36	38.13	50.9	
	2746538	58493	BH50346AS	6' 12	MOLYBDENUM	190		40	V	15.39	24.4	33.41	42.42	
	2746362	58393	BH50344AS	6' 12.7	NICKEL	118		8	V	19.81	40.37	60.93	81.49	
	4880323	58494	BH00071AS	6 0-9.5	NICKEL	102		40	JA	19.81	40.37	60.93	81.49	
	2700718	59493	BH50520AS	0'-6.3	NICKEL	91.7		8	V	19.81	40.37	60.93	81.49	
	2746532	58493	BH50346AS	6' 12	NICKEL	91.2		8	V	19.81	40.37	60.93	81.49	
	2700850	63193	BH50618AS	12' 20'	NICKEL	84.9		8	V	19.81	40.37	60.93	81.49	
	2700720	59493	BH50520AS	0' 6.3'	SILVER	36		2	V	5.7	15.1	24.5	33.9	
133 1	2743661	56393	BH50212AS	2'-6'	ANTIMONY	33.2		12	JA	6.56	9.4	12.24	15.08	
	2743617	56393	BH50213AS	6-8	ANTIMONY	19.8		12	JA	6.56	9.4	12.24	15.08	
	4961491	57294	BH00091AS	0 0-4.0	BERYLLIUM	22.8		5	V	4.66	9.43	14.2	18.97	
	2743664	56393	BH50212AS	2'-6'	CADMIUM	56.9		1	V	0.64	0.88	1.12	1.36	
	4961493	57294	BH00091AS	0 0-4.0	CADMIUM	15.2		5	V	0.64	0.88	1.12	1.36	
	2743620	56393	BH50213AS	6-8"	CADMIUM	3.2		1	JA	0.64	0.88	1.12	1.36	
	2743642	56393	BH50211AS	0' 2'	CADMIUM	2		1	JA	0.64	0.88	1.12	1.36	
	2743668	56393	BH50212AS	2'-6'	COPPER	2920		5	V	12.59	25.36	38.13	50.9	
	4961497	57294	BH00091AS	0 0-4.0	COPPER	365		25	V	12.59	25.36	38.13	50.9	
	2743646	56393	BH50211AS	0' 2'	COPPER	158		5	V	12.59	25.36	38.13	50.9	
	2743624	56393	BH50213AS	6-8"	COPPER	83.6		5	V	12.59	25.36	38.13	50.9	
	4961504	57294	BH00091AS	0 0-4.0	MOLYBDENUM	470		200	V	15.39	24.4	33.41	42.42	
	2743674	56393	BH50212AS	2'-6'	SILVER	158		2	V	5.7	15.1	24.5	33.9	
	133 2	2463060	56893	BH50238AS	4 8.3	ANTIMONY	149		12	JA	6.56	9.4	12.24	15.08
		2686979	58793	BH50406AS	0'-6.1	ANTIMONY	24.2		12	JA	6.56	9.4	12.24	15.08
2687045		58793	BH50409AS	18' 24	ANTIMONY	21		12	JA	6.56	9.4	12.24	15.08	
2463062		56893	BH50238AS	4 8.3	BERYLLIUM	131		1	V	4.66	9.43	14.2	18.97	
2462717		56993	BH50201AS		CADMIUM	24.9		1	V	0.64	0.88	1.12	1.36	
2463063		56893	BH50238AS	4 8.3	CADMIUM	17.6		1	JA	0.64	0.88	1.12	1.36	
2463041		56893	BH50237AS	2-4	CADMIUM	2.6		1	JA	0.64	0.88	1.12	1.36	
2425178		56993	BH50202AS	8 1 14	CADMIUM	1.6		1	V	0.64	0.88	1.12	1.36	

Table 4 4 (Continued)

IHSS/Site	Sequence		Sample N	Depth Interval	Constituent	Result in mg/kg	Qualifier	Reporting		Mean (X STD DEV) f background	Mean	X	1	X=2	X=3
	ID	Locatio						Limit	Valid						
	2463067	56893	BH50238AS	4 8.3	COPPER	1380		5	V		12.59	25.36	38.13	50.9	
	2462721	56993	BH50201AS		COPPER	149		5	V		12.59	25.36	38.13	50.9	
	2463045	56893	BH50237AS	2-4	COPPER	64.1		5	V		12.59	25.36	38.13	50.9	
	2463077	56893	BH50238AS	4 8.3	MOLYBDENUM	129		40	V		15.39	24.4	33.41	42.42	
	2463071	56893	BH50238AS	4 8.3	NICKEL	4750		8	V		19.81	40.37	60.93	81.49	
	2463073	56893	BH50238AS	4 8.3	SILVER	190		2	V		5.7	15.1	24.5	33.9	
	2462727	56993	BH50201AS		SILVER	41.2		2	V		5.7	15.1	24.5	33.9	
133.3	2700342	61193	BH50503AS	6' 10'	CADMIUM	1.4		1	JA		0.64	0.88	1.12	1.36	
133.4	2703228	58993	BH50480AS	0' 6.4	ANTIMONY	51.5		12	JA		6.56	9.4	12.24	15.08	
	2743727	58093	BH50314AS	0'-8'	ANTIMONY	50.5		12	JA		6.56	9.4	12.24	15.08	
	3374234	59093	BH50667AS	0'-6'	ANTIMONY	33		12	JA		6.56	9.4	12.24	15.08	
	2462972	55993	BH50161AS	4' 9.3	ANTIMONY	28		12	JA		6.56	9.4	12.24	15.08	
	2462950	55993	BH50151AS	0'-6'	ANTIMONY	19.6		12	JA		6.56	9.4	12.24	15.08	
	2703310	58993	BH50482AS	6.4 12'	ANTIMONY	19.45		12	JA		6.56	9.4	12.24	15.08	
	2519083	55793	BH50308AS	6' 12'	ANTIMONY	16.4		12	JA		6.56	9.4	12.24	15.08	
	2462953	55993	BH50151AS	0'-6'	CADMIUM	42.3		1	V		0.64	0.88	1.12	1.36	
	2462975	55993	BH50161AS	4 9.3	CADMIUM	39.9		1	V		0.64	0.88	1.12	1.36	
	2743730	58093	BH50314AS	0'-8'	CADMIUM	26.7		1	V		0.64	0.88	1.12	1.36	
	5422759	55694	BH00041AS	0 0-6 0	CADMIUM	11.2	N	0.644	Y		0.64	0.88	1.12	1.36	
	2743686	58093	BH50315AS	10' 12'	CADMIUM	2.1		1	JA		0.64	0.88	1.12	1.36	
	2462931	55993	BH50162AS	0' 2'	CADMIUM	1.5		1	JA		0.64	0.88	1.12	1.36	
	5422762	55694	BH00042AS	6 0-10 6	CADMIUM	1.4	N	0.655	Y		0.64	0.88	1.12	1.36	
	5422783	55694	BH00041AS	0 0-6 0	COPPER	2520		0.43	Y		12.59	25.36	38.13	50.9	
	2462957	55993	BH50151AS	0'-6'	COPPER	957		5	V		12.59	25.36	38.13	50.9	
	2743734	58093	BH50314AS	0'-8'	COPPER	880		5	V		12.59	25.36	38.13	50.9	
	2462979	55993	BH50161AS	4 9.3	COPPER	755		5	V		12.59	25.36	38.13	50.9	
	5422786	55694	BH00042AS	6 0-10 6	COPPER	66.4		0.437	Y		12.59	25.36	38.13	50.9	
	2743738	58093	BH50314AS	0'-8'	NICKEL	115		8	V		19.81	40.37	60.93	81.49	
	2462983	55993	BH50161AS	4 9.3	NICKEL	93.2		8	V		19.81	40.37	60.93	81.49	
	2462985	55993	BH50161AS	4 9.3	SILVER	311		2	V		5.7	15.1	24.5	33.9	
	2743740	58093	BH50314AS	0'-8'	SILVER	106		2	V		5.7	15.1	24.5	33.9	
	2462963	55993	BH50151AS	0'-6'	SILVER	53.3		2	V		5.7	15.1	24.5	33.9	
	5422835	55694	BH00041AS	0 0-6 0	SILVER	50.7		0.644	Y		5.7	15.1	24.5	33.9	
133.5	2358296	55193	BH50099AS	6'-8'	COPPER	390		5	V		12.59	25.36	38.13	50.9	
142.11	1883223	50292	BH50008AS	0' 14.5'	CADMIUM	1.8		1	JA		0.64	0.88	1.12	1.36	
TDEM-1	5209212	55294	BH00033AS	12.0-15.2	NICKEL	355		40	JA		19.81	40.37	60.93	81.49	
TDEM-2	5372394	55994	BH00034AS	0 0-6 0	ANTIMONY	16.3	N	0.497	Y		6.56	9.4	12.24	15.08	
	5372409	55994	BH00034AS	0 0-6 0	BERYLLIUM	446		0.248	Y		4.66	9.43	14.2	18.97	
	5372414	55994	BH00034AS	0 0-6 0	CADMIUM	71		0.745	Y		0.64	0.88	1.12	1.36	
	5284171	56094	BH00037AS	0 0-6 0	CADMIUM	35.3		5	Y		0.64	0.88	1.12	1.36	
	5284199	56094	BH00038AS	6 0-12 0	CADMIUM	8.8		5	Y		0.64	0.88	1.12	1.36	
	5372417	55994	BH00035AS	6 0-11 2	CADMIUM	5.2		0.734	Y		0.64	0.88	1.12	1.36	
	5284255	56094	BH00040AS	18 0-22 0	CADMIUM	2.1		5	Y		0.64	0.88	1.12	1.36	
	5372438	55994	BH00034AS	0 0-6 0	COPPER	8850		0.745	Y		12.59	25.36	38.13	50.9	
	5284175	56094	BH00037AS	0 0-6 0	COPPER	1150		25	Y		12.59	25.36	38.13	50.9	
	5372441	55994	BH00035AS	6 0-11 2	COPPER	758		0.734	Y		12.59	25.36	38.13	50.9	
	5284203	56094	BH00038AS	6 0-12 0	COPPER	309		25	Y		12.59	25.36	38.13	50.9	
	5284259	56094	BH00040AS	18 0-22 0	COPPER	124		25	Y		12.59	25.36	38.13	50.9	
	5284231	56094	BH00039AS	12 0-18 0	COPPER	85		25	Y		12.59	25.36	38.13	50.9	
	5372471	55994	BH00034AS	0 0-6 0	MOLYBDENUM	65.1		3.72	Y		15.39	24.4	33.41	42.42	
	5372476	55994	BH00034AS	0 0-6 0	NICKEL	255	EN	2.98	Y		19.81	40.37	60.93	81.49	
	5284184	56094	BH00037AS	0 0-6 0	NICKEL	93		40	Y		19.81	40.37	60.93	81.49	
	5372495	55994	BH00034AS	0 0-6 0	SILVER	209	E	0.993	Y		5.7	15.1	24.5	33.9	
	5372498	55994	BH00035AS	6 0-11 2	SILVER	51.3	E	0.979	Y		5.7	15.1	24.5	33.9	

These data are graphically displayed Figures 4-4a and 4b.

Table 4 5
Summary of Radionuclide COCs Exceeding Background in Subsurface Soil

IHSS/S t	Seque	Location	Sample	Depth	Constituent	Result	Qualifier	Reporting	Valid.	Mean (X STD DEV) of background				
	ID		No.	Interval		PC/G		Limit		Mean	X = 1	X = 2	X = 3	
Exceeds th Background Mean but is less than Background Mean plus one Standard Deviation														
115/196	2262673	50992	BH50138AS	0'-6	U233234	1.7	B	0.005	A	0.779	1.711	2.643	3.575	
	2689770	58693	BH50349AS	12 19 5	U233234	1.645	B	0.021	A	0.779	1.711	2.643	3.575	
	2695013	58593	BH50347AS	0'-6	U233234	1.641		0.045962	V	0.779	1.711	2.643	3.575	
	2262631	50892	BH50123AS	8 16	U233234	1.6	B	0.02	A	0.779	1.711	2.643	3.575	
	5068976	57594	BH00082AS	60-120	U233234	1.51		0.03	Y	0.779	1.711	2.643	3.575	
	2262638	50892	BH50121AS	0'-6	U233234	1.5	B	0.016	A	0.779	1.711	2.643	3.575	
	2689784	58693	BH50405AS	25 5 29 5	U233234	1.5	B	0.01	A	0.779	1.711	2.643	3.575	
	3671054	59793	BH50486AS	13 3 15 3	U233234	1.4974		0.0304	Y	0.779	1.711	2.643	3.575	
	3671058	61293	BH50505AS	6' 10 6	U233234	1.4867		0.0544	Y	0.779	1.711	2.643	3.575	
	2695034	58593	BH50404AS	12.5 18 1	U233234	1.434		0.058313	V	0.779	1.711	2.643	3.575	
	3671536	61293	BH50508AS	0' 2	U233234	1.4322		0.0261	Y	0.779	1.711	2.643	3.575	
	2262659	50792	BH50105AS	0' 10	U233234	1.4	B	0.02	A	0.779	1.711	2.643	3.575	
	2642403	58393	BH50343AS	0'-6	U233234	1.4	B	0.015	A	0.779	1.711	2.643	3.575	
	3671214	59593	BH50554AS	14.4 16 4	U233234	1.3878		0.0177	Y	0.779	1.711	2.643	3.575	
	3671527	59593	BH50540AS	0' 2	U233234	1.3299		0.0209	Y	0.779	1.711	2.643	3.575	
	5069652	56694	BH00096AS	00-60	U233234	1.322		0.0157	V	0.779	1.711	2.643	3.575	
	5011953	56694	BH00122AS	43 0-150 0	U233234	1.32		0.0251	V	0.779	1.711	2.643	3.575	
	2262694	50692	BH50087AS	0'-6	U233234	1.3	B	0.016	A	0.779	1.711	2.643	3.575	
	2253001	50692	BH50088AS	6' 12	U233234	1.3		0.013	A	0.779	1.711	2.643	3.575	
	2262687	50992	BH50140AS	0' 16	U233234	1.3	B	0.044	A	0.779	1.711	2.643	3.575	
	5069644	56694	BH00095AS	00-60	U233234	1.286		0.0179	V	0.779	1.711	2.643	3.575	
	3671043	59293	BH50441AS	12' 18 9	U233234	1.2769		0.0212	Y	0.779	1.711	2.643	3.575	
	3671042	59293	BH50440AS	6' 12	U233234	1.2688		0.0227	Y	0.779	1.711	2.643	3.575	
	3671409	63193	BH50617AS	6' 12	U233234	1.254		0.0391	Y	0.779	1.711	2.643	3.575	
	2695027	58593	BH50403AS	6' 12.5	U233234	1.252		0.084029	V	0.779	1.711	2.643	3.575	
	3671406	60993	BH50588AS	0'-6	U233234	1.2378		0.0216	Y	0.779	1.711	2.643	3.575	
	2262680	50992	BH50139AS	6' 12	U233234	1.2	B	0.027	A	0.779	1.711	2.643	3.575	
	3671407	61093	BH50603AS	6' 13	U233234	1.1888		0.0465	Y	0.779	1.711	2.643	3.575	
	3671211	59593	BH50552AS	0'-6	U233234	1.18155		0.022	Y	0.779	1.711	2.643	3.575	
	3671533	58693	BH50644AS	0' 2	U233234	1.1507		0.0243	Y	0.779	1.711	2.643	3.575	
	3671210	59493	BH50522AS	12.9' 17 8	U233234	1.1312		0.0222	Y	0.779	1.711	2.643	3.575	
	5069636	56694	BH00111AS	00-35 0	U233234	1.118		0.0178	V	0.779	1.711	2.643	3.575	
	5011945	56694	BH00113AS	43 0-150 0	U233234	1.108		0.0465	V	0.779	1.711	2.643	3.575	
	2252994	50592	BH50066AS	0' 32	U233234	1.1		0.015	A	0.779	1.711	2.643	3.575	
	5017732	57594	BH00121AS	24 0-105 0	U233234	1.098		0.0164	V	0.779	1.711	2.643	3.575	
	5186001	59494	BH00152AS	00-5 9	U233234	1.094		0.0241	V	0.779	1.711	2.643	3.575	
	3671535	59293	BH50444AS	0' 2	U233234	1.089		0.0363	Y	0.779	1.711	2.643	3.575	
	3671041	59293	BH50439AS	0'-6	U233234	1.0885		0.028	Y	0.779	1.711	2.643	3.575	
	5012726	57594	BH00085AS	18 0-23 0	U233234	1.087		0.0143	V	0.779	1.711	2.643	3.575	
	3671052	59793	BH50484AS	0' 7 3	U233234	1.0815		0.0257	Y	0.779	1.711	2.643	3.575	
	3671206	59193	BH50457AS	2' 8	U233234	1.07715		0.0234	Y	0.779	1.711	2.643	3.575	
	5186041	59894	BH00164AS	19.9-31.9	U233234	1.074		0.0166	V	0.779	1.711	2.643	3.575	
	3671408	63193	BH50616AS	0'-6	U233234	1.074		0.0221	Y	0.779	1.711	2.643	3.575	
	5069668	56694	BH00112AS	00-41 0	U233234	1.073		0.0216	V	0.779	1.711	2.643	3.575	
	3671047	59393	BH50477AS	6' 8	U233234	1.0705		0.0179	Y	0.779	1.711	2.643	3.575	
	3671053	59793	BH50485AS	5.3 11 3	U233234	1.0659		0.0257	Y	0.779	1.711	2.643	3.575	
	5069660	56694	BH00098AS	60-100	U233234	1.063		0.0139	V	0.779	1.711	2.643	3.575	
	3671537	59793	BH50488AS	0' 2	U233234	1.0586		0.0569	Y	0.779	1.711	2.643	3.575	
	3671410	63193	BH50618AS	12 20	U233234	1.0381		0.0352	Y	0.779	1.711	2.643	3.575	
	3671525	58593	BH50427AS	0' 2	U233234	1.0261		0.0543	Y	0.779	1.711	2.643	3.575	
3671531	59493	BH50524AS	4 2	U233234	1.0234		0.022	Y	0.779	1.711	2.643	3.575		
3671046	59393	BH50476AS	0'-6	U233234	1.0051		0.0233	Y	0.779	1.711	2.643	3.575		
5112058	58294	BH00050AS	00-40	U233234	1.005		0.0244	V	0.779	1.711	2.643	3.575		
2252987	50692	BH50089AS	0' 14	U233234	1		0.046	A	0.779	1.711	2.643	3.575		
2262652	50792	BH50104AS	0'-6	U233234	1	B	0.012	A	0.779	1.711	2.643	3.575		
4954843	58294	BH00050AS	00-40	U233234	0.9946		0.0452	V	0.779	1.711	2.643	3.575		
2253015	50392	BH50016AS	25 30	U233234	0.98		0.026	A	0.779	1.711	2.643	3.575		
5112050	57994	BH00047AS	00-6.3	U233234	0.9612		0.0174	V	0.779	1.711	2.643	3.575		
2642382	58693	BH50417AS	6' 12	U233234	0.96	B	0.042	A	0.779	1.711	2.643	3.575		
3671524	59393	BH50465AS	0' 2	U233234	0.9536		0.0262	Y	0.779	1.711	2.643	3.575		
2253022	50392	BH50015AS	18 24	U233234	0.91		0.015	A	0.779	1.711	2.643	3.575		
5185985	57094	BH00147AS	00-40 0	U233234	0.8814		0.0328	V	0.779	1.711	2.643	3.575		
5068968	58494	BH00071AS	60-9.5	U233234	0.87		0.02	Y	0.779	1.711	2.643	3.575		
2425815	51092	BH50153AS	0'-6	U233234	0.84		0.1	A	0.779	1.711	2.643	3.575		

Table 4-5 (Continued)

IHSS/S t	Sequence		Sample No.	Depth Interval	Constituent	Result PCI/G	Qualifier	Reporting		Mean + (X STD DEV) of background			
	ID	Location						Limit	Valid	Mean	X 1	X=2	X=3
	5068975	57594	BH00078AS	0-6-0	U233234	0.82		0.02	Y	0.779	1.711	2.643	3.575
	5112074	58794	BH00054AS	0-0-2.4	U233234	0.8117		0.0227	V	0.779	1.711	2.643	3.575
	2425823	51092	BH50154AS	0' 12	U233234	0.81		0.04	A	0.779	1.711	2.643	3.575
	4954842	57994	BH00047AS	0-0-6.3	U233234	0.7816		0.0312	V	0.779	1.711	2.643	3.575
	2262602	50492	BH50037AS	0'-6'	U235	0.068	J	0.033	A	0.022	0.068	0.114	0.16
	3671543	58593	BH50427AS	0' 2	U235	0.0662		0.0305	Y	0.022	0.068	0.114	0.16
	2642374	58693	BH50348AS	0-6	U235	0.066	J	0.039	A	0.022	0.068	0.114	0.16
	2262686	50992	BH50140AS	0' 16	U235	0.064	J	0.028	A	0.022	0.068	0.114	0.16
	2695035	58593	BH50404AS	12.5 18.1	U235	0.0638		0.048526	V	0.022	0.068	0.114	0.16
	3671078	59793	BH50486AS	13.3 15.3	U235	0.0632		0.0186	Y	0.022	0.068	0.114	0.16
	3671551	58693	BH50644AS	0' 2	U235	0.0627		0.0243	Y	0.022	0.068	0.114	0.16
	3671415	61093	BH50603AS	6 13	U235	0.0626		0.0243	Y	0.022	0.068	0.114	0.16
	3671234	59493	BH50522AS	12.9 17.8	U235	0.0622		0.0176	Y	0.022	0.068	0.114	0.16
	2253056	50592	BH50063AS	6' 12	U235	0.061	J	0.022	A	0.022	0.068	0.114	0.16
	5068984	58494	BH00068AS	0-0-6.0	U235	0.06		0.01	Y	0.022	0.068	0.114	0.16
	2253035	50392	BH50013AS	6' 12	U235	0.058	J	0.028	A	0.022	0.068	0.114	0.16
	5069653	56694	BH00096AS	0-0-6.0	U235	0.05681		0.0179	V	0.022	0.068	0.114	0.16
	2252993	50592	BH50066AS	0' 32	U235	0.055	J	0.015	A	0.022	0.068	0.114	0.16
	3335594	58393	BH50418AS	19.5 21.5	U235	0.054	U	0.2	A	0.022	0.068	0.114	0.16
	5017733	57594	BH00121AS	24.0-105.0	U235	0.05395		0.0124	V	0.022	0.068	0.114	0.16
	5186042	59894	BH00164AS	19.9-31.9	U235	0.05001		0.0202	V	0.022	0.068	0.114	0.16
	2642402	58393	BH50343AS	0'-6'	U235	0.05	J	0.04	A	0.022	0.068	0.114	0.16
	3671416	63193	BH50616AS	0'-6'	U235	0.0499		0.0175	Y	0.022	0.068	0.114	0.16
	3671235	59593	BH50552AS	0'-6'	U235	0.04975		0.0174	Y	0.022	0.068	0.114	0.16
	5011954	56694	BH00122AS	43.0-150.0	U235	0.04971		0.0215	V	0.022	0.068	0.114	0.16
	5185994	57094	BH00148AS	0-0-40.0	U235	0.0494		0.0464	V	0.022	0.068	0.114	0.16
	5112075	58794	BH00054AS	0-0-2.4	U235	0.04938		0.0227	V	0.022	0.068	0.114	0.16
	4954855	58694	BH00052AS	0-0-2.9	U235	0.0491		0.0201	A	0.022	0.068	0.114	0.16
	3671555	59793	BH50488AS	0' 2	U235	0.0477		0.032	Y	0.022	0.068	0.114	0.16
	2262644	50892	BH50122AS	6' 12	U235	0.047	J	0.02	A	0.022	0.068	0.114	0.16
	3671067	59293	BH50441AS	12' 18.9'	U235	0.0462		0.0213	Y	0.022	0.068	0.114	0.16
	2253042	50392	BH50012AS	0'-4.5	U235	0.046	J	0.013	A	0.022	0.068	0.114	0.16
	3671549	59493	BH50524AS	4 2	U235	0.0449		0.0221	Y	0.022	0.068	0.114	0.16
	5069669	56694	BH00112AS	0-0-41.0	U235	0.0427		0.0175	V	0.022	0.068	0.114	0.16
	2642381	58693	BH50417AS	6' 12	U235	0.041	J	0.02	A	0.022	0.068	0.114	0.16
	5012727	57594	BH00085AS	18.0-23.0	U235	0.04041		0.0186	V	0.022	0.068	0.114	0.16
	5068993	57594	BH00082AS	6.0-12.0	U235	0.04		0.02	Y	0.022	0.068	0.114	0.16
	5011946	56694	BH00113AS	43.0-150.0	U235	0.03948		0.0293	V	0.022	0.068	0.114	0.16
	4954856	58794	BH00054AS	0-0-2.4	U235	0.038		0.0349	A	0.022	0.068	0.114	0.16
	2425816	51092	BH50153AS	0'-6'	U235	0.037	U	0.1	A	0.022	0.068	0.114	0.16
	5186026	59494	BH00160AS	11.9-17.9	U235	0.03697		0.0119	V	0.022	0.068	0.114	0.16
	5112051	57994	BH00047AS	0-0-6.3	U235	0.0369		0.0226	V	0.022	0.068	0.114	0.16
	3671542	59393	BH50465AS	0' 2	U235	0.0367		0.0208	Y	0.022	0.068	0.114	0.16
	3671071	59393	BH50477AS	6 8	U235	0.0365		0.0179	Y	0.022	0.068	0.114	0.16
	5069645	56694	BH00095AS	0-0-6.0	U235	0.03605		0.0251	V	0.022	0.068	0.114	0.16
	5185986	57094	BH00147AS	0-0-40.0	U235	0.03358	J	0.0383	V	0.022	0.068	0.114	0.16
	3671230	59193	BH50457AS	2 8	U235	0.0324		0.016	Y	0.022	0.068	0.114	0.16
	5069637	56694	BH00111AS	0-0-35.0	U235	0.03215		0.0178	V	0.022	0.068	0.114	0.16
	2262679	50992	BH50139AS	6' 12	U235	0.032	J	0.027	A	0.022	0.068	0.114	0.16
	2262609	50492	BH50038AS	6' 12	U235	0.031	J	0.024	A	0.022	0.068	0.114	0.16
	2425824	51092	BH50154AS	0' 12	U235	0.029	J	0.02	A	0.022	0.068	0.114	0.16
	5186034	59894	BH00162AS	17.9-19.9	U235	0.02872		0.0203	V	0.022	0.068	0.114	0.16
	3671553	59293	BH50444AS	0' 2	U235	0.0283		0.019	Y	0.022	0.068	0.114	0.16
	2253000	50692	BH50088AS	6' 12	U235	0.028	J	0.021	A	0.022	0.068	0.114	0.16
	5012735	57594	BH00086AS	24.0-60.0	U235	0.02745		0.023	V	0.022	0.068	0.114	0.16
	2262616	50492	BH50039AS	12 18	U235	0.027	U	0.034	A	0.022	0.068	0.114	0.16
	4954854	58294	BH00050AS	0-0-4.0	U235	0.0264		0.0277	V	0.022	0.068	0.114	0.16
	5186018	59494	BH00159AS	11.9-17.9	U235	0.02591		0.00701	V	0.022	0.068	0.114	0.16
	2695028	58593	BH50403AS	6' 12.5	U235	0.02501	J	0.062254	V	0.022	0.068	0.114	0.16
	3671066	59293	BH50440AS	6 12	U235	0.0247		0.0228	Y	0.022	0.068	0.114	0.16
	5069661	56694	BH00098AS	6.0-10.0	U235	0.02267		0.0169	V	0.022	0.068	0.114	0.16
	3671089	59293	BH50439AS	0'-6'	U238	1.1067		0.0242	Y	0.733	1.109	1.485	1.861
	2262650	50792	BH50104AS	0'-6'	U238	1.1	B	0.005	A	0.733	1.109	1.485	1.861
	2262678	50992	BH50139AS	6' 12	U238	1.1	B	0.027	A	0.733	1.109	1.485	1.861
	3335595	58393	BH50418AS	19.5 21.5	U238	1.1		0.2	A	0.733	1.109	1.485	1.861

Table 4-5 (Continued)

IHSS/S t	Seque ce		Sample No.	Depth Interval	Constituent	Result in PCI/G	Qualifier	Reporting		Valid	Mean + (X STD DEV) of background			
	ID	Locatio						Limit			Mean	X=1	X=2	X=3
	3671254	59193	BH50457AS	2' 8	U238	1 0743		0 016		Y	0 733	1 109	1 485	1 861
	5185995	57094	BH00148AS	0 0-40 0	U238	1 05		0 0464		V	0 733	1 109	1 485	1 861
	3671091	59293	BH50441AS	12' 18 9	U238	1 0343		0 0213		Y	0 733	1 109	1 485	1 861
	4954865	58294	BH00050AS	0 0-4 0	U238	1 0285		0 0277		V	0 733	1 109	1 485	1 861
	5112060	58294	BH00050AS	0 0-4 0	U238	1 026		0 016		V	0 733	1 109	1 485	1 861
	5011947	56694	BH00113AS	43 0-150 0	U238	1 024		0 0357		V	0 733	1 109	1 485	1 861
	5017734	57594	BH00121AS	24 0-105 0	U238	1 006		0 00702		V	0 733	1 109	1 485	1 861
	5185987	57094	BH00147AS	0 0-40 0	U238	1 003		0 0328		V	0 733	1 109	1 485	1 861
	5186043	59894	BH00164AS	19 9-31 9	U238	1 003		0 0286		V	0 733	1 109	1 485	1 861
	2253013	50392	BH50016AS	25 30	U238	1	B	0 016		A	0 733	1 109	1 485	1 861
	2262615	50492	BH50039AS	12 18	U238	1	B	0 022		A	0 733	1 109	1 485	1 861
	3671101	59793	BH50485AS	5 3 11 3	U238	0 99695		0 0204		Y	0 733	1 109	1 485	1 861
	3671258	59493	BH50522AS	12 9' 17 8	U238	0 9901		0 0176		Y	0 733	1 109	1 485	1 861
	3671426	63193	BH50618AS	12 20	U238	0 9872		0 0198		Y	0 733	1 109	1 485	1 861
	3671561	58593	BH50427AS	0' 2	U238	0 9806		0 0305		Y	0 733	1 109	1 485	1 861
	3671560	59393	BH50465AS	0' 2	U238	0 9621		0 0208		Y	0 733	1 109	1 485	1 861
	3671094	59393	BH50476AS	0' 6	U238	0 9601		0 0185		Y	0 733	1 109	1 485	1 861
	2253048	50592	BH50062AS	0' 6	U238	0 96	B	0 024		A	0 733	1 109	1 485	1 861
	2253062	50592	BH50064AS	12 18	U238	0 96	B	0 019		A	0 733	1 109	1 485	1 861
	5069662	56694	BH00098AS	6 0-10 0	U238	0 9555		0 0118		V	0 733	1 109	1 485	1 861
	2262622	50492	BH50040AS	18 24	U238	0 94	B	0 011		A	0 733	1 109	1 485	1 861
	5069000	58494	BH00071AS	6 0-9 5	U238	0 91		0 02		Y	0 733	1 109	1 485	1 861
	5112052	57994	BH00047AS	0 0-6 3	U238	0 8997		0 0174		V	0 733	1 109	1 485	1 861
	2425825	51092	BH50154AS	0' 12	U238	0 87		0 02		A	0 733	1 109	1 485	1 861
	3671100	59793	BH50484AS	0' 7 3	U238	0 868		0 0204		Y	0 733	1 109	1 485	1 861
	2253069	50592	BH50065AS	18 24	U238	0 86	B	0 009		A	0 733	1 109	1 485	1 861
	2425817	51092	BH50153AS	0' 6	U238	0 86		0 1		A	0 733	1 109	1 485	1 861
	3671095	59393	BH50477AS	6' 8	U238	0 854		0 0179		Y	0 733	1 109	1 485	1 861
	2253076	50492	BH50041AS	30' 38	U238	0 84	B	0 013		A	0 733	1 109	1 485	1 861
	5112076	58794	BH00054AS	0 0-2 4	U238	0 8314		0 0195		V	0 733	1 109	1 485	1 861
	5186011	59494	BH00155AS	5 9-11 9	U238	0 8124		0 0187		V	0 733	1 109	1 485	1 861
	4954866	58694	BH00052AS	0 0-2 9	U238	0 8072		0 0201		A	0 733	1 109	1 485	1 861
	4954867	58794	BH00054AS	0 0-2 4	U238	0 8068		0 0349		A	0 733	1 109	1 485	1 861
	2262601	50492	BH50037AS	0' 6	U238	0 8	B	0 033		A	0 733	1 109	1 485	1 861
	5069007	57594	BH00078AS	0 0-6 0	U238	0 8		0 01		Y	0 733	1 109	1 485	1 861
	2253041	50392	BH50012AS	0' 4 5	U238	0 79	B	0 013		A	0 733	1 109	1 485	1 861
	5068999	58494	BH00068AS	0 0-6 0	U238	0 79		0 01		Y	0 733	1 109	1 485	1 861
	2262608	50492	BH50038AS	6' 12	U238	0 76	B	0 014		A	0 733	1 109	1 485	1 861
	5112068	58694	BH00052AS	0 0-2 9	U238	0 7421		0 0265		V	0 733	1 109	1 485	1 861
	5186035	59894	BH00162AS	17 9-19 9	U238	0 7367		0 0309		V	0 733	1 109	1 485	1 861
133 1	2550476	56493	BH50219AS	0' 6	U233234	1 5	B	0 017		A	0 779	1 711	2 643	3 575
	2525792	56293	BH50206AS	0' 6	U233234	1 441		0 052		A	0 779	1 711	2 643	3 575
	2439080	56193	BH50176AS	0' 2	U233234	1 1	B	0 011		A	0 779	1 711	2 643	3 575
	2439108	56193	BH50304AS	18 25	U233234	1	B	0 01		A	0 779	1 711	2 643	3 575
	2550469	56493	BH50220AS	0' 2	U233234	0 95	B	0 019		A	0 779	1 711	2 643	3 575
	2525785	56293	BH50210AS	0' 2	U233234	0 9302		0 037		A	0 779	1 711	2 643	3 575
	3671045	58893	BH50459AS	6' 12	U233234	0 9009		0 024		Y	0 779	1 711	2 643	3 575
	2439087	56193	BH50177AS	0' 6	U233234	0 89	B	0 021		A	0 779	1 711	2 643	3 575
	3335579	58893	BH50646AS	0' 2	U233234	0 88		0 2		A	0 779	1 711	2 643	3 575
	2439094	56193	BH50178AS	6' 11 4	U233234	0 8	B	0 013		A	0 779	1 711	2 643	3 575
	2439101	56193	BH50303AS	12 18	U233234	0 79	B	0 017		A	0 779	1 711	2 643	3 575
	2550468	56493	BH50220AS	0' 2	U235	0 068	J	0 019		A	0 022	0 068	0 114	0 16
	2439079	56193	BH50176AS	0' 2	U235	0 054	J	0 011		A	0 022	0 068	0 114	0 16
	3671068	58893	BH50458AS	0' 6	U235	0 0366		0 0207		Y	0 022	0 068	0 114	0 16
	2525800	56293	BH50207AS	6' 10	U235	0 03042	J	0 043		A	0 022	0 068	0 114	0 16
	3671069	58893	BH50459AS	6' 12	U235	0 0223		0 0164		Y	0 022	0 068	0 114	0 16
	2525801	56293	BH50207AS	6' 10'	U238	1 1085		0 057		A	0 733	1 109	1 485	1 861
	2439085	56193	BH50177AS	0' 6'	U238	1 1	B	0 021		A	0 733	1 109	1 485	1 861
	2439106	56193	BH50304AS	18 25	U238	1 1	B	0 01		A	0 733	1 109	1 485	1 861
	2439092	56193	BH50178AS	6' 11 4	U238	1 1	B	0 022		A	0 733	1 109	1 485	1 861
	3335581	58893	BH50646AS	0' 2	U238	0 97		0 2		A	0 733	1 109	1 485	1 861
	2439099	56193	BH50303AS	12 18	U238	0 91	B	0 053		A	0 733	1 109	1 485	1 861
	2550460	56193	BH50305AS	23 30	U238	0 82	B	0 015		A	0 733	1 109	1 485	1 861
133.2	2625468	57193	BH50246AS	0' 2	U233234	1 625		0 116367		A	0 779	1 711	2 643	3 575
	2522237	57293	BH50251AS	0' 2	U233234	1 6	B	0 013		A	0 779	1 711	2 643	3 575

Table 4 5 (Continued)

IHSS/S t	Sequen	Locatio	Sampl	Depth	Result	PCI/G	Qualifier	Reporting	Valid	Mean + (X STD DEV) of background			
	ID		No.					Interval		Constituent	Limit	Mean	X = 1
	2522258	57293	BH50254AS	12 18	U233234	16	B	0017	A	0.779	1.711	2.643	3.575
	2550609	57493	BH50261AS	0' 2	U233234	15	B	0014	A	0.779	1.711	2.643	3.575
	2625475	57193	BH50247AS	0' 5.5	U233234	1.499		0066429	A	0.779	1.711	2.643	3.575
	2467547	56993	BH50202AS	8.1 14	U233234	1.48		0033	V	0.779	1.711	2.643	3.575
	2522286	57393	BH50257AS	0'-6.6	U233234	14	B	0029	A	0.779	1.711	2.643	3.575
	2522307	57393	BH50260AS	16.1 24.1	U233234	14	B	0012	A	0.779	1.711	2.643	3.575
	2522314	57393	BH50291AS	22.1 26.1	U233234	14	B	0014	A	0.779	1.711	2.643	3.575
	2522293	57393	BH50258AS	4.6 12.1	U233234	14	B	0013	A	0.779	1.711	2.643	3.575
	3670886	58793	BH50406AS	0'-6.1	U233234	1.3926		00284	Y	0.779	1.711	2.643	3.575
	2465693	57593	BH50299AS	0'-6	U233234	13	B	0047	A	0.779	1.711	2.643	3.575
	2522265	57293	BH50255AS	20' 26	U233234	1.2	B	0022	A	0.779	1.711	2.643	3.575
	2550616	57493	BH50262AS	0'-6	U233234	12	B	0039	A	0.779	1.711	2.643	3.575
	2467542	57093	BH50242AS	0'-6	U233234	1.18		0	V	0.779	1.711	2.643	3.575
	3671538	58793	BH50645AS	0' 2	U233234	1.1409		00314	Y	0.779	1.711	2.643	3.575
	3670887	58793	BH50407AS	6.1 12	U233234	1.1229		00285	Y	0.779	1.711	2.643	3.575
	2467543	57093	BH50241AS	0' 2	U233234	1.11		0013	V	0.779	1.711	2.643	3.575
	2625489	57193	BH50250AS	7 13	U233234	1.107		0096004	A	0.779	1.711	2.643	3.575
	2522300	57393	BH50259AS	10.2 18.1	U233234	1.1	B	0014	A	0.779	1.711	2.643	3.575
	2550455	57493	BH50265AS	18 20	U233234	1.1	B	0017	A	0.779	1.711	2.643	3.575
	2465686	57593	BH50298AS	0' 2	U233234	1.1	B	0041	A	0.779	1.711	2.643	3.575
	2465714	57593	BH50301AS	12 14	U233234	1.1	B	001	A	0.779	1.711	2.643	3.575
	2465700	57593	BH50300AS	6' 12	U233234	1.1	B	0014	A	0.779	1.711	2.643	3.575
	2624779	56893	BH50236AS	0' 2	U233234	1.077		0049377	A	0.779	1.711	2.643	3.575
	2525820	56893	BH50240AS	14.3 20.3	U233234	1.02595		0044	A	0.779	1.711	2.643	3.575
	3670889	58793	BH50409AS	18 24	U233234	1.009		00285	Y	0.779	1.711	2.643	3.575
	2522279	57393	BH50256AS	0' 2	U233234	1	B	0012	A	0.779	1.711	2.643	3.575
	3670890	58793	BH50410AS	24 28.4	U233234	0.9837		00178	Y	0.779	1.711	2.643	3.575
	3670888	58793	BH50408AS	12 18	U233234	0.9751		00176	Y	0.779	1.711	2.643	3.575
	2465707	57593	BH50294AS	6' 12	U233234	0.97	B	0014	A	0.779	1.711	2.643	3.575
	2467541	57093	BH50243AS	6' 12.3	U233234	0.956		0014	V	0.779	1.711	2.643	3.575
	2467546	56993	BH50199AS	0'-4	U233234	0.932		0026	A	0.779	1.711	2.643	3.575
	2525813	56893	BH50239AS	8.3 14.3	U233234	0.9233		0046	A	0.779	1.711	2.643	3.575
	2467537	57093	BH50276AS	30.7' 36.1	U233234	0.803		0013	V	0.779	1.711	2.643	3.575
	2467506	56993	BH50202AS	8.1 14	U235	0.0641		0023	V	0.022	0.068	0.114	0.16
	2465706	57593	BH50294AS	6' 12	U235	0.061	J	0036	A	0.022	0.068	0.114	0.16
	2522236	57293	BH50251AS	0' 2	U235	0.06	BJ	0022	A	0.022	0.068	0.114	0.16
	2467514	57093	BH50245AS	18.6 24	U235	0.0524		0013	V	0.022	0.068	0.114	0.16
	2467507	56993	BH50204AS	20.7' 26.7'	U235	0.0502		0	V	0.022	0.068	0.114	0.16
	2467515	57093	BH50243AS	6' 12.3	U235	0.0481		0	V	0.022	0.068	0.114	0.16
	2525821	56893	BH50240AS	14.3 20.3	U235	0.046647		0044	A	0.022	0.068	0.114	0.16
	2625476	57193	BH50247AS	0' 5.5	U235	0.04503	J	0068914	A	0.022	0.068	0.114	0.16
	3670913	58793	BH50409AS	18 24	U235	0.045		00195	Y	0.022	0.068	0.114	0.16
	2522250	57293	BH50253AS	6' 12	U235	0.044	BJ	0012	A	0.022	0.068	0.114	0.16
	3671556	58793	BH50645AS	0' 2	U235	0.044		0025	Y	0.022	0.068	0.114	0.16
	3670912	58793	BH50408AS	12 18	U235	0.0431		00177	Y	0.022	0.068	0.114	0.16
	2522264	57293	BH50255AS	20 26	U235	0.042	BJ	0034	A	0.022	0.068	0.114	0.16
	3670911	58793	BH50407AS	6.1 12	U235	0.0389		00195	Y	0.022	0.068	0.114	0.16
	2467517	56993	BH50203AS	14.3 20.7	U235	0.0374		0	V	0.022	0.068	0.114	0.16
	2467504	56993	BH50198AS	0' 2	U235	0.0367		0	V	0.022	0.068	0.114	0.16
	2522299	57393	BH50259AS	10.2 18.1	U235	0.034	BJ	0014	A	0.022	0.068	0.114	0.16
	2550608	57493	BH50261AS	0' 2	U235	0.034	J	0014	A	0.022	0.068	0.114	0.16
	2467513	57093	BH50276AS	30.7' 36.1	U235	0.0334		0013	V	0.022	0.068	0.114	0.16
	3670910	58793	BH50406AS	0'-6.1	U235	0.0317		00194	Y	0.022	0.068	0.114	0.16
	3670914	58793	BH50410AS	24 28.4	U235	0.0291		00179	Y	0.022	0.068	0.114	0.16
	2522278	57393	BH50256AS	0' 2	U235	0.029	BJ	0012	A	0.022	0.068	0.114	0.16
	2465699	57593	BH50300AS	6' 12	U235	0.028	U	0044	A	0.022	0.068	0.114	0.16
	2467510	57093	BH50275AS	24 30.7	U235	0.0279		0	V	0.022	0.068	0.114	0.16
	2550628	57493	BH50264AS	12 18	U238	1.1	B	0016	A	0.733	1.109	1.485	1.861
	2467564	57093	BH50241AS	0' 2	U238	1.03		0	V	0.733	1.109	1.485	1.861
	2550614	57493	BH50262AS	0'-6	U238	1	B	0071	A	0.733	1.109	1.485	1.861
	2465712	57593	BH50301AS	12 14	U238	1	B	001	A	0.733	1.109	1.485	1.861
	2465684	57593	BH50298AS	0' 2	U238	0.98	B	0016	A	0.733	1.109	1.485	1.861
	2522277	57393	BH50256AS	0' 2	U238	0.97	B	0012	A	0.733	1.109	1.485	1.861
	2525822	56893	BH50240AS	14.3 20.3	U238	0.96475		0057	A	0.733	1.109	1.485	1.861
	3670936	58793	BH50408AS	12 18	U238	0.9464		00223	Y	0.733	1.109	1.485	1.861

Table 4-5 (Continued)

IHSS/S t	Sequence		Sample No	Depth		Result	Qualifier	Reporting		Valid	Mean (X STD DEV) of background			
	ID	Location		Interval	Constituent	PC/G		Limit	Mean		X = 1	X = 2	X = 3	
133.3	3670938	58793	BH50410AS	24' 28.4	U238	0.9037		0.0179	Y		0.733	1.109	1.485	1.861
	2550621	57493	BH50263AS	6' 12	U238	0.82	B	0.024	A		0.733	1.109	1.485	1.861
	2467549	56993	BH50198AS	0' 2	U238	0.779		0.014	V		0.733	1.109	1.485	1.861
	2439129	56593	BH50221AS	0' 2	U233234	1.6	B	0.06	A		0.779	1.711	2.643	3.575
	3671220	63093	BH50559AS	15' 20	U233234	1.5392		0.0478	Y		0.779	1.711	2.643	3.575
	2439115	56693	BH50226AS	0' 2	U233234	1.4	B	0.011	A		0.779	1.711	2.643	3.575
	3671215	59693	BH50556AS	0' 6	U233234	1.3268		0.0245	Y		0.779	1.711	2.643	3.575
	2550490	56793	BH50233AS	6' 12	U233234	1.3	B	0.027	A		0.779	1.711	2.643	3.575
	3671218	59693	BH50557AS	6' 12	U233234	1.2384		0.0282	Y		0.779	1.711	2.643	3.575
	2439143	56593	BH50223AS	6' 12	U233234	1.2	B	0.11	A		0.779	1.711	2.643	3.575
	2439122	56693	BH50227AS	0' 6	U233234	1.2	B	0.035	A		0.779	1.711	2.643	3.575
	2439136	56593	BH50222AS	0' 6	U233234	1.1	B	0.011	A		0.779	1.711	2.643	3.575
	3335586	61393	BH50650AS	0' 2	U233234	1		0.1	A		0.779	1.711	2.643	3.575
	3671224	61493	BH50583AS	0' 8.5	U233234	0.9959		0.0291	Y		0.779	1.711	2.643	3.575
	2550504	56793	BH50232AS	0' 6	U233234	0.99	B	0.016	A		0.779	1.711	2.643	3.575
	3671221	61393	BH50570AS	0' 6	U233234	0.98865		0.0219	Y		0.779	1.711	2.643	3.575
	3671222	61393	BH50576AS	0' 10	U233234	0.9853		0.0178	Y		0.779	1.711	2.643	3.575
	3335607	61493	BH50651AS	0' 2	U233234	0.93		0.2	A		0.779	1.711	2.643	3.575
	3671056	61193	BH50503AS	6' 10	U233234	0.89635		0.0165	Y		0.779	1.711	2.643	3.575
	2625482	56593	BH50224AS	13' 17	U233234	0.8024		0.062641	A		0.779	1.711	2.643	3.575
	3671225	61493	BH50585AS	8.5' 15.9'	U233234	0.7885		0.0259	Y		0.779	1.711	2.643	3.575
	2550503	56793	BH50232AS	0' 6	U235	0.058	J	0.016	A		0.022	0.068	0.114	0.16
	3671239	59693	BH50556AS	0' 6	U235	0.0547		0.0195	Y		0.022	0.068	0.114	0.16
	3671249	61493	BH50585AS	8.5' 15.9	U235	0.0529		0.0205	Y		0.022	0.068	0.114	0.16
	3671245	61393	BH50570AS	0' 6	U235	0.0496		0.0174	Y		0.022	0.068	0.114	0.16
	3671248	61493	BH50583AS	0' 8.5	U235	0.04935		0.0179	Y		0.022	0.068	0.114	0.16
	2439121	56693	BH50227AS	0' 6	U235	0.048	J	0.013	A		0.022	0.068	0.114	0.16
	3671080	61193	BH50503AS	6' 10	U235	0.0438		0.0165	Y		0.022	0.068	0.114	0.16
	3671250	61493	BH50584AS	5.5' 13.5	U235	0.0399		0.0206	Y		0.022	0.068	0.114	0.16
	3671243	59693	BH50558AS	12' 15.5	U235	0.0388		0.0226	Y		0.022	0.068	0.114	0.16
	3671244	63093	BH50559AS	15' 20'	U235	0.03265		0.0293	Y		0.022	0.068	0.114	0.16
	2550486	56793	BH50234AS	10' 12	U235	0.03	J	0.023	A		0.022	0.068	0.114	0.16
	2625483	56593	BH50224AS	13' 17'	U235	0.02713	J	0.066717	A		0.022	0.068	0.114	0.16
133.4	3335588	61393	BH50650AS	0' 2	U238	1.1		0.1	A		0.733	1.109	1.485	1.861
	3335609	61493	BH50651AS	0' 2	U238	1.1		0.1	A		0.733	1.109	1.485	1.861
	3671266	59693	BH50557AS	6' 12	U238	1.0966		0.0283	Y		0.733	1.109	1.485	1.861
	3671270	61393	BH50576AS	0' 10	U238	1.0892		0.0178	Y		0.733	1.109	1.485	1.861
	2625484	56593	BH50224AS	13' 17	U238	1.034		0.043704	A		0.733	1.109	1.485	1.861
	3671104	61193	BH50503AS	6' 10	U238	0.9435		0.0165	Y		0.733	1.109	1.485	1.861
	3671268	63093	BH50559AS	15' 20	U238	0.922		0.0293	Y		0.733	1.109	1.485	1.861
	3671273	61493	BH50585AS	8.5' 15.9	U238	0.9084		0.0205	Y		0.733	1.109	1.485	1.861
	3671267	59693	BH50558AS	12' 15.5	U238	0.80475		0.0226	Y		0.733	1.109	1.485	1.861
	2550485	56793	BH50234AS	10' 12	U238	0.79	B	0.023	A		0.733	1.109	1.485	1.861
	2525869	55993	BH50162AS	0' 2	U233234	1.6		0.032	A		0.779	1.711	2.643	3.575
	2439059	55593	BH50059AS	12' 18	U233234	1.5	B	0.02	A		0.779	1.711	2.643	3.575
	2439073	55593	BH50083AS	24' 26	U233234	1.5	B	0.018	A		0.779	1.711	2.643	3.575
	2653841	55793	BH50307AS	0' 6	U233234	1.484		0.070402	A		0.779	1.711	2.643	3.575
	2522230	55593	BH50057AS	0' 6	U233234	1.4	B	0.012	A		0.779	1.711	2.643	3.575
	2439052	55593	BH50058AS	6' 12	U233234	1.4	B	0.048	A		0.779	1.711	2.643	3.575
	2439066	55593	BH50082AS	18' 24	U233234	1.3	B	0.019	A		0.779	1.711	2.643	3.575
	3671529	59093	BH50648AS	0' 2	U233234	1.2966		0.0292	Y		0.779	1.711	2.643	3.575
	2653774	55693	BH50101AS	6' 12	U233234	1.246		0.068371	A		0.779	1.711	2.643	3.575
	2525771	55893	BH50141AS	0' 2	U233234	1.242		0.045	A		0.779	1.711	2.643	3.575
	2653855	55693	BH50113AS	18' 24.5	U233234	1.23		0.08605	A		0.779	1.711	2.643	3.575
	2525778	55893	BH50149AS	0' 6	U233234	1.138		0.045	A		0.779	1.711	2.643	3.575
	2525764	55993	BH50187AS	9' 3.15	U233234	1.12		0.029	A		0.779	1.711	2.643	3.575
	3671040	59093	BH50413AS	12' 16.3	U233234	1.0768		0.0206	Y		0.779	1.711	2.643	3.575
	2653781	55693	BH50102AS	12' 18	U233234	1.013		0.039622	A		0.779	1.711	2.643	3.575
	2695396	58093	BH50313AS	0' 2	U233234	0.962		0.034	A		0.779	1.711	2.643	3.575
	2653862	55793	BH50310AS	18.4' 22.4	U233234	0.9452		0.152185	A		0.779	1.711	2.643	3.575
	3671039	59093	BH50412AS	6' 12	U233234	0.8874		0.0284	Y		0.779	1.711	2.643	3.575
	2653869	55793	BH50309AS	12.4' 18.4	U233234	0.8694		0.134509	A		0.779	1.711	2.643	3.575
	2439065	55593	BH50082AS	18' 24	U235	0.068	J	0.019	A		0.022	0.068	0.114	0.16
	2525856	56093	BH50271AS	2' 8	U235	0.068		0.037	A		0.022	0.068	0.114	0.16
	3671062	59093	BH50411AS	0' 6	U235	0.0679		0.0187	Y		0.022	0.068	0.114	0.16

Table 4 5 (Continued)

IHSS/S t	Seque ID	Locatio	Sample No.	Depth Interval	Constituent	Result in PCI/G	Qualifier	Reporting Limit	Valid.	Mean + (X STD DEV) of background			
										Mean	X 1	X=2	X=3
	2653768	55693	BH50100AS	0'-6	U235	0.06624	J	0.101381	A	0.022	0.068	0.114	0.16
	2653856	55693	BH50113AS	18' 24.5	U235	0.05969	J	0.08605	A	0.022	0.068	0.114	0.16
	2439058	55593	BH50059AS	12 18	U235	0.057	J	0.012	A	0.022	0.068	0.114	0.16
	2695362	58093	BH50313AS	0' 2	U235	0.0544		0.012	A	0.022	0.068	0.114	0.16
	2653842	55793	BH50307AS	0'-6	U235	0.05322	J	0.0671	A	0.022	0.068	0.114	0.16
	2525779	55893	BH50149AS	0'-6	U235	0.051		0.038	A	0.022	0.068	0.114	0.16
	2525772	55893	BH50141AS	0' 2	U235	0.04773		0.047	A	0.022	0.068	0.114	0.16
	2525870	55993	BH50162AS	0' 2	U235	0.04672		0.032	A	0.022	0.068	0.114	0.16
	2653782	55693	BH50102AS	12 18	U235	0.04228		0.039622	A	0.022	0.068	0.114	0.16
	2653775	55693	BH50101AS	6' 12	U235	0.03611	J	0.062515	A	0.022	0.068	0.114	0.16
	3671064	59093	BH50413AS	12 16.3	U235	0.0355		0.0163	Y	0.022	0.068	0.114	0.16
	2525765	55993	BH50187AS	9.3 15	U235	0.03232		0.029	A	0.022	0.068	0.114	0.16
	2653870	55793	BH50309AS	12.4 18.4	U235	0.02892	J	0.115726	A	0.022	0.068	0.114	0.16
	2653863	55793	BH50310AS	18.4 22.4	U235	0.02519	J	0.122162	A	0.022	0.068	0.114	0.16
	2439072	55593	BH50083AS	24 26	U235	0.025	J	0.01	A	0.022	0.068	0.114	0.16
	2525780	55893	BH50149AS	0'-6	U238	1.107		0.045	A	0.733	1.109	1.485	1.861
	2439064	55593	BH50082AS	18 24	U238	1.1	B	0.012	A	0.733	1.109	1.485	1.861
	3671088	59093	BH50413AS	12 16.3	U238	1.0812		0.0163	Y	0.733	1.109	1.485	1.861
	2653871	55793	BH50309AS	12.4 18.4	U238	1.041		0.13171	A	0.733	1.109	1.485	1.861
	2653864	55793	BH50310AS	18.4 22.4	U238	1.012		0.131379	A	0.733	1.109	1.485	1.861
	3671087	59093	BH50412AS	6' 12	U238	0.8945		0.0174	Y	0.733	1.109	1.485	1.861
	3671086	59093	BH50411AS	0'-6	U238	0.8053		0.0187	Y	0.733	1.109	1.485	1.861
133.5	2451950	55293	BH50106AS	0'-6	U233234	1.7	B	0.017	A	0.779	1.711	2.643	3.575
	2451936	55193	BH50090AS	0'-6	U233234	1.5	B	0.015	A	0.779	1.711	2.643	3.575
	2451943	55193	BH50099AS	6'-8	U233234	1.3	B	0.029	A	0.779	1.711	2.643	3.575
	2420060	55493	BH50033AS	6' 12.4	U233234	1.23		0.018	V	0.779	1.711	2.643	3.575
	2451957	55293	BH50107AS	6' 10'	U233234	1	B	0.01	A	0.779	1.711	2.643	3.575
	2451935	55193	BH50090AS	0'-6	U235	0.053	J	0.035	A	0.022	0.068	0.114	0.16
	2420028	55493	BH50034AS	12.4 19.3	U235	0.0477		0.01	V	0.022	0.068	0.114	0.16
	2420026	55393	BH50164AS	6' 12	U235	0.0382		0	V	0.022	0.068	0.114	0.16
	2420016	55393	BH50165AS	12' 17.2	U235	0.03505		0	V	0.022	0.068	0.114	0.16
	2420027	55493	BH50169AS	22.3 30.2	U235	0.024		0.015	V	0.022	0.068	0.114	0.16
	2467511	55393	BH50116AS	18.2 23.8	U235	0.0236		0.018	V	0.022	0.068	0.114	0.16
	2451955	55293	BH50107AS	6' 10	U238	0.97	B	0.01	A	0.733	1.109	1.485	1.861
133.6	2451999	54993	BH50042AS	6' 10	U233234	1.5	B	0.011	A	0.779	1.711	2.643	3.575
	2451978	54893	BH50017AS	0'-6.5	U233234	1.4	B	0.016	A	0.779	1.711	2.643	3.575
	2451985	54893	BH50031AS	4.4 12	U233234	1.4	B	0.012	A	0.779	1.711	2.643	3.575
	2451992	54993	BH50035AS	0'-6	U233234	1.3	B	0.01	A	0.779	1.711	2.643	3.575
	2451971	55093	BH50131AS	6' 13.2	U233234	1.1	B	0.02	A	0.779	1.711	2.643	3.575
	2451964	55093	BH50060AS	0'-6	U233234	1	B	0.026	A	0.779	1.711	2.643	3.575
	2451970	55093	BH50131AS	6' 13.2	U235	0.048	J	0.008	A	0.022	0.068	0.114	0.16
	2451963	55093	BH50060AS	0'-6	U235	0.045	J	0.008	A	0.022	0.068	0.114	0.16
	2451998	54993	BH50042AS	6' 10	U235	0.04	BJ	0.011	A	0.022	0.068	0.114	0.16
	2451962	55093	BH50060AS	0'-6	U238	1.1	B	0.032	A	0.733	1.109	1.485	1.861
142.10	2262666	51193	BH50168AS	0' 10'	U233234	1	B	0.005	A	0.779	1.711	2.643	3.575
	2045287	50092	BH50000AS	0' 14.8	U233234	0.8288		0	A	0.779	1.711	2.643	3.575
	2262665	51193	BH50168AS	0' 10	U235	0.065	J	0.012	A	0.022	0.068	0.114	0.16
	2262664	51193	BH50168AS	0' 10'	U238	1.1	B	0.005	A	0.733	1.109	1.485	1.861
	2045289	50092	BH50000AS	0' 14.8	U238	0.9557		0	A	0.733	1.109	1.485	1.861
142.11	2045303	50292	BH50008AS	0' 14.5	U233234	0.8856		0	A	0.779	1.711	2.643	3.575
Concret Pad	5112082	56194	BH00043AS	0.0-6.0	U233234	1.014		0.0171	V	0.779	1.711	2.643	3.575
	4954841	56194	BH00043AS	0.0-6.0	U233234	0.8961		0.0228	V	0.779	1.711	2.643	3.575
	5112083	56194	BH00043AS	0.0-6.0	U235	0.05152		0.0223	V	0.022	0.068	0.114	0.16
	4954852	56194	BH00043AS	0.0-6.0	U235	0.0465		0.0228	V	0.022	0.068	0.114	0.16
Magneti	3671430	64693	BH50638AS	0'-6	U233234	1.419		0.0254	Y	0.779	1.711	2.643	3.575
Anomaly	3335628	64693	BH50654AS	0' 2	U233234	1.4		0.2	A	0.779	1.711	2.643	3.575
W of 133	3671433	64593	BH50634AS	0'-6	U233234	1.3243		0.0183	Y	0.779	1.711	2.643	3.575
	3335621	64593	BH50653AS	0' 2	U233234	1.3		0.2	A	0.779	1.711	2.643	3.575
	3671435	64593	BH50636AS	12 18	U233234	1.2928		0.0218	Y	0.779	1.711	2.643	3.575
	3671431	64693	BH50639AS	6' 12	U233234	1.2445		0.029	Y	0.779	1.711	2.643	3.575
	3671432	64693	BH50640AS	12 16	U233234	1.2145		0.026	Y	0.779	1.711	2.643	3.575
	3335614	64493	BH50652AS	0' 2	U233234	1.2		0.2	A	0.779	1.711	2.643	3.575
	3671434	64593	BH50635AS	6' 12	U233234	1.1822		0.0313	Y	0.779	1.711	2.643	3.575
	3671436	64593	BH50637AS	18 20'	U233234	1.1003		0.0318	Y	0.779	1.711	2.643	3.575

Table 4-5 (Continued)

IHSS/S t	Seque ID	Locatio	Sample No	Depth Interval	Constatue t	Result PCI/G	Qualifier	Reporting		Mean (X STD DEV) of background			
								Limit	Valid	Mean	X 1	X=2	X=3
	3671437	64493	BH50630AS	0'-6'	U233234	1.0744		0.0208	Y	0.779	1.711	2.643	3.575
	3671438	64493	BH50631AS	6' 12	U233234	0.9867		0.0342	Y	0.779	1.711	2.643	3.575
	3335629	64693	BH50654AS	0' 2	U235	0.067	U	0.1	A	0.022	0.068	0.114	0.16
	3671454	64593	BH50636AS	12 18	U235	0.0534		0.0219	Y	0.022	0.068	0.114	0.16
	3671452	64593	BH50634AS	0'-6	U235	0.0499		0.0184	Y	0.022	0.068	0.114	0.16
	3671457	64493	BH50631AS	6' 12	U235	0.0331		0.0271	Y	0.022	0.068	0.114	0.16
	3671456	64493	BH50630AS	0'-6'	U235	0.0311		0.0208	Y	0.022	0.068	0.114	0.16
	3671453	64593	BH50635AS	6' 12	U235	0.0269		0.0248	Y	0.022	0.068	0.114	0.16
	3671450	64693	BH50639AS	6' 12	U235	0.0269		0.0199	Y	0.022	0.068	0.114	0.16
	3335630	64693	BH50654AS	0' 2	U238	1.1		0.1	A	0.733	1.109	1.485	1.861
	3671472	64593	BH50635AS	6' 12	U238	1.034		0.0248	Y	0.733	1.109	1.485	1.861
S133	3335600	57793	BH50329AS	0' 2	U233234	1.5		0.2	A	0.779	1.711	2.643	3.575
	3671526	57893	BH50355AS	0' 2	U233234	1.2179		0.0443	Y	0.779	1.711	2.643	3.575
	2695402	57993	BH50320AS	0'-6	U233234	0.866		0.047	A	0.779	1.711	2.643	3.575
	3671530	57993	BH50643AS	0' 2	U233234	0.8516		0.0236	Y	0.779	1.711	2.643	3.575
	2695398	57793	BH50322AS	6.3 12	U233234	0.794		0.06	A	0.779	1.711	2.643	3.575
	3671548	57993	BH50643AS	0' 2	U235	0.048		0.0236	Y	0.022	0.068	0.114	0.16
	2695358	57793	BH50321AS	0' 5 75	U235	0.0427		0.012	A	0.022	0.068	0.114	0.16
	2695370	57793	BH50323AS	12.2 18 2	U235	0.0382		0.022	A	0.022	0.068	0.114	0.16
	3671544	57893	BH50355AS	0' 2	U235	0.037		0.0303	Y	0.022	0.068	0.114	0.16
	2725144	57793	BH50338AS	24 28 9	U235	0.0353		0.019	A	0.022	0.068	0.114	0.16
	2695359	57993	BH50320AS	0'-6'	U235	0.035		0.03	A	0.022	0.068	0.114	0.16
	2725145	57893	BH50339AS	0'-6	U235	0.0321		0.022	A	0.022	0.068	0.114	0.16
	2725147	57893	BH50341AS	12.4 17 8	U235	0.0309		0.021	A	0.022	0.068	0.114	0.16
	2725142	57793	BH50324AS	18.8 24 4	U235	0.02965		0.02	A	0.022	0.068	0.114	0.16
	2725157	57893	BH50342AS	18.7 26 4	U235	0.0288		0.026	A	0.022	0.068	0.114	0.16
	2725146	57893	BH50340AS	6' 12.4	U235	0.0229		0.021	A	0.022	0.068	0.114	0.16
	2695418	57793	BH50322AS	6.3 12	U238	1.06		0.021	A	0.733	1.109	1.485	1.861
	3335602	57793	BH50329AS	0' 2	U238	1		0.1	A	0.733	1.109	1.485	1.861
	3671566	57993	BH50643AS	0' 2	U238	0.8516		0.0236	Y	0.733	1.109	1.485	1.861
	2695423	57993	BH50320AS	0'-6'	U238	0.845		0.024	A	0.733	1.109	1.485	1.861
TDEM 1	5362681	55194	BH00029AS	6.0-12.0	U233234	1.71		0.0252	Y	0.779	1.711	2.643	3.575
	5362713	55294	BH00033AS	12.0-15.2	U233234	1.457		0.0167	Y	0.779	1.711	2.643	3.575
	5362689	55194	BH00030AS	12.0-16.1	U233234	1.445		0.017	Y	0.779	1.711	2.643	3.575
	5362697	55294	BH00031AS	0.0-6.0	U233234	1.429		0.0127	Y	0.779	1.711	2.643	3.575
	5362705	55294	BH00032AS	6.0-12.0	U233234	1.25		0.0201	Y	0.779	1.711	2.643	3.575
	5012752	60094	BH00089AS	0.0-5.0	U233234	0.8786		0.0287	V	0.779	1.711	2.643	3.575
	5362714	55294	BH00033AS	12.0-15.2	U235	0.05756		0.0143	Y	0.022	0.068	0.114	0.16
	5362698	55294	BH00031AS	0.0-6.0	U235	0.05567		0.0114	Y	0.022	0.068	0.114	0.16
	5012753	60094	BH00089AS	0.0-5.0	U235	0.05098		0.0197	V	0.022	0.068	0.114	0.16
	5362706	55294	BH00032AS	6.0-12.0	U235	0.0491		0.0172	Y	0.022	0.068	0.114	0.16
TDEM 2	5362690	55194	BH00030AS	12.0-16.1	U235	0.0375		0.0159	Y	0.022	0.068	0.114	0.16
	5292586	56094	BH00039AS	12.0-18.0	U233234	1.23		0.0217	Y	0.779	1.711	2.643	3.575
	4954840	55894	BH00036AS	0.0-6.0	U233234	1.0095		0.0238	V	0.779	1.711	2.643	3.575
	5112042	55894	BH00036AS	0.0-6.0	U233234	0.8552		0.023	V	0.779	1.711	2.643	3.575
	4954851	55894	BH00036AS	0.0-6.0	U235	0.0584		0.0301	V	0.022	0.068	0.114	0.16
	5112043	55894	BH00036AS	0.0-6.0	U235	0.05301		0.0128	V	0.022	0.068	0.114	0.16
TDEM W133	5292587	56094	BH00039AS	12.0-18.0	U235	0.03363		0.0186	Y	0.022	0.068	0.114	0.16
	5068966	58894	BH00064AS	0.0-2.7	U233234	1.11		0.01	Y	0.779	1.711	2.643	3.575
W209	5068998	58894	BH00064AS	0.0-2.7	U238	0.97		0.01	Y	0.733	1.109	1.485	1.861
	2695387	57693	BH50319AS	0'-6	U233234	1.03		0.042	A	0.779	1.711	2.643	3.575
W209	3335572	57693	BH50642AS	0' 2	U233234	0.86		0.2	A	0.779	1.711	2.643	3.575
	2695356	57693	BH50319AS	0'-6'	U235	0.0659		0.016	A	0.022	0.068	0.114	0.16
	3335573	57693	BH50642AS	0' 2	U235	0.042	U	0.2	A	0.022	0.068	0.114	0.16
	3335574	57693	BH50642AS	0' 2	U238	0.85		0.1	A	0.733	1.109	1.485	1.861
Exceeds the Background Mean plus one Standard Deviation but is less than Background Mean plus two Standard Deviations													
115/196	3671208	59493	BH50521AS	6.9' 12 9'	U233234	2.6248		0.0251	Y	0.779	1.711	2.643	3.441
	2642375	58693	BH50348AS	0'-6'	U233234	2	B	0.015	A	0.779	1.711	2.643	3.441
	3671213	59593	BH50553AS	6' 12	U233234	1.9101		0.0306	Y	0.779	1.711	2.643	3.441
	2262645	50892	BH50122AS	6' 12	U233234	1.8	B	0.02	A	0.779	1.711	2.643	3.441
	2689777	58693	BH50350AS	19.5 25 5	U233234	1.8	B	0.019	A	0.779	1.711	2.643	3.441
	3671057	61293	BH50504AS	0'-6	U233234	1.7503		0.0283	Y	0.779	1.711	2.643	3.441
	2689776	58693	BH50350AS	19.5 25 5	U235	0.11	BJ	0.011	A	0.022	0.068	0.114	0.153
	3671081	61293	BH50504AS	0'-6	U235	0.1051		0.0194	Y	0.022	0.068	0.114	0.153

Table 4-5 (Continued)

IHSS/S't	Seque ce		Sampl No.	Depth Interval	Constituent	Result		Reporting Limit	Valid.	Mean + (X STD DEV) of background			
	ID	Locatio				PCI/G	Qualifier			Mean	X 1	X=2	X=3
	2262693	50692	BH50087AS	0'-6	U235	0.096	J	0.016	A	0.022	0.068	0.114	0.153
	2262658	50792	BH50105AS	0' 10	U235	0.091	J	0.006	A	0.022	0.068	0.114	0.153
	2253063	50592	BH50064AS	12 18	U235	0.09	J	0.029	A	0.022	0.068	0.114	0.153
	3671414	60993	BH50588AS	0'-6'	U235	0.088		0.0216	Y	0.022	0.068	0.114	0.153
	3671238	59593	BH50554AS	14.4 16.4	U235	0.0843		0.0178	Y	0.022	0.068	0.114	0.153
	3671237	59593	BH50553AS	6' 12	U235	0.084		0.0188	Y	0.022	0.068	0.114	0.153
	3671076	59793	BH50484AS	0' 7.3	U235	0.0832		0.0204	Y	0.022	0.068	0.114	0.153
	2689783	58693	BH50405AS	25.5 29.5	U235	0.081	BJ	0.01	A	0.022	0.068	0.114	0.153
	5068985	58494	BH00071AS	6.0-9.5	U235	0.08		0.02	Y	0.022	0.068	0.114	0.153
	2262637	50892	BH50121AS	0'-6	U235	0.079	J	0.005	A	0.022	0.068	0.114	0.153
	2262623	50492	BH50040AS	18 24	U235	0.078	J	0.011	A	0.022	0.068	0.114	0.153
	2262651	50792	BH50104AS	0'-6	U235	0.078	J	0.005	A	0.022	0.068	0.114	0.153
	2262672	50992	BH50138AS	0'-6	U235	0.078	J	0.005	A	0.022	0.068	0.114	0.153
	3671545	59593	BH50540AS	0' 2	U235	0.0769		0.021	Y	0.022	0.068	0.114	0.153
	2695014	58593	BH50347AS	0'-6	U235	0.075495		0.04943	V	0.022	0.068	0.114	0.153
	2253021	50392	BH50015AS	18 24	U235	0.074	J	0.015	A	0.022	0.068	0.114	0.153
	3671554	61293	BH50508AS	0' 2	U235	0.0732		0.0207	Y	0.022	0.068	0.114	0.153
	3671418	63193	BH50618AS	12 20	U235	0.0724		0.0198	Y	0.022	0.068	0.114	0.153
	2262630	50892	BH50123AS	8 16	U235	0.072	J	0.012	A	0.022	0.068	0.114	0.153
	5186002	59494	BH00152AS	0.0-5.9	U235	0.07051		0.0232	V	0.022	0.068	0.114	0.153
	3671070	59393	BH50476AS	0'-6	U235	0.07		0.0185	Y	0.022	0.068	0.114	0.153
	3671417	63193	BH50617AS	6' 12	U235	0.0685		0.022	Y	0.022	0.068	0.114	0.153
	3671077	59793	BH50485AS	5.3 11.3	U235	0.0683		0.0204	Y	0.022	0.068	0.114	0.153
	2689768	58693	BH50349AS	12' 19.5	U238	1.45	B	0.021	A	0.733	1.109	1.485	1.807
	3671262	59593	BH50554AS	14.4 16.4	U238	1.448		0.0178	Y	0.733	1.109	1.485	1.807
	3671572	61293	BH50508AS	0' 2	U238	1.4435		0.0207	Y	0.733	1.109	1.485	1.807
	2695036	58593	BH50404AS	12.5 18.1	U238	1.437		0.048526	V	0.733	1.109	1.485	1.807
	2253020	50392	BH50015AS	18 24	U238	1.4	B	0.015	A	0.733	1.109	1.485	1.807
	2642401	58393	BH50343AS	0'-6	U238	1.4	B	0.015	A	0.733	1.109	1.485	1.807
	5069008	57594	BH00082AS	6.0-12.0	U238	1.39		0.02	Y	0.733	1.109	1.485	1.807
	3671102	59793	BH50486AS	13.3 15.3	U238	1.338		0.0186	Y	0.733	1.109	1.485	1.807
	3671425	63193	BH50617AS	6' 12	U238	1.3345		0.022	Y	0.733	1.109	1.485	1.807
	5069646	56694	BH00095AS	0.0-6.0	U238	1.323		0.0224	V	0.733	1.109	1.485	1.807
	3671563	59593	BH50540AS	0' 2	U238	1.3128		0.021	Y	0.733	1.109	1.485	1.807
	2252992	50592	BH50066AS	0' 32	U238	1.3	B	0.015	A	0.733	1.109	1.485	1.807
	2262629	50892	BH50123AS	8' 16	U238	1.3	B	0.012	A	0.733	1.109	1.485	1.807
	2262685	50992	BH50140AS	0' 16	U238	1.3	B	0.024	A	0.733	1.109	1.485	1.807
	2695029	58593	BH50403AS	6' 12.5	U238	1.262		0.057886	V	0.733	1.109	1.485	1.807
	3671573	59793	BH50488AS	0' 2	U238	1.2495		0.032	Y	0.733	1.109	1.485	1.807
	3671106	61293	BH50505AS	6' 10.6	U238	1.2409		0.0544	Y	0.733	1.109	1.485	1.807
	5069654	56694	BH00096AS	0.0-6.0	U238	1.236		0.0129	V	0.733	1.109	1.485	1.807
	5011955	56694	BH00122AS	43.0-150.0	U238	1.234		0.0272	V	0.733	1.109	1.485	1.807
	3671571	59293	BH50444AS	0' 2	U238	1.2333		0.0239	Y	0.733	1.109	1.485	1.807
	3671424	63193	BH50616AS	0'-6	U238	1.2261		0.0175	Y	0.733	1.109	1.485	1.807
	5069638	56694	BH00111AS	0.0-35.0	U238	1.214		0.0159	V	0.733	1.109	1.485	1.807
	5186003	59494	BH00152AS	0.0-5.9	U238	1.212		0.0164	V	0.733	1.109	1.485	1.807
	5012728	57594	BH00085AS	18.0-23.0	U238	1.209		0.0143	V	0.733	1.109	1.485	1.807
	3671259	59593	BH50552AS	0'-6	U238	1.192		0.0174	Y	0.733	1.109	1.485	1.807
	3671090	59293	BH50440AS	6' 12	U238	1.1855		0.0287	Y	0.733	1.109	1.485	1.807
	5069670	56694	BH00112AS	0.0-41.0	U238	1.171		0.0175	V	0.733	1.109	1.485	1.807
	3671567	59493	BH50524AS	4 2	U238	1.1581		0.0221	Y	0.733	1.109	1.485	1.807
133 1	3671044	58893	BH50458AS	0'-6	U233234	1.8486		0.0207	Y	0.779	1.711	2.643	3.441
	2525786	56293	BH50210AS	0' 2	U235	0.08865		0.044	A	0.022	0.068	0.114	0.153
	3335580	58893	BH50646AS	0' 2	U235	0.076	U	0.2	A	0.022	0.068	0.114	0.153
	2439086	56193	BH50177AS	0'-6	U235	0.073	J	0.021	A	0.022	0.068	0.114	0.153
	2525793	56293	BH50206AS	0'-6	U235	0.06913		0.048	A	0.022	0.068	0.114	0.153
	3671093	58893	BH50459AS	6' 12	U238	1.2577		0.0207	Y	0.733	1.109	1.485	1.807
	2550474	56493	BH50219AS	0'-6	U238	1.2	B	0.017	A	0.733	1.109	1.485	1.807
2	2522244	57293	BH50252AS	0'-6	U233234	2.2	B	0.026	A	0.779	1.711	2.643	3.441
	2522272	57293	BH50292AS	26 30'	U233234	1.8	B	0.047	A	0.779	1.711	2.643	3.441
	2522313	57393	BH50291AS	22.1 26.1	U235	0.11	BJ	0.014	A	0.022	0.068	0.114	0.153
	2625469	57193	BH50246AS	0' 2	U235	0.09712		0.096297	A	0.022	0.068	0.114	0.153
	2465685	57593	BH50298AS	0' 2	U235	0.092	J	0.026	A	0.022	0.068	0.114	0.153
	2625490	57193	BH50250AS	7' 13	U235	0.09156		0.077064	A	0.022	0.068	0.114	0.153
	2467516	57093	BH50241AS	0' 2	U235	0.0775		0	V	0.022	0.068	0.114	0.153

Table 4-5 (Continued)

IHSS/S t	Seque ID	Locatio	Sampl No.	Depth Interval	Constitue t	Result PCI/G	Qualifier	Reporting		Mean + (X STD DEV) of background			
								Limit	Valid	Mean	X = 1	X=2	X=3
	2522285	57393	BH50257AS	0'-6'	U235	0.077	BJ	0.018	A	0.022	0.068	0.114	0.153
	2522292	57393	BH50258AS	4' 6" 12'	U235	0.075	BJ	0.013	A	0.022	0.068	0.114	0.153
	2465713	57593	BH50301AS	12' 14'	U235	0.072	J	0.017	A	0.022	0.068	0.114	0.153
	2467508	57093	BH50242AS	0'-6'	U235	0.0705		0.015	V	0.022	0.068	0.114	0.153
	2625470	57193	BH50246AS	0' 2'	U238	1.478		0.150293	A	0.733	1.109	1.485	1.807
	2522298	57393	BH50259AS	10' 2" 18'	U238	1.4	B	0.044	A	0.733	1.109	1.485	1.807
	2550607	57493	BH50261AS	0' 2'	U238	1.4	B	0.014	A	0.733	1.109	1.485	1.807
	2465691	57593	BH50299AS	0'-6'	U238	1.4	B	0.015	A	0.733	1.109	1.485	1.807
	3671574	58793	BH50645AS	0' 2'	U238	1.3915		0.025	Y	0.733	1.109	1.485	1.807
	3670934	58793	BH50406AS	0'-6'	U238	1.3452		0.0194	Y	0.733	1.109	1.485	1.807
	2525815	56893	BH50239AS	8' 3" 14'	U238	1.324		0.026	A	0.733	1.109	1.485	1.807
	2522263	57293	BH50255AS	20' 26'	U238	1.3	B	0.013	A	0.733	1.109	1.485	1.807
	2522305	57393	BH50260AS	16' 1" 24'	U238	1.3	B	0.012	A	0.733	1.109	1.485	1.807
	2465705	57593	BH50294AS	6' 12'	U238	1.3	B	0.023	A	0.733	1.109	1.485	1.807
	3670935	58793	BH50407AS	6' 12'	U238	1.2094		0.0195	Y	0.733	1.109	1.485	1.807
	2522312	57393	BH50291AS	22' 1" 26'	U238	1.2	B	0.023	A	0.733	1.109	1.485	1.807
	2550453	57493	BH50265AS	18' 20'	U238	1.2	B	0.017	A	0.733	1.109	1.485	1.807
	2465698	57593	BH50300AS	6' 12'	U238	1.2	B	0.024	A	0.733	1.109	1.485	1.807
	2467559	57093	BH50242AS	0'-6'	U238	1.19		0.015	V	0.733	1.109	1.485	1.807
	3670937	58793	BH50409AS	18' 24'	U238	1.1706		0.0195	Y	0.733	1.109	1.485	1.807
	2467558	57093	BH50243AS	6' 12' 3"	U238	1.16		0	V	0.733	1.109	1.485	1.807
	2467566	56993	BH50199AS	0'-4'	U238	1.11		0.026	A	0.733	1.109	1.485	1.807
	2625491	57193	BH50250AS	7' 13'	U238	1.11		0.087781	A	0.733	1.109	1.485	1.807
133.3	3671055	61193	BH50500AS	0'-6'	U233234	1.8225		0.0335	Y	0.779	1.711	2.643	3.441
	2550497	56793	BH50231AS	0' 2'	U233234	1.8	B	0.033	A	0.779	1.711	2.643	3.441
	3671246	61393	BH50576AS	0' 10'	U235	0.1087		0.0178	Y	0.022	0.068	0.114	0.153
	3671242	59693	BH50557AS	6' 12'	U235	0.1074		0.0283	Y	0.022	0.068	0.114	0.153
	2439128	56593	BH50221AS	0' 2'	U235	0.082	J	0.053	A	0.022	0.068	0.114	0.153
	3671079	61193	BH50500AS	0'-6'	U235	0.0809		0.0206	Y	0.022	0.068	0.114	0.153
	2439135	56593	BH50222AS	0'-6'	U235	0.08	J	0.011	A	0.022	0.068	0.114	0.153
	2439114	56693	BH50226AS	0' 2'	U235	0.069	J	0.011	A	0.022	0.068	0.114	0.153
	3671263	59693	BH50556AS	0'-6'	U238	1.48435		0.0246	Y	0.733	1.109	1.485	1.807
	2550495	56793	BH50231AS	0' 2'	U238	1.4	B	0.06	A	0.733	1.109	1.485	1.807
	2550502	56793	BH50232AS	0'-6'	U238	1.4	B	0.016	A	0.733	1.109	1.485	1.807
	2439134	56593	BH50222AS	0'-6'	U238	1.3	B	0.019	A	0.733	1.109	1.485	1.807
	2439120	56693	BH50227AS	0'-6'	U238	1.3	B	0.022	A	0.733	1.109	1.485	1.807
	2439141	56593	BH50223AS	6' 12'	U238	1.2	B	0.12	A	0.733	1.109	1.485	1.807
	3671269	61393	BH50570AS	0'-6'	U238	1.1674		0.0174	Y	0.733	1.109	1.485	1.807
	3671272	61493	BH50583AS	0' 8' 5"	U238	1.13495		0.0179	Y	0.733	1.109	1.485	1.807
133.4	3671051	58993	BH50482AS	6' 4" 12'	U233234	2.6331		0.0389	Y	0.779	1.711	2.643	3.441
	2695389	58093	BH50315AS	10' 12'	U233234	2.46		0.034	A	0.779	1.711	2.643	3.441
	2653767	55693	BH50100AS	0'-6'	U233234	2.058		0.12179	A	0.779	1.711	2.643	3.441
	2653834	55793	BH50306AS	0' 2'	U233234	1.958		0.099847	A	0.779	1.711	2.643	3.441
	2525855	56093	BH50271AS	2' 8"	U233234	1.735		0.044	A	0.779	1.711	2.643	3.441
	2439051	55593	BH50058AS	6' 12'	U235	0.11	J	0.015	A	0.022	0.068	0.114	0.153
	3671547	59093	BH50648AS	0' 2'	U235	0.0724		0.0232	Y	0.022	0.068	0.114	0.153
	2653776	55693	BH50101AS	6' 12'	U238	1.44		0.049486	A	0.733	1.109	1.485	1.807
	2439071	55593	BH50083AS	24' 26'	U238	1.4	B	0.018	A	0.733	1.109	1.485	1.807
	2525766	55993	BH50187AS	9' 3" 15'	U238	1.367		0.04	A	0.733	1.109	1.485	1.807
	2522228	55593	BH50057AS	0'-6'	U238	1.3	B	0.012	A	0.733	1.109	1.485	1.807
	2439057	55593	BH50059AS	12' 18'	U238	1.2	B	0.012	A	0.733	1.109	1.485	1.807
	3671565	59093	BH50648AS	0' 2'	U238	1.1991		0.0232	Y	0.733	1.109	1.485	1.807
	2653857	55693	BH50113AS	18' 24' 5"	U238	1.169		0.062282	A	0.733	1.109	1.485	1.807
133.5	2451942	55193	BH50099AS	6' 8"	U235	0.1	BJ	0.011	A	0.022	0.068	0.114	0.153
	2451956	55293	BH50107AS	6' 10'	U235	0.098	BJ	0.01	A	0.022	0.068	0.114	0.153
	2451949	55293	BH50106AS	0'-6'	U235	0.09	J	0.017	A	0.022	0.068	0.114	0.153
	2420013	55493	BH50033AS	6' 12' 4"	U235	0.0831		0	V	0.022	0.068	0.114	0.153
	2451934	55193	BH50090AS	0'-6'	U238	1.4	B	0.015	A	0.733	1.109	1.485	1.807
	2451941	55193	BH50099AS	6' 8"	U238	1.4	B	0.011	A	0.733	1.109	1.485	1.807
	2420082	55493	BH50034AS	12' 4" 19' 3"	U238	1.34		0	V	0.733	1.109	1.485	1.807
133.6	2451977	54893	BH50017AS	0'-6' 5"	U235	0.09	J	0.016	A	0.022	0.068	0.114	0.153
	2451991	54993	BH50035AS	0'-6'	U235	0.083	BJ	0.01	A	0.022	0.068	0.114	0.153
	2451976	54893	BH50017AS	0'-6' 5"	U238	1.3	B	0.007	A	0.733	1.109	1.485	1.807
	2451983	54893	BH50031AS	4' 4" 12'	U238	1.3	B	0.031	A	0.733	1.109	1.485	1.807

Table 4 5 (Continued)

IHSS/S't	Seque ID	Locatio	Sample N	Depth Interval	Constitue t	Result		Reporting		Valid.	Mean + (X STD DEV) of background			
						PCI/G	Qualifier	Limit			Mean	X = 1	X = 2	X = 3
Concret Pad	2451969	55093	BH50131AS	6' 13.2	U238	1.2	B	0.02	A		0.733	1.109	1.485	1.807
	5112084	56194	BH00043AS	0.0-6.0	U238	1.454		0.0145	V		0.733	1.109	1.485	1.807
	4954863	56194	BH00043AS	0.0-6.0	U238	1.2218		0.0334	V		0.733	1.109	1.485	1.807
Magn t Anomaly W of 133	3671439	64493	BH50632AS	12 14	U233234	2.2162		0.0754	Y		0.779	1.711	2.643	3.441
	3671449	64693	BH50638AS	0'-6	U235	0.074		0.0202	Y		0.022	0.068	0.114	0.153
	3671471	64593	BH50634AS	0'-6	U238	1.3318		0.0184	Y		0.733	1.109	1.485	1.807
	3671468	64693	BH50638AS	0'-6	U238	1.3286		0.0202	Y		0.733	1.109	1.485	1.807
	3335616	64493	BH50652AS	0' 2	U238	1.3		0.2	A		0.733	1.109	1.485	1.807
	3671475	64493	BH50630AS	0'-6	U238	1.2046		0.0208	Y		0.733	1.109	1.485	1.807
	3335623	64593	BH50653AS	0' 2	U238	1.2		0.1	A		0.733	1.109	1.485	1.807
	3671470	64693	BH50640AS	12 16	U238	1.167		0.0206	Y		0.733	1.109	1.485	1.807
	3671473	64593	BH50636AS	12 18	U238	1.1653		0.0219	Y		0.733	1.109	1.485	1.807
	3671474	64593	BH50637AS	18 20	U238	1.1475		0.0217	Y		0.733	1.109	1.485	1.807
	3671476	64493	BH50631AS	6' 12	U238	1.1303		0.0271	Y		0.733	1.109	1.485	1.807
	3671469	64693	BH50639AS	6' 12	U238	1.1098		0.0199	Y		0.733	1.109	1.485	1.807
S133	2695361	57793	BH50322AS	6.3 12	U235	0.0814		0.053	A		0.022	0.068	0.114	0.153
	2695360	57993	BH50316AS	4.9 8.1	U235	0.07345		0.026	A		0.022	0.068	0.114	0.153
	3671562	57893	BH50355AS	0' 2	U238	1.1521		0.0303	Y		0.733	1.109	1.485	1.807
TDEM 1	5362673	55194	BH00028AS	0.0-6.0	U233234	1.845		0.021	Y		0.779	1.711	2.643	3.441
	5362682	55194	BH00029AS	6.0-12.0	U235	0.08957		0.022	Y		0.022	0.068	0.114	0.153
	5362674	55194	BH00028AS	0.0-6.0	U235	0.0855		0.018	Y		0.022	0.068	0.114	0.153
	5362699	55294	BH00031AS	0.0-6.0	U238	1.42		0.0139	Y		0.733	1.109	1.485	1.807
	5362707	55294	BH00032AS	6.0-12.0	U238	1.404		0.0232	Y		0.733	1.109	1.485	1.807
	5362715	55294	BH00033AS	12.0-15.2	U238	1.4		0.0177	Y		0.733	1.109	1.485	1.807
	5362691	55194	BH00030AS	12.0-16.1	U238	1.341		0.0146	Y		0.733	1.109	1.485	1.807
TDEM 2	5292588	56094	BH00039AS	12.0-18.0	U238	1.427		0.023	Y		0.733	1.109	1.485	1.807
	5112044	55894	BH00036AS	0.0-6.0	U238	1.243		0.0184	V		0.733	1.109	1.485	1.807
DEM W133	5068983	58894	BH00064AS	0.0-2.7	U235	0.07		0.01	Y		0.022	0.068	0.114	0.153
9	2695403	57693	BH50319AS	0'-6	U238	1.18		0.033	A		0.733	1.109	1.485	1.807
Exceeds the Background Mean plus two Standard Deviations but is less than Background Mean plus three Standard Deviations														
115/196	2689769	58693	BH50349AS	12' 19.5	U235	0.1491	BJ	0.012	A		0.022	0.068	0.114	0.16
	3671231	59493	BH50520AS	0'-6.3	U235	0.1386		0.0179	Y		0.022	0.068	0.114	0.16
	3671232	59493	BH50521AS	6.9' 12.9	U235	0.13665		0.0199	Y		0.022	0.068	0.114	0.16
	2689782	58693	BH50405AS	25.5 29.5	U238	1.8	B	0.016	A		0.733	1.109	1.485	1.861
	3671261	59593	BH50553AS	6' 12	U238	1.7904		0.0188	Y		0.733	1.109	1.485	1.861
	2262671	50992	BH50138AS	0'-6	U238	1.7	B	0.005	A		0.733	1.109	1.485	1.861
	2642373	58693	BH50348AS	0'-6	U238	1.7	B	0.015	A		0.733	1.109	1.485	1.861
	2689775	58693	BH50350AS	19.5 25.5	U238	1.7	B	0.019	A		0.733	1.109	1.485	1.861
	3671422	60993	BH50588AS	0'-6	U238	1.6485		0.0216	Y		0.733	1.109	1.485	1.861
	2252999	50692	BH50088AS	6' 12	U238	1.6	B	0.013	A		0.733	1.109	1.485	1.861
	2262657	50792	BH50105AS	0' 10	U238	1.6	B	0.02	A		0.733	1.109	1.485	1.861
	2262636	50892	BH50121AS	0'-6	U238	1.6	B	0.005	A		0.733	1.109	1.485	1.861
	2262643	50892	BH50122AS	6' 12	U238	1.6	B	0.02	A		0.733	1.109	1.485	1.861
	2695015	58593	BH50347AS	0'-6	U238	1.5995		0.045962	V		0.733	1.109	1.485	1.861
	3671105	61293	BH50504AS	0'-6	U238	1.527		0.0283	Y		0.733	1.109	1.485	1.861
	2252985	50692	BH50089AS	0' 14	U238	1.5	B	0.025	A		0.733	1.109	1.485	1.861
	2642380	58693	BH50417AS	6' 12	U238	1.5	B	0.061	A		0.733	1.109	1.485	1.861
133 1	2695393	56393	BH50211AS	0' 2	U233234	3.27		0.022	A		0.779	1.711	2.643	3.575
	2525794	56293	BH50206AS	0'-6	U238	1.621		0.043	A		0.733	1.109	1.485	1.861
	2439078	56193	BH50176AS	0' 2	U238	1.5	B	0.011	A		0.733	1.109	1.485	1.861
	2550467	56493	BH50220AS	0' 2	U238	1.5	B	0.049	A		0.733	1.109	1.485	1.861
133 2	2522251	57293	BH50253AS	6' 12	U233234	2.9	B	0.038	A		0.779	1.711	2.643	3.575
	2522243	57293	BH50252AS	0'-6	U235	0.15	BJ	0.015	A		0.022	0.068	0.114	0.16
	2522271	57293	BH50292AS	26 30	U235	0.13	BJ	0.018	A		0.022	0.068	0.114	0.16
	2522257	57293	BH50254AS	12 18	U235	0.12	BJ	0.01	A		0.022	0.068	0.114	0.16
	2522235	57293	BH50251AS	0' 2	U238	1.8	B	0.013	A		0.733	1.109	1.485	1.861
	2522256	57293	BH50254AS	12 18	U238	1.8	B	0.01	A		0.733	1.109	1.485	1.861
	2522284	57393	BH50257AS	0'-6.6	U238	1.6	B	0.011	A		0.733	1.109	1.485	1.861
	2624781	56893	BH50236AS	0' 2	U238	1.531		0.067023	A		0.733	1.109	1.485	1.861
	3671528	61193	BH50649AS	0' 2	U233234	3.2214		0.0286	Y		0.779	1.711	2.643	3.575
133.3	3671546	61193	BH50649AS	0' 2	U235	0.1417		0.0227	Y		0.022	0.068	0.114	0.16
	2439142	56593	BH50223AS	6' 12	U235	0.12	J	0.059	A		0.022	0.068	0.114	0.16
	2439113	56693	BH50226AS	0' 2	U238	1.6	B	0.031	A		0.733	1.109	1.485	1.861

Table 4 5 (Continued)

IHSS/ t	Sequenc ID	Locatio	Sample No.	Depth Interval	Constituent	Result i PCI/G	Qualifier	Reporting Limit	Valid	Mean + (X STD DEV) of background			
										Mean	X = 1	X=2	X=3
133.4	2550481	56793	BH50233AS	6' 12	U238	1.6	B	0.045	A	0.733	1.109	1.485	1.861
	3671075	58993	BH50482AS	6.4 12	U235	0.1568		0.0181	Y	0.022	0.068	0.114	0.16
	2695366	58093	BH50315AS	10 12	U235	0.151		0.029	A	0.022	0.068	0.114	0.16
	2653835	55793	BH50306AS	0' 2	U235	0.1377		0.053241	A	0.022	0.068	0.114	0.16
	2522229	55593	BH50057AS	0-6	U235	0.12	BJ	0.012	A	0.022	0.068	0.114	0.16
	2439050	55593	BH50058AS	6' 12	U238	1.8	B	0.026	A	0.733	1.109	1.485	1.861
	2525773	55893	BH50141AS	0' 2	U238	1.7		0.047	A	0.733	1.109	1.485	1.861
	2653843	55793	BH50307AS	0-6	U238	1.546		0.053116	A	0.733	1.109	1.485	1.861
133.6	2695412	58093	BH50313AS	0' 2	U238	1.5		0.021	A	0.733	1.109	1.485	1.861
	2451984	54893	BH50031AS	4.4 12	U235	0.12	J	0.036	A	0.022	0.068	0.114	0.16
	2451990	54993	BH50035AS	0-6	U238	1.5	B	0.017	A	0.733	1.109	1.485	1.861
Magnet Anomaly W of 133	2451997	54993	BH50042AS	6' 10	U238	1.5	B	0.011	A	0.733	1.109	1.485	1.861
	3335615	64493	BH50652AS	0' 2	U235	0.14	U	0.2	A	0.022	0.068	0.114	0.16
	3335622	64593	BH50653AS	0' 2	U235	0.14	U	0.2	A	0.022	0.068	0.114	0.16
S133	3671477	64493	BH50632AS	12 14	U238	1.6662		0.0497	Y	0.733	1.109	1.485	1.861
TDEM 1	3335601	57793	BH50329AS	0' 2	U235	0.14	U	0.2	A	0.022	0.068	0.114	0.16
TDEM 2	5362683	55194	BH00029AS	60-120	U238	1.636		0.0207	Y	0.733	1.109	1.485	1.861
	4954862	55894	BH00036AS	00-60	U238	1.4931		0.0301	V	0.733	1.109	1.485	1.861
Exceeds the Background Mean plus three Standard Deviations													
115/196	2642396	58493	BH50346AS	6' 12	U233234	30	B	0.015	A	0.779	1.711	2.643	3.575
	2642410	58393	BH50344AS	6' 12.7	U233234	9.3	B	0.047	A	0.779	1.711	2.643	3.575
	2642389	58493	BH50345AS	0-6	U233234	9.1	B	0.02	A	0.779	1.711	2.643	3.575
	3671207	59493	BH50520AS	0-6.3	U233234	3.7629		0.0343	Y	0.779	1.711	2.643	3.575
	2642395	58493	BH50346AS	6' 12	U235	2.3		0.015	A	0.022	0.068	0.114	0.16
	2642409	58393	BH50344AS	6' 12.7	U235	0.53		0.02	A	0.022	0.068	0.114	0.16
	3671082	61293	BH50505AS	6' 10.6	U235	0.3395		0.0431	Y	0.022	0.068	0.114	0.16
	2642388	58493	BH50345AS	0-6	U235	0.32		0.02	A	0.022	0.068	0.114	0.16
	2642394	58493	BH50346AS	6' 12	U238	12	B	0.025	A	0.733	1.109	1.485	1.861
	2642408	58393	BH50344AS	6' 12.7	U238	7.2	B	0.062	A	0.733	1.109	1.485	1.861
	2262692	50692	BH50087AS	0-6	U238	3.1	B	0.042	A	0.733	1.109	1.485	1.861
	3671255	59493	BH50520AS	0-6.3	U238	2.9341		0.0179	Y	0.733	1.109	1.485	1.861
	2642387	58493	BH50345AS	0-6	U238	2.9	B	0.037	A	0.733	1.109	1.485	1.861
	3671423	61093	BH50603AS	6' 13	U238	2.2229		0.0306	Y	0.733	1.109	1.485	1.861
	3671256	59493	BH50521AS	6.9' 12.9'	U238	2.21265		0.0199	Y	0.733	1.109	1.485	1.861
133.1	2695392	56393	BH50212AS	2-6	U233234	117		0.36	Z	0.779	1.711	2.643	3.575
	2695390	56393	BH50213AS	6' 8	U233234	13.2		0.089	A	0.779	1.711	2.643	3.575
	5069676	57294	BH00091AS	00-40	U233234	9934		0.0159	V	0.779	1.711	2.643	3.575
	2695364	56393	BH50212AS	2-6	U235	19.5		0.6	Z	0.022	0.068	0.114	0.16
	2695367	56393	BH50213AS	6' 8	U235	1.7		0.08	A	0.022	0.068	0.114	0.16
	5069677	57294	BH00091AS	00-40	U235	0.6879		0.0111	V	0.022	0.068	0.114	0.16
	2695365	56393	BH50211AS	0' 2	U235	0.47		0.028	A	0.022	0.068	0.114	0.16
	2695408	56393	BH50212AS	2-6	U238	1130		0.49	Z	0.733	1.109	1.485	1.861
	2695406	56393	BH50213AS	6' 8	U238	120		0.065	A	0.733	1.109	1.485	1.861
	5069678	57294	BH00091AS	00-40	U238	38.37		0.00627	V	0.733	1.109	1.485	1.861
	2695409	56393	BH50211AS	0' 2	U238	26.1		0.023	A	0.733	1.109	1.485	1.861
	3671092	58893	BH50458AS	0-6	U238	2.7069		0.0207	Y	0.733	1.109	1.485	1.861
	2525787	56293	BH50210AS	0' 2	U238	2.101		0.049	A	0.733	1.109	1.485	1.861
133.2	2624795	56893	BH50238AS	4-8.3	U233234	105.7		0.275116	A	0.779	1.711	2.643	3.575
	2624787	56893	BH50237AS	2-4	U233234	33.03		0.062518	A	0.779	1.711	2.643	3.575
	2467548	56993	BH50200AS	8.1 10.1	U233234	15.3		0.028	V	0.779	1.711	2.643	3.575
	2624796	56893	BH50238AS	4 8.3	U235	37.68		0.227704	A	0.022	0.068	0.114	0.16
	2624788	56893	BH50237AS	2-4	U235	1.015		0.067032	A	0.022	0.068	0.114	0.16
	2467518	56993	BH50200AS	8.1 10.1	U235	0.916		0	V	0.022	0.068	0.114	0.16
	2465692	57593	BH50299AS	0-6	U235	0.18	J	0.026	A	0.022	0.068	0.114	0.16
	2550615	57493	BH50262AS	0-6	U235	0.17	J	0.023	A	0.022	0.068	0.114	0.16
	2624797	56893	BH50238AS	4 8.3	U238	1160		0.194178	A	0.733	1.109	1.485	1.861
	2467562	56993	BH50200AS	8.1 10.1	U238	29.7		0.028	V	0.733	1.109	1.485	1.861
	2624789	56893	BH50237AS	2-4	U238	19.41		0.057163	A	0.733	1.109	1.485	1.861
	2467561	56993	BH50202AS	8.1 14	U238	2.97		0.023	V	0.733	1.109	1.485	1.861
	2522242	57293	BH50252AS	0-6	U238	2.5	B	0.026	A	0.733	1.109	1.485	1.861
	2522249	57293	BH50253AS	6' 12	U238	2.3	B	0.02	A	0.733	1.109	1.485	1.861
	2522291	57393	BH50258AS	4.6' 12.1	U238	2.1	B	0.021	A	0.733	1.109	1.485	1.861
	2522270	57293	BH50292AS	26' 30	U238	2	B	0.03	A	0.733	1.109	1.485	1.861

Table 4-5 (Continued)

IHSS/S t	Sequence		Sample No.	Depth		Result in PC/G	Qualifier	Reporting		Mean + (X STD DEV) of background			
	ID	Location		Interval	Constituent			Limit	Valid.	Mean	X=1	X=2	X=3
	2625477	57193	BH50247AS	0' 5.5	U238	1923		004808	A	0.733	1.109	1.485	1.861
133.3	2550489	56793	BH50233AS	6' 12	U235	0.26	J	0.027	A	0.022	0.068	0.114	0.16
	3671564	61193	BH50649AS	0' 2	U238	9.344		0.0227	Y	0.733	1.109	1.485	1.861
	3671103	61193	BH50500AS	0' 6	U238	46052		0.0206	Y	0.733	1.109	1.485	1.861
	2439127	56593	BH50221AS	0' 2	U238	2.4	B	0.06	A	0.733	1.109	1.485	1.861
133.4	5411953	55694	BH00042AS	60-106	U233234	241		4.73	Y	0.779	1.711	2.643	3.575
	2695394	58093	BH50314AS	0' 8	U233234	126		0.77	A	0.779	1.711	2.643	3.575
	2695395	58093	BH50314AS	0' 8	U233234	126		0.18	Z	0.779	1.711	2.643	3.575
	2525876	55993	BH50151AS	0' 6	U233234	113.3		0.069	A	0.779	1.711	2.643	3.575
	2525757	55993	BH50161AS	4 9.3	U233234	84.93		0.238	A	0.779	1.711	2.643	3.575
	5411952	55694	BH00041AS	00-60	U233234	58.4		1	Y	0.779	1.711	2.643	3.575
	3671532	58993	BH50647AS	0' 2	U233234	25 7624		0.0444	Y	0.779	1.711	2.643	3.575
	3671049	58993	BH50480AS	0' 6.4	U233234	12.9864		0.0476	Y	0.779	1.711	2.643	3.575
	2525877	55993	BH50151AS	0' 6	U235	17		0.066	A	0.022	0.068	0.114	0.16
	5411957	55694	BH00042AS	60-106	U235	16.1		4.5	Y	0.022	0.068	0.114	0.16
	2695369	58093	BH50314AS	0' 8	U235	10		0.23	Z	0.022	0.068	0.114	0.16
	2695363	58093	BH50314AS	0' 8	U235	6.64		0.37	A	0.022	0.068	0.114	0.16
	5411956	55694	BH00041AS	00-60	U235	5.84		0.685	Y	0.022	0.068	0.114	0.16
	2525758	55993	BH50161AS	4 9.3	U235	5.624		0.207	A	0.022	0.068	0.114	0.16
	3671550	58993	BH50647AS	0' 2	U235	1.5278		0.0352	Y	0.022	0.068	0.114	0.16
	3671073	58993	BH50480AS	0' 6.4	U235	0.65315		0.0249	Y	0.022	0.068	0.114	0.16
	5411961	55694	BH00042AS	60-106	U238	848		3.63	Y	0.733	1.109	1.485	1.861
	2695411	58093	BH50314AS	0' 8	U238	519		0.088	Z	0.733	1.109	1.485	1.861
	2695410	58093	BH50314AS	0' 8	U238	485		0.63	A	0.733	1.109	1.485	1.861
	2525759	55993	BH50161AS	4-9.3	U238	244.2		0.187	A	0.733	1.109	1.485	1.861
	5411960	55694	BH00041AS	00-60	U238	216		0.749	Y	0.733	1.109	1.485	1.861
	2525878	55993	BH50151AS	0' 6	U238	183		0.059	A	0.733	1.109	1.485	1.861
	3671568	58993	BH50647AS	0' 2	U238	97.2346		0.0352	Y	0.733	1.109	1.485	1.861
	3671097	58993	BH50480AS	0' 6.4	U238	47 1546		0.0249	Y	0.733	1.109	1.485	1.861
	2695405	58093	BH50315AS	10' 12	U238	8.5		0.03	A	0.733	1.109	1.485	1.861
	3671099	58993	BH50482AS	6.4 12	U238	8.27275		0.0265	Y	0.733	1.109	1.485	1.861
	2653836	55793	BH50306AS	0' 2	U238	3.338		0.091294	A	0.733	1.109	1.485	1.861
	2525871	55993	BH50162AS	0' 2	U238	2.522		0.043	A	0.733	1.109	1.485	1.861
	2525857	56093	BH50271AS	2' 8	U238	2.414		0.044	A	0.733	1.109	1.485	1.861
	2653769	55693	BH50100AS	0' 6	U238	2.195		0.145224	A	0.733	1.109	1.485	1.861
133.5	2451948	55293	BH50106AS	0' 6	U238	2.3	B	0.007	A	0.733	1.109	1.485	1.861
	2420074	55493	BH50033AS	6' 12.4	U238	2.07		0.018	V	0.733	1.109	1.485	1.861
M.A.W 133	3671458	64493	BH50632AS	12 14	U235	0.3204		0.0394	Y	0.022	0.068	0.114	0.16
TDEM 1	5362675	55194	BH00028AS	00-60	U238	1.951		0.0235	Y	0.733	1.109	1.485	1.861
TDEM 2	5394391	55994	BH00034AS	00-60	U233234	288.2869		5.764328	Y	0.779	1.711	2.643	3.575
	5292570	56094	BH00037AS	00-60	U233234	21.24		0.0126	Y	0.779	1.711	2.643	3.575
	5292594	56094	BH00040AS	180-220	U233234	15.31		0.048	Y	0.779	1.711	2.643	3.575
	5292578	56094	BH00038AS	60-120	U233234	11.94		0.0411	Y	0.779	1.711	2.643	3.575
	5394393	55994	BH00035AS	60-11.2	U233234	10.1869		0.162069	Y	0.779	1.711	2.643	3.575
	5394395	55994	BH00034AS	00-60	U235	36.11686		3.601073	Y	0.022	0.068	0.114	0.16
	5394397	55994	BH00035AS	60-11.2	U235	0.849322		0.138323	Y	0.022	0.068	0.114	0.16
	5292571	56094	BH00037AS	00-60	U235	0.7023		0.0113	Y	0.022	0.068	0.114	0.16
	5292595	56094	BH00040AS	180-220	U235	0.6218		0.0306	Y	0.022	0.068	0.114	0.16
	5292579	56094	BH00038AS	60-120	U235	0.3899		0.0338	Y	0.022	0.068	0.114	0.16
	5394399	55994	BH00034AS	00-60	U238	933.0405		3.936487	Y	0.733	1.109	1.485	1.861
	5394401	55994	BH00035AS	60-11.2	U238	22.84702		0.138323	Y	0.733	1.109	1.485	1.861
	5292572	56094	BH00037AS	00-60	U238	16.62		0.0137	Y	0.733	1.109	1.485	1.861
	5292596	56094	BH00040AS	180-220	U238	15.75		0.0416	Y	0.733	1.109	1.485	1.861
	5292580	56094	BH00038AS	60-120	U238	10.93		0.0455	Y	0.733	1.109	1.485	1.861

These data are graphically displayed on Figures 4-5 and 5b.

Table 4 6
Summary of Organic COCs in Subsurface Soil

IHSS	S quen ID	Location	Sample No	Depth Interval	Constituent	Result in ug/kg	Qualifier	Reporting Limit	Valid.
Detected at concentration less than Reporting Limit									
115/196	2744797	58493	BH50345AS	0-6	B nzo()anthracene	330	J	330	A
	2086490	50992	BH50139AS	6 12	B nzo()anthracene	240	J	330	A
	2632850	58593	BH50403AS	6 12.5	Benzo(a)anthracene	180	J	330	A
	2744293	58393	BH50343AS	0 6	B nzo()anthracene	170	J	330	A
	2035976	50492	BH50037AS	0-6	B nzo()anthracene	130	J	330	A
	2086132	50692	BH50087AS	0 6	B nzo()anthracene	44	J	330	A
	2744803	58493	BH50345AS	0 6	B nzo()pyren	280	J	330	A
	2086496	50992	BH50139AS	6 12	B nzo()pyrene	250	BJ	330	A
	5045251	57594	BH00087AS	84 9 90 4	B nzo()pyr ne	130	J	330	A
	5045343	57594	BH00086AS	24 0-60 0	B nzo(a)pyrene	110	J	330	A
	2744299	58393	BH50343AS	0-6	Benzo(a)pyrene	100	J	330	A
	2632856	58593	BH50403AS	6 12.5	B nzo()pyrene	98	J	330	A
	5160749	59894	BH00164AS	19 9 31 9	B nzo()pyre	58	J	330	A
	2086138	50692	BH50087AS	0 6	B nzo(a)pyrene	47	J	330	A
	2086494	50992	BH50139AS	6 12	B nzo(b)fluoranth ne	260	BJ	330	A
	2744297	58393	BH50343AS	0 6	Benzo(b)fluoranthene	250	J	330	A
	2632854	58593	BH50403AS	6 12.5	Benzo(b)fluoranthene	220	J	330	A
	2035980	50492	BH50037AS	0 6	B nzo(b)fluoranthene	100	J	330	A
	2086136	50692	BH50087AS	0 6	Benzo(b)fluoranthene	81	J	330	A
Exceeds Reporting Limit but is less than ten times the Reporting Limit									
115/196	2711716	59493	BH50520AS	0-6 3	Benzo()anthracene	2400		330	V
	2712569	59493	BH50520AS	0-6 3	Benzo(a)anthracene	2200	D	330	Z
	2712398	59493	BH50521AS	6 9 12.9	B nzo(a)anthracene	1700	D	330	Z
	2744971	58693	BH50349AS	12 19 5	B nzo(a)anthracene	1500		330	V
	2745063	58693	BH50349AS	12 19 5	Benzo(a)anthracene	1400	D	330	Z
	2711300	59493	BH50521AS	6 9 12.9	Benzo(a)anthracene	1310		330	V
	2086398	50992	BH50138AS	0 6	Benzo(a)anthracene	1300		330	V
	2086582	50992	BH50140AS	0 16	Benzo(a)anthracene	950		330	V
	2086766	51092	BH50154AS	0 12'	Benzo(a)anthracene	860		330	V
	2086674	51092	BH50153AS	0 6	Benzo(a)anthracene	850		330	V
	2744527	58393	BH50344AS	6 12.7	B nzo(a)anthracene	510		330	V
	2745322	58693	BH50348AS	0 6	Benzo(a)anthracene	500		330	V
	2711482	59493	BH50522AS	12 9 17 8	B nzo(a)pyrene	3200	E	330	Z
	2711722	59493	BH50520AS	0-6 3	Benzo(a)pyrene	2200		330	V
	2712575	59493	BH50520AS	0-6 3	Benzo(a)pyrene	2200	D	330	Z
	2712404	59493	BH50521AS	6 9 12.9	B nzo()pyren	1700	D	330	Z
	2744977	58693	BH50349AS	12 19 5	Benzo()pyrene	1400		330	V
	2086404	50992	BH50138AS	0 6	B nzo()pyrene	1300	B	330	V
	2711306	59493	BH50521AS	6 9 12.9	B nzo()pyrene	1220		330	V
	2745069	58693	BH50349AS	12 19 5	B nzo(a)pyrene	1200	D	330	Z
	2086588	50992	BH50140AS	0 16	Benzo(a)pyrene	920	B	330	V
	2086680	51092	BH50153AS	0 6	Benzo(a)pyrene	840		330	V
	2086772	51092	BH50154AS	0 12	B nzo()pyrene	830		330	V
	5141798	56694	BH00122AS	43 0-150 0	B nzo()pyrene	480	J	330	A
	5140749	57594	BH00121AS	24 0-105 0	B nzo()pyr ne	470	J	330	A
	2744533	58393	BH50344AS	6 12.7	B nzo()pyre	460		330	V
	2745328	58693	BH50348AS	0 6	B nzo()pyrene	390		330	V
	5141710	56694	BH00113AS	43 0-150 0	B nzo()pyrene	350	J	330	A
	2711720	59493	BH50520AS	0-6 3	B nzo(b)fluoranth	2700		330	V
	2712573	59493	BH50520AS	0-6 3	B nzo(b)fluoranth ne	2500	D	330	Z

Table 4 6 (Continued)

IHSS	Sequence		Sample N	Depth Interval	Constituent	Result		Reporting		Valid.
	ID	Location				in ug/kg	Qualifier	Limit		
	2712402	59493	BH50521AS	6 9 12 9	B nzo(b)fluoranthene	1900	D	330	Z	
	2711304	59493	BH50521AS	6 9 12 9	B nzo(b)fluoranthene	1610		330	V	
	2086402	50992	BH50138AS	0 6	B nzo(b)fluoranthene	1500	B	330	V	
	2744975	58693	BH50349AS	12 19 5	B nzo(b)fluoranthene	1500		330	V	
	2745067	58693	BH50349AS	12 19 5	Benzo(b)fluoranth ne	1500	D	330	Z	
	2086586	50992	BH50140AS	0 16	B nzo(b)fluoranthene	1000	B	330	V	
	2086770	51092	BH50154AS	0 12	B nzo(b)fluoranth ne	940		330	V	
	2086678	51092	BH50153AS	0 6	Benzo(b)fluoranthene	910		330	V	
	2744531	58393	BH50344AS	6 12 7	Benzo(b)fluoranthene	660		330	V	
	2745326	58693	BH50348AS	0 6	B nzo(b)fluoranth ne	520		330	V	
	2744801	58493	BH50345AS	0 6	Benzo(b)fluoranthene	370		330	V	
	2604357	58693	BH50417AS	6 12	PCB 1254	960	X	160	V	
	2087591	50992	BH50140AS	0 16	PCB 1254	870		160	V	
	2702888	61093	BH50603AS	6 13	PCB 1254	860		160	V	
	2704838	59493	BH50520AS	0-6 3	PCB 1254	630		160	V	
	2087535	50992	BH50138AS	0-6	PCB 1254	600		160	V	
	2087619	51092	BH50153AS	0 6	PCB 1254	500		160	V	
	2604133	58393	BH50344AS	6 12.7	PCB 1254	440		160	V	
	2087563	50992	BH50139AS	6 12	PCB 1254	320		160	V	
	2087647	51092	BH50154AS	0 12	PCB 1254	240		160	V	
	2604189	58493	BH50345AS	0-6	PCB 1254	210		160	V	
Exceeds ten times the Reporting Limit but is less than on hundred time the Reporting Limit										
115/196	2711476	59493	BH50522AS	12 9 17 8	B nzo()anthracene	4300	E	330	Z	
	2712481	59493	BH50522AS	12 9 17 8	B nzo()anthracene	3700	D	330	V	
	2712487	59493	BH50522AS	12 9 17 8	B nzo()pyrene	3800	D	330	V	
	2712485	59493	BH50522AS	12 9 17 8	Benzo(b)fluoranth ne	4500	D	330	V	
	2711480	59493	BH50522AS	12 9 17 8	B nzo(b)fluoranth ne	4100	E	330	Z	
Exceeds one hundred times the Reporting Limit										
115/196	2745413	58693	BH50417AS	6 12	Benzo()anthracene	48000		330	JA	
	2745491	58693	BH50417AS	6 12	Benzo(a)anthracene	40000	D	330	Z	
	2745419	58693	BH50417AS	6 12	B nzo()pyrene	43000		330	JA	
	2745497	58693	BH50417AS	6 12	B nzo(a)pyre	35000	DJ	330	Z	
	2745417	58693	BH50417AS	6 12	Benzo(b)fluoranth ne	48000		330	JA	
	2745495	58693	BH50417AS	6 12	B nzo(b)fluoranthene	40000	D	330	Z	
These data are graphically displayed on Figures 4-6a and 6b										

Summary of Metal COCs Exceeding Background Mean in Subsurface Soil

IHSS	Sequence	Location	Sample	Sample	TGC	Constituent	Result	Reporting	Mean	STD DEV of background			
	ID		No	Date			1 up/1	Qualifier		Limit	Valid.	X	1
Exceeds the Background Mean but is less than Background Mean plus one Standard Deviation													
115/196	5196762	58094	GW50102AS	12/21/94	DISSOLVED ALUMINUM	319	U	200	JA	113.66	708.46	1303.26	1898.06
	5196791	58094	GW50103AS	12/21/94	DISSOLVED ALUMINUM	264	U	200	JA	113.66	708.46	1303.26	1898.06
	2815138	59493	GW01166WC	8/11/93	DISSOLVED ALUMINUM	200	U	200	JA	113.66	708.46	1303.26	1898.06
	5368668	59894	GW02201GA	3/7/95	DISSOLVED BARIUM	113	B	200	Y	84	117.1	150.2	183.3
	4927315	59593	GW01619GA	10/24/94	DISSOLVED BARIUM	108	B	9	V	84	117.1	150.2	183.3
	3526634	59593	GW01481WC	11/10/93	DISSOLVED BARIUM	106	B	23	V	84	117.1	150.2	183.3
	5170624	60293	GW50143AS	1/22/95	DISSOLVED BARIUM	85.4	B	200	V	84	117.1	150.2	183.3
	5473754	57594	GW02352GA	4/11/95	DISSOLVED BERYLLIUM	2.5	U	5	Y	2.22	2.91	3.6	4.29
	5170567	57894	GW50141AS	1/22/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170596	57894	GW50161AS	1/22/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5196765	58094	GW50102AS	12/21/94	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5196794	58094	GW50103AS	12/21/94	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5196823	58594	GW50104AS	12/21/94	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	4674393	59493	GW01247GA	8/18/94	DISSOLVED BERYLLIUM	2.5	U	5	V	2.22	2.91	3.6	4.29
	5201436	59493	GW50113AS	1/4/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5201519	59493	GW50111AS	1/4/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170310	59593	GW50131AS	1/11/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170741	59594	GW02058GA	1/25/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5368752	59694	GW02202GA	3/7/95	DISSOLVED BERYLLIUM	2.5	U	5	Y	2.22	2.91	3.6	4.29
	5170625	60293	GW50143AS	1/22/95	DISSOLVED BERYLLIUM	2.5	U	5	V	2.22	2.91	3.6	4.29
	5170654	60293	GW50144AS	1/22/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170857	60893	GW50157AS	1/26/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170799	61093	GW50151AS	1/25/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170828	61093	GW50154AS	1/25/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170397	61293	GW50126AS	1/7/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5201867	63193	GW50130AS	1/10/95	DISSOLVED BERYLLIUM	2.5	U	5	V	2.22	2.91	3.6	4.29
	5201664	63893	GW50120AS	1/5/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5201635	63993	GW50119AS	1/5/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5201606	64093	GW50118AS	1/5/95	DISSOLVED BERYLLIUM	2.5	U	5	JA	2.22	2.91	3.6	4.29
	5170634	60293	GW50143AS										

Table 4-7 (Continued)

IHSS	Sequence		Sample	Sample	TGC	Constituent	Result		Reporting				Mean (X ± STD DEV) of background			
	ID	Location	No	Date			μg/l	Q	After	Limit	Valid	Mean	X ± 1	X ± 2	X ± 3	
115/196	5170306	59493	GW50131AS	1/11/95	DISSOLVED	ALUMINUM	900		200	V	113.66	708.46	1303.26	1898.06		
	3526633	59493	GW01480WC	11/9/93	DISSOLVED	BARIUM	647		23	V	84	117.1	150.2	183.3		
	4940461	59493	GW01618GA	10/20/94	DISSOLVED	BARIUM	457		1	V	84	117.1	150.2	183.3		
	281511	59493	GW01166WC	8/11/93	DISSOLVED	BARIUM	7		200	V	84	117.1	150.2	183.3		
	2763878	59493	GW01024WC	6/24/93	DISSOLVED	BARIUM	396		17	V	84	117.1	150.2	183.3		
	4674392	59493	GW01247GA	8/18/94	DISSOLVED	BARIUM	393		200	V	84	117.1	150.2	183.3		
	5201663	63893	GW50120AS	1/5/95	DISSOLVED	BARIUM	348		200	V	84	117.1	150.2	183.3		
	5329028	59493	GW02176GA	3/9/95	DISSOLVED	BARIUM	344		12	V	84	117.1	150.2	183.3		
	5201518	59493	GW50114AS	1/4/95	DISSOLVED	BARIUM	340		200	V	84	117.1	150.2	183.3		
	5201435	59493	GW50113AS	1/4/95	DISSOLVED	BARIUM	326		200	V	84	117.1	150.2	183.3		
	5201634	63993	GW50119AS	1/5/95	DISSOLVED	BARIUM	315		200	V	84	117.1	150.2	183.3		
	5201605	64093	GW50118AS	1/5/95	DISSOLVED	BARIUM	238		200	V	84	117.1	150.2	183.3		
	5207158	56994	GW02089GA	2/3/95	DISSOLVED	BARIUM	216		12	V	84	117.1	150.2	183.3		
	5170740	59594	GW02058GA	1/25/95	DISSOLVED	BARIUM	213		200	V	84	117.1	150.2	183.3		
	3526953	59493	GW01480WC	11/9/93	DISSOLVED	MANGANESE	10500		2	V	32.66	120.09	207.52	294.95		
	2763890	59493	GW01024WC	6/24/93	DISSOLVED	MANGANESE	4240		1	V	32.66	120.09	207.52	294.95		
	2815151	59493	GW01166WC	8/11/93	DISSOLVED	MANGANESE	3650		15	V	32.66	120.09	207.52	294.95		
	5201643	63993	GW50119AS	1/5/95	DISSOLVED	MANGANESE	3530		15	V	32.66	120.09	207.52	294.95		
	4940471	59493	GW01618GA	10/20/94	DISSOLVED	MANGANESE	3480		1	V	32.66	120.09	207.52	294.95		
	5201672	63893	GW50120AS	1/5/95	DISSOLVED	MANGANESE	3170		15	V	32.66	120.09	207.52	294.95		
	5201527	59493	GW50114AS	1/4/95	DISSOLVED	MANGANESE	3130		15	V	32.66	120.09	207.52	294.95		
	5201444	59493	GW50113AS	1/4/95	DISSOLVED	MANGANESE	2960		15	V	32.66	120.09	207.52	294.95		
	4674402	59493	GW01247GA	8/18/94	DISSOLVED	MANGANESE	2920		15	V	32.66	120.09	207.52	294.95		
	5329290	59493	GW02176GA	3/9/95	DISSOLVED	MANGANESE	2510		1	V	32.66	120.09	207.52	294.95		
	5368819	71494	GW02241GA	3/14/95	DISSOLVED	MANGANESE	2090		15	Y	32.66	120.09	207.52	294.95		
	5201614	64093	GW50118AS	1/5/95	DISSOLVED	MANGANESE	1300		15	V	32.66	120.09	207.52	294.95		
	5170750	59594	GW02058GA	1/25/95	DISSOLVED	MANGANESE	1160		15	V	32.66	120.09	207.52	294.95		
	5170866	60893	GW50157AS	1/26/95	DISSOLVED	MANGANESE	1100		15	V	32.66	120.09	207.52	294.95		
	3342481	59593	GW01167WC	8/13/93	DISSOLVED	MANGANESE	761		2	V	32.66	120.09	207.52	294.95		
	2763948	59593	GW01025WC	6/24/93	DISSOLVED	MANGANESE	680		1	V	32.66	120.09	207.52	294.95		
	4779662	59593	GW01248GA	8/18/94	DISSOLVED	MANGANESE	608		2	V	32.66	120.09	207.52	294.95		
	5170319	59593	GW50131AS	1/11/95	DISSOLVED	MANGANESE	514		15	V	32.66	120.09	207.52	294.95		
	5170406	61293	GW50126AS	1/7/95	DISSOLVED	MANGANESE	356		15	JA	32.66	120.09	207.52	294.95		
	5389285	59593	GW02175GA	3/6/95	DISSOLVED	MANGANESE	21		0.6	Y	32.66	120.09	207.52	294.95		
133	5198889	55394	GW50106AS	12/22/94	DISSOLVED	MANGANESE	843		15	V	32.66	120.09	207.52	294.95		
	5201556	63793	GW50115AS	1/4/95	DISSOLVED	MANGANESE	765		15	V	32.66	120.09	207.52	294.95		
	2657494	58793	GW01017WC	6/18/93	DISSOLVED	MANGANESE	515		15	V	32.66	120.09	207.52	294.95		
	2815180	58793	GW01168WC	8/12/93	DISSOLVED	MANGANESE	480		15	V	32.66	120.09	207.52	294.95		
	3526955	58793	GW01482WC	11/10/93	DISSOLVED	MANGANESE	477		2	V	32.66	120.09	207.52	294.95		
142	2393067	51193	GW00466WC	3/20/93	DISSOLVED	BARIUM	257		200	V	84	117.1	150.2	183.3		
	4927310	51193	GW01612GA	10/24/94	DISSOLVED	BARIUM	244		9	V	84	117.1	150.2	183.3		
	4927313	51193	GW01613GA	10/24/94	DISSOLVED	BARIUM	243		9	V	84	117.1	150.2	183.3		
	4779516	51193	GW01242GA	8/18/94	DISSOLVED	BARIUM	239		14	V	84	117.1	150.2	183.3		
	5252975	51193	GW02110GA	2/8/95	DISSOLVED	BARIUM	239		12	V	84	117.1	150.2	183.3		
	3449296	51193	GW01477WC	11/12/93	DISSOLVED	BARIUM	235.5		200	V	84	117.1	150.2	183.3		
	2614566	51193	GW00672WC	4/26/93	DISSOLVED	BARIUM	234.5		17	V	84	117.1	150.2	183.3		
	4779517	51193	GW01243GA	8/19/94	DISSOLVED	BARIUM	226		14	V	84	117.1	150.2	183.3		
	3342245	51193	GW01163WC	8/16/93	DISSOLVED	BARIUM	219.5		16	V	84	117.1	150.2	183.3		
	3449306	51193	GW01477WC	11/12/93	DISSOLVED	MANGANESE	3005		15	V	32.66	120.09	207.52	294.95		
	2393077	51193	GW00466WC	3/20/93	DISSOLVED	MANGANESE	2930		15	V	32.66	120.09	207.52	294.95		
	4927512	51193	GW01612GA	10/24/94	DISSOLVED	MANGANESE	2910		1	V	32.66	120.09	207.52	294.95		
	2614578	51193	GW00672WC	4/26/93	DISSOLVED	MANGANESE	2890		1	V	32.66	120.09	207.52	294.95		
	4927515	51193	GW01613GA	10/24/94	DISSOLVED	MANGANESE	2850		1	V	32.66	120.09	207.52	294.95		
	779660	51193	GW01243GA	8/19/94	DISSOLVED	MANGANESE	2810		2	V	32.66	120.09	207.52	294.95		
	4779659	51193	GW01242GA	8/18/94	DISSOLVED	MANGANESE	2780		2	V	32.66	120.09	207.52	294.95		
	3342257	51193	GW01163WC	8/16/93	DISSOLVED	MANGANESE	2775		2	V	32.66	120.09	207.52	294.95		
	5253105	51193	GW02110GA	2/8/95	DISSOLVED	MANGANESE	2470		1	V	32.66	120.09	207.52	294.95		

These data are graphically displayed on Figures 4-7 and 7b

Table 4-8
Summary of Radionuclide COCs Exceeding Background Mean in Groundwater

IHSS	Sequence	Location	Sampl	Sample	TGC	Constituent	Resul	Qualifier	Reporting	Valid	Mean	Mean	(X	STD	DEV)	of background
	ID		No.	Date			in PCI/L		Limit		Mean	X 1	X 2	X 3		
Exceeds the Background Mean b is less than background Mean plus one Standard Deviation																
115/196	5186130	61093	GW50154AS	1/25/95	DISSOLVED	U233234	16.06		0.204	Y		6.914	32.354	57.794	83.234	
	5179279	59793	GW50133AS	1/15/95	DISSOLVED	U233234	14.14		0.124	V		6.914	32.354	57.794	83.234	
	5186114	61093	GW50151AS	1/25/95	DISSOLVED	U233234	14.05		0.328	Y		6.914	32.354	57.794	83.234	
	2891018	61093	GW50012AS	7/13/93	DISSOLVED	U233234	11.5	B	0.042	A		6.914	32.354	57.794	83.234	
	5186131	61093	GW50154AS	1/25/95	DISSOLVED	U235	0.6157		0.223	Y		0.195	0.835	1.475	2.115	
	5179280	59793	GW50133AS	1/15/95	DISSOLVED	U235	0.5459		0.124	V		0.195	0.835	1.475	2.115	
	2891046	63193	GW50013AS	7/12/93	DISSOLVED	U235	0.53	J	0.075	A		0.195	0.835	1.475	2.115	
	3348328	59593	GW01167WC	8/13/93	DISSOLVED	U235	0.37	J	0.22	A		0.195	0.835	1.475	2.115	
	4780715	59593	GW01248GA	8/18/94	DISSOLVED	U235	0.351491		0.219133	V		0.195	0.835	1.475	2.115	
	2891017	61093	GW50012AS	7/13/93	DISSOLVED	U235	0.34	J	0.071	A		0.195	0.835	1.475	2.115	
	5126081	58094	GW50102AS	12/21/94	DISSOLVED	U235	0.3006		0.18	V		0.195	0.835	1.475	2.115	
	5422179	56994	GW02089GA	2/3/95	DISSOLVED	U235	0.269029		0.137205	Y		0.195	0.835	1.475	2.115	
	5014072	59593	GW01619GA	10/24/94	DISSOLVED	U235	0.231264	Y	0.184722	A		0.195	0.835	1.475	2.115	
	2891291	59593	GW01025WC	6/24/93	DISSOLVED	U235	0.2	BJ	0.059	A		0.195	0.835	1.475	2.115	
	5456180	59393	GW02175GA	3/6/95	DISSOLVED	U235	0.195893		0.121974	Y		0.195	0.835	1.475	2.115	
5179281	59793	GW50133AS	1/15/95	DISSOLVED	U238	10.61		0.124	V		4.832	22.502	40.172	57.842		
2891016	61093	GW50012AS	7/13/93	DISSOLVED	U238	8.8		0.071	A		4.832	22.502	40.172	57.842		
2891045	63193	GW50013AS	7/12/93	DISSOLVED	U238	5.4		0.14	A		4.832	22.502	40.172	57.842		
133.2	3348392	58793	GW01168WC	8/12/93	DISSOLVED	AM241	0.018		0.005	V		0.011	0.021	0.031	0.041	
	5178939	56594	GW50105AS	12/22/94	DISSOLVED	U235	0.2769		0.163	Y		0.195	0.835	1.475	2.115	
142.10	2595924	50092	GW00465WC	3/21/93	DISSOLVED	U235	0.39		0.115	A		0.195	0.835	1.475	2.115	
	3548656	50092	GW0176WC	11/9/93	DISSOLVED	U235	0.347146		0.13696	Y		0.195	0.835	1.475	2.115	
	5014067	51193	GW01613GA	10/24/94	DISSOLVED	U235	0.312575	Y	0.159788	A		0.195	0.835	1.475	2.115	
	80708	5193	GW01242GA	8/18/94	DISSOLVED	U235	0.271692		0.289707	V		0.195	0.835	1.475	2.115	
	2626193	50092	GW00670WC	4/27/93	DISSOLVED	U235	0.25	J	0.14	A		0.195	0.835	1.475	2.115	
	5424574	50092	GW02174GA	2/21/95	DISSOLVED	U235	0.21	U	0.46	Y		0.195	0.835	1.475	2.115	
	Exceeds the Background Mean plus one Standard Deviation but is less than background Mean plus two Standard Deviations															
115/196	5186115	61093	GW50151AS	1/25/95	DISSOLVED	U235	1.076		0.283	Y		0.195	0.835	1.475	2.115	
	5186132	61093	GW50154AS	1/25/95	DISSOLVED	U238	28.18		0.223	Y		4.832	22.502	40.172	57.842	
	5186116	61093	GW50151AS	1/25/95	DISSOLVED	U238	26.97		0.255	Y		4.832	22.502	40.172	57.842	
142.10	3548575	50092	GW01476WC	11/9/93	DISSOLVED	RA226	0.386215		0.2391	V		0.258	0.368	0.478	0.588	
Exceeds the Background Mean plus two Standard Deviations but is less than background Mean plus three Standard Deviations																
115/196	2889861	59593	GW01025WC	6/24/93	DISSOLVED	RA226	0.56	B	0.07	A		0.258	0.368	0.478	0.588	
133.2	2889862	58793	GW01017WC	6/18/93	DISSOLVED	RA226	0.55	B	0.08	A		0.258	0.368	0.478	0.588	
142.10	2889793	50092	GW00670WC	4/27/93	DISSOLVED	RA226	0.55		0.2	A		0.258	0.368	0.478	0.588	
Exceeds the Background Mean plus three Standard Deviations																
115/196	3548576	59493	GW01480WC	11/9/93	DISSOLVED	RA226	1.02928		0.16835	V		0.258	0.368	0.478	0.588	
	5387052	71494	GW02241GA	3/14/95	DISSOLVED	RA226	0.8898		0.0337	Y		0.258	0.368	0.478	0.588	
These data are graphically displayed on Figures 4-8a and 8b.																

These data are graphically displayed on Figures 4-8a and 8b.

Table 4-9
Summary of Radionuclide COCs Exceeding Background Mean in Surface Water

IHSS/Site	Sequence ID	Locatio	Sample N	Sample Date	TGC	Constituent	Result in PC/L	Qualifier	Reporting Limit	Valid	Mean (X)	STD DEV	of background
Exceeds the Background Mean b												Mean	X 1
less than Background Mean plus one Standard Deviation												X-2	X-3
142	2596118	SW50193	SW50208JE	3/4/93	TOTAL	U233234	0.5		0.02	A	0.4862	1.0362	1.5862
	2596158	SW50293	SW50210JE	3/24/93	TOTAL	U238	73		0.282	A	0.3642	0.7962	1.2282
	2596156	SW50193	SW50208JE	2/4/93	TOTAL	U238	0.43		0.039	A	0.3642	0.7962	1.2282
SID	25961	SW507	SW50203JE	2/4/93	DISSOLVED	U23 234			0.033		92	5 3	34
	2802121	SW027	SW50222JE	5/17/93	DISSOLVED	U23234	2.0995		0.287212	A	0.92	5.13	9.34
	2802105	SW507	SW5022 JE	5/ 3	ISSOLVED	U23 234	.85		0.3 4962	A	92	5 13	9.34
	2802107	SW507	SW50221JE	5/17/93	DISSOLVED	U238	3.049		0.168335	A	0.708	3.949	7.19
	2802123	SW027	SW50222JE	5/1/93	ISSOLVED	U238	4495		0.256975		0.708	949	7.19
	2596168	SW507	SW50217JE	3/29/93	DISSOLVED	U238	0.88		0.026	A	0.708	3.949	7.19
	2596163	SW027	SW50220JE	2/9/93	DISSOLVED	U238	0.8		0.032	A	708	3.949	7.1
	5020062	SW027	SW00545GS	10/17/94	TOTAL	AM241	0.011		0.01	V	0.0039	0.0119	0.0199
	897475	SW500	SW50000AS	0/5/92	TOTAL	AM24	009538		0		0039	0 9	0. 99
	2802094	SW507	SW50221JE	5/1/93	TOTAL	AM241	0.007072	J	0.010152	A	0.0039	0.0119	0.0199
	2802109	SW027	SW50222JE	5/ 93	TOTAL	AM24	006386	J	0.010758	A	0.0039	0.0119	0.0199
	1897478	SW500	SW50000AS	0/5/92	TOTAL	U233234	0.7748		0.156	A	0.4862	1.0362	1.5862
	2596126	SW027	SW50218JE	2/9/93	TOTAL	U233234	0.77		0.228	A	0.4862	1.0362	1.5862
	897480	SW500	SW50000AS	0/5/92	TOTAL	U238	0.6967		0.22	A	0.3642	0.7962	1.2282
Woman Ch.	23 602	SW026	SW502 3WC	4/92	DISSOLVED	U233234	2.103		0	A	0.92	5.13	9.34
	2616182	SW026	SW50201JE	3/24/93	DISSOLVED	U233234	1.8		0.1458	A	0.92	5.13	9.34
	25	SW50	SW50205JE	3/24/93	ISSOLVED	U23 234	.537		0.264	A	92	5 1	9.34
	2616200	SW029	SW50204JE	2/4/93	DISSOLVED	U233234	.5		0.14767	A	0.92	5.13	9.34
	26 6227	SW03	SW50207JE	2/4/93	ISSOLVED	U23 234	.3		0. 4242	A	0.92	5. 3	9.34
	2549161	SW040	SW50211JE	3/24/93	DISSOLVED	U233234	1.0705		0.226	A	0.92	5.13	9.34
	23 6 6	SW029	SW50216WC	4/92	DISSOLVED	U233234	00875			A	0.92	5 3	9.34
	2616245	SW107	SW50214JE	3/24/93	DISSOLVED	U233234	0.99		0.20696	A	0.92	5.13	9.34
	232 604	SW026	SW50213WC	4/92	DISSOLVED	U238	1.304		0	A	0.708	3.949	7.19
	2616184	SW026	SW50201JE	3/24/93	DISSOLVED	U238	1.1		0.1335	JA	0.708	3.949	7.19
	2616229	SW03	SW50207JE	3/24/93	DISSOLVED	U238	1.1		0.15164	JA	0.708	3.949	7.19
	2102016	SW033	SW50221WC	11/4/92	DISSOLVED	U238	0.9946		0.131	A	0.708	3.949	7.19
	2101998	SW501	SW50219WC	4/92	DISSOLVED	U238	0.8965		0.16	A	0.708	3.949	19
	2616202	SW029	SW50204JE	3/24/93	DISSOLVED	U238	0.76		0.12081	JA	0.708	3.949	7.19
	2549 35	SW501	SW50205JE	3/24/93	DISSOLVED	U238	0. 52		0.274	A	0.708	3.949	7.19
	2616167	SW029	SW50204JE	3/24/93	TOTAL	AM241	0.0094		0.00629	A	0.0039	0.0119	0.0199
	23 1606	SW029	SW50216WC	1/4/92	TOTAL	AM241	0.009255	J	0	Z	0.0039	0.0119	0.0199
	2103896	SW034	SW50220WC	11/4/92	TOTAL	AM241	0.005712	J	0	A	0.0039	0.0119	0.0199
	26 6248	SW107	SW50214JE	3/24/93	TOTAL	AM241	0.0053	U	0.00642		0.0039	0.0119	0.0199
	2616257	SW041	SW50215JE	3/24/93	TOTAL	AM241	0.0045	U	0.00654	A	0.0039	0.0119	0.0199
	2024634	SW040	SW50223WC	1/4/92	TOTAL	AM241	0.0041 7	J	0	A	0.0039	0.01 9	0.0199
	2103906	SW033	SW50221WC	11/4/92	TOTAL	U233234	0.9116		0.141	A	0.4862	1.0362	1.5862
	26 6236	SW03	SW50207JE	3/24/93	TOTAL	U233234	0.88		0.18413	A	0.4862	1.0362	1.5862
	2675623	SW55193	SW70040JE	5/24/93	TOTAL	U233234	0.69	B	0.15	A	0.4862	1.0362	1.5862
	26161 5	SW029	SW50204JE	3/24/93	TOTAL	U238	0.77		0.17916	JA	0.3642	0.7962	.2282
	2549141	SW506	SW50208JE	3/24/93	TOTAL	U238	0.6992		0.335	A	0.3642	0.7962	1.2282
	03908	SW033	SW50221WC	4/92	TOTAL	U238	0.583	J	0.215		0.3642	7962	1.2282
Exceeds the Background Mean plus one Standard Deviation but is less than Background Mean plus two Standard Deviations													
SID	5020064	SW027	SW00545GS	10/17/94	TOTAL	U233234	2		0.3	V	0.4862	1.0362	1.5862
	2596164	SW027	SW50218JE	3/29/93	TOTAL	U238	1.026		0.114	A	0.3642	0.7962	1.2282
Woman Ch.	232159	SW026	SW50213WC	4/92	TOTAL	U233234	1.429		0.197	A	0.4862	1.0362	1.5862
	2103892	SW501	SW50219WC	11/4/92	TOTAL	U233234	1.346		0.149	A	0.4862	1.0362	1.5862
	2549 25	SW50	SW50205JE	3/24/93	TOTAL	U233234	.244		0.216	A	0.4862	0.962	.5862
	2549139	SW506	SW50208JE	3/24/93	TOTAL	U233234	1.133		0.335	A	0.4862	1.0362	1.5862
	2321607	SW029	SW50216WC	4/92	TOTAL	U233234	1.0664		0	A	0.4862	1.0362	1.5862
	2549153	SW040	SW50211JE	3/24/93	TOTAL	U233234	1.066		0.207	A	0.4862	1.0362	1.5862
	2616193	SW026	SW50201JE	3/24/93	TOTAL	U238	1.2		0.19753	JA	0.3642	0.7962	1.2282
	2103894	SW501	SW50219WC	11/4/92	TOTAL	U238	1.131		0.189	A	0.3642	0.7962	1.2282
	2616238	SW033	SW50207JE	3/24/93	TOTAL	U238	1.1		0.16477	JA	0.3642	0.7962	1.2282
	2321609	SW029	SW50216WC	11/4/92	TOTAL	U238	0.94385		0.114	A	0.3642	0.7962	1.2282
	2549127	SW501	SW50205JE	3/24/93	TOTAL	U238	9082		0.245	A	0.3642	0.7962	1.2282
	2549155	SW040	SW50211JE	3/24/93	TOTAL	U238	0.8653		0.174	A	0.3642	0.7962	1.2282
Exceeds the Background Mean plus two Standard Deviations but is less than Background Mean plus three Standard Deviations													
SID	2596155	SW507	SW50203JE	3/24/93	DISSOLVED	U238	.5		0.032	A	0.708	3.949	7.19
	2802113	SW027	SW50222JE	5/17/93	TOTAL	U233234	1.9755		0.256933	A	0.4862	1.0362	1.5862
	5020066	SW027	SW00545GS	0/17/94	TOTAL	U238	.5		0.2	V	0.3642	7962	1.2282
Woman Ch.	26 6191	SW026	SW50201JE	3/24/93	TOTAL	U233234	1.9		0.22804	A	0.4862	1.0362	1.5862
	26 6173	SW029	SW50204JE	3/24/93	TOTAL	U233234			0.15809	A	0.4862	1.0362	1.5862
	2321595	SW026	SW50213WC	11/4/92	TOTAL	U238	1.437		0.171	A	0.3642	0.7962	1.2282
	267562	SW551 3	SW70040JE	5/24/93	TOTAL	U238	1.3	B	0.22	A	0.3642	0.7962	1.2282
Exceeds the Background Mean plus three Standard Deviations													
1 2	2596228	SW50293	SW50210JE	3/24/93	TOTAL	AM241	0.38		0.202	A	0.0039	0.0119	0.0199
SID	2596234	SW027	SW50218JE	3/29/93	TOTAL	AM241	0.18		0.228	A	0.0039	0.0119	0.0199
	2596224	SW507	SW50203JE	3/24/93	TOTAL	AM24	075		0.079		0.0039	9	0. 99
	2802098	SW507	SW50221JE	5/17/93	TOTAL	U233234	4.675		0.196649		0.4862	0.962	1.5862
	2596	SW507	SW50203JE	3/24/93	TOTAL	233234			0.056		4862	0.962	1.5862
	2596154	SW507	SW50203JE	3/24/93	TOTAL	U238	7		0.052	A	0.3642	0.7962	1.2282
	2802100	SW507	SW50221JE	5/ 93	TOTAL	U238	5.206		0. 96649	V	0.3642	0.7962	1.2282
	2802115	SW027	SW50222JE	5/1/93	TOTAL	U238	2.144		0.365052	V	0.3642	0.7962	1.2282

These data are graphically displayed on Figure 4-10.

Summary of Metal COCs Exceeding Background Mean in Stream Sediments

Sequence			Sample		Result		Reporting		Mean (X ± STD DEV) of background			
IHSS	ID	Locatio	No.	C nstituent	in mg/kg	Qualifier	Limit	Valid.	Mean	X ± 1	X±2	X±3
Exceeds the Background Mean but is less than Background Mean plus one Standard Deviation												
Wmn. Ck.	1883115	SED501	SD50004WC	COPPER	14.5		5	JA	10.24	18.01	25.78	33.55
Wmn. Ck.	1883255	SED506	SD50008WC	COPPER	13.4		5	JA	10.24	18.01	25.78	33.55
Exceeds the Background Mean plus one Standard Deviation but is less than Background Mean plus two Standard Deviations												
SID	1883072	SED025	SD50002WC	ZINC	164	E	4	JA	53.86	136.94	220.02	303.1
Exceeds the Background Mean plus two Standard Deviations but is less than Background Mean plus three Standard Deviations												
SID	1883059	SED025	SD50002WC	COPPER	27.1		5	V	10.24	18.01	25.78	33.55
Exceeds the Background Mean plus three Standard Deviations												
SID	1883171	SED507	SD50005WC	COPPER	135.5		5	JA	10.24	18.01	25.78	33.55
SID	1883176	SED507	SD50005WC	MERCURY	3.05		0.1	JA	0.09	0.15	0.21	0.27
SID	1883184	SED507	SD50005WC	ZINC	709	E	4	JA	53.86	136.94	220.02	303.1

These data are graphically displayed in Figures 4-11 and 11b.

IHSS	Seq ence	Location	Sample	Constituent	Resul	Q alifier	Reporting	Valid	Mean (X STD DEV) of background			
	ID		No.		PC/G		Limit		Mean	X 1	X=2	X=3
Exceeds th Background Mean bu is less than Background Mean plus one Standard Deviation												
SID	2341693	SED025	SD50002WC	AM241	0.29		0.021	A	0.173	0.657	1.141	1.625
	2341717	SED507	SD50005WC	AM241	0.25		0.007	A	0.173	0.657	1.141	1.625
	2341697	SED025	SD50002WC	PU239240	1.6		0.007	V	0.537	2.147	3.757	5.367
	2341721	SED507	SD50005WC	PU239240	0.915		0.006	V	0.537	2.147	3.757	5.367

5 0 CHEMICAL FATE AND TRANSPORT

This chapter discusses the chemical fate and transport modeling performed in support of the HHRA for OU 5. The objectives of this modeling were to simulate the transport of COCs from OU 5 to potential exposure points for human receptors under present and anticipated future site conditions and to provide information needed for the evaluation of potential remedial alternatives at OU 5.

5 1 POTENTIAL ROUTES OF MIGRATION

Figures 5 1 through 5 7 illustrate potential routes of migration for groundwater, surface water, and air, respectively. Understanding these routes of migration is not only fundamental to chemical fate and transport modeling, but also is the basis for assessing potential exposure routes to human receptors for the risk assessment. The potential routes of migration in each environmental medium are discussed briefly below. The human health exposure assessment is presented in detail in TM12 (DOE 1995b) and is discussed in Section 6 4.

The hydrogeologic profile of the OU 5 groundwater flow and contaminant transport system, including saturated and unsaturated zones, illustrates the potential migration of contaminants from a source (e.g., the landfill area). This potential migration route runs through the unsaturated and saturated zones of the UHSU to the creek or to seeps along the hillsides adjacent to Woman Creek (Figure 5 1). The profile also depicts the potential contamination of groundwater and soils with VOCs. Once the contaminants reach the seeps, they evaporate or migrate downslope in surface flow or near surface groundwater flow in the unconsolidated material to the creek. They may then be transported via surface water processes. Surface water processes are discussed in Sections 2 3 and 3 4. VOC contaminants in the unsaturated zone could be mobilized by desorption, dissolution, or vaporization from contaminated soil. Once mobilized, contaminants would migrate to the surface and escape into the atmosphere by volatilization. The contaminants could also migrate into groundwater.

The hydrogeologic profile (Figure 5 1) does not include all of the contaminant sources—such as metals and particulate radioactive contamination in soils—that may exist at the site. However, under the hydrogeochemical conditions of OU 5, metals and radionuclides are not expected to be very mobile. Therefore, migration of metals and radionuclides through the groundwater pathway is considered to be

negligible and is not illustrated in Figure 5.1. Nevertheless, the selected transport model has the capability to incorporate radioactive decay and sorption of radionuclides.

The profile of surface water pathways (Figure 5.2) illustrates the numerous potential mechanisms for contaminant migration. Storm water runoff may transport contaminated soils to surface waters through erosion with subsequent transport to downstream receptors. Surface waters and suspended sediments may be impacted from the discharge of contaminated groundwater via seeps and springs. Once groundwater borne contaminants reach surface waters, the potential migration routes are identical to those described above for contaminated storm water.

The air emissions and dispersion models selected to assess concentrations of air contaminants at sensitive receptors estimated the exposure point concentrations for the exposure pathways associated with air transport (Figure 5.3). VOCs may be transported through the vadose zone from underlying soils or groundwater and may intrude into a hypothetical building located within OU 5 (volatilization into indoor air and subsequent inhalation by a future onsite office worker). Chemicals in surface soils may be transported via fugitive particulate emissions from OU 5 to onsite exposure points (inhalation of particulates by the future onsite outdoor worker and ecological researcher). Fugitive dust emissions from OU 5 may also result in the deposition of chemicals in airborne particulates on surface soils and plants.

5.2 CONTAMINANT MOBILITY AND BEHAVIOR

Potential mechanisms for the release of contaminants from OU 5 sources are described in Section 5.1 above and are discussed in additional detail in Exposure Assessment TM for the HHRA TM12 (DOE 1995b) for those pathways determined to be significant to the HHRA. Observed contaminant distributions at OU 5 are the result of chemical and physical interactions between contaminants and the environmental media in which the contaminant resides. These interactions involve processes that determine the transport and fate of contaminants in site soils, sediments, surface waters, and groundwater. These processes include, but are not limited to, adsorption/desorption reactions (including ion exchange), oxidation/reduction, complexation, precipitation/dissolution, volatilization, hydrolysis, dehalogenation, radioactive and chemical decay, and biodegradation.

Contaminant behaviors and mobilities as determined in the fate and transport models described in the following sections are derived from the physical and chemical properties of individual contaminants in the context of the physical and chemical properties of the site as determined from field and laboratory data collected for the specific media at OU 5. Each of the fate and transport models described below are capable of modeling the processes affecting contaminant mobility applicable to the medium/media being modeled. The capabilities of the models are described in detail in TM13 (DOE 1994b) and are summarized in the following sections. In all cases when model parameters affecting contaminant mobility were varied in order to achieve calibration, the parameter estimates used were those that would provide the most conservative results for use in the HHRA.

5.3 CHEMICAL FATE AND-TRANSPORT MODELING

The following sections discuss the procedures followed for the modeling of contaminant fate and transport in groundwater, surface water, and air and the results of this modeling. For each modeling effort, the rationale used for selecting the specific numerical modeling codes is also discussed. Additional detail regarding the selection of fate and transport models is provided in TM13 (DOE 1994b).

5.3.1 Groundwater Modeling

This section describes the groundwater modeling, including flow and solute transport modeling in the groundwater system and simulation of contaminant transport in the vadose zone.

5.3.1.1 Purpose

The purpose of the OU 5 groundwater modeling was to provide an evaluation of contaminant transport via the groundwater pathway in order to support the OU 5 HHRA. This purpose was satisfied by the production of a realistic representation of the subsurface system which was used to estimate contaminant concentrations at locations that are relevant to risk assessment. These locations include areas where potentially contaminated groundwater might flow into Woman Creek. The model area covered by the modeling is depicted on Figure 5-4.

5 3 1 2 Scope

The scope of the groundwater modeling is limited to providing estimates of concentrations of COCs that originate in OU 5 IHSSs. Concentrations are calculated at regularly spaced points in a grid that covers present and possible future contaminant plumes. Radium 226, barium, and manganese have been identified as the only COCs in groundwater (DOE 1995a).

5 3 1 3 Design

Buried ash and debris in OU 5 are potential sources for groundwater contamination. The base elevations of some of these sources are located above the water table and are separated from the water table by unconsolidated surficial materials (such as colluvium). Consequently, some contaminant movement is through unsaturated material above the water table (vadose zone) and the remainder of the subsurface transport pathway is within the saturated zone. For the purposes of the present modeling, numerical flow and transport modeling was used to simulate contaminant movement below the water table in the groundwater system. A one-dimensional solute transport modeling code was used to represent contaminant transport above the water table (i.e., the vadose zone).

Selection of Model Codes Groundwater flow and contaminant transport modeling are combined to produce a representation of contaminant movement in a subsurface system. Computer codes that perform the modeling are commonly called models. Many types of models are available. Mathematical models range from the solution of simple equations to very complex computer programs. In general, the greater the complexity of the model, the closer its behavior approaches that of the actual system (Javandel 1984). Therefore, more complex mathematical models tend to produce better estimates of the actual behavior of the system than simpler mathematical models. The physical systems and processes can be more completely represented in complex models. The selection of a mathematical groundwater model is guided by the complexity of the actual groundwater system, the amount and quality of data available, and the degree of representativeness needed. Model selection for OU 5 is discussed in detail in TM13 (DOE 1994b).

Selection of the Groundwater Flow Model The OU 5 groundwater system is complex. There is a large amount of data for the groundwater system, and a good representation of the groundwater system is

appropriate due to the importance of the HHRA. The risk assessment may be partially based on the results of groundwater modeling. Consequently, a complex mathematical model was selected for simulation of the groundwater flow system.

The complexity of the groundwater flow system is caused by the following site conditions:

- Location of the IHSSs on the slope of a valley wall where the surficial materials include heterogeneous colluvium, landslide deposits, and artificial fill, which result in a wide range of hydraulic conductivity along the flow path.
- Groundwater flowing downhill along an irregular bedrock surface.
- Highly variable saturated thickness between the bedrock surface and the water table, including some areas where the bedrock surface is consistently above the water table.
- Complex water table configuration, and
- Areal variation of groundwater recharge rate, as indicated by different vegetation types.

A complex numerical modeling code, MODFLOW, was selected to simulate the complex groundwater flow system in OU 5. MODFLOW is a widely used finite-difference modeling code developed by the U.S. Geological Survey (USGS) (McDonald and Harbaugh, 1988). The simulated geologic medium is discretized into rectangular volumes (cells).

Selection of the Contaminant Transport Model The complexity of the factors affecting contaminant transport in the groundwater system is indicated by

- The irregular shape of IHSS 115 (Original Landfill)
- The irregular distribution of contamination in the groundwater and soils, and
- The variation of contaminant concentrations in groundwater and soils.

The numerical modeling code selected to simulate the complex transport of dissolved contaminants in the groundwater system was MT3D (Papadopoulos and Assoc., 1992). This code places imaginary particles into the flow system simulated by MODFLOW. The particles are generated in cells that represent contaminant sources. Multiple cells may be used to represent large, irregularly shaped sources. Each particle represents a certain mass of contaminant. These particles move with the groundwater. MT3D can simulate variable rates of contaminant supply at the source. The contaminant mass represented by particles in a cell at any given time may be converted to a corresponding contaminant concentration.

Selection of the Vadose Zone Model The computer code selected to simulate the transport of contaminants downward from a buried source through the vadose zone to the water table was ONED 3 (Beljin and van der Heijde 1993). This code is a one dimensional solute transport model which uses a mass flux boundary condition at the upstream end of the model (Javandel 1984). This simple representation of contaminant transport in the vadose zone is conservative because it represents the shortest possible pathway to the water table. It is compatible with the amount and quality of relevant data that are available for the vadose zone in OU 5. Although the actual OU 5 vadose system is complex, a high degree of representativeness is not needed to produce conservative results.

Model Code Verification MODFLOW has been successfully applied to many complex flow problems and is a widely used and well documented finite difference groundwater flow model supported by the USGS. Verification of MODFLOW has been performed by comparing the numerical results with analytical solutions to the partial differential equation for groundwater flow through porous media (Anderson 1993). MT3D verification is described in Chapter 7 of the user's manual (Papadopoulos and Assoc. 1992).

5.3.1.4 Groundwater Flow Model

The preceding sections used the term *model* to refer to computer codes. This section will use *model* to refer to the actual simulation of OU 5 conditions produced by using MODFLOW. Usage of *model* is revealed by the context.

Time Dependency Groundwater flow in the numerical model is treated as steady state. The steady flow assumption significantly reduces the calibration effort compared to simulating transient flow and attempting to calibrate against time varying heads. Furthermore, steady flow modeling reduces the amount of input required by MT3D.

The long term behavior of the groundwater system is adequately represented by steady conditions because transient short term fluctuations in the configuration of the water table will not significantly affect the long term movement of contaminants. Only long term movement is relevant to risk assessment involving future COC concentrations in groundwater.

Grid The model grid (Figures 5 5a through d) is extensive enough to include all of the IHSSs in OU 5 that were found to contain contaminants during the OU 5 RFI/RI field investigation. The grid includes the reach of Woman Creek that passes through OU 5 and is aligned with the course of the creek. Woman Creek receives groundwater inflow during high water table stages and may carry contaminated groundwater downstream mixed with surface water from other sources. The grid also includes local features that could affect the groundwater flow system including the SID and Pond C 2. The French drain on the 881 Hillside is included as a no flow boundary.

The grid contains only one layer which is sufficient to represent groundwater flow in relatively permeable surficial materials above the relatively impermeable claystone bedrock surface. Bedrock is the undifferentiated Arapahoe and Laramie Formations which contain sandstone lenses however no significant thickness greater than 5 feet of permeable sandstone was found in contact with the surficial materials in OU 5 boreholes. Therefore no representation of Arapahoe Formation or Laramie Formation sandstone is included in the model.

The grid spacing near the IHSSs that are potential sources of groundwater contamination is 50 feet. The spacing is increased to 100 feet elsewhere in the model. In accordance with accepted practice a transitional spacing of 75 feet is used between the small and large cells (Trescott, 1976). Using larger cells in the peripheral parts of the model has little effect on the model results. Contaminant sources and plumes are not located in these areas so small cells are not needed for detailed solute transport analysis. Hydraulic conductivity zones with dimensions less than 100 feet are not relevant and may be treated by using equivalent hydraulic conductivities (Freeze and Cherry 1979) applied to 100 foot distances.

Model Boundaries The undifferentiated Arapahoe/Laramie Formation (claystone bedrock) underlying the surficial materials is relatively impermeable (EG&G 1995a). Consequently the base of the model was treated as a no-flow boundary. The bedrock surface is uneven so this boundary is uneven.

The model is composed primarily of active cells which represent the part of the model where groundwater movement is simulated. The lateral boundaries of the active cells are shown in Figures 5 5a through d. The boundaries approximate the OU 5 boundary on the north and west sides of the model. The eastern boundary was placed so as to include effects of Pond C 2 and the Woman Creek diversion on groundwater flow to Woman Creek.

The south boundary of the active cells follows Woman Creek west of Pond C 2. This boundary is a groundwater divide and is simulated as a constant head boundary. This type of boundary is suitable because the average water table elevation at Woman Creek is within the limited range between the creek bottom and bedrock. This limited range is indicated by average water level elevations in monitoring wells located near the creek. It is also indicated by a seepage study that showed Woman Creek within OU 5 to be losing water most of the year (Fedors and Warner 1993).

Initially, the active part of the model grid extended to the south of Woman Creek, and the creek was represented by the MODFLOW river package. However, early model runs were not successful because the water table beneath Woman Creek is too close to the bedrock surface. Consequently, some cells at Woman Creek became dry during head oscillations while model runs were converging, even when underrelaxation was used. This problem was solved by using constant heads in the cells following Woman Creek. Because no contaminant sources are known to be present south of Woman Creek, the southern part of the model became extraneous, and these cells were inactivated.

Most of the remaining boundary of the active part of the model is represented by constant heads, because water levels at a boundary can be more accurately estimated than flux or a proportionality constant for the general head boundary package. Estimation of the constant heads at boundaries is facilitated because the water table must be within the thin surficial deposits. Furthermore, heads are indicated by some monitoring wells that are present near the model boundaries.

No flow boundaries were used where the model boundary is parallel to the water table gradient. A no flow boundary also follows the French drain on the 881 Hillside. The drain is treated as completely effective in preventing downslope movement of groundwater.

Bedrock Elevation Bedrock elevation throughout the OU 5 area was mapped using bedrock surface data from boreholes. In areas of sparse coverage, the thickness of surficial materials and the configuration of the land surface were considered when interpreting the configuration of the bedrock surface. The model behavior is very sensitive to bedrock configuration because water flows downhill on the bedrock surface. Consequently, bedrock elevations supplied to the individual cells were transferred from the bedrock map (Figure 3-5) to the MODFLOW input file by hand to avoid any unrealistic values that might be generated by software interpolation and extrapolation.

Hydraulic Conductivity Zones of initial hydraulic conductivity corresponded to the areal distribution of units on the Surficial Geologic Map of the Rocky Flats Site and Vicinity (Shroba and Carrara, 1994). Five surficial materials are mapped within the active model area. They are landslide deposits, colluvium, Rocky Flats Alluvium, Piney Creek Alluvium, and artificial fill. Landslide deposits and colluvium were lumped together in the initial hydraulic conductivity zones due to their similar origin and texture. Consequently, there were four zones of initial hydraulic conductivity as shown on Figures 5.6a through d.

The initial estimate of hydraulic conductivity for the zones representing colluvial material and artificial fill was 0.0029 feet per day (ft/day), which is in the range of conductivity values for a silt matrix (Freeze and Cherry, 1979). Shroba and Carrara (1994) describe the colluvial deposits as silty sand, sandy silt, clayey silt, and silty clay. The textural composition of the fill is similar to the colluvium and landslide deposits.

The initial estimate of hydraulic conductivity for the Rocky Flats Alluvium was 2.6 ft/day, which is within the range of values reported for pumping tests and slug tests adjacent to OU 5 (about 0.005 to 8.8 ft per day).

The initial estimate of hydraulic conductivity for the Piney Creek Alluvium along Woman Creek was 34.6 ft/day. This value is based on the geometric mean of late-march drawdown in a delayed yield analysis of test data from a well near Woman Creek west of Pond C-1 (Doty and Associates, 1992).

Recharge No site-specific recharge studies are available to provide hard data for recharge estimates for OU 5. Consequently, recharge was treated as a calibration parameter for OU 5 modeling. Previous modeling studies at the Site have used recharge values ranging from 2.96 inches per year to 2.25 inches per year (DOE 1993k, EG&G 1993b, EG&G 1994f, Fedors and Warner 1993, ICF Kaiser 1993). However, initial recharge estimates were made to begin the calibration with realistic recharge zones and relative recharge rates. The initial recharge zones were based on vegetation types shown on the Rocky Flats Plant Vegetation Map (DOE 1992c, Figure 3.2.3). Initial recharge estimates are presented in Table 5.1. These estimates are based on precipitation minus consumptive use for the period from May 1993 through April 1994, which is the period used to calculate the water table calibration targets described below. Precipitation at the Site for the period was 14.73 inches (EG&G 1993a, 1994c). The monthly distribution of the precipitation is shown in Table 5.2. Figures 5.5a through d show the initial allocation of recharge rates to the model grid. Positive recharge indicates inflow to a cell. Negative recharge

indicates outflow from a cell and represents net extraction by phreatophytes. The uncertainty associated with these recharge rates is large and they were changed during the model calibration. However, relative rates associated with the vegetation types were retained.

The Blaney Criddle Method was used to estimate consumptive use for the initial estimates of relative recharge because the method is well established and documented. In addition, Blaney Criddle consumptive use coefficients have been published for many vegetation types, including natural vegetation types that occur in semi-arid regions. Applicability of the Blaney Criddle Method at the Site was investigated by comparing potential evapotranspiration (PET) calculated by the Blaney Criddle method to PET calculated by the more elaborate Penman Method when Site climatic data are used. The Penman calculations were made by Koffer (1989). The Blaney Criddle calculations were made by employing the consumptive use coefficients for short green grass (Quackenbush and Phelan, 1965). Results are shown in Figure 5.8. The plots for monthly PET are similar for the two methods, except for an unexplained atypical data point for the month of May in the Penman curve.

The consumptive use rates calculated by the Blaney Criddle method for the period May 1993 through April 1994 are shown on Table 5.3. These calculated rates correspond to water used by plants that are relatively well watered. However, much of the modeled area is a south-facing hillside that becomes dry in the summer. The grasses wilt and turn brown, indicating the development of a soil moisture deficiency. Experiments with grasses at Fort Collins, Colorado, have shown that grass remains green when irrigated at about 50 percent of the Blaney Criddle consumptive use rate and continues to live when moisture supply is only about 20 percent of that required for optimum growth (Quackenbush and Phelan, 1965). Using this behavior as a guide, a medial value of 33 percent of the calculated consumptive use rates in the dry grassland areas was used as a rough approximation of actual consumptive use. Consumptive use by phreatophytes calculated by the Blaney-Criddle Method was adjusted upward (three percent increase). This adjustment is consistent with the slightly higher PET calculated by the more elaborate Penman equation for July through mid-September (Figure 5.8).

When recharge rates shown in Table 5.1 are compared to the precipitation distribution in Table 5.2 and potential evapotranspiration shown on Figure 5.8, they suggest that groundwater recharge for the dominant dryland vegetation types may represent a large proportion of precipitation during the part of the year when evapotranspiration rates are low. This calculated amount of recharge seems plausible, however,

it could be greater than actual recharge because the soil moisture deficiency developed between precipitation events in the growing season is unknown

The hydrographs shown in Figure 5.9 are in general agreement with winter/spring recharge. They show a tendency to have low water levels in the summer and a rise in water levels beginning sometime in the September to December interval. Well 58793 is an exception. It shows only a slight rise by March suggesting a more delayed response to recharge. Actual recharge is unlikely to be much greater than the initial recharge estimates because the annual recharge approaches the measured amount of spring precipitation.

Due to large values of PET (Approximately 40 inches per year ([Fedors and others 1993]) the recharge rates at the Site are probably considerably less than the spring precipitation. Previous documented studies contain lower estimates of recharge. Due to the uncertainty in the recharge estimate it was considered as a calibration parameter subject to restrictions obtained from previous modeling studies.

Calibration Development of the groundwater flow model included calibration to representative water levels measured in monitoring wells. Calibration involves modifying model variables that are not accurately known. In the present model these calibration variables are hydraulic conductivity and recharge rate. Modification of bedrock elevation and boundary heads was also necessary in some cells where they had not been measured. The variables are changed in successive trial computer runs until the field measured hydraulic heads are adequately approximated by the model. The values assigned to the variables must be within the ranges appropriate for the hydrologic and geologic conditions of the area. Calibration does not produce a unique solution to the problem of representing the actual system, because more than one combination of parameters may cause hydraulic heads to be approximated equally well. However, if adequate constraints are applied to the values of the variables, calibration can produce a realistic solution for a complex problem. The representativeness of the solution may be judged by comparison of values assigned to model variables to measured values in the model area and to values reported in the scientific literature for similar subsurface materials and recharge conditions.

If sufficient data are available, the predictive capability of the model may be validated by testing its ability to predict heads that were not included in the calibration. In the present case, insufficient data are

available to test the predictive capability of the flow model. However, an analysis of uncertainty in the contaminant concentrations predicted by the linked flow and transport model was performed.

Calibration Targets Selection of calibration targets involved identifying a period when water levels were representative and water level data were relatively abundant. The period selected was May 1, 1993 to April 30, 1994. Long term precipitation data from the Boulder, Colorado station (NOAA National Climatic Data Center) shows that precipitation in 1993 was normal (Figure 5-10). Precipitation data for all of 1994 are not yet available. Monitoring well hydrographs also indicate normal hydrologic conditions in 1993-1994 (Figure 5-11). Most of the existing monitoring wells and wellpoints in OU 5 were installed in 1993, and water level measurements from these wells and wellpoints are available for the period from May 1993 through April 1994.

Target water levels are restricted to those wells screened in the surficial material and that record water levels above the bedrock top throughout the selected period. Wells that satisfied this restriction were wells 5686, 6586, 7086, 51193, 58793, 59493, and 59593. The locations of these wells are shown on Figure 5-5A. Average water levels in the wells for the selected period were used as the target water levels. Hydrographs displayed in Figure 5-9 show the degree of representativeness of the average water level for the selected period. Departures from the mean are generally less than two feet and the mean is not affected by extreme values. Wells that were consistently dry throughout this period were also considered in the calibration. Consistently dry wells were 50192, 50292, and 61293. Calibration included producing dry model cells at these well locations.

Most of the water level data in the OU 5 area are from wells and wellpoints that do not satisfy the criteria for target water levels. However, data from these wells were considered semi-quantitatively in the calibration by calculating average water levels regardless of the period represented or the number of water levels available. Dry measurements were not included in the average. These averages were treated as secondary information for identifying any further modifications that should be made in model variables to obtain agreement with all available data.

Calibration Procedure The general calibration procedure was to start with initial estimates of the calibration parameters (hydraulic conductivity and recharge) and minimize deviations from them. Water level elevations on the hillslope were found to be sensitive to bedrock configuration and boundary heads.

and some adjustment from initial estimates in certain cells was also required. The initial estimates of values for the calibration parameters were based on analysis of available climatologic, hydrologic, and geologic data. This calibration procedure is equivalent to estimating the parameters of the groundwater flow system and then improving the estimate via model calibration. If sufficient site specific data are available for the calibration parameters (hydraulic conductivity and recharge) and geologic controls (bedrock elevation), the expected result is a realistic model.

The first phase of the calibration involved adjusting parameter values to produce calculated water levels below land surface elevations throughout the model. Model parameters were adjusted after successive modeling runs until all heads were below land surface elevations. Boundary conditions were also altered during the first phase of the calibration. The southern boundary of the model consisted of constant heads in the southernmost row of the model, with Woman Creek simulated by the MODFLOW river package. However, as discussed in Section 5.3.1.4, some river cells contained bedrock elevations estimated at only a foot below the streambed elevation. These cells converted to dry cells prior to completion of the modeling run. The dry cells produced by the numerical process resulted in unrealistically high calculated heads north of Woman Creek. When riverbed conductance (capacity to transmit water) was increased to prevent the conversion to dry cells, the model did not converge. Consequently, cells along the course of Woman Creek were converted to constant head cells to obtain better results. Cells south of Woman Creek were inactivated. For cells along reaches of the creek that lose water most of the year, the head was initially set 0.5 feet below the stream bottom elevation. For cells along reaches classified as gaining, the head was initially set 0.5 feet above the bottom elevation. Gaining and losing reaches were based on results of an infiltration/exfiltration study conducted from December 1991 through October 1992 (Fedors and Warner, 1993). Setting heads 0.5 feet below the elevation of the stream bottom is consistent with a field search that revealed no bedrock exposed at the stream. The initial constant heads were subject to change during subsequent calibration runs, if necessary, to adequately simulate heads measured in observation wells near the stream.

The change of the southern model boundary condition did not represent a significant change in representativeness and usefulness of the model. The change eliminated riverbed conductance as a calibration parameter that would have to be adjusted to produce heads in the river cells. Instead, heads were supplied directly as a constant head boundary. Groundwater flow south of the creek is not needed for

solute transport analysis because no contaminant sources were identified there by soil borings during the OU 5 field investigation

Additional convergence problems were caused by cells converting to dry cells during the modeling runs if the wetting capability in the BCF2 package was inactive. However, when wetting capability in BCF2 was activated, wet/dry oscillations were produced. To eliminate this oscillation, BCF2 wetting was inactivated and extreme under relaxation (dampening of head oscillations) was used in the model to prevent drying of cells early in the simulation run. Calculated heads near dry cells were inspected on spreadsheets during the calibration process. When dry cells produced by calibration runs were not realistic and caused adverse effects on the calibration, model parameters were modified to increase flow to these cells.

During the first phase of calibration, hydraulic conductivity in the initial zone 1 (colluvium and landslide materials) was increased from the initial value of 0.00288 ft/day to 7.0 ft/day west of Pond C 2 and to 1.152 ft/day east of Pond C 2. Zone 2 (fill) was increased from an initial value of 0.00289 ft/day to 0.185 ft/day. These increases in hydraulic conductivity are within the range expected for these materials. These changes reduced heads in hillslope areas throughout the model. A new zone was created from zone 1 east of the Woman Creek diversion around Pond C 2 to reduce heads east of the pond. The hydraulic conductivity initially assigned to this zone was 5.76 ft/day. Heads east of Pond C 2 were also reduced by extending the initial zone 4 (alluvium) to cover alluvial material shown on a worm's eye map of geologic materials present at the bedrock surface (EG&G 1995a). In addition, constant heads along Woman Creek east of Pond C 2 were reduced to 0.5 feet above bedrock. Other minor adjustments were made to bedrock elevations and constant head boundaries to reduce water levels below land surface in local areas. Hydraulic conductivity in the zones representing colluvium, landslide material, and fill was adjusted further in local areas.

During the first phase of calibration, the effectiveness of reducing recharge to reduce heads was tested by setting recharge zones 6, 8, and 9 (grassland and disturbed areas on the hillside) to zero. The effect on water levels south of the east end of the Original Landfill near cell (17, 51) (row, column) showed that although the head in the cell (17, 51) was reduced by 6 feet, it was still 2 feet above the land surface. It was necessary to increase hydraulic conductivity in the area to reduce the head to below land surface. Because this test showed that recharge adjustment was less effective for calibration than varying hydraulic conductivity, recharge was subordinated to hydraulic conductivity as a calibration parameter.

The goal of the second phase of the calibration was to reduce deviations of calculated heads from target heads and to produce dry cells where monitoring wells are consistently dry. This phase primarily involved local adjustment of hydraulic conductivity to raise or lower calculated heads corresponding to individual target heads. In addition, constant heads were adjusted along some reaches of Woman Creek and localized sections of the northern boundary. Phase 2 produced a model in which all interpolated heads were within a half foot of heads in target wells and dry wells were represented by dry cells. This is a high degree of calibration. The root mean squared residual is 0.22 (Table 5.4) whereas a good calibration would only require the statistic to be less than 2.0. This calibration criterion is based on the dimensionless error variance measure of goodness of fit (Cooley 1977) and calibrated models described in Anderson and Woessener (1991).

The third phase of the calibration was a refinement in which water level information from miscellaneous wells and wellpoints was used to check the representativeness of the model. Data from an additional 49 water level observation points were assembled and average water levels were calculated. These averages represented different periods, included variable numbers of measurements, and did not include instances when wells were reported to be dry. Although such information at any point does not necessarily provide a good representation of long term water levels, the model should be compatible with them. Consequently, the averages were placed in a HeadCompare (Papadopoulos & Assoc. 1993) input file as secondary observed water levels. Interpolated model heads were compared to these secondary water levels to identify observation points where model heads were not compatible with miscellaneous observations.

One point of incompatibility was at well point 62893 in cell (6, 83) which measured water levels in a wet area. This wet area is believed to be caused by an impedance to groundwater flow from downslope decreases in hydraulic conductivity. Simulated heads were too low at this location and hydraulic conductivity was decreased in a new zone downslope to reflect the probable cause for the wet area. New hydraulic conductivity zones were also introduced to obtain better model results by increasing water levels in the vicinity of well point 52193 in cell (20, 34) and well point 53292 in cell (12, 72) and by decreasing water levels near well 52693 in cell (14, 62).

Constant heads at Woman Creek were changed near wellpoints 53593, 53993 and 54793 in cells (21, 96) (13, 107) and (8, 135) respectively to reflect their proximity to the creek. Additional miscellaneous

changes in constant heads and local hydraulic conductivities were necessary to maintain calibration in the target wells and deal with minor calculated head incompatibilities with the secondary data points

The third phase also involved improving the agreement between model hydraulic conductivities and hydraulic conductivities from aquifer tests that were conducted within the active area of the model. The hydraulic conductivity in cell (13 68) was reduced from 7.0 to 6.0 ft/day to obtain agreement with a slug test in well 59593. Hydraulic conductivity near well 51193 was changed to 15 ft/day which agrees with pumping test results and treats the cells as being transitional between nearby cells that were 34.56 and 7.0 ft/day. The transitional nature of this area could be caused by the presence of alluvium in the area covered by the cell. The third phase produced a well-calibrated model; however, the hydraulic conductivity of much of the colluvium that covers a large part of the model area remained at the high value introduced in the first phase of the calibration.

High values for hydraulic conductivity were used to reduce water levels at this early calibration stage because reducing recharge rates to zero did not produce adequate water level reduction. The final phase of calibration was an adjustment so that hydraulic conductivity in the colluvium agreed with pumping test results obtained from colluvium on the 881 Hillside (there were no successful pump tests for colluvial wells within the active model area). The 881 Hillside is located north of the middle part of the active model. Much of the colluvium in the model remained at the value of 7.0 ft/day set in phase one of the calibration. However, the average hydraulic conductivity for drawdown recovery tests reported for the 881 Hillside is 0.95 ft/day. To bring hydraulic conductivity of colluvium in the model into better agreement with this value, hydraulic conductivities throughout the model were divided by 7.0 to bring the large areas of colluvium down to 1.0 ft/day. All recharge values in the model were also divided by 7.0 to maintain the calibration. The resulting recharge values were still within the range of possible values because uncertainty associated with the initial values was large. A few additional changes in model hydraulic conductivity values were made to maintain agreement between model hydraulic conductivity values and pumping test results within the active part of the model. Minor adjustments in model parameters were also made at this time. Some boundary heads were changed to bring them into better agreement with monitoring well data, and hydraulic conductivities and recharge rates were changed in a wet area near the east end of the Original Landfill where particle tracking indicated that the shape of a hydraulic conductivity zone was not natural. The resulting hydraulic conductivities and recharge rates

were still within realistic ranges throughout the model and this result was accepted as the calibrated flow model

Calibration Results The degree of calibration produced by the modeling is indicated by Table 5.4. The maximum residual for target water levels is 0.27 feet. The degree of correspondence between calculated heads and secondary water levels is shown by Table 5.5. The largest absolute residual for a secondary water level is 6.54 feet for well point 60693. This well point is only 78 feet from well point 60593 which has an absolute residual of only 1.12 feet. These wellpoints have only two water level measurements each and are in an area with a relatively steep sloping land surface. Well 63093 has a residual of 6.46 ft. It has only two measurements and is 82 feet from well 51493 which has 10 measurements and an absolute residual of just 0.20 feet. Well point 54193 has an absolute residual of 5.70 feet. It is only 28 feet from 54093 which has an absolute residual of just 0.35 feet. Both 54093 and 54193 are in the same 50 x 100 foot model cell. The model is not intended to represent such small scale hydrologic features. Well point 62793 has an absolute residual of 5.20 feet. Its water level is based on only two measurements taken at about the same time. The well is along the same topographic contour as well 59793 which is about 75 feet away and has a residual of 2.48. Because one of the calculated water levels is higher than the measured one and the other is lower than the measured one the model results are reasonably representative. The remainder of the residuals for secondary water level data indicate that the model results are compatible with the secondary data considering the data distribution in space and time.

The final distribution of hydraulic conductivity values in the model is shown on Figures 5.12a through d and Table 5.6. A detailed map of hydraulic conductivity is in Appendix F. The initial four zones of hydraulic conductivity which ranged from 0.00288 ft/day for colluvial and landslide material to 34.56 ft/day for alluvium evolved into 25 zones ranging from 0.014 ft/day in a heterogeneous area in the south central part of the Original Landfill to 29 ft/day for alluvium east of Pond C.2.

The final range of hydraulic conductivity in colluvium and landslide areas is 0.0357 to 28.6 ft/day. The calibrated value of 2.86 and 0.063 ft/day were applied to zones in the vicinity of Ash Pit IHSSs 133.1 and 133.2 respectively. As previously stated most of the colluvium and landslide area in the model was assigned a hydraulic conductivity of 1.00 ft/day. These values for colluvium are in the range of expected values for silt and silty sand given by Freeze and Cherry (1979) and are compatible with the description of the colluvium. In addition hydraulic conductivities corresponding to alluvial material were expanded into

the area originally treated as colluvial and landslide material near Woman Creek. This expansion suggests that alluvium is present beneath colluvium at a few places near the creek. The final range of hydraulic conductivity in artificial fill was 0.0143 to 0.929 ft/day, which is consistent with some of the fill composed of disturbed and compacted colluvium.

The final range of hydraulic conductivity of alluvium near Woman Creek was 4.94 to 28.6 ft/day. The final range of hydraulic conductivity for Rocky Flats Alluvium was 0.357 to 0.429.

The final bedrock configuration is shown in Figures 5.13 A through D, 5.14, and 5.15. The model was sensitive to bedrock configuration because the groundwater is flowing down the bedrock slope through thin surficial materials. Recharge zones and recharge rates resulting from the calibration are shown in Figure 5.14 and Table 5.7. The simulated water table configuration is shown in Figure 5.15, which also reflects the final constant head values in boundary cells.

Water Budget. The water budget for the model is shown in Table 5.8. The inflow from constant head cells is nearly all from the cells along the northern boundary of the model and represents groundwater from upslope areas. This contribution is from groundwater flowing along the bedrock surface that slopes southward toward the OU 5 area.

Nearly all outflow to constant head cells is to cells along the southern boundary of the model. This boundary follows Woman Creek and the outflow represents discharge of groundwater to the stream during periods of high water table when the stream is gaining. It represents an average flow of 0.036 cubic feet per second or 26.6 ac ft/year. In the real system, this water would evaporate from Ponds C 1 and C 2 or be carried around Pond C 2 by the Woman Creek diversion. Actual discharges for Woman Creek in the Pond C 1 and C 2 area range from about 300 to 1975 acre feet per year, corresponding to 0.4 to 2.72 cubic feet per second (ASI 1991). The simulated water budget represents a minor contribution to Woman Creek flow.

Particle Tracking. Results of particle tracking are shown in Figures 5.16a through d. The particle tracking was performed using MODPATH (Pollock 1989). This software uses output from MODFLOW to compute the path and rate of movement of water from selected source locations. Although particle tracking does not include the effects of dispersion, it provides a good overview of the nature of the flow.

system and potential rate of contaminant movement. It is helpful in identifying the sources for contaminants observed in groundwater and provides initial information on the rate of contaminant movement.

Estimates of effective porosity must be supplied to MODPATH in addition to the output from MODFLOW. The effective porosity estimates used to produce the particle tracks are shown on Table 5.6. They are based on a general relationship between specific yield and hydraulic conductivity (Luthin 1966 Figure 10.10). Specific yield is similar to effective porosity (Fetter 1980). Effective porosity in each cell of the model was determined by the hydraulic conductivity in the cell. As shown in Table 5.6, these effective porosities ranged from 0.01 for the lowest hydraulic conductivity (0.0143 ft/day) to 0.19 for the highest hydraulic conductivity (2.86 ft/day).

The particle tracks show that the groundwater flow rate is variable throughout the model area and that paths are deflected around areas of relatively low hydraulic conductivity. Pond C-2 captures groundwater from sources to the west of the pond. Groundwater originating east of Pond C-2, including seepage from the Woman Creek Diversion, moves toward Woman Creek where it exits the eastern edge of the model.

5.3.1.5 Solute Transport Model

COCs in Groundwater In order to assess the potential risk to human health from exposure to OU 5 groundwater, constituents of the groundwater were evaluated as potential chemicals of concern. TM11 (DOE 1995a) defines COCs as metals or radionuclides whose concentrations exceed background concentrations and organic chemicals present at levels greater than analytical detection limits. Eleven groundwater constituents were identified as COCs for OU 5, including five metals and six radioactive elements (DOE 1995). They are aluminum, barium, manganese, vanadium, beryllium, americium-241, plutonium-239/240, radium-226, uranium-233/234, uranium-235, and uranium-238. Further discussion of the COCs and the methods of their selection are provided in TM11 (DOE 1995a).

Target Wells As potential calibration targets for solute transport modeling, OU 5 wells were evaluated with respect to the eleven COCs. Only 1993 analytical data were used in this evaluation, corresponding to the time period selected for the flow model calibration. All analytical data for dissolved constituents in groundwater collected from OU 5 RFI/RI wells were reviewed for occurrences of the COCs. Of these data

results flagged as rejected (R) laboratory replicate (LR) field blank (FB) trip blank (TB) and rinsate were removed from the data set. Additionally duplicates were averaged with the corresponding real samples and all results listed as non detects were set at values of one half the detection limit (DOE 1995a). To detect the presence of a COC in concentrations that satisfactorily set it apart from the background population, well maxima for each COC were screened for values above background mean plus two standard deviations. This screening provides a means of identifying chemicals that are present in concentrations greater than most of the background population and which therefore may reflect actual contamination. The screening procedure resulted in the identification of three COCs: barium, manganese, and radium 226. The eleven COCs, the screening values, the well means, and the results of the screening procedure are presented in Table 5.9.

Target Concentrations. Inspection of the 1993 data for the COCs showed no general trends in concentration over time (Table G.1, Appendix G). During this relatively short period, the observed concentration in each well was sufficiently stable that any general temporal trend that may exist was too small to separate from the scatter of the data. The scatter of the data at each well may be caused by many factors, including short term variation in groundwater recharge rate, variation in source concentration, and geochemical variability of the aquifer system combined with temporal variation in flow direction and rate. In such aquifer systems, the population of random variations in concentration at an observation point might be expected to be approximately normally distributed about a central value (Mood and Graybill 1963). This central value (population mean) is the most representative value because concentrations near this value will be most frequently observed. Because a sample mean is an unbiased estimate of the population mean, the mean of observed concentrations for each contaminant at a well was used to generate a target value at that well.

The chemical specific means from each well were compared to the background mean of that chemical. Target concentrations for each COC were established by subtracting the background means from the well means. Those means that were found to be greater than the background mean were used as calibration targets. Those that fell below background mean were considered zero for the purposes of calibration. This second screening resulted in targets for the three COCs. This information is presented in Table 5.10. Borehole logs and completion details of the target wells 58793, 59493, 59593, 50092, and 51193 are presented in Appendix H.

Sources for COCs In order to identify potential sources for the three COCs the following documents were reviewed

- Historical Release Report for the Rocky Flats Plant, EG&G Rocky Flats Volume I Text, Manual No 21100 TR 12501 01 June 1992 Pages SE 1 to SE 14 SW 1 to SW 16 400-1 to 400 2 800 1 to 800 2 900 1 to 900 2 and 900 10 to 900 12
- Health Studies on Rocky Flats Phase 1 Rocky Flats Toxicologic Review and Dose Reconstruction Task 3/4 Draft Report, ChemRisk February 1992

In the sections reviewed in the Historical Release Report (HRR) (EG&G 1992i) there is no mention of spills or releases of radium 226 barium or manganese or chemicals containing these constituents There are however several references to depleted uranium sources which may account for the presence of radium 226

Neither barium nor manganese are contained in the list of materials of concern as selected in Task 2 of the Health Studies on Rocky Flats Manganese is not referenced anywhere in the HRR. However barium is mentioned once in the document as barium chromate listed on the 1988/89 inventories of the chemicals for buildings 559 and 771 One pound was reported in a utility room in Building 559 and another pound was reported in Room 180F in Building 771

From this review no distinct sources of barium or manganese have been identified It appears unlikely that the barium chromate located in the buildings in 1989 would be a possible source of barium However if its earlier presence on site were undocumented that occurrence could be a source No source of manganese related to plant operations was identified

IHSS 115 The three COCs in the Original Landfill (IHSS 115) wells appear to be related to the same source the northernmost former filter backwash pond Pond 6 (IHSS 196) Wells 59593 and 59493 are on the same particle track (Figure 5 16) originating at the site of the former pond Well 59493 has a mean of 1 03 pCi/l for radium 226 and well 59593 has a mean of 0 56 pCi/l for radium 226 These values are consistent with the supposition that the pond is the source of the radium 226 and that well 59493 is closer to the source than 59593 This relationship is also supported in the manganese means of 6 130 $\mu\text{g/l}$ in well 59493 and 575 7 $\mu\text{g/l}$ in well 59593

Pond 6 is mentioned in a discussion of the Southwest Buffer Zone Section 3 4 of the HRR (EG&G 1992i) as PAC reference number SW 196 (IHSS 196) the backwash pond for the water treatment plant. This

pond apparently originated as an evaporation/settling pond and was used for the backflushing of sand filters from the Waste Treatment Plant located north of the Original Landfill. The location of the pond is noted as about 800 feet south of Building 124; this is consistent with TM15 (DOE 1994a) maps but not with the HRR map. The site of the pond may have originally been used as an incineration pit for the burning of contaminated waste from Building 444 and also as a dump site for ashes from the plant incinerator, graphite, used caustic drums, and general trash. The area was probably used as a burn pit for only one or two years (1952–1954) prior to the construction of the evaporation/settling pond between January and March 1955 (EG&G 1992i). A likely source of the radium is the incinerator ash derived from uranium-contaminated (depleted uranium) waste from Building 444, although radium-226 is not noted. There is no estimate of the mass of uranium in the HRR.

Well logs from 59493, the well constructed within the Original Landfill at the south end of the Pond 6, indicate that landfill debris, including graphite and broken glass, extend to within 1.2 to 2.2 feet above bedrock (bedrock at 14.1 feet). The water table was two feet below ground surface during drilling in June 1993 and was five to six feet below ground surface during pump testing in August 1993 (DOE 1994a). This is interpreted to mean that the source is below the water table. The area of the former pond as shown on TM15 maps is based on aerial photography and is estimated as 45 feet in diameter and circular in shape. The size is very close to that of the model cell size in the Original Landfill area, 50 feet by 50 feet.

IHSS 133 The relationship of the COCs in well 58793 to a source in the north ash pit of IHSS 133.2 is supported by the particle tracks generated by MODPATH (Figure 5.16). In addition, the presence of radium is consistent with the history of the ash pit, in that ash buried in the pit contained depleted uranium (EG&G 1992i) and ash sample monitoring in 1956 showed 1.9 grams of depleted uranium per kilogram of ash (1.7 kilograms/ton). The south ash pit is not modeled as a source, even though target well 58793 is located just to the south and downgradient of the south ash pit. The pit does not show up on a time domain electromagnetic survey and therefore probably does not contain metal (DOE 1994a). Additionally, borings in the south trench did not encounter ash material (DOE 1994a).

The HRR describes the pits as trenches, 150 to 200 feet long, 12 feet wide, 10 feet deep, and covered with 3 feet of earth. However, the HRR also contains documentation of a trench as eight feet deep with six feet of compacted ash and two feet of earth cover. The ash pits/trenches were in use from 1959–1968. The HRR does not indicate when each trench was filled, but the 133.2 pit is not present in 1966 aerial

photography and is present with no apparent overgrowth in a 1969 photograph. The trenches were closed in 1968. The 133.2 trench was probably opened in 1967. This year will be used as the time of contaminant introduction to the vadose zone, giving a total transport time of 26 years to the end of 1993 (the midpoint of the modeled period).

Logs of boreholes 56893 and 56993 (DOE 1994a) within the trench indicate that ash is present 2.4 to 7.7 feet below ground surface (6019.7–6025.0) in 56893 and 4.0 to 8.7 feet below ground surface (6016.3–6021.0) in 56993, giving an average thickness of fill of 5.0 feet. This number is somewhat consistent with the trench design fill depth of six feet mentioned above. No ash was encountered in the third of the three boreholes in the trench, borehole 57093. However, the borehole is located along the northern edge of the approximately 200 foot long and 40 to 45 foot wide trench depicted on TM15 maps and may be outside of the area containing waste. Based on information provided in the HRR and borehole data, the source appears to be a volume 175 feet long, five feet thick and 12 feet wide.

IHSS 142 The target wells for IHSS 142 are wells 51193 and 50092, both located immediately east of Pond C-1 dam near Woman Creek. Because the wells are downgradient from the pond, it is postulated that Pond C-1 is the source of contaminants found in these wells. A boring through the center of the dam (Merrick & Company 1992) indicates that the dam is not keyed to bedrock; in fact, approximately eight feet of unconsolidated material underlies the clayey gravel of dam fill, strongly suggesting a hydraulic path for contaminant transport from the pond.

Radium 226 can be traced back to Pond C-1 as a source, particularly because Pond C-1 sediments contain americium, plutonium, and uranium. Uranium 238 is a COC for surface water in OU-5. The first introduction of uranium is not known. Reported occurrences include the following:

- In October 1954, backwash water drained through the Original Landfill burning pit down to Woman Creek. The pit was used as a dump for uranium-contaminated incinerator ash and for burning of contaminated waste from Building 444 (used for manufacture of uranium and beryllium components).
- A steam condensate release (2,700 gallons) from Building 881 to Pond 7, and Pond 7 overflowed to Pond C-1. This release occurred in September 1955. Building 881 housed enriched uranium components.
- Drainage from the 903 Pad area occurred over its lifetime from 1955 or 1958 through June 1968. Waste stored at the 903 Pad included uranium from Building 444 (depleted uranium).

Vadose Zone Transport Logs of materials encountered in boreholes 56893 and 56993 indicate that constituents released from Ash Pit 133 2 must traverse about nine feet of material in the vadose zone to reach the water table (DOE 1994a) Nine feet is the distance from the elevation of the bottom of ash in borehole 56993 to the elevation of the water table calculated by MODFLOW Transport through this vadose zone was simulated with a one dimensional model as described in Section 5 3 1 1

A simulation using the distribution coefficient of 0 67 ml/g which corresponds to the radium 226 distribution coefficient in the calibrated MT3D model and a downward seepage velocity of 0 0013 ft/day showed that the radium 226 would not yet have arrived at the water table by 1993 The downward seepage velocity was calculated from

$$Q_{pw} = Q_r/n \text{ in which}$$

Q_{pw} is the seepage rate (L/T)

Q_r is the groundwater recharge rate (L/T) and

n is effective porosity (dimensionless)

The groundwater recharge rate was set at 0 0002286 ft/day (from the calibrated MODFLOW run) and n was 0 03 the effective porosity from Table 5 6 and Figure F 1 Appendix F

The mechanism for rapid transport of COCs through the vadose zone beneath the ash pit has not been investigated and is not known For the present modeling the rapid transport was simulated by reducing the distribution coefficient to zero This simulation shows the 50 percent C/C concentration arriving at the water table in about three years (Figure 5 17) Based upon this result, MT3D source loading beneath the ash pit was initiated three years after the ash pit was constructed Because the ash pit was constructed in 1969 the impact to groundwater was assumed to begin in 1972 for purposes of the MT3D simulations The MT3D source loading rate was considered to be constant from 1972 onward

Transport Model The MT3D simulation of contaminant transport in the groundwater system is described in this section

Interface with Groundwater Flow Model MT3D requires values for discharge across each cell face as a model input. These discharges are derived from the flow model MODFLOW/mt, an enhanced version of

MODFLOW provided with MT3D contains an interface package LinkMT3D. LinkMT3D allows MODFLOW to write heads and fluxes along cell faces into an unformatted file which is then used as an input file to MT3D.

Grid The same grid that was used for MODFLOW was used for MT3D facilitating linkage of the models. The size of the MT3D model was reduced by making irrelevant cells located west (upstream) of the IHSSs inactive.

Model Boundaries The MT3D boundaries are the same as those used for the MODFLOW model. The constant heads along Woman Creek allow movement of COCs out of the system.

Stress Periods The model execution consists of two stress periods for each COC. The first stress period is 18 years (6574 days) in length beginning in 1952 when Pond 6 (IHSS 196) was first used as an incinerator pit. The stress period ends (and the second begins) with the arrival of COCs at the water table beneath the ash pit in IHSS 133.2 in 1970. This second stress period lasts 24 years to the mid point of the RFI/RI investigation in 1994.

Calibration The numerical solute transport model was calibrated by adjusting input parameters to produce simulated concentrations that were close to target concentrations for the wells identified as containing COCs. Professional judgment was used to decide when the simulated concentrations were close enough to target concentrations to support human health risk assessment. A separate calibration was performed for each COC (radium 226, barium, and manganese). The simulated plumes from Pond 6 (IHSS 196) and Ash Pit 133.2 are independent. Changing the source concentration for one plume does not affect concentrations in the other.

The calibration for each COC was a two step process. First, the distribution coefficient was adjusted by successive trials until the ratio of simulated concentration values in the two wells in the Pond 6 (IHSS 196) plume approximated the ratio of the target concentration values in the two wells. Second, the source concentration values for each plume were adjusted by multiplying them by the ratio of target concentration value to calculated concentration value at wells in the plume. Calculated and target concentrations will match when this procedure is followed.

The initial estimate of longitudinal dispersivity was 45 feet. This estimate was based on the formula $\alpha_L = 0.1L$ where α_L is longitudinal dispersivity and L is the contaminant travel distance. This scale dependence is discussed by Walton (1985) and Droppo and others (1991). In the present case, the travel distance was taken as 450 feet, which is the distance from Pond 6 to the farthest observation well containing radium 226 activities above background, well 59593. The ratio between longitudinal and transverse (lateral) dispersivity was set at $0.2\alpha_L$, which is consistent with the recommendation of Droppo and others (1991) and with ratios given by Walton (1985). The effectiveness of adjusting dispersivity for calibration was examined by increasing longitudinal dispersivity by one order of magnitude while holding the initial distribution coefficient constant at 100 ml/g (Table 4.1, Streng and Peterson 1989). This change resulted in a decrease in the computed ratio between wells 59493 and 59593 from 1.66×10^6 to 182.8. The observed ratio is 2.9. Therefore, no combination of dispersivity and source loading could produce the desired ratio, because source loading will have no effect on the ratio. Calibration cannot be achieved solely by manipulating dispersivity. Consequently, the dispersivity was returned to its original estimated value, which is consistent with published scale dependent values. This dispersivity was retained throughout the calibration. The results of the calibration are presented in Table 5.11. The computed concentrations for well 59493 were interpolated from the four adjacent cell nodes, because the well is located where the concentration gradient is high. Other wells were adequately represented by calculated concentrations at the nearest node.

Analytical Transport at Pond C 1 Simulation of contaminant transport from Pond C 1 was accomplished by one dimensional analytical modeling using ONED 3. This procedure was adopted because the transport from the pond is along the bottom of the Woman Creek valley, which is represented by constant head boundary cells in the MT3D model. MT3D does not simulate transport in the boundary cells. The one dimensional analytical simulation is conservative because it does not include the dissipation produced by transverse dispersion. The results of the calibration to wells downstream from Pond C 1 are shown in Table 5.11. No useful data were found on total contaminant mass deposited in the source.

Future Concentrations The calibrated solute transport models were used to calculate future concentrations of COCs in groundwater near Woman Creek. Concentrations were calculated for thirty years from the present, based on exposure duration guidance in accordance with Risk Assessment Guidance for Superfund (RAGS) (EPA 1989, Chapter 6.0). The greatest calculated thirty year

concentrations are for cells located along Woman Creek (Table 5 12) These represent the greatest concentrations for groundwater that would flow into Woman Creek from the model area during high groundwater stages when the creek is gaining water in the reach through OU 5

These concentrations were calculated by extending the simulation period of the calibrated transport models by 30 years The source loading obtained in the model calibration was treated as remaining constant for the 30 years so the only input variable changed was the duration of the simulation period the use of undiminished source loading is conservative because it neglects the possible effects of source depletion and decay

Uncertainty Analysis Uncertainty is caused by various attributes of the models The hydrogeology conceptual model while attempting to account for what is known about the OU 5 hydrogeologic system may not actually reflect reality Some uncertainty in the results of the groundwater flow and transport modeling is caused by uncertainty in the variables that must be input, including hydraulic conductivity groundwater recharge distribution coefficients and dispersivities The finite-difference approximation of the groundwater system also contributes to uncertainty because the finite-difference representation of the system is much simpler than the real groundwater system Additional uncertainty arises from the non unique model calibration which can be achieved with more than one set of values for the variables

The uncertainty in the COC concentrations was accounted for by calculating worst-case concentrations for each COC The worst case is represented by the greatest 30 year concentration at Woman Creek that is not improbable This worst case approach requires calculation of an upper limit for the concentrations at Woman Creek The upper limit was calculated using a statistical procedure The general procedure was the following

- 1 The plume that produced the greatest 30 year concentration at Woman Creek was identified
- 2 Observation (target) wells near the axis of the plume were identified
- 3 Where two observation wells were near the axis the well nearest Woman Creek was selected for statistical analysis
- 4 The 95 percent confidence interval for the mean of the reported concentrations of each contaminant was calculated
- 5 The maximum likely concentration for each contaminant at the observation well was calculated by adding the confidence interval to the mean concentration.
- 6 The ratio of maximum likely concentration and mean concentration was calculated

- 7 The MT3D model was run for each COC until its concentration at Woman Creek reached a steady state (would not increase whatever the duration of the model run)
- 8 The greatest steady state concentration at Woman Creek was multiplied by the ratio calculated in item 6 to produce the maximum likely concentration (i.e. the worst-case concentration)

In step 1 the greatest 30 year concentration was chosen because it corresponds to the greatest risk. In step 2 observation wells near the plume axis were selected because concentrations from such wells are more representative of the variation of maximum concentrations. In step 3 more than one reported concentration is required for calculation of the 95 percent confidence limits for the mean. The 95 percent confidence interval for the mean was calculated using a sample variance and the t-distribution with a critical region of 0.025 (two tailed test). This test is described in Dixon and Massey (1957).

Regarding steps 4, 5, and 6 the 95 percent confidence interval is conservative because the probability of a measured concentration exceeding the upper confidence limit is only 2.5 percent, if the population is normally distributed. If no well in the plume had more than one concentration measurement, then the concentration of the well nearest the axis was multiplied by ten to get the maximum likely concentration (Smith 1989).

In step 7 the steady state concentration is equal to or greater than the maximum calculated 30-year concentration at Woman Creek. It also implies that the leading edge of the plume has intercepted the creek, so that the worst-case groundwater velocity is considered. Consequently using the steady state concentration is conservative.

Step 8 yields the worst case concentration because the ratio of the maximum likely concentration to the calculated concentration is the same at any point in the steady state portion of a plume. The results of the uncertainty analysis are shown in Table 5.13. The degree of uncertainty in concentrations that are related to human health risk is indicated by the differences in worst-case concentrations and greatest thirty year concentrations reported in Table 5.12. In general differences are less than an order of magnitude.

5.3.2 Surface-Water Modeling

This section documents the surface water chemical fate and transport model and parameters used. COCs analyzed and the statistical results of the simulation models runs over multiple 30 year time periods.

5 3 2 1 Purpose

The objectives of the OU 5 surface water modeling of the Woman Creek watershed are as follows

- To characterize the general surface water system of OU 5 using a semi regional scale surface water flow and transport model
- To support the HHRA portion of the RFI/RI for OU 5 This was accomplished by simulating the transport of COCs from OU 5 to potential exposure points for human receptors under present and anticipated future site conditions and as needed for ecological receptors
- To support the evaluation of potential remedial alternatives for the FS at OU 5

5 3 2 2 Scope

The scope of the surface water modeling is limited to providing simulated concentrations of the COCs detected within the OU 5 Areas of Concern (AOCs) Concentrations have been simulated at various points along the Woman Creek thalweg for which there are documented stream gage and water-quality data. These points were chosen in order to calibrate the model to observed data.

Once calibrated the surface water model was used to simulate COC concentrations based on thirty different 30 year climatological time series The daily mean concentration of each of the time series was determined for each of the COCs From these thirty daily means one mean concentration was determined for each COC This process was performed for eleven COCs americium 241 barium copper lithium mercury plutonium 239/240 strontium, uranium 233/234 uranium 235 uranium 238 and zinc

5 3 2 3 Description of Modeled Area

Woman Creek Watershed OU 5 is located within the Woman Creek drainage basin (Figure 5 18) which generally trends west to east Although seasonal flows can be low Woman Creek receives continuous flow from Antelope Springs Creek. Detention Ponds C 1 and C 2 are located within the eastern reach of the Woman Creek basin Pond C 1 is located on the Woman Creek channel whereas Pond C 2 is located off the Woman Creek channel Pond C 2 receives relatively minor local flow from its surrounding drainage basin It receives the majority of its flow from the SID located on the northern flank of the Woman Creek basin Woman Creek drains OU 5 and discharges via Mower Ditch into Mower Reservoir During periods of high flow Woman Creek may discharge directly to Standley Lake

The Smart Ditch South Boulder Diversion Canal Rocky Flats Lake and Coal Creek are water storage and/or conveyance facilities located near the upper part of the Woman Creek watershed Rocky Flats Lake collects irrigation flows from the Last Chance ditch for storage before discharging into Smart 1 and 2 ditches Flows conveyed eastward in the Smart 1 ditch are used to maintain water storage in the D Series pond located south of Woman Creek. A headgate on Smart 1 ditch allows irrigation flows to be diverted to Woman Creek Records and information provided by the ditch operator indicate that water is rarely diverted to Woman Creek from Smart 1 ditch South Boulder Diversion Canal (SBDC) flows across the Woman Creek watershed from north to south in an elevated un lined earthen ditch At the crossing with Woman Creek, the SBDC flows are carried over the creek in a metal flume Leakage does occur from this flume with the SBDC contributing minor amounts of water to the drainage Coal Creek is a natural drainageway flowing northeast past the western edge of the Woman Creek watershed. At this point the contributing watershed area of Coal Creek is approximately 15.1 square miles

South Interceptor Ditch The SID collects runoff from the southern industrial area and diverts it eastward to Pond C 2 (Figure 5.18) The Pond C 2 water is not discharged to Woman Creek but is pumped to the Broomfield Diversion Ditch (around Great Western Reservoir) approximately semi annually (DOE 1992a)

The SID was constructed in 1980 to intercept surface runoff that previously entered Woman Creek Since construction of the SID in 1980 Woman Creek has not received runoff directly from the southern part of the plant facility Surface water flow in the SID is intermittent and usually occurs only following precipitation events or snowmelt When flow is low water tends to pond in several low areas of the ditch The SID begins approximately 200 feet east of the Ash Pits (IHSS 133) and extends for almost two miles to Pond C 2 passing through the Original Landfill (IHSS 115) The SID is approximately four to eight feet in depth and is unlined

Areas of Concern For HHRA's conducted at the Site on site exposures will be evaluated in separate AOCs identified in the operable unit AOCs are defined as one or several contaminant source areas that are in close proximity and can be evaluated as a unit in the HHRA A detailed description of the AOCs and the associated IHSSs in OU 5 are presented in TM12 (DOE 1995b)

Three AOCs have been identified in OU 5 (Figure 5.18) and are identified as

- AOC No 1 The landfill area is located north of Woman Creek, and the SID passes through the lower part
- AOC No 2 The ash pits are located north of Woman Creek, and the SID begins east of this AOC
- AOC No 3 Contains the SID Woman Creek, and Ponds C 1 and C 2

5 3 2 4 General Design

The surface water model will contribute to the overall HHRA effort by simulating the fate and transport of COCs along several exposure pathways. The profile of surface water pathways (Figure 5 2) illustrates the numerous potential mechanisms for human exposures. Storm water runoff may transport contaminated soils to surface waters through erosion with subsequent transport to downstream receptors (DOE 1994b).

The Woman Creek streamflow can be attributed to storm runoff from both rainfall and snowmelt, groundwater inflow and inflows originating from irrigation ditches. Each of these sources has been included in the flow and transport model.

Surface water and sediment associated chemicals can be transported from sources located within the watershed from groundwater inflows or from sediments located along the stream and reservoir bottoms. These chemicals are then transported during baseflow or highflow runoff events in Woman Creek. Dissolved chemicals can be transported in the water and sediment associated chemicals can be transported with the sediment moved along the stream reaches.

5 3 2 5 Fate-and-Transport Model

Selection of Model Codes The surface water modeling of the Woman Creek watershed was done using the Hydrologic Simulation Program Fortran Version 10 (HSPF10) (Bicknell and others 1993). The ANNIE program (Lumb and others 1990) was used to manipulate meteorological and other types of data for input into the HSPF10 computer model.

The HSPF10 model was selected due to its flexibility and ability to be expanded to meet future project demands. HSPF10 permits simulation of branching one dimensional stream/reservoir systems with

groundwater simulation and pond simulation also available. The model is capable of simulating water and sediment budgets, water temperature, dissolved oxygen, biochemical oxygen demand (BOD), organic nitrogen, ammonia, nitrogen, nitrate, nitrogen, organic phosphorus, dissolved phosphorus, pesticides, pH, CO₂, total inorganic carbon, alkalinity, plankton populations, arbitrary nonconservative constituents using a first-order decay function and conservative constituents.

Verification of Model Codes. Verification is the process that demonstrates if the computer program correctly performs its stated mathematical capabilities (Brooks and Coplan, 1988). Code verification involves comparing numerical code results with analytical solutions (Cole and others, 1988). HSPF10 modules have been verified using empirical formulas and analytical solutions for the various processes being simulated (Crawford and Lindsey, 1966; Ambrose and Barnwell, 1989).

5.3.2.6 Model Capabilities

The HSPF10 computer modeling code is a comprehensive package for simulation of watershed hydrology and water quality. Figure 5.19 shows the hydrologic cycle components that are simulated using the HSPF10 model. HSPF10 is the only comprehensive modeling code of watershed hydrology and water quality that allows the integrated simulation of land and soil runoff with instream hydraulic and sediment/chemical interactions (Ambrose and Barnwell, 1989).

The surface water flow in the model is treated as varying with time (unsteady). The basin geometry is input into the model enabling simulation of real time conditions. External variables are input as hourly values and the simulated results are output as daily values.

Precipitation and Runoff. Hydrologic simulation in HSPF10 is performed using moisture accounting techniques initially developed in the Stanford Watershed Model (Crawford and Lindsey, 1966). This technique computes the movement of water into, between, and out of a set of conceptual storages using a fixed time step. Figure 5.20 is a flow chart of the precipitation and runoff processes that are simulated in the HSPF10 surface water code. Figure 5.21 is a schematic diagram showing the interrelationships between the precipitation, ground storages, evapotranspiration, surface runoff, and streamflow. Rainfall and/or snowfall are subject to interception by vegetation. If the interception storages are full, water infiltrates into the soil layers (if not limited by the upper zone storage capacity). Water that does not

infiltrate the upper zone exits the system as surface or interflow outflows. Water that infiltrates the upper zone storage and subsurface can then be routed into and/or through the upper, lower, and active groundwater storage layers based on the available capacities of those storage layers. If all these storage capacities are exceeded, water leaves the system as active groundwater outflow. Evapotranspiration is calculated for all of the above storage layers before capacity exceedance is calculated.

Soil Erosion and Sediment Transport Soil erosion from the watershed in HSPF10 is simulated as illustrated in Figure 5-22. Erosion can occur either due to particle detachment from rainfall impact and subsequent washoff, or as a result of rill and gully scour. Sediment transport along each stream reach is intended to simulate the transport, deposition, and scour of inorganic sediment in free-flowing stream reaches and mixed reservoirs.

Stream and Pond Hydraulics Flow routing is modeled using the catchment stream network technique which is divided into separate calculations for reaches and flow routes that proceed from upstream to downstream. The stream network can be of any complexity, including flows that are split and later recombined downstream. Impoundments (ponds, lakes, and reservoirs) also are included, although HSPF10 assumes such impoundments to be completely mixed; that is, stratification is not modeled. The site reservoir modeled in this study, Pond C-1, has been determined to be fully mixed based on its depth and turnover ratio (Appendix A).

Contaminant Fate and Transport Several important mechanisms affect the chemicals being modeled, including partitioning between dissolved and particulate phases, interactions between chemicals in the water column and the sediment bed, and any of a number of chemical-specific decay flux processes, such as volatilization, biodegradation, and oxidation. Figure 5-23 is a flow chart of the pollutant fate processes that are simulated in the HSPF10 surface water model.

5.3.2.7 Model Structure

This surface water model includes the Woman Creek segments and contributing watershed beginning at the upper end of the watershed extending east to Indiana Street (Figure 5-24). The model uses both pervious land modules and stream reach/reservoir modules to simulate the total Woman Creek surface

water system. The regional model may be expanded in the future to include Woman Creek segments downstream of Indiana Street and/or other watersheds for investigations other than the OU 5 RFI/RI

Six pervious land basins and five stream and/or reservoir segments or reaches were used to model the Woman Creek watershed (Figure 5-24). Table 5-14 describes the geometric properties of the basins and stream/reservoir reaches used in the HSPF10 model. Beginning at the upstream end of the watershed and moving eastward, reach 1 extends east to the South Boulder Diversion Canal. Reach 2 extends to the west boundary of the Site at surface water monitoring sites GS05 and GS06. Reach 3 extends to the confluence of Woman Creek with Antelope Spring Creek. Reach 4 extends to GS17 (upstream of Pond C-1). Reach 5 extends to the outlet of Pond C-1 at GS07, and reach 6 extends to Indiana Street at GS01 and GS02.

The stream reaches and contributing pervious land basins were set up to allow calibration of the water balance portion of the model at the gaging station sites located at the downstream end of each stream reach. These were also used for the calibration of the sediment transport portion of the model based on sediment deposition into Pond C-1.

5.3.2.8 Climatological Conditions

The following hourly climatological data are needed for the HSPF10 modeling application:

- total precipitation depth
- mean air temperature
- mean dewpoint temperature
- mean wind speed
- total solar radiation
- mean evaporation rates and
- potential evapotranspiration rates

For this modeling application, use these specified daily records for the period from July 1989 through April 1994 have been compiled into daily values (Appendix A). All data, with the exception of the evaporation and evapotranspiration rates, were recorded at the Site west buffer zone meteorological station (W-MetSta). The basic data were recorded in 15-minute increments using an automated meteorological

recording system. This system consists of individual recording devices that relay the data to a data logger which has a one way telemetry link to a computer database located on the site.

The data obtained from the W MetSta had the date, time, and all six meteorological parameters on a single line delimited by commas. These data were reformatted through the creation of a separate computer code in order to format the data for input into the Watershed Data Management (WDM) file. The comma delimited file was first converted to a space-delimited format. The six parameter space-delimited 15 minute interval file was then converted to six separate space delimited 15 minute interval files with a format compatible with the WDM input requirements.

Upon entering the files into the WDM it was discovered that significant data were missing and that much of the data were out of range. Therefore, the files were then manually edited by inserting missing data with appropriate data from a similar adjacent time period. The out-of range data were revised as required.

Precipitation The basic data for precipitation were recorded as total accumulated depth in inches over a 15 minute interval. These raw data were aggregated into an hourly time series sequence for use as input into the HSPF10 computer program. These data were then plotted in order to check for missing and out of range values. Missing data were manually added based on the data available from the tables of daily precipitation values obtained from the W MetSta for the NPDES Stormwater Discharge Permit Application report (ASI 1993). The hourly values were further aggregated to daily values and tables were generated for the daily precipitation values (Appendix A). Table 5.15 provides a summary of monthly and annual precipitation at the Site from 1971 through 1994.

Air Temperature The basic data for air temperature were recorded as the mean temperature in degrees celsius over each 15 minute interval. These raw data were converted to degrees fahrenheit and aggregated into a mean hourly time series sequence for use as input into the HSPF10 computer program. These data were then plotted in order to check for missing and out-of range values. Missing data were manually inserted by copying data from an adjacent day and corresponding time period. Out-of range data were determined to be air temperatures that are higher than 122 degrees fahrenheit or less than minus 58 degrees fahrenheit. No out-of range data were found. All adjusted data were checked for reasonableness. The mean hourly values were aggregated to maximum and minimum daily values and tables were generated showing daily maximum and minimum air temperatures (Appendix A).

Dew Point Temperature The basic data for dew point temperature were recorded as the average dew point temperature in degrees celsius over each 15 minute interval. These raw data were converted to degrees fahrenheit and aggregated into a mean hourly time series sequence for use as input into the HSPF10 computer program. These data were then plotted in order to check for missing and out-of range values. Missing data were manually inserted by copying data from an adjacent day and corresponding time period. Out-of range data were determined to be dew point temperatures that are higher than the corresponding air temperature or less than minus 58 degrees fahrenheit. These values were edited to be equal or slightly less than the air temperature. All adjusted data were checked for reasonableness. The mean hourly values have been further aggregated to maximum and minimum daily values and tables have been generated showing daily maximum and minimum dew point temperatures (Appendix A).

Wind Speed The basic data for windspeed were recorded as the average horizontal wind speed in meters per second over each 15 minute interval. These raw data were converted to miles per hour (mph) and aggregated into a mean hourly time series sequence for use as input into the HSPF10 computer program. These data then were plotted in order to check for missing and out-of range values. Missing data were manually inserted by copying data from an adjacent day and corresponding time period. Out-of range data were determined to be mean one hour wind speeds higher than 75 mph. No out-of range data were found. All adjusted data were checked for reasonableness. The mean hourly values were further aggregated to mean daily values and tables were generated showing the daily mean of wind speeds (Appendix A).

Solar Radiation The basic data for solar radiation were recorded as the average solar radiation in watts per square meter over each 15 minute interval. These raw data were converted to langley's per hour and aggregated into a mean one hour interval time series sequence for use as input into the HSPF10 computer program. These data were then plotted in order to check for missing and out-of range values. Missing data were manually inserted by copying data from an adjacent day and corresponding time period. Out-of range data were determined to be a mean hourly solar radiation rate higher than 1000 watts per hour. The out-of range data were examined, found to be reasonable, and left unchanged. All adjusted data were checked for reasonableness. The mean hourly values were aggregated to mean daily values and tables were generated showing the daily mean for solar radiation rates (Appendix A).

Evaporation The monthly mean data for evaporation rates were calculated by Andis Berzins (EG&G ER/SWD pers commun August 20 1993) based on observed data from the Great Western Reservoir.

located approximately one mile northeast of the Woman Creek drainage basin. These data were provided in inches per hour for each one month interval between October 1991 and September 1992. These mean monthly values were disaggregated into mean hourly evaporation rates for use in the HSPF10 computer program. Summary tables have been generated showing the daily mean rates of evaporation (Appendix A).

Potential Evapotranspiration Because data for potential evapotranspiration were not available from the MetSta, the required mean hourly time series sequence were developed using the available meteorological data as input to the code (Kusalaas and Kunkel 1993). The input parameters were air and dew point temperature, solar radiation, and wind speed. These parameters were downloaded from the WDM as four three year one hour time series and then each time series was divided into three one year time series. The four variables were then combined into one time series for each of the three years and reformatted to become the input data. The three resultant one hour time series of evapotranspiration were reformatted then combined into a single three year long time series and input into the WDM. Summary tables have been generated showing the daily mean rates of evapotranspiration (Appendix A).

5.3.2.9 External Inflows

It has been determined that lateral inflows of groundwater are entering the Woman Creek watershed from sources that located outside the watershed boundaries (EG&G 1995c). Based on inspections of topographic maps (USGS 1971, 1979 and 1980) it was determined that the Rocky Flats Lake, SBDC and Coal Creek (Figure 5.24) which are all located upgradient of Woman Creek, can contribute water to the alluvium. This contributory water later appears as surface water runoff in Woman Creek.

A time series plot of surface flows was developed from gain/loss flow measurements at Station 13, located on Antelope Spring Creek immediately upstream of its confluence with Woman Creek (Fedors and Warner 1993). Monthly flow rate measurements taken January through December during 1992 and 1993 were averaged and the results plotted (Figure 5.25). A time series sequence of mean daily values was developed by interpolating between the monthly values. The annual recorded precipitation in 1992 was 13.7 in. and in 1993 was 11.7 in., slightly less than the median value of 13.9 inches between 1971 and 1994 (Table 5.25). This precipitation time series sequence was duplicated and used to represent all years.

used during both the model calibration and the 30 year simulation period. The Antelope Spring Creek time series sequence was added to Basin 4 as surface inflow.

Hydrographs of the water levels in wells 1989 (Antelope Springs Creek), 2689 (Woman Creek) and 5386 (South Woman Creek) (Figure 5-26) and the surface level of Rocky Flats Lake (Figure 5-27) were developed and the seasonal trends were found to be similar. This would indicate that the inflow of groundwater is relatively uniform throughout the upper part of the Woman Creek watershed near the western boundary of the Site. Therefore, the Antelope Spring Creek time series sequence was added to Basins 2 and 3 as a source of lateral inflow of groundwater.

The SBDC passes through the upper part of Basin 2, delivering water from Gross Reservoir, located north and west of the Site, to Arvada Reservoir, located south of the Site. The headgate records indicate the time periods that the ditch is carrying flow and the dry periods. No stage or flow data were obtained. These records were obtained from the Denver Water Board (DWB, 1995). The exfiltration rate from the ditch to the groundwater was determined to be 0.06 in/hr during the periods with flow and zero when the ditch was dry. This time series sequence was added to Basin 2 to represent a source of lateral inflow of groundwater.

The uppermost part of the Woman Creek watershed extends approximately 1.6 miles west of Highway 93 (Figure 5-24) to the foothills at the point where Coal Creek flows into the plains area. The stream gage records for Coal Creek (Coal Creek near Plainview, No. 06730300) were obtained from the Colorado Water Resources Division on November 15, 1994, for water years (WY) 1986 to 1993. These data were used to develop an average annual time series sequence to be used for all of the future simulation years as representative of lateral groundwater inflow into Basin 1. Figure 5-28 shows the 1986 to 1993 average mean daily discharge for Coal Creek at the Plainview gaging station.

5.3.2.10 Soils

One of the most important factors that influences the sediment transport processes is surface soil grain size. Grain size analyses were performed by Colorado State University (CSU) on 115 surface soil samples collected from OU 2, OU 5, and OU 6 during the Phase II OU 2 RFI/RI (EG&G, 1995c). Results indicate

that 49 percent of grains from the samples have diameters greater than 100 microns (μm) 22 percent of grain sizes are between 10 and 100 μm and 30 percent of grain sizes are less than 10 μm

In the Unified Soil Classification System particles smaller than 74 μm are considered to be fines (silt or clay) Thus a high percentage of surface soils in the area are fine grained soils Fine grained surface soils are more easily transported by runoff than are coarser grained soils The high percentage of clay also provides a larger surface to volume ratio which allows more adsorption sites per volume of soil than does a coarser grained soil The higher capacity for adsorbed contaminants results in a higher potential for contaminant migration

5 3 2 11 Chemicals of Concern

PCOCs are those metals or radionuclides whose concentrations exceed a statistical screening above background concentrations and VOCs whose concentrations exceed the reported detection limits The COCs used in this OU 5 surface water model have been identified in TM11 (DOE 1995a) These COCs can be found in one or more media, such as surficial soils groundwater surface water pond sediments and stream sediments For the purposes of the HSPF10 model the COCs found in surface water and stream/pond sediments have been modeled

A total of 11 COCs have been identified for inclusion in the HSPF10 fate and transport model (Table 5 16) These chemicals have been grouped into four different sets of three (or two) based on their general geochemical behavior and the media in which they are found

Surface Water COCs Six of the eleven COCs were detected in the surface water sampled in Woman Creek These chemicals are listed below

- Barium
- Lithium
- Strontium
- Americium 241
- Uranium 233/234
- Uranium 238

Barium lithium and strontium are COCs for surface water only. These elements are also alkaline or alkaline earth metals with similar geochemical behavior. Therefore these COCs have been grouped together as Group 1 for calibration and HSPF10 simulation purposes. The remaining COCs in the list are found in several media, as shown in Table 5.16.

Sediment COCs Eight of the eleven COCs were detected in the pond and stream sediments sampled in Pond C 1 and Woman Creek, respectively. These chemicals are listed below.

- Copper
- Mercury
- Zinc
- Americium 241
- Plutonium 239/240
- Uranium 233/234
- Uranium 235
- Uranium 238

Copper, mercury, and zinc are all metals that are found in Woman Creek stream sediments (mercury and zinc are also found in Pond C 1 sediments). These three COCs have been grouped together as Group 2 for calibration and HSPF10 simulation purposes. Americium 241 and plutonium 239/240, both of which are radionuclides, are found in pond and stream sediments and have been included in Group 3. Uranium 233/234, uranium 235, and uranium 238 are radionuclides that are found in Pond C 1 sediments and have been included together in Group 4.

Source Terms Source term concentrations were calculated for both the calibration and simulation of the COC concentrations in surface water. Table 5.16 provides a listing of the COCs and indicates the media in which the chemical has been detected. For the model calibration, the COCs associated with surficial soils were used as source term data. Groundwater inflow concentrations were checked and it was found that groundwater did not appear to be contributing surface water COCs to the flow regime. In order for the data to be used as a calibration source term value, the following criteria must be satisfied:

- Source term media must be located upstream of the COC media (observed target data)
- The source term data must have originated within an AOC
- The data must have been collected as part of the OU 5 FSP

Each source term value was calculated as a mean concentration of a COC within the associated sub basin. The Thiessen polygon method was used to determine the area of influence for each sampling location within the AOC. The remainder of the watershed was assumed to have a zero concentration of each COC. An area weighted concentration for each COC located in each watershed sub-basin was calculated for input into both the calibration and simulation models.

For the purposes of the HSPF10 model calibration, the source terms were calculated with the assumption that the SID was in place and functional. Therefore, in the landfill (AOC 1) only the COCs located south of the SID were included in the calculations. Conversely, in the ash pits (AOC 2) and in Woman Creek and Pond C 1 (AOC 3) all the observed COC concentration data were used in the computation of source terms contributing to the observed concentrations found in Woman Creek and Pond C 1.

For the purposes of the HSPF10 future concentration model simulation, the source terms were calculated assuming the SID had been abandoned. The COC concentrations north of the SID within the landfill area (AOC 1) were included in the composite source term calculations. This assumption will permit surface runoff and any associated contaminants to drain south into Woman Creek during the 30-year simulation runs.

5.3.2.12 HSPF10 Model Calibration

Calibration of the HSPF10 computer model is required before the model can be reliably used for simulation purposes. The model was calibrated to past observed conditions for which six months of continuous data were available. The following sections describe the targets, procedures, and results of the model calibration process.

Calibration Targets Three documented hydrologically dependent conditions were calibrated:

- Water budget
- Sediment transport
- Concentrations of COCs

These conditions were modeled in individual modules and each process was calibrated in the above listed sequence in order to systematically calibrate the entire model.

Water Budget Calibration Targets The observed hydrograph data and the associated rating curve equations for gage station GS01 GS02 GS05 GS06 GS07 and GS17 were obtained from EG&G SWD Table 5 17 lists each gage station its general location the type of flow recording device in place and the rating equation for depth versus flow The data were plotted and reviewed for reasonableness Each gage station was found to have missing and erroneous data at various times throughout the stream gaging periods Based on the reliable data available the watershed mass balance and hydrograph shapes were calibrated for the period beginning on April 9 1993 and ending on September 26 1993

A field investigation revealed that the corrugated metal culvert carrying Woman Creek flows under Indiana Street (GS01) had a high point in the middle resulting in 0 29 feet of ponded water upstream of the invert of the culvert The rating curve was analyzed and found to be accurate for stages of two feet or more and incorrect for stages less than two feet.

Therefore the hydrograph data obtained for GS01 had to be adjusted using a 0 29 foot stage shift and a revised rating curve No associated stage data were available because the flows were adjusted by EG&G without corresponding stage adjustments Therefore the stage for each associated flow had to be determined mathematically from the rating-curve equation (EG&G 1994d) A polynomial equation was developed for the existing rating curve data. By substituting the flow value into the equation, the corresponding stage was determined That stage was then decreased by 0 29 feet and all negative stage values were set to zero A new rating curve was developed and a polynomial equation was developed for that rating curve The revised hydrograph values were obtained mathematically using the revised stage values in the new rating-curve equation The resultant hydrograph values are approximately half of the previous values

The rating curve for GS02 was analyzed and found to be inaccurate for low stages The same procedure used for GS01 was used to revise the GS02 rating curve The revised hydrograph for GS02 was combined with GS01 and used as the target for calibration of Woman Creek. The remaining gage station data were reviewed and found to be reliable for use in calibrating the water balance portion of the HSPF10 model

Sediment Transport Calibration Targets Empirical data for total suspended sediment (TSS) (Table 5 18) along Woman Creek and for the total accumulation of pond bottom sediments within Pond C 1 were chosen as calibration targets for the sediment transport portion of the HSPF10 model Data used for

calibration included TSS values measured during the OU 5 field sampling phase of the Phase I RFI/RI and TSS values measured in high flow samples collected during other Site programs (EG&G 1994e). The calibration time period was expanded from the six months used for water mass balance to seven years for the sediment transportation. Three pond bottom sediment core samples were taken on November 5, 1992, two of which had core depths of six inches and one that had core depths between 6 and 12 inches. The average accumulated sediment in the bottom of Pond C-1 since the pond was constructed in 1973 was estimated to be 8 to 10 inches. Therefore, over the twenty year period that Pond C-1 has been in operation, the average sediment accumulation was calculated to be approximately 0.4 inches per year, or roughly three inches in a seven year period.

Water Quality Calibration Targets Table 5-16 provides a listing of the COCs and indicates the media in which the chemical has been detected. For the model calibration, the concentrations of COCs associated with both surface water and stream/pond sediments were used as observed target data. Each target concentration was calculated as a mean concentration of a COC within the associated watershed sub-basin. To determine the area of influence for each sampling location along Woman Creek (AOC-3), an average stream width of five feet was used, and the stream length was measured from topographic maps. An area weighted concentration for each COC located in each watershed sub-basin was calculated for input into both the calibration and simulation models. For the three pond bottom sediment samples, the arithmetic average of the observed concentrations was calculated for use as the observed target values.

Calibration Procedure A surface water flow and transport model is generally calibrated by adjusting a set of model parameters to produce simulated flows, TSS concentrations, and chemical concentrations that match field measured values within a quantifiable range of error or within reasonable limits. There are basically two ways of adjusting model parameters to achieve calibration:

1. manual trial and error adjustment, and
2. automated parameter estimation

Calibration of the HSPF10 computer model for the Woman Creek drainage basin was achieved using the manual trial and error method.

Water Budget Calibration Procedure The flow module was calibrated by isolating each of the six sub-basins and achieving a mass balance within each sub-basin while using the observed hydrograph data.

from the upstream basins as inflow and the observed hydrograph data at the outflow point as the calibration target. After the individual sub basins were calibrated, the model was restructured allowing the simulated outflow of each upstream basin to be the inflow to the adjoining downstream basin.

Two methods were used for comparing observed data to simulated flow rates and mass volumes:

1. **Quantitative comparisons** The simulated mean daily flows and observed flows were each summed to obtain the total simulated and observed mass volume at each calibration location for the six month period (April to September 1993). The percent differences between the observed and simulated results were then calculated for each location.
2. **Qualitative comparisons** The time series sequences of observed and simulated hydrograph data were plotted and the results were compared to determine the similarities or differences in the data. Specifically, the magnitude and temporal location of the hydrograph peaks were compared.

The simulated hydrograph shape and peak flow rate were adjusted only after the simulated mass balance was found to be within 25 percent of observed values.

Sediment Transport Calibration Procedure After the flow models were calibrated and integrated into a single model, the sediment calibration was performed. The first sediment calibration procedure was to approximate the estimated three inches of sediment accumulation to have occurred in Pond C 1 during the last seven years. The seven year time frame was chosen based on the greatest length of site specific continuous meteorological data that was available without significant data gaps. It is imperative to obtain the greatest length of time available because the bulk of sediment can accumulate during a very few widely separated high intensity precipitation events. It is also important to use site specific data when available.

The seven year time period covers the dates of January 1, 1986 through December 31, 1992. Data for 1993 were not included because a full year of data was not available at time of calibration. Full years only were used in the sediment calibration because the sediment transport is seasonally dependent, and estimation errors are likely to occur when extrapolating incomplete years to a complete year. Furthermore, the start and end dates of the year should occur during a relatively inactive period, i.e., when little or no rainfall occurs.

Simulated sediment accumulation in Pond C 1 was compared against the sediment target and sediment transport parameters were adjusted to bring the simulated sediment budget within 10 percent of the target sediment budget. The significant parameters used to calibrate the sediment processes for the pervious land basins are

- soil detachment by precipitation
- soil scour due to precipitation and
- soil washoff due to precipitation

The significant parameters used to calibrate the sediment processes for the stream reaches are

- settling velocity of the sediment particles
- critical shear stress of particles for resuspension of bed sediments and
- critical deposition stress for deposition of suspended sediments

After the sediment accumulation approximated the target accumulation the frequency and magnitude of the sediment transport was calibrated. The time frame chosen for this portion of the calibration was the same as the flow calibration: May to September 1993. This period encompasses the only three sampling events when TSS in Woman Creek was measured during high flow events. The observed TSS values in stream reaches 2, 3 and 4 were used as the calibration target values. The TSS values in stream reach 6 (downstream of Pond C 1) have been influenced by the detention effects by Pond C 1 and therefore reach 6 was not considered in the sediment calibration.

The parameters used to adjust the frequency and magnitude of the simulated TSS in the Woman Creek stream reaches are the same as those used in the accumulation calibration. TSS calibration involves adjusting HSPF10 model sediment parameter values until the simulated TSS concentrations for both relatively small and large storm events adequately approximate the observed TSS concentrations on target dates. This procedure is based on the fact that the sediment source of the TSS in a stream reach will vary based upon the size and intensity of the storm event. That is, small storm events have a tendency to generate TSS by scouring the stream bed while receiving little washoff from the pervious land basins. Conversely, during larger storm events, contributions from pervious land basins to TSS increase significantly. Therefore, the ratio of sediment load from the basins to the sediment scoured from the reaches was adjusted until the proper sediment magnitude and frequency were reached. The two

calibrations methods discussed in this section were then iteratively repeated until both sediment calibration targets were satisfied

Water Quality Calibration Procedure The water quality calibration of the OU 5 surface water model was accomplished using two distinct methods. These calibration methods are analogous to the methods used in the sediment model calibration where the calibration target values were total sediment accumulation in Pond C 1 and point TSS values as measured in the water column. This relationship is explicit because the COCs are considered to be closely associated with sediments. In the case of fate and transport of constituents the calibration targets are

- Concentration values of bed sediment associated constituents in Pond C 1 accumulated since source placement and
- The average values of the suspended sediment associated and dissolved constituents in the stream reaches

The first calibration method involves simulating the fate and transport of a constituent from an upgradient source area to a downgradient depositional area, where the resulting depth and concentration of the constituent are known. This method is useful for the initial calibration of the fate and transport parameters for the model and for a gross characterization of the system. The second method involves fine tuning the water-quality calibration parameters in order to simulate the actual water-quality concentrations as closely as possible.

The actual accumulation calibration was performed by simulating the deposition of the COCs currently present in AOC 3 by using AOCs 1 and 2 as the constituent sources. Water-quality fate and transport parameters were adjusted until the concentrations simulated for AOC 3 reasonably matched the existing concentrations present in AOC 3 as determined by field sampling. The following assumptions are inherent in the calibration.

- Any COCs currently present in AOC 3 are the result of transport from AOC 1 and 2 and are not attributable to any other source term
- The length of time from source placement to sampling date of the calibration target can be reasonably estimated
- The model input and boundary conditions used for the simulations represent the actual conditions present during the time from source placement to measurement date and
- The source term is constant and not depleted

The water quality calibration was performed on both a 7 3/4 year and 30 year time frame. The 7 3/4 year time frame selected was the same period used in the sediment transport calibration with the meteorological data extended three quarters of a year to include dates when storm-event TSS measurements were taken for OU 5. The period January 1, 1986 to September 30, 1993 was the primary calibration period because the data are site specific to the Site.

Thirty year meteorological data sets generated for use when running simulations for the HHRA and discussed in Section 5.3.2.13.1 were also used during the water quality calibration as a qualitative calibration check. It was determined the 30 year sets could function in this capacity because source placement is thought to have occurred between 43 years and 20 years ago. It is fairly certain no source existed prior to the opening of Rocky Flats Plant in 1952.

It is also assumed that a significant amount of the source term material was in place 20 years ago. This is the estimated point in time at which the Original landfill and incinerator had been operating for approximately 20 years. Using 30 years as the source placement time frame yields a 70 percent to 150 percent uncertainty of the source initiation. This range is well within the criteria required for a qualitative calibration check.

The simulated concentrations in Pond C 1 were compared against the bed sediment concentration targets when calibrating with the 7 3/4 year set and the water-quality and sediment transport parameter values were adjusted to bring the simulated concentrations to within 25 percent of the target concentrations. The 7 3/4 year simulation period is roughly 25 percent of the 30 year source term placement time period. The significant parameter used in calibrating the quality processes are the adsorption/desorption rates of the constituents. Other parameter values such as partition coefficients (K_d) (Table 5.19) or quantity of constituent associated with transported sediment are either calculations, field measurements, or literature values.

It is assumed all the COCs modeled are sediment associated although they may exist in the dissolved state during water quality processes. That is, hydrolysis, oxidation, first-order decay, biodegradation, etc., are not considered relevant for the OU 5 COCs.

Once the simulated bed concentrations approximated the observed results the suspended sediment water quality concentrations and dissolved water quality concentrations were calibrated. Because adsorption/desorption was the only water quality parameter used in the calibration, the adjustment of simulated dissolved concentrations directly affects the bed associated concentrations (i.e. increasing the water column concentrations will decrease the bed concentrations). The calibration of the dissolved constituents was performed to further define the ratio of pervious land sediment washoff to sediment scour from the stream reaches. For example, using a high desorption value for a constituent results in much of the transported constituent leaving the OU 5 system in the dissolved flow. This fate then requires the transport of greater amounts of sediment from the source areas to achieve the target concentration in the bed sediments of Pond C 1. If during the iteration between adsorbed and dissolved concentration calibrations a realistic simulation of both concentrations could not be obtained, it was necessary to return to the sediment calibration to adjust the pervious land washoff (constituent source) and stream scour (clean sediments) ratio. In this manner the calibration loop for the bed concentration, water-column concentration, sediment accumulation, and TSS was iteratively performed until all three calibrations were satisfied.

After calibration was completed the model was run using the 30 year meteorological data sets as a qualitative check. High intensity precipitation events were investigated to determine if the resulting maximum water quality concentrations are reasonable and if the means/medians of the 30 year data sets approximate the measured values.

Calibration Results The results of the HSPF10 model calibration for the water budget, sediment transport, and water quality modules are presented in this section. The individual modules have been calibrated to achieve the best correlation to observed data for that module while balancing the calibration results of the other two modules within as narrow a range as possible.

Water Budget Calibration Results Figures 5-29a through d show the calibration hydrographs at each of the gage stations along the mainstream of Woman Creek. The individual hydrographs of the simulation runs and observed gage station flow data were quantitatively and qualitatively compared.

The quantitative results for each sub-basin analyzed have been shown in the respective figures and tabulated in Table 5-20. The comparison of the total observed and simulated mass volumes indicates that

the model under simulates the volume by 25 percent at GS05 and over simulates the volumes by 22 percent at GS02. The under simulation of volumes at GS05 reflects the approximately 250 000 cubic feet of observed flows during the May 15 to May 26 1993 time period which are considered to be over estimated due to instrument error. The overall mass balance is considered satisfactory.

The temporal spacing of the simulated storm peaks compares favorably with the observed storm peaks. However, for the April 13 1993 storm event, the magnitudes of the peak flows are under simulated, whereas the peak flows for storms during the time period from June 20 to September 15 1993 are over simulated.

Sediment Transport Calibration Results The calibration results for the 7 year bottom sediment accumulation for Pond C 1 are summarized in Figure 5 30. The simulated depth of 0 25 feet represents 100 percent of the target accumulation goal of 0 25 feet, as discussed in Section 5 3 2 12. Sediment Transport Calibration Targets of this document.

It was not possible to precisely calibrate to a specific target value because the range of sediment accumulation in Pond C 1 has been estimated at 0 66 to 1 0 feet. Any calibration within the calculated target range could be considered valid. Therefore, the final calibration value was determined when the sediment module was modified to be calibrated to observed TSS values.

Observed and calibrated TSS values for reaches 2 3 and 4 of Woman Creek are shown in Figures 5 31A through 5 31C. The average values for the reaches were also calculated because measured TSS values are highly variable and dependent upon location of the sampling site. Therefore, an average daily TSS value for all of the stream segments combined was considered in the calibration. The average observed and simulated TSS values for Woman Creek stream reaches are presented in Figure 5 31D. The average TSS values were used to objectively finalize the sediment calibration parameters. When each reach was individually calibrated, there still existed some latitude in determining the final calibration parameters for the system as a whole. At this point, the sediment calibration parameters were adjusted to best match the average observed TSS without significantly affecting the individual reach calibrations.

Reaches 5 and 6 of the model were not directly calibrated to observed values. Pond C 1 (reach 5) was not sampled for TSS during storm event sampling. Because storm-event TSS values are the primary

calibration criteria, this reach was limited to a qualitative comparison of estimated baseflow TSS values. Similarly, the four sampling locations that are situated in reach 6 were not sampled during storm events and therefore can not be reliably used for sediment calibration.

This lack of observed TSS data for reaches 5 and 6 however is not critical to the calibration of the sediment model. Pond C 1 is highly efficient in functioning as a sediment trap and is not expected to discharge any significant amount of suspended sediment. Also, because reaches 2, 3, and 4 were calibrated using the same sediment calibration parameters (as opposed to using different initial and/or boundary values for each reach), reach 6 was calibrated using the same sediment calibration parameters.

The final simulated TSS peaks shown in Figure 5.31 are somewhat lesser in magnitude than in the original TSS calibration because the sediment calibration is ultimately dependent upon the water quality calibration. This adjustment was required to adequately calibrate the simulated COC water quality concentrations. The calibration is considered within the range expected of sediment transport models.

Water Quality Calibration Results Water-quality calibration was performed for data collected over seven years; the results are depicted graphically on Figure 5.32. Additionally, qualitative checks were performed to scrutinize the model's response to large precipitation events. This check was accomplished by using a few of the 30-year data sets developed for the HHRA simulations as input to the model and obtaining a mean of the predicted concentrations for all COCs.

The construction of the SID during the middle of the estimated accumulation period for pond sediments complicates the calibration process. It is impossible to quantify the degree of accumulation of COCs in the sediments of Pond C 1 before the SID construction and compare it to the accumulation in the pond after the SID construction. The 7-year calibrations that are extrapolated to 30-year estimates were performed with the SID in place for the following reasons:

- The observed target values for the water column were measured with the SID in place.
- The flow and sediment models were calibrated to the period after construction of the SID, and
- Water quality calibration derived while excluding source areas north of the SID produces conservative concentration values.

The fate and transport of mercury was not calibrated because the observed source area for mercury is insufficient to produce the required target value in Pond C 1. Because mercury is highly volatile, the source area would begin to deplete itself immediately after placement. Thus, the sampled source area measurements for mercury are considered unreliable for use as a calibration source term.

Parameter values for mercury were obtained by using the parameters of calibrated COCs whose behavior during fate and transport processes would best approximate that of mercury. Given the COCs investigated in this project, copper or zinc are the most similar in behavior to mercury (EG&G 1995g). Because the copper and zinc were calibrated to identical parameter values, these same values were used for mercury during the simulations for the HHRA.

The observed COC concentrations, along with the results of the 7 year simulation period (with the SID in place), the extrapolated 30 year simulation results (with the SID in place), and the extrapolated 30 year simulation results (without the SID in place) are listed in Tables 5-21 and 5-22 for the four COC groups considered. For Group 1, there is no target for the streambed sediment, because these constituents are not COCs for that medium.

The results for the 7 year simulation were multiplied by 4.28 to estimate the sediment accumulation for a 30 year period with the SID in place. Concentration estimates for a 30 year period without the SID in place were estimated by multiplying the previous results (i.e., 30 years with the SID) by 1.5 times the quotient of the source concentration north of SID divided by the source concentration south of SID. This ratio represents a source area upgradient of the SID that is 1.5 times greater in size than the area downgradient of the SID, along with its respective change in COC concentrations.

The 7 year with the SID scenario represents the condition with the minimum simulated concentrations, and the 30 year without the SID scenario represents the condition with the maximum simulated concentrations. The simulated concentrations for the bottom sediment quality were compared to the observed COC concentrations and reported as a percentage of the observed concentration. Because the simulated concentrations for each stream reach and each COC group vary greatly, a mean of all percentages was determined (see Table 5-22). The mean of these percentages brackets the observed concentrations listed in Table 5-22.

The mean water column and sediment associated calibrations are within plus or minus one order of magnitude which is sufficient resolution for the HHRA. The mean 7 year simulation of the water-column COC concentrations for individual COCs ranged from 0.3 percent to 48.3 percent, with a mean estimation of 22.8 percent of observed concentrations (see Table 5.21). For streambed associated COCs the mean of the 7 year with the SID and 30 year without the SID simulation ranged from 63.4 percent to 781.8 percent of the observed concentrations (see Table 5.22).

A review of the percent differences between simulated and observed concentrations in the Pond C 1 water column reveals that Group 3 COCs are under simulated by 2 to 3 orders of magnitude. The simulated americium 241 and plutonium 239/240 activities in Pond C 1 were not increased for the following reasons:

- the adsorption/desorption parameters for Group 3 are set at the lowest possible values thus maximizing accumulation in bed sediments
- the adsorption/desorption parameters for Group 2 metals which are over simulated in bed concentrations are set at their highest effective value thus minimizing simulated bed concentrations and
- sediment accumulation in Pond C 1 is already simulated at the permissible upper range of the estimated sediment target value

An attempt to increase the simulated, bed load activities of americium 241 and plutonium 239/240 would result in unrealistic behavior of the entire simulated sediment/water system, given the three factors listed above.

5.3.2.13 Fate-and-Transport Modeling

The final task of the OU 5 modeling was to estimate the future concentrations of COCs along Woman Creek in support of HHRA for the OU 5 RFI/RI. This involved estimating long term average concentrations of COCs in the stream flow, sediment in the Pond C 1 and in Woman Creek at Indiana Street. These estimates were based on the results of thirty 30 year simulations. This section discusses the generation of thirty 30 year meteorological data series and the results of the 30 HSPF10 simulations.

30 Year Time Series The 30 year climate data generated by the CLIGEN model (Nicks 1985) were used as input to the HSPF10 model to simulate the conditions for the last 30 years. Though it is not assumed

that any of the 30 year meteorological data sets precisely simulates the conditions of the last 30 years it is assumed the CLIGEN data sets are fairly representative of average 30 year conditions. Therefore the maximum, minimum, and mean values for the simulated concentrations were used to bracket the target concentration values.

Source Terms Source terms for the 30 year simulation runs were calculated for the simulation of the COC concentrations in the water column. The source terms in the model calibration were used with some modifications for the simulation runs. Specifically, COC concentrations in sediment sampled from the SID were used as a source term for sediments and water flowing into Woman Creek. Also, COC concentrations in surficial soils of the original landfill, which is located north of the SID in AOC 1, were included in the chemical loading for basin washoff that may enter Woman Creek during a storm event.

Simulation Results Simulation and result summaries for both the water column (dissolved) and sediment associated (total) fractions of the eleven COCs in surface water media are provided in Tables 5-23 through 5-26. In addition, mean daily concentrations have been determined at the downstream end of four stream reaches along Woman Creek, as follows:

- Reach 3: confluence with Antelope Spring Creek
- Reach 4: approximately 400 ft upstream of Pond C-1
- Reach 5: Pond C-1
- Reach 6: Indiana Street (east boundary of the Site)

The results of these statistical summaries are shown in Tables 5-23 through 5-26 for COC groups 1 through 4, respectively, and have been used as input for the HHRA.

"In order to condense the simulated mean daily concentrations produced from the four groups of thirty 30 year computer runs (120 computer runs) to a series of values more easily used in the HHRA, the daily means were statistically summarized. The first step involved condensing the data in each of the thirty 30 year simulations for each COC group to 30 mean daily concentrations, resulting in 30 mean daily concentrations for each of the 11 COCs. These 30 mean daily concentrations were then statistically summarized to produce a final mean daily concentration for each COC.

5 3 3 Air Modeling

5 3 3 1 Air Modeling Objectives

Wind suspension of potentially contaminated soil from the IHSSs within OU 5 to downwind receptors has been identified as the mechanism for several exposure pathways. Human exposure could occur by inhalation, ingestion, or dermal contact of this airborne contaminated particulate matter. Receptor populations are current and future on-site workers, future on-site ecological researchers, and open space users. The air pathways for these receptors have been designated as potentially complete, although relatively insignificant, and have been selected for quantitative risk assessment (DOE 1995b).

The purpose of the air dispersion modeling is to estimate COC concentrations and deposition rates at the potential receptor locations of interest. These specific point exposure concentration and deposition values will provide input to the risk calculations of the HHRA.

5 3 3 2 Selection of Air Models

The air dispersion model selected for the OU 5 HHRA is the Fugitive Dust Model (FDM) (Winges 1991). Development of the FDM has been sponsored by EPA Region X to address the concentration and deposition of particulate matter from fugitive dust sources. The FDM is described fully in TM13 (DOE 1994b) as well as in the source document (Winges 1991).

5 3 3 3 Wind Resuspension Potential Study Objectives

Air dispersion modeling provides the primary basis for assessing the inhalation risks posed by windblown, contaminated dust to current and future on-site workers. Perhaps the most critical input parameters to air dispersion models are those associated with the source terms. In OU 5, the important source input factors are the contaminant levels in the surface soils and the wind resuspension potentials of those soils. The original investigations of the OU 5 RFI/RI Work Plan focused on the contaminant levels in the surface soils, and those findings are discussed extensively in TM15. The objective of the additional air-quality study was to assess the wind resuspension potential of the soils in the IHSSs in OU 5.

In 1993 EG&G Rocky Flats Inc conducted a field investigation throughout OU 3 to determine the wind resuspension potentials of the soils in the areas east of Indiana Street (DOE 1994c) The OU 3 study utilized a portable wind tunnel That study yielded important information about the wind erosion potential of the OU 3 areas possibly the most valuable of which was the calculation of specific threshold friction velocities and threshold wind speeds of the sites that were examined Friction velocity which is a measure of the wind shear at the erodible surface characterizes the capacity of the wind to cause movement of surface particles Threshold friction velocity is the minimum velocity that results in particle movement. Threshold wind speed is equivalent wind speed at a specified elevation above the ground surface for example approximately 30 feet (10 meters) the standard height of a reference anemometer The purpose of the study of wind resuspension potential in the Woman Creek Drainage was to estimate the threshold friction velocities of the OU 5 sites and compare these to the results of the OU 3 wind tunnel study If the OU 5 investigation results compare favorably with the threshold friction velocity values determined in the OU 3 wind tunnel study then the OU 3 data can be utilized reliably for the OU 5 RFI/RI air dispersion modeling and henceforth the HHRA

Methodology for the Study of Wind Resuspension Potential The investigation of the wind resuspension or erosion potential of contaminated soils in areas of interest in OU 5 including IHSS 115 IHSS 133 the surface disturbance south of IHSS 133 IHSS 209 and the surface disturbance west of IHSS 209 was proposed as a phased approach The first phase involved a limited field investigation of the site and comparisons of these results with those of the more intensive wind tunnel study that was performed at OU 3 If the first phase results were inconclusive then a second phase was recommended. The second phase would be the replication at OU 5 of the intensive field studies that were conducted in 1993 at OU 3

The wind resuspension study relied on the rapid assessment methodology described by Cowherd and others (1985) The field examinations consisted of observations about sites selected as representative of the areas of interest in both OU 3 and OU 5 (see Figures 2.5 through 2.7 for observation locations) At each location visual examinations of soil type and conditions and vegetative cover were conducted The soil type was characterized along with the soil moisture and presence or absence of soil crusting The extent of bare soil vegetative cover and other nonerodible elements (gravels and cobbles larger than 1 cm diameter) were estimated Finally a soil sieving procedure was conducted at each location with 4 mm 2 mm 1 mm 0.5 mm and 0.25 mm sieves to estimate the aggregate size mode of the surface soil From the estimate of the aggregate size mode the threshold friction velocity of the soil was determined from a

figure in the reference document. A correction factor was calculated to account for the increase in threshold friction velocity due to the nonerodible elements

In working with the rapid assessment method several limitations and difficulties with the procedures and calculations were encountered. The reference document (Cowherd and others 1985) cautions that the procedures provide only a first-cut, order of magnitude estimate of exposure in limited applications. Nevertheless, the Cowherd method is endorsed as affording a degree of accuracy consistent with simplified quantitative estimation procedures (EPA 1988b). Approaches such as the Soil Conservation Service method (Woodruff and Siddoway 1965) to estimate wind erosion apply to annual losses from crop land and cannot be applied to generate short term estimates. The Cowherd method was selected because of the current land use of the Site, the nature of the soils and vegetative cover in OU 5, and the episodic high wind events characteristic of the region.

Certain assumptions incorporated into the rapid assessment method somewhat limited the interpretations of the OU 5 study. Most apparent was the utilization of only a few sieve sizes to estimate the mode of the aggregate size. Soil elements larger than 1 cm (nonerodible elements) were not included in the sieve analysis. At some locations this fraction composed the most volumetric fraction. Standard soil sieving techniques quantify the fractions by weight. The Cowherd rapid assessment method calls for visual estimates of the relative sizes of the catches. Investigators for this study improved the technique by volumetrically measuring the individual fractions to estimate the mode. In addition, it was difficult to estimate how much of the nonerodible elements were embedded in the ground surface. When in doubt, 50 percent seemed like a reasonable estimate. A serious limitation that was noted by the investigators was the poor quantitative accounting for the mitigating effects of partial vegetative cover. Correction factors for nonerodible elements could not be assigned values greater than 10 due to limitations in the graph accompanying the reference document.

Results and Discussion of Wind Resuspension Study Field work was performed from January 20 to January 27, 1995. Weather conditions during the month prior to the field study were unusually dry. All soils were dry during the study period. Ambient temperatures were unseasonably warm, in the 40 °F and 50 °F ranges. Daytime winds during the study period were light from the southeast and east.

The 1993 OU 3 wind tunnel study examined four terrestrial sites. These same four terrestrial sites were investigated as part of this study of wind resuspension potential (Figure 2.5). Sites T 1, T 2, and T 3 of the OU 3 wind tunnel study were chosen for that study as representative of the soil and vegetation conditions on areas directly east of the Site. Conditions were somewhat different at each site. At T 1 the soil was a clayey silt with some fine gravels and vegetative cover was fair to good. Location T 3 was three fourths of a mile or more east of T 1. Here the soil was a silty sandy gravel. Although the vegetative cover was far less than at T 1, the other nonerodible elements provided a comparable overall coverage. Location T 2 displayed a silty sand with fair vegetative cover. The fourth terrestrial location T 4 was about two miles southeast of the other three OU 3 wind tunnel study sites. It had been selected because it was characteristically different from the other three sites. The soil was a silty sand and although the aggregate size mode was comparable to two of the other OU 3 sites, the vegetative and other nonerodible cover at this fourth location was minimal.

Ten locations, in two groups of five each, were chosen as representative of soil and vegetation conditions within IHSS 115 (Figure 2.6). Surface slopes throughout the Original Landfill are fairly steep, 15 percent to 40 percent and facing south. Locations 115AQ1 through 115AQ5 were situated west to east along the top of the landfill slope. Soils were gravelly sands with larger aggregate size modes and noticeable bare soil. The extent of nonerodible elements, both gravels, cobbles, and vegetation, was variable. Location 115AQ5 was somewhat down the slope and displayed a smaller aggregate size mode and more vegetative cover. The remaining locations in IHSS 115, 115AQ6 through 115AQ10, were situated east to west along the lower elevations of the landfill. They were characterized generally by smaller aggregate size modes and very good vegetative cover.

Within IHSS 133, five locations were examined as representative of conditions in that area of interest (Figure 2.7). Area slopes were gentle, approximately five percent with a south orientation. Soils were gravelly sands and sandy silts with smaller aggregate size modes. Vegetative cover was excellent, usually complete.

At this writing, the three surface disturbance areas on the south side of Woman Creek are not considered areas of contaminant concern and have not included as radiological sources in the air dispersion modeling for the OU 5 RFI/RI. Fewer locations within these three areas were examined in this wind resuspension study.

The Surface Disturbance South of IHSS 133 is located on a flat hilltop on the south side of Woman Creek. Within this area, two locations identified as SASH AQ16 and SASH AQ17 were investigated (Figure 2 8). Soils were gravelly sands indicative of a hilltop situation. The aggregate size modes were smaller. Vegetative cover was very good.

IHSS 209 is a large, basically level surface disturbance area on another hilltop on the south side of Woman Creek. Three locations identified as 209AQ18 through 209AQ20 within IHSS 209 were examined (Figure 2 9). The soils on this hilltop were generally sandy gravels exhibiting larger aggregate modes. Vegetative cover was only fair, but other nonerodible elements added conspicuous protection from wind erosion.

The Surface Disturbance West of IHSS 209 is a moderately sloping hillside, north facing, on the south side of Woman Creek. Two locations, W209AQ21 and W209AQ22, were examined in this homogeneous area (Figure 2 9). Gravelly and clayey sands characterized the slope. Aggregate size modes were smaller. Vegetative cover was uniformly very good.

The results of the OU 5 study of wind resuspension potential are summarized in Table 2 11. The rapid assessment method produced values for threshold friction velocities at the four OU 3 wind tunnel study sites that were within the same order of magnitude, but higher by several factors, as the results of the actual OU 3 wind tunnel study (Table 2 12). Field observations of the vegetative and soil conditions at both the OU 3 wind tunnel study sites and throughout OU 5 found that the two areas generally were comparable. Aggregate size modes of soil particles were typically larger throughout OU 5 than in OU 3. The vegetative cover was generally more extensive in OU 5 than in OU 3, excepting the top of the slope at the Original Landfill and IHSS 209.

The threshold friction velocities calculated for the OU 5 locations were consistently higher, sometimes by an order of magnitude, than the values reported in the OU 3 wind tunnel study. Consequently, the threshold wind speed values from the OU 3 study can be applied to the air-dispersion modeling for the OU 5 RFI/RI and HHRA with the confidence that conservative health protecting assumptions are being exercised.

The rapid assessment method yielded values that are conservative estimates of the threshold friction velocities and threshold wind speeds around OU 5. With the availability of the results of the wind tunnel study at OU 3 where field conditions are generally comparable to OU 5, more accurate values are not required at this time for air dispersion modeling.

5.3.3.4 Conceptual Model for Air Transport of COCs

COCs in surface soils may be transported via emissions of fugitive particulate matter to onsite and offsite exposure points. Inhalation of contaminated particulate matter is a potentially complete exposure pathway for current and future outdoor workers, ecological researchers, and open space users. Potential contaminant intake and corresponding risks associated with these media will be evaluated in the HHRA (DOE 1995b).

5.3.3.5 Assumptions and Limitations for Air Model

The FDM is based on the well known analytical Gaussian plume formulation that constitutes the basis of almost all atmospheric-dispersion models approved by EPA for regulatory use (Turner 1970, EPA 1986). The FDM incorporates an improved gradient transfer deposition algorithm based on analytical equations of Ermak (1977) for computing concentration and deposition values of fugitive particulate matter at user selected receptors. The line source and area algorithms in the FDM are those in the CALINE3 model. The CALINE series is also based on the analytical Gaussian equation and is a preferred regulatory model of EPA (EPA 1986).

Assumptions and limitations inherent in the FDM include those common to all air-dispersion models based on the Gaussian plume equation:

- The source emission rate is assumed to be constant.
- Diffusion in the direction of transport is assumed to be small compared with advection by wind speed in that direction.
- The material diffused is assumed to be a stable gas or aerosol that remains suspended in the air over long periods.
- All pollutants are assumed to exhibit perfect reflection from the ground and from an upper inversion surface.

- A mean wind speed is assumed to be representative of the diffusing layer chosen
- The mean wind speed direction specifies the x axis
- Wind speed is assumed to be constant and the turbulent fluctuations in the x direction are much greater than in the y or z-directions
- The time averaged concentrations of plume constituents are assumed to be distributed normally in both cross wind and vertical directions
- Values of sigma y and sigma z are representative for a sampling time of about 10 minutes
- Downwind concentration values are limited to receptors with 50 km of the source (Turner 1970)

With the FDM deposition routine these assumptions and limitations apply

- Eddy diffusivities are assumed to be functions only of downwind distance
- Eddy diffusivity is assumed to be constant for all space and time
- Concentration and deposition values are numerically integrated for a large number of cases involving different meteorological conditions different particle sizes and different release heights in the FDM program A numerical solution was developed to correct the concentration values so that approximate mass conservation is obtained for all cases In general for particles smaller than 10 microns the corrections are very small for all cases examined Correction factors are built into the FDM and the use of corrections factors is entirely transparent to the user (Winges 1991)

A number of assumptions relating to the input parameters for air-dispersion modeling for OU 5 were incorporated into the study

- The particle size distribution of the parent soil determines the size distribution of suspended particles This assumption is based on discussions in the *Superfund Exposure Assessment Manual* (EPA 1988b)
- Potential emissions of fugitive particulate matter from the area sources are limited to those generated by wind erosion. There is no vehicular traffic on the sources
- Particulate emissions are zero when wind speeds are less than the threshold wind speed
- Erosion potential is completely and evenly depleted in one hour of an episodic wind event that exceeds the threshold wind speed For wind events lasting more than one hour the erosion potential is renewed at each subsequent hour

5 3 3 6 Setup and Calibration of Air Model

This section describes in detail the FDM input parameters regarding sources meteorology and receptors. A discussion about the calibration or verification of the model is also presented.

Area Sources Area sources must be specified as rectangles for the FDM. Coordinates and dimensions in feet were obtained from the Louisville Quadrangle 7.5 minute series (topographical) map (USGS 1979). The last five digits of the coordinates were manually converted to meters for the FDM source input parameters.

For the OU 5 study, five area sources of radiological contamination were modeled (Figure 5.33A). These areas were selected on the basis of the analytical results for surface soil samples with radionuclide activities greater than those of the background UTLs. They were defined and modeled prior to the decisions regarding the definition of the three AOCs in OU 5. FDM source input coordinates and dimensions (in meters) and radionuclide levels are presented in Table 5.27A.

Within IHSS 115, three area sources of radiological contamination were modeled. The sources of radiological contamination in the landfill are thought to be exhumed materials that were brought to the surface during past disturbances of landfill materials. Source 1 was specified as a rectangle to encompass a cluster of samples in the middle of the IHSS that showed radionuclide activities greater than those of corresponding UTLs. The rectangle was designated to represent uniform emissions within the source. Radionuclide levels were obtained by averaging the results of 18 surface soil samples collected within the rectangle. Although only 13 samples within the rectangle actually showed radionuclide activities greater than the UTLs, data for all surface sample points within the rectangle (excepting those two exhibiting unusually high results) were averaged together to represent the area wide average. Source 2 was drawn as a small 25 ft square centered on one surface soil sample that showed unusually elevated levels of uranium isotopes within the Source 1 rectangle. The americium 241 and plutonium 239/240 results for the Source 2 sample were negative values, so a source strength of zero was assigned for modeling purposes. Similarly, Source 3 was drawn as a 50 ft square centered to represent a distinct area in the western portion of IHSS 115 where one surface sample showed elevated levels of uranium isotopes.

IHSS 133 the ash pits was represented by Sources 4 and 5 as two contiguous rectangles. Source 4 was drawn as a larger rectangle encompassing IHSS 133 6 133 5 133 4 133 1 and 133 3 and nearby surface soil sample points. Source 5 was drawn as a smaller rectangle encompassing the IHSS 133 2 pits and two surface soil sample points just east of IHSS 133 2. Radiological contamination is distributed more or less evenly across IHSS 133 that is there are no outstanding hot spots. Both rectangles representing IHSS 133 were assigned radionuclide levels obtained from the averages of all surface soil samples collected for the IHSS. The number of analyzed samples varied with constituent: 19 samples for americium 241, 22 for plutonium 239/240, 17 for uranium 233/234, 22 for uranium 235, and 21 for uranium 238.

For the OU 5 study, five area sources of organic and metallic chemical contamination were modeled (Figure 5-33B). These five areas are not the same as those for the area sources modeled for radiological contamination, although their locations are similar and were selected where results of statistically identified COCs were clustered. The FDM source input coordinates and dimensions (in meters) and the concentrations of organic and metallic COCs are presented in Table 5-27B.

IHSS 115 contained four area sources of surface soil contamination. Source 1 was drawn as a 10-acre square covering the approximate middle third of the old landfill. Source 1 contained elevated levels of all 11 COCs. Mean concentrations of COCs were obtained by averaging the results of as many as 35 surface soil samples within the area. There are three small areas within the 10-acre Source 1 area, from which samples yielded results that were one or more orders of magnitude higher than the other sample results in Source 1. These higher results were not included in the Source 1 averaging but were treated as distinct, smaller area sources. Source 2 was drawn as a 25 ft square centered on one surface soil sample that showed higher levels of benzo(a)anthracene, benzo(a)pyrene, benzo(b)fluoranthene, dibenzo(a,h)anthracene, fluoranthene, indeno(1,2,3-c,d)pyrene, and pyrene. Source 3 was drawn as a 25 ft square centered on one surface soil sample that showed higher levels of dibenzo(a,h)anthracene, fluoranthene, and indeno(1,2,3-c,d)pyrene. Source 4 was drawn as a 25 ft square centered on one surface soil sample that showed higher levels of silver.

IHSS 133 contained one area source for the surface soil COCs. Source 5 was drawn as a 10-acre rectangle covering the southeast portion of the ash pits (IHSS 133).

Particle Size Information Particle size distribution and density characteristics were obtained from the Phase I RFI/RI field geotechnical investigation of OU 5 surface soils (DOE 1994a). On the basis of discussions presented in the *Superfund Exposure Assessment Manual* (EPA 1988b), three particle size classes were selected: particles $\leq 10 \mu\text{m}$ aerodynamic equivalent diameter that are available for inhalation, particles 10–30 μm diameter range that are suspendible and can be transported considerable distances downwind, and particles 30–100 μm diameter range that abrade the soil surface and dislodge smaller particles but themselves settle within a few hundred feet of the source. The midpoints of each class were selected as the characteristic particle size diameters: 5 μm , 20 μm , and 65 μm .

For particles less than 20 μm , the particle size distribution of the parent soil determines the size distribution of suspended particles (EPA 1988b). Field investigations of the grain size distributions were conducted for IHSS 115, the surface disturbance west of IHSS 209, IHSS 209, and the surface disturbance south of the IHSS 133 ash pits (Table 5-28). The soil grain size distribution of IHSS 115 was assigned to IHSS 133.

Threshold Wind Speed Friction velocity, which is a measure of the wind shear at the erodible surface, characterizes the capacity of the wind to cause surface particle movement. Threshold friction velocity is the minimum velocity that results in soil movement. Threshold wind speed is the equivalent wind speed at an elevation above ground surface, for example, 10 meters above ground, which is the standard height of a reference anemometer.

The soil surfaces of all IHSSs within OU 5 are nonhomogeneous, at least partially vegetated and impregnated with other nonerodible elements, such as pebbles, cobbles, and boulders. Such nonhomogeneous surfaces are characterized by the limited availability of erodible soil (Cowherd and others 1985). Such surfaces have high threshold wind speeds for the commencement of wind erosion, and particulate emission rates tend to decay rapidly during an erosion event.

In 1993, EG&G Rocky Flats, Inc., contracted Midwest Research Institute to perform a study to quantify wind resuspension emissions of particulate matter from the soils and sediments of OU 3 (DOE 1994c). The test sites were concentrated in three locations: the shore around Standley Reservoir, the shore around Great Western Reservoir, and four terrestrial sites east of Indiana Street. When site conditions were undisturbed, the average threshold wind speed of the four terrestrial sites was $>102 \text{ m/hr}$. When site

conditions were severely disturbed by vehicular traffic the average threshold wind speed of three terrestrial sites was 42 mi/hr (18.92 m/s) (The fourth terrestrial site was not examined in a disturbed condition)

Two approaches were applied to determine the threshold wind speed for OU 5 conditions Both approaches were based on a rapid assessment methodology outlined by Cowherd and others (1985) to estimate the threshold friction velocities of soils The first approach used the detailed geotechnical data for OU 5 surface soil samples obtained in the Phase I RFI/RI field investigation (DOE 1994a) to estimate the soil particle size distribution mode Data were corrected for nonerodible elements as discussed in Appendix A of Cowherd and others (1985) Finally the corrected threshold friction velocity was calculated to be approximately 150 cm/s The corresponding threshold wind speed at a 10 m reference anemometer is 24.4 m/s (54.6 mi/hr) When hourly averaged meteorological data for the five years 1988 through 1993 collected at the Rocky Flats Plant were examined not one hour exceeded this OU 5 calculated threshold wind speed of 24.4 m/s

The second approach to estimate a threshold wind speed for OU 5 conditions actually implemented the Cowherd rapid assessment methodology in the IHSSs throughout OU 5 and at the four terrestrial sites examined in the 1993 OU 3 wind tunnel study (Section 2.2.1.7.4) The rapid assessment field study estimated threshold friction velocities at the OU 3 locations two to five times higher than those determined by the OU 3 wind tunnel study The rapid assessment field study estimated threshold wind speeds for OU 5 conditions at 150 mi/hr to 400 mi/hr

The average 10 m threshold wind speed determined for the three severely disturbed terrestrial sites in the OU 3 wind tunnel study (18.92 m/s) was used for the air dispersion modeling of wind resuspended contaminated soils from OU 5 This selection was considered to be conservative because soils at the OU 5 sites generally display more non erodible elements (vegetation and pebbles cobbles and boulders) than the three OU 3 locations and moreover are not disturbed A total of 11 days throughout the 5 year period were identified with wind speeds exceeding this lower threshold wind speed

A threshold friction velocity of 1.17 m/s was calculated from the 10 m threshold wind speed of 18.92 m/s by using the logarithmic velocity profile equation (EPA 1985 Seinfeld 1986) A macro scale roughness height for Rocky Flats 1.5 cm was used in the calculation (DOE 1994c)

Erosion Potential and Emission Rates The erosion potential for a dry exposed surface is given by

$$P(u) = 58(u - u_t)^2 - 25(u - u_t) \quad (\text{Equation 5 3 3 1})$$

where

$$P(u) = \text{erosion potential } g/m^2$$

$$u = \text{friction velocity } m/s$$

$$u_t = \text{threshold friction velocity } m/s$$

This equation for erosion potential was determined empirically for industrial coal piles and other exposed materials using a portable wind tunnel like that utilized for the OU 3 wind tunnel study (EPA 1985 Midwest Research Institute 1988). The OU 3 wind tunnel study (DOE 1994c) found that this equation for industrial wind erosion potential substantially exceeds the measured erosion potentials for the highly disturbed surfaces tested in OU 3.

Again using the logarithmic velocity profile equation the ground surface wind speed is related to the 10 m wind speed $u_{(10m)}$ by $0.062u_{(10m)}$

For the OU 5 conditions discussed above the erosion potential equation becomes

$$P(u) = 58(0.062u - 1.17)^2 + 25(0.062u - 1.17) \quad g/m^2 \quad (\text{Equation 5 3 3 2})$$

where

$$u = u_{(10m)} \text{ wind speed at 10 meters}$$

Completing the multiplications the equation becomes

$$P(u) = 0.222952u^2 - 6.86464u + 50.1462 \quad (\text{Equation 5 3 3 3})$$

Assuming that the entire erosion potential is depleted in a 1 hour episodic wind event, the particulate matter emission rate can be calculated by dividing the $P(u)$ equation by 3 600 s/hr

$$E_{PM} = 6.19311E-05u^2 - 1.90684u + 1.39295E-02 \quad (\text{Equation 5 3 3 4})$$

where

E_{PM} = fugitive particulate matter emission rate $g/m^2 s$

$u = u_{(10m)}$ wind speed at 10 meters

The erosion potential and the emission rate equations are dependent on wind speed in a quadratic format that the most current published version of the FDM version 94040 cannot accommodate. The FDM versions available through the EPA Technology Transfer Network are written in a first-order relationship to wind speed. Because of this limitation, Mr. Kirk Winges, the author of the FDM, prepared a special version of the 94040 FDM that provides the additional capability of entering emission sources as a quadratic formula for the threshold wind speed case (Winges 1994). The modification is in Card 14A of the FDM input file, which is written in the format

$$E_{PM} = G_1 u^2 + G_2 u + G_3 \quad (\text{Equation 5 3 3 5})$$

where

E_{PM} = fugitive particulate matter emission rate $g/m^2 s$ sometimes termed Q

$\left. \begin{matrix} G_1 \\ G_2 \\ G_3 \end{matrix} \right\} = \text{coefficients determined as discussed for Equations 5 3 3 3 and 5 3 3-4}$

$u = u_{(10m)}$ wind speed at 10 meters

The range of the FDM output values is limited to values that are neither too small nor too large for the number of significant figures and decimal point placement available in the model. If the concentration or deposition results are too small, the FDM reports the results as 0.0000. If the concentration or deposition results are too large, the FDM reports the results as *****. To accommodate this limitation, a multiplier can be applied to the G coefficients so that the FDM will provide actual numerical results. The multiplier is selected on a case-by-case basis, typically by trial and error, depending on the order of magnitude of the COC concentration. Interpreting the model output results must be done with this multiplier in mind because the multiplier determines the order of magnitude of the output values (Table 5 29).

A COC emission rate is determined by multiplying the fugitive particulate matter emission rate by the COC concentration in the soil (pCi/g of soil for radionuclides)

$$E_{\text{aminan}} = X (E_{PM}) \quad (\text{Equation 5 3 3 6})$$

where

E_{toxin} = COC emission rate $\text{pCi/m}^2 \text{ s}$

X = contaminant concentration pCi/g

E_{PM} = fugitive particulate matter emission rate $\text{g/m}^2 \text{ s}$

To summarize the coefficients G_1 , G_2 , G_3 in the quadratic wind speed-dependent equation for Card 14A of the FDM were determined multiplying the coefficients of the terms in the emission rate equation for fugitive particulate matter first by an arbitrary multiplier and second by the COC concentration. The FDM output values are in terms of COC not particulate matter concentrations and depositions the magnitudes of which were determined by the selected multiplier. This process is summarized for americium 241 (Table 5.30). The values for all constituents are evident in the source terms of the FDM input files presented in Appendices I through L.

Meteorological Input EG&G Air Quality Department provided preprocessed meteorological data for the full calendar years 1989 through 1993. Data originated from the Site meteorological tower which is located about 2 km northwest of OU 5. Instrumentation is at 10 m elevation above ground level. The site meteorological data are collected in 15 minute averages. However, this time period is not suitable for air dispersion modeling with the FDM. Consequently, the meteorological information were compiled into 1 hour averages. Input included wind speed (m/s), wind direction (degrees from north), stability class (Turner classification), mixing height (m), and ambient temperature (degrees Kelvin). Stability classes were determined from the standard deviation of the horizontal wind direction (EPA 1986). Mixing heights were estimated from Holzworth (1972). Missing data were treated according to EPA policies (EPA 1986).

Receptors Selection of receptors was based on the potentially complete and relatively insignificant exposure pathways that were previously selected for quantitative risk assessment for exposures to radionuclides, organic compounds, and metals (DOE 1995b). Potential receptors are associated with unspecified locations in the three AOCs within the OU 5 study area. AOC1 is IHSS 115, the original landfill. AOC2 is IHSS 133, the ash pits, and AOC3 is the Woman Creek drainage.

For modeling of maximum impacts of potential receptor points associated with AOC1 and AOC2 north south rows of receptors at 100 ft spacing were positioned on the east (downwind) edge of the larger rectangular area sources discussed above or directly east of the area sources that were rotated from the north south axis (Tables 5 31A and 5 31B Figures 5 34A and 5 34B) These receptors were dubbed the Near Group receptors The Near Group receptors for modeling of radionuclide COCs and organic compound COCs although termed alike were positioned somewhat differently because the area sources for each type of contamination were drawn differently The Near Group receptors were modeled using the FDM convergent algorithm for area sources

For modeling of maximum impacts within AOC3 the Woman Creek drainage a Grid Group of receptors at 1 000 ft spacings throughout the entire OU 5 study area was designed Receptor #22 was closest to Woman Creek and also downwind from IHSSs 115 and 133 To the Grid Group were added RAAMP samplers 13 14 23 32 and 38 (Table 5 31C Figure 5 35) RAAMP samplers 13 14 23 and 38 are situated in or near the Woman Creek Drainage RAAMP sampler 32 was chosen as an upwind background sampler The Grid Group was modeled using the 5 line integration default for area sources

Verification Verification of the FDM for the OU 5 investigation was accomplished by comparing model output with ambient air monitoring data collected by the RAAMP and special OU 5 samplers The conclusions of these verification procedures relate to the accuracy of the model and the uncertainty of the output Ambient air data available for verification are limited to those months when data from the OU 5 samplers were reported and when winds exceeding the threshold wind speed of 18 92 m/s were recorded by the Rocky Flats Plant meteorological tower

Three special OU 5 ambient air samplers were installed in the summer of 1992 and became operable in October 1992 Sampler S102 is located north and west of OU 5 as an upwind monitor Sampler S100 is situated downwind of IHSS 115 Sampler S101 is placed downwind of IHSS 133 Procedures for the OU 5 samplers are the same as for the RAAMP samplers filters are collected biweekly Once a month the two filters collected from each air monitoring station are composited prior to isotopic analysis Radionuclides analyzed for the OU 5 filters are americium 241 plutonium 239/240 uranium 233/234 uranium 235 and uranium 238 As of March 1 results of 12 samples from each monitor representing the period October 9 1992 to August 4 1993 had been entered into RFEDS Of the 12 samples only the first

two samples (October 9 1992 and November 10 1992) had been completely validated at the time of this modeling

RAAMP samplers 13 14 23 and 38 are in or near the Woman Creek drainage. However RAAMP data did not prove useful for verification purposes because filters from these samplers are analyzed only for plutonium 239/240. Furthermore the locations of these samplers were chosen to monitor sitewide conditions rather than point sources or even area sources such as OU 5.

During the period October 9 1992 to August 4 1993 only the period December 30 1992 to January 26 1993 exhibited wind speeds with 1 hour averages exceeding the selected threshold wind speed of 18.92 m/s (42.32 mi/hr). These occurred on January 21 1993 hours 8 and 9 when winds averaged 22.96 m/s and 19.23 m/s respectively. The wind speed of 22.96 m/s is the highest 1 hour average wind speed recorded for the years 1989 through 1993.

Verification runs for the FDM using the five line integration default modeled the period January 1 31 1993. Model output was compared with the OU 5 ambient air data for the period December 30 1992 to January 26 1993 (Table 5.32). FDM input and output files for the verifications runs are included in Appendix I. Model runs utilizing the convergent algorithm for near source receptors produced output results substantially the same as model runs with the five line integration. Model results for americium 241 were two and four orders of magnitude below ambient levels for plutonium, model results were one order of magnitude below ambient levels. Model output values for uranium 233/234 and uranium 235 fell within the same order of magnitude as the ambient data. Model results for uranium 238 were one order of magnitude above the ambient data.

Uncertainty and Accuracy A succinct discussion of the accuracy and uncertainty of models is presented in EPA's *Guidelines on Air Quality Models* (EPA 1986). Air-dispersion models are more reliable for longer term averaged concentrations than for short term concentrations at specific locations. Models are reasonably reliable for estimating the magnitude of highest concentrations occurring sometime somewhere in the area. Air dispersion models are recognized to exhibit an accuracy within a factor of two and are typically more accurate.

Model uncertainties fall into two categories: inherent and reducible. Inherent uncertainties arise from unmeasured or unknown conditions of an event and may vary among repetitions of the event. Such uncertainties would exist in even the perfect model and may account for a typical range of variation in output values of as much as 50 percent. Reducible uncertainties are associated with the model and its input conditions. Improvements in the physics of the model and the accuracy of the input parameters can minimize the amount of reducible uncertainty.

Improvements to the mathematical algorithms of a sanctioned public-domain model like the FDM are generally limited. As discussed above, the source input mechanism of the FDM was adjusted by the model developer to account for the quadratic form of the wind-erosion equation as applied in this study (Winges 1994). This modification addressed input formats rather than model mathematics.

Two important issues relate to the verification of the air dispersion model in the OU 5 situation. The first is the multiplicity of radionuclide sources in the OU 5 and the Site vicinity. The sources of the radionuclides on the OU 5 sampler media do not originate solely from the IHSSs of OU 5. An examination of the OU 5 sampler data for the period December 30, 1992 to January 26, 1993 for americium-241 illustrates this point (Table 5-32). Americium-241 levels on the upwind sampler S102 are higher than on the downwind samplers S101 and S100. Restricting the emission sources that contribute to any receptor in the site vicinity, such as the OU 5 samplers for verification purposes, to the IHSSs of OU 5 is a simplifying convention for modeling purposes only. In actuality, there are no real world ambient data attributable only to OU 5 sources.

The second issue concerns the wind resuspension rate of contaminated soil. As of the date of this report, a study of the wind resuspension potential, such as that conducted at OU 3 (DOE 1994c), has not been performed for OU 5. As a result, the values obtained in the OU 3 study were assumed to be applicable to OU 5 for the purposes of OU 5 air-dispersion modeling. Several model runs were performed to investigate the sensitivity of the FDM to values for roughness height and threshold friction velocity. Roughness height was varied from 0.022 cm to 1.5 cm. Threshold friction velocity was varied from 40 cm/s to 117 cm/s. Threshold wind speed was maintained at 18.92 m/s. The model output values generally remained within the same or one order of magnitude during this sensitivity analysis (i.e., the FDM is relatively insensitive to variations related to threshold friction velocity).

Comparison of the model results with ambient air data collected at OU 5 samplers and sensitivity runs indicates that the FDM output values of radionuclide concentrations are accurate within one order of magnitude

5 3 3 7 Results of Air Modeling

Air modeling runs to estimate the maximum values for deposition and exposure concentrations at the selected OU 5 receptor points were performed with the FDM using the input parameters described in Section 5 3 3 5. The input and output files for the FDM runs for radionuclide COCs are included in Appendix J for organic COCs in Appendix K and for metal COCs in Appendix L.

Modeling exercises utilizing the five line integration algorithm on the grid group of receptors were conducted for each of the five years of available meteorological data (1989 through 1993) to ascertain the year of maximum exposure. The year demonstrating the maximum values for annual average concentration and deposition for the selected receptors was 1990 (Table 5 33). The year 1990 exhibited 14 hours of 1 hour average wind speeds exceeding the selected threshold wind speed of 18 92 m/s. These high winds occurred in three episodes. For high wind episodes lasting more than one hour it was assumed that the erosion potential was renewed with each successive hour.

During 1990 the highest 24 hour averages of ambient concentration and deposition of COCs for the downwind receptors occurred on December 14 (Table 5 34). The highest 1 hour average wind speed during 1990 was 22 72 m/s which occurred toward the end of a sustained high wind episode during Hour 22 on December 14. For all of 1990 the maximum 1 hour concentration and deposition values for selected OU 5 receptors generally occurred during that hour or on another hour of December 14 (Table 5 35). The times of the maximum values for the receptors vary somewhat because the readings at a particular receptor depend on wind direction as well as wind speed.

5 3 4 Indoor Air Modeling

5 3 4 1 Objectives of Indoor Air Modeling

The scenario of the intrusion of soil gases through the below grade foundation floor and walls of a future on site office building has been identified as significant air exposure pathway for the OU 5 IHSSs (DOE 1995b). Presently no buildings are located in OU 5. The objective of the indoor air modeling was to estimate the exposure concentrations of COCs that are released into indoor air by intrusion of the gaseous phase directly from the vadose zone of the soils surrounding the floors and walls of future building foundations.

5 3 4 2 Selection of Indoor Air Model

EPA provides technical guidance for assessing potential indoor air impacts for contaminated sites (EPA 1992a). For modeling the concentrations of chemical vapors in indoor air due to soil gas entry the Johnson Ettinger models are recommended (EPA 1992a, Johnson and Ettinger 1991). The model equation corresponding to an infinite contaminant source and vapor infiltration through cracks/openings in the foundation is the most useful for general application. This model equation was selected for supporting the HHRA of potential indoor air impacts for OU 5. It is described fully in TM13 (DOE 1994b) as well as in the resource documents (EPA 1992a, Johnson and Ettinger 1991).

5 3 4 3 Conceptual Model for Indoor Air

The transport of contaminants from soil gas into a building foundation is understood to occur by a combination of convective and diffusive transport mechanisms. The relative significance of these mechanisms depends on site characteristics. In the case where the contaminant source lies directly beneath the foundation the convection mechanism dominates the transport of vapors into the building. If the source is distant from the foundation, transport is controlled by diffusion from the source to the foundation. Potential contaminant risks associated with indoor air of future buildings contaminated from VOCs in soils adjacent to the foundation will be evaluated in the HHRA.

5 3 4 4 Assumptions and Limitations for Indoor Air Model

Assumptions and limitations inherent in the Johnson Ettinger equation corresponding to the general application in which the contaminant source is infinite with respect to the modeling time of interest and vapor infiltration is through cracks or openings in the foundation, include the following

- The distance from the source to the building is assumed not to change with time and is assumed not to change in composition over the time of interest for the calculation
- The contaminant source is assumed to lie directly beneath the foundation
- The modeling equation applies to structures with crawl spaces and slab floor construction with solid (i.e. poured concrete) below grade walls. Other Johnson Ettinger modeling equations correspond to cases in which soil gas transport into buildings is substantially higher through relatively permeable materials (e.g. concrete block construction below grade) than through foundation cracks and openings or to cases in which a contaminant is located near the building and decreases over time (EPA 1992a)

5 3 4 5 Set Up and Calibration of Indoor-Air Model

Information concerning dimensions and ventilation characteristics of typical commercial buildings for Jefferson County Colorado was obtained from the Jefferson County Building Department (Nihiser pers comm 1993). This information along with building material published in the source documents (EPA 1992a Johnson and Ettinger 1991) was used to determine those additional properties required for the indoor air modeling of the intrusion of soil gas into future onsite building structures (Table 5 36)

A real time soil gas survey was conducted as part of the Phase I RFI/RI field investigation. The purpose of this survey was to identify areas of VOC contamination within IHSS 115 and IHSS 196. The methodology and findings of the soil gas survey are discussed in TM15 (DOE 1994a). The survey resulted in the identification of three areas of anomalous concentrations of organic compounds above the reporting limits. The three identified VOCs were 1,1,1 TCA, TCE, and PCE (Table 5 37).

The volumetric flow rate of a soil gas into a building foundation is related to the vapor viscosity of the gas. Vapor viscosity is inversely proportional to temperature (Table 5 38). The lower values for vapor viscosity were used in the Johnson Ettinger calculations.

The Johnson Ettinger equation calculates a ratio (α) of the gas concentration inside the building to the soil gas concentration at the source

(Equation 5 3 4 1)

$$\alpha = \frac{[D_T^{eff} A_B / Q_{bldg} L_T] * \exp(Q_{s,il} L_{crack} / D_{crack}^{crack} A_{crack})}{\{ \exp(Q_{s,il} L_{crack} / D_{crack}^{crack} A_{crack}) + [D_T^{eff} A_B / Q_{bldg} L_T] + [D_T^{eff} A_B / Q_{s,il} L_T] [\exp(Q_{s,il} L_{crack} / D_{crack}^{crack} A_{crack}) - 1] \}}$$

where

$$\alpha = C_{bldg} / C_{source} \quad \text{vapor concentration in building/vapor concentration at source (i.e. soil)}$$

$$D_T^{eff} = \text{overall effective diffusion coefficient (cm}^2\text{/sec)}$$

$$A_B = \text{cross sectional area through which contaminants may pass (approximated by area of floor and below grade walls (cm}^2\text{))}$$

$$Q_{bldg} = \text{building ventilation rate (cm}^3\text{/sec)}$$

$$L_T = \text{distance from contaminant source to building foundation (cm)}$$

$$Q_{s,il} = \text{volumetric flow rate of soil gas into the building (cm}^3\text{/sec)}$$

$$L_{crack} = \text{thickness of foundation (cm)}$$

$$D_{crack}^{crack} = \text{effective vapor pressure diffusion coefficient through a crack (cm}^2\text{/sec)}$$

$$A_{crack} = \text{area of cracks/openings through which vapors can pass (cm}^2\text{)}$$

If the source lies directly beneath the foundation as it would in the exposure scenario of contaminated soil adjacent to the foundation then α approaches the value $Q_{s,il} / Q_{bldg}$

The soil gas flow rate Q_{soil} is likely to be dependent of the basement crack area, A_{crack} soil type and stratigraphy building underpressurization and basement geometry For simplicity Q_{soil} is estimated by

(Equation 5 3 4 2)

$$Q_{s,il} = 2\pi \Delta P k_v X_{crack} / \mu \ln(2Z_{crack} / r_{crack})$$

where

$$r_{crack} / Z_{crack} \ll 1$$

(Equation 5 3 4 2 is an analytical solution for flow to a cylinder of length X_{crack} and radius r_{crack} located at a depth Z_{crack} below the surface This is an idealized model for soil gas flow to cracks located at floor/wall seams)

where

ΔP = building pressure difference relative to ambient pressure (g/cm sec^2)

k_v = soil permeability to vapor flow (cm^2)

X_{crack} = total floor/wall seam perimeter distance (cm)

μ = vapor viscosity (g/cm sec)

Z_{crack} = depth of crack below ground surface (cm)

and

r_{crack} = $\eta A_B / X_{\text{crack}}$

where

η = A_{crack} / A_B so that $0 \leq \eta \leq 1$

For a contaminant source adjacent to the building ($L_T = 0$) α is proportional to the soil permeability to vapor flow k_v at $k_v > 10^{-8} \text{ cm}^2$ (permeable soils) The effect of crack size on contaminant intrusion rates will be relatively insignificant in the limit of convective-dominated transport.

Resolution of uncertainty cannot be addressed fully within the scope of this assessment The future exposure scenarios for onsite office structures are hypothetical Calibration of any indoor air models with actual onsite measurements is not feasible

5 3 4 6 Results of Indoor Air Modeling

Execution of the Johnson Ettinger model was performed for the building soil and chemical properties as outlined in Section 5 3 4 5 A typical future onsite commercial building was considered to be 6 000 ft^2 (557 m^2) with 0 5 air changes per hour and a building underpressure of 1 Pa (10 g/cm s^2) Modeling was performed for the building sizes and air changes per hour indicated in Table 5 3 6 A range of underpressure values was not modeled The relationship of underpressure air to indoor air concentrations in the model is linear a ten fold increase in building would increase indoor gas concentrations by ten A single soil permeability of 10 darcy ($10 \times 10^{-8} \text{ cm}^2$) was modeled as typical Soil permeability also linearly affects indoor air concentrations of COCs in the model a ten fold increase in soil permeability

would increase indoor gas concentrations by ten. The maximum concentrations of soil gases detected during the field investigation were used as input to the model. Results of the modeling study are presented as typical values and as ranges of values for concentrations of identified VOCs in the basement areas of the hypothetical buildings (Table 5.39).

A number of studies referenced in the EPA guidance document (EPA 1992a) have indicated that the mean concentration of radon in basements is about twice the mean value for above ground living spaces. The conclusion of these studies can be extended to organic gases. The levels of air contaminant concentrations in the working spaces of future onsite buildings are estimated to be approximately half those in the associated basements as presented in Table 5.39.

WIND DISPERSION/
VOLATILIZATION

ALLUVIUM/
COLLUVIUM

GROUNDWATER PATHWAY

BEDROCK

SOUTH
INTERCEPTOR
DITCH

EVAPOTRANSPIRATION

SURFACE AND
NEAR SURFACE
FLOW

SEEP

WOMAN
CREEK

WATER TABLE

LANDFILL

POTENTIALLY
CONTAMINATED
SOILS

CONCEPTUAL GROUNDWATER PATHWAYS

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-1

Drawn NLM 7/21/95

Date

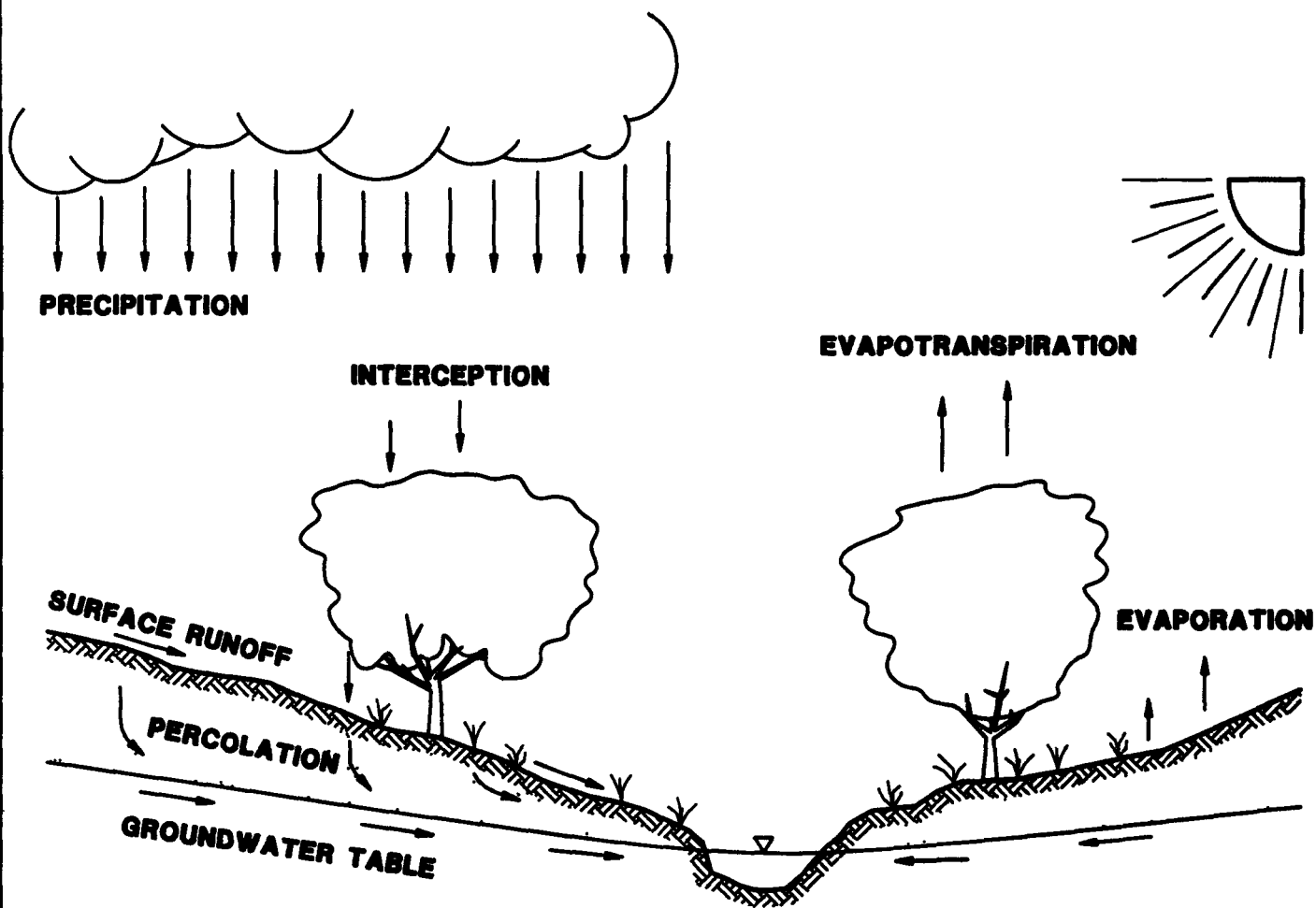
Checked 7/29/95

Date

Approved

Date

FILE OU5-5-1 DWG



Source Bicknell and Others (1993)

Drawn	NAU 8/1/92
Checked	727 8/1/95
App oved	
	Date

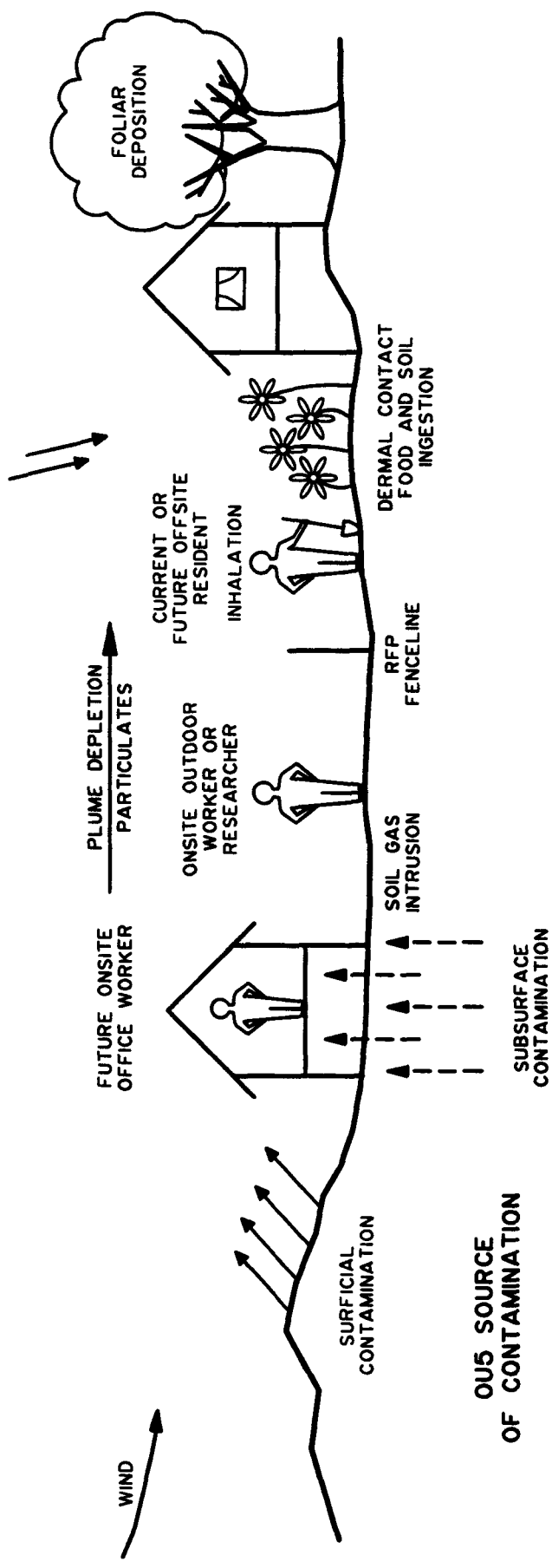
FILE OU5-5-2 DWG

CONCEPTUAL SURFACE - WATER PATHWAYS
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OU5 - WOMAN CREEK PRIORITY DRAINAGE
RPI/RI REPORT
FIGURE 5-2

RELEASE MECHANISMS
 SOIL EROSION FUGITIVE
 PARTICULATE EMISSIONS
 GAS INTRUSION INTO BUILDINGS

TRANSPORT MEDIUM
 AIRBORNE TRANSPORT
 AND DISPERSION

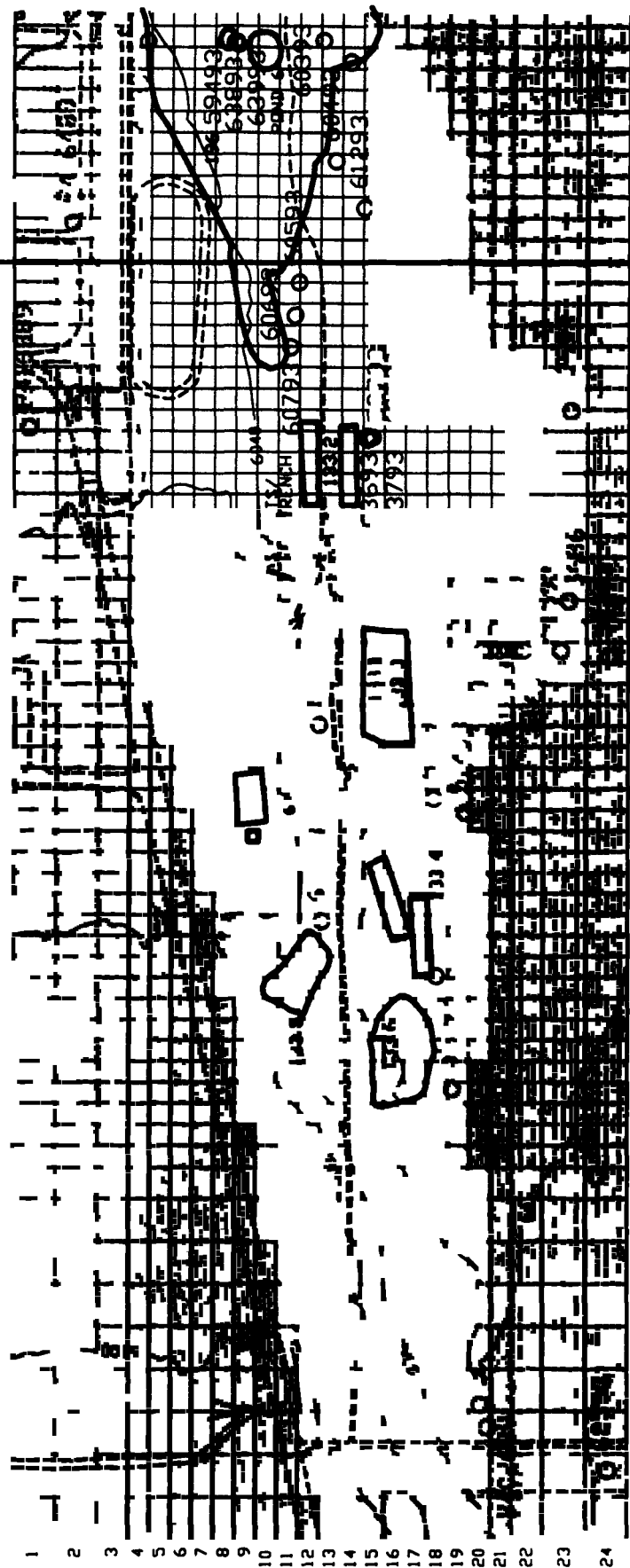
HYPOTHETICAL
 EXPOSURE ROUTES



CONCEPTUAL AIR PATHWAYS	
Drawn	NAH 8/1/95
Checked	7-7 8/1/95
Approved	
Date	
Date	
Date	
FILE OU5-5-3 DWG	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
OU5 - WOMAN CREEK PRIORITY DRAINAGE	
RPT/RI REPORT	
FIGURE 5-3	

Mat h
LI F Qu
S 5B

Mat h
Line F Qu
S 5B



Legend

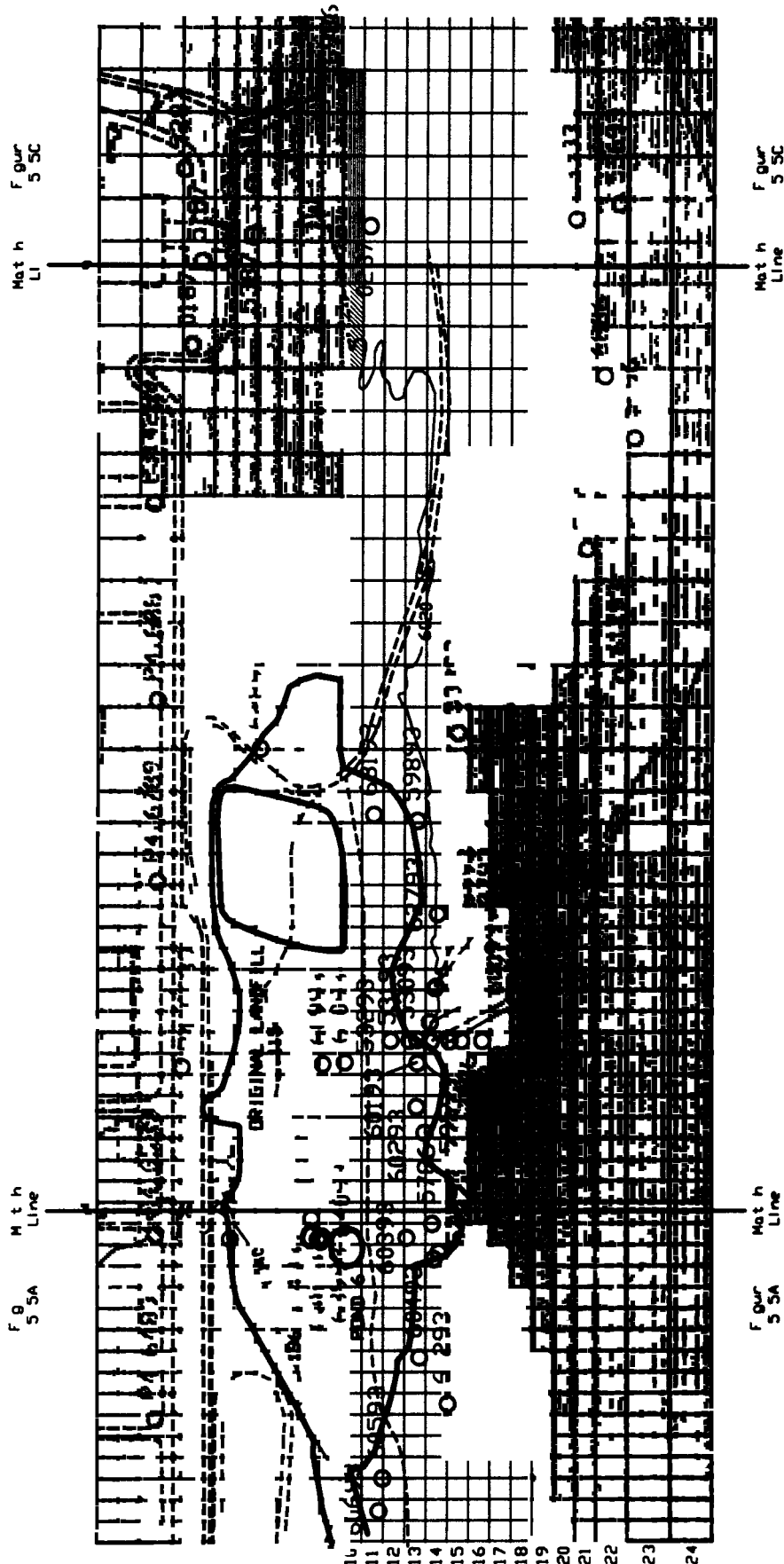
- No Flow
- Constant Head
- Monitoring W II
- Co to r Line 20
- Road
- Individual Hazardous Substance Sit

63093

200 feet

Drawn	2MB 8/9/95
Checked	7/27/95
Approved	
	FILE 5 SA.DWG

OU5 GROUNDWATER FLOW MODEL GRID
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OU5 WOMAN CREEK PRIORITY DRAINAGE
RPI/RI REPORT
FIGURE 6-5A



Legend

61893

Monitoring Well

Topographi Contour Lin 20

Road

Individual Hazard u S betance Site

No Flow

Constant Head

N

200 feet

Drawn *LAB* 8/9/95

Check d *JP* 8/9/95

Approved _____

Date _____

FILE DUS 5 SB.DWG

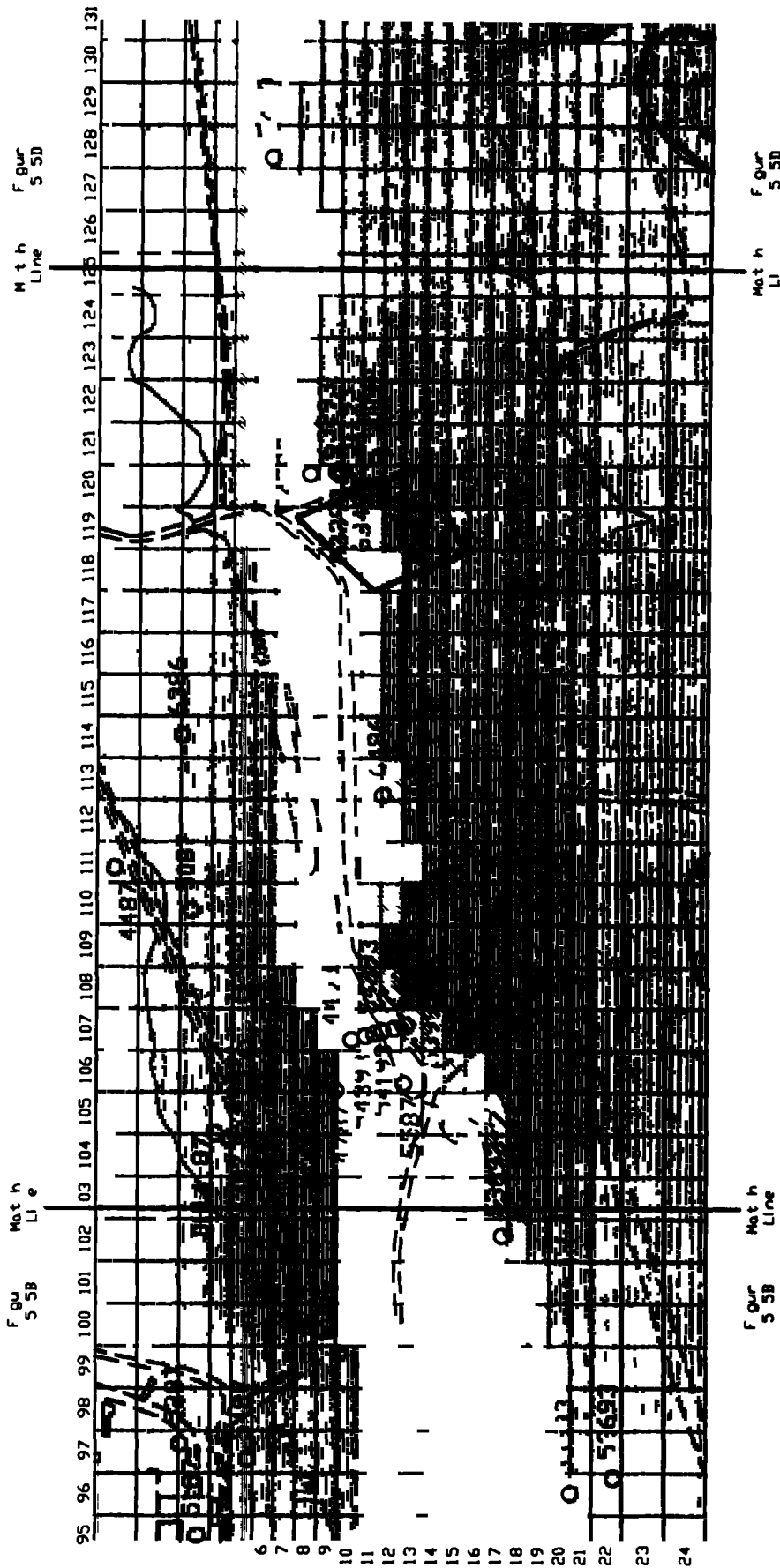
OU5 GROUNDWATER FLOW MODEL GRID

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

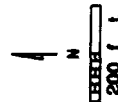
OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/RE REPORT

FIGURE 5-5B



- Legend**
- No Flow
 - Monitoring Well
 - Topographic Contour Line 20
 - == Road
 - Individual Hazardous Substance Site



Drawn	LAB 8/19/95
Checked	7/27 8/9/95
Approved	Date
	Da

FILE 5 SC DVG
OUG5 GROUNDWATER FLOW MODEL GRID
ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE
OUG5 WOMAN CREEK PRIORITY DRAINAGE
RPI/IN REPORT
FIGURE 5-5C

Figure 5 SC

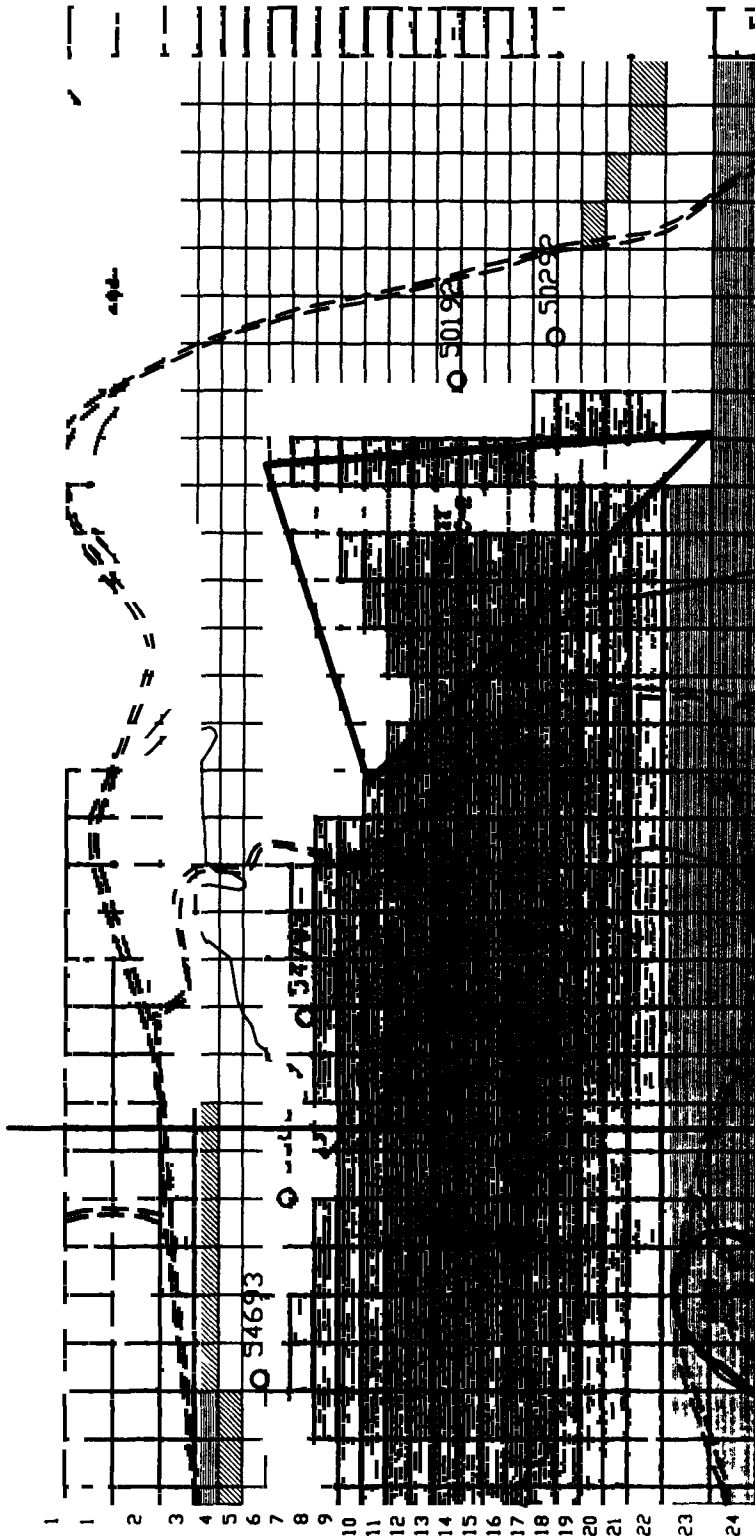


Figure 5 SC

Legend

- No Flow
- Constant Head
- Monitoring Well
- Topographical Contour Li 20
- Road
- Individual Hazardous Substance Site

Drawn	RAB 5/9/95
Checked	7/9/95
Approved	
Date	

FILE OUS 5 SD.DWG

OUS5 GROUNDWATER FLOW MODEL GRID

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-6D

Math Line Figure 5 6B

Math Line Figure 5 6B



- N Flow
- Zone 1 = (2.00 10³) ft/day
 - Zone 2 = (2.00x10³) ft/day
 - Zone 3 = (2.00) ft/day
 - Zone 4 = (34.56) ft/day

== Road
--- Individual Hazard u S betan e Site

N
200 feet

Legend

Dr wn BAR 8/9/95
 Checked 7/7 8/9/95
 Appr d _____
 Date _____

FILE OUS 5 6A.DWG

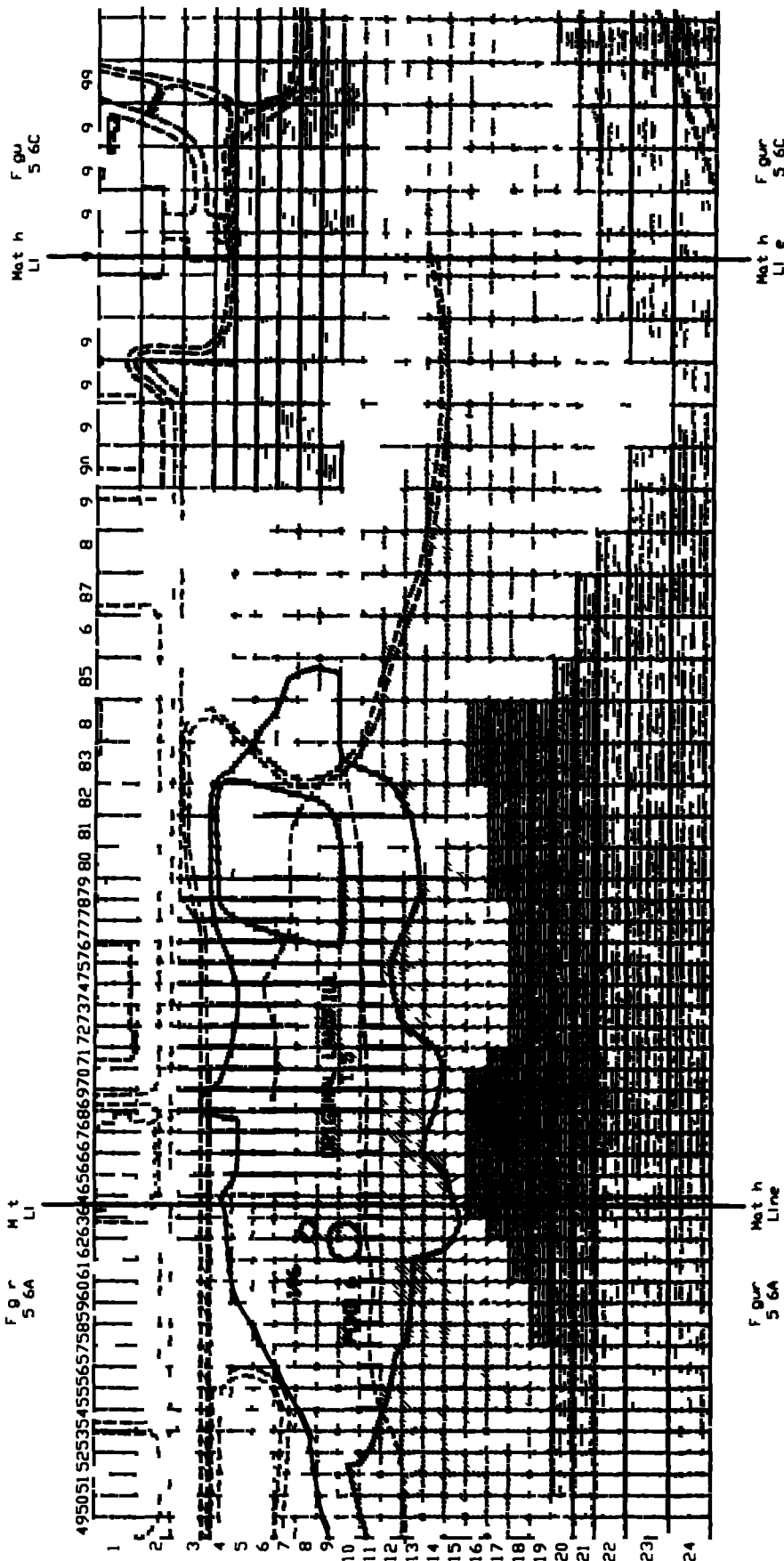
OU5 GROUNDWATER FLOW MODEL INITIAL HYDRAULIC CONDUCTIVITY ZONES

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-6A



Legend

- No Flow
- Zone 1 = (2.88 10³) ft/day
- Zone 2 = (2.88x10³) ft/day
- Zone 3 = (2.59) ft/day
- Zone 4 = (34.56) ft/day

Drawn SPB 8/9/95
 Checked 7/9 8/9/95
 Approved _____
 Date _____

FILE OUS 5 6B

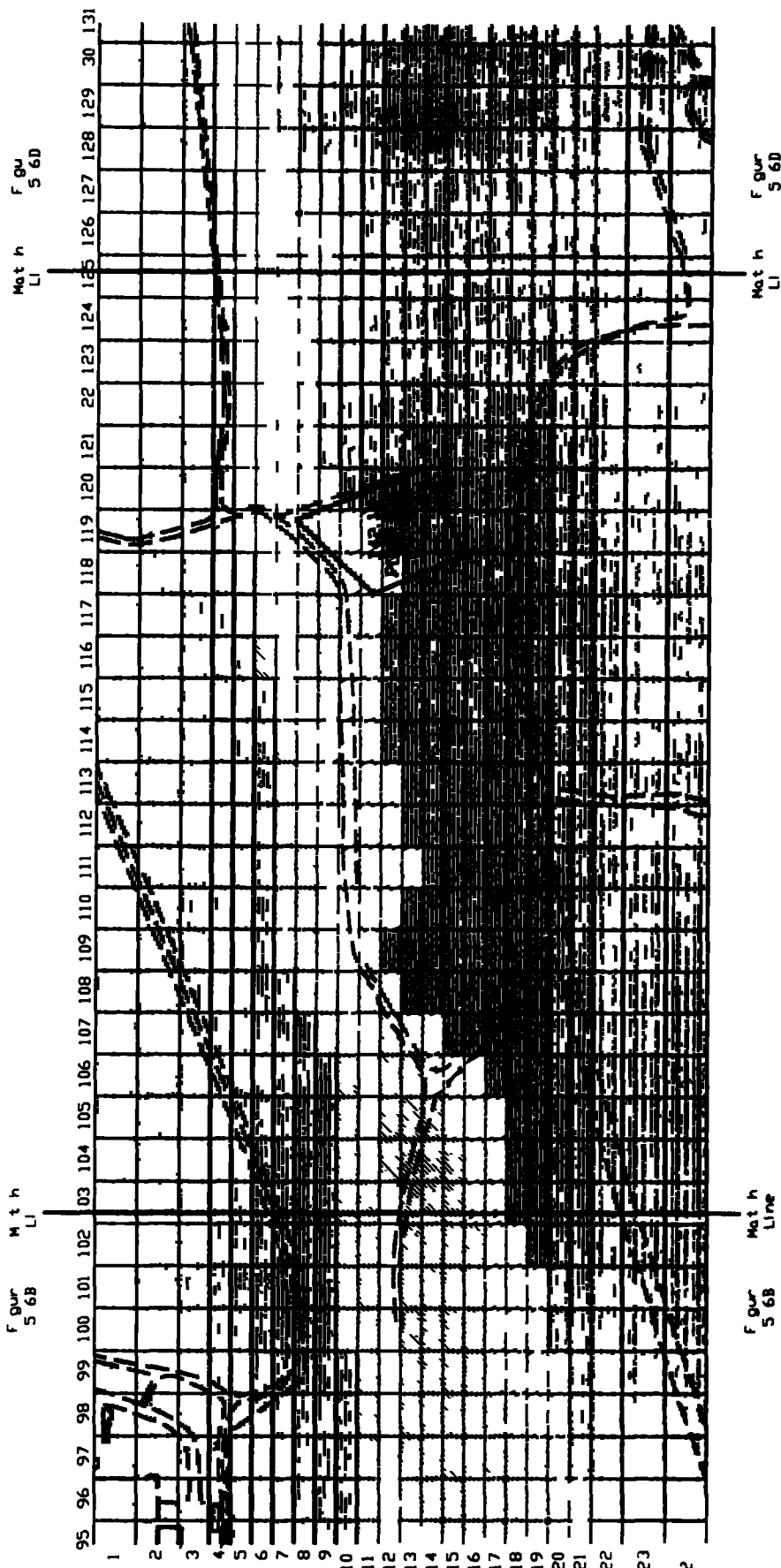
OUS GROUNDWATER FLOW MODEL INITIAL HYDRAULIC CONDUCTIVITY ZONES

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/IE REPORT

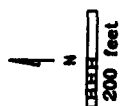
FIGURE 5-6B



Legend

- No Flow
- Zone 1 - (2.88 10³) ft/day
- Zone 2 - (2.89x10³) ft/day
- Zone 3 (2.59) ft/day
- Zone 4 - (34.56) ft/day

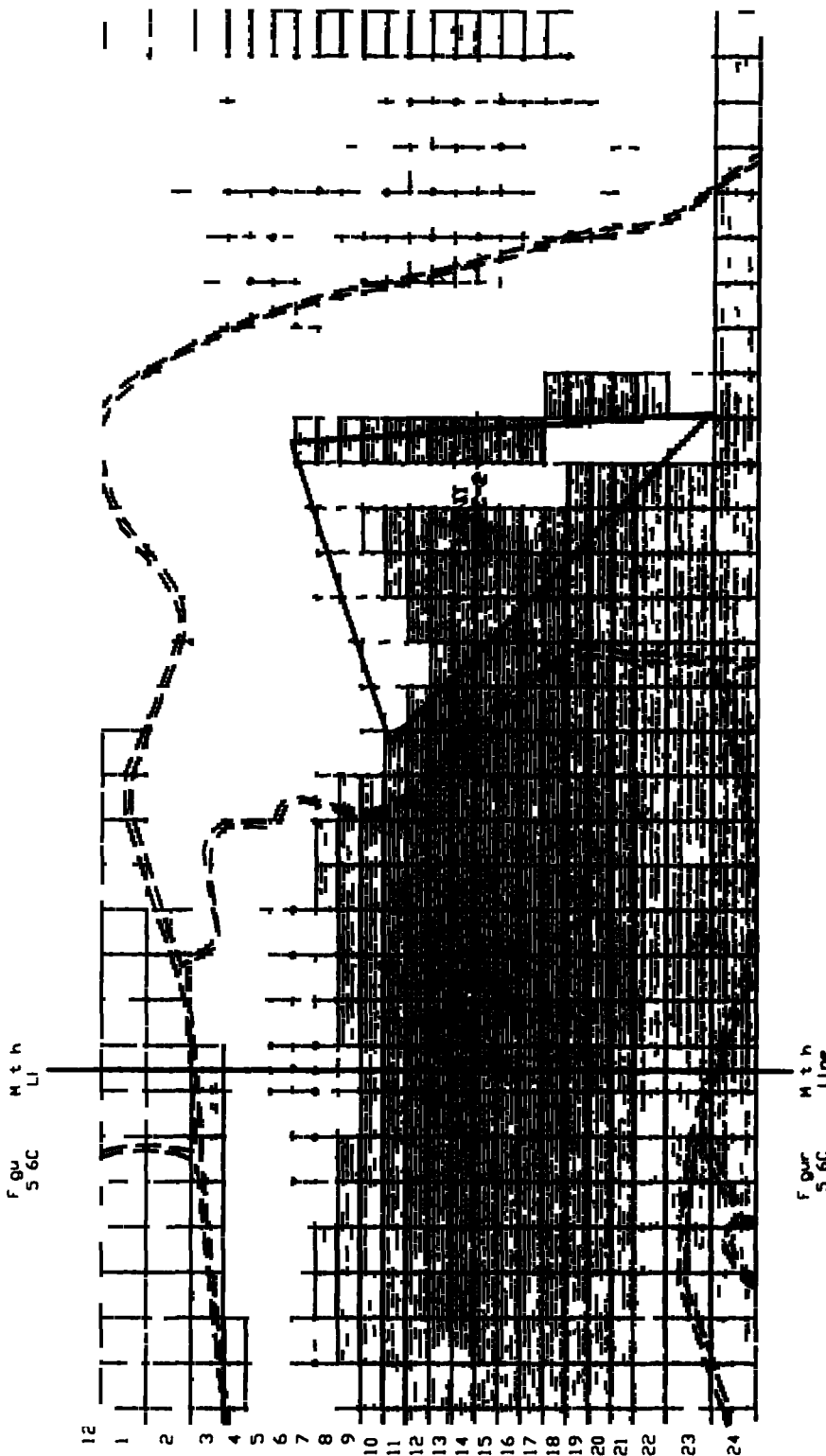
- Road
- Individual Hazard
- Setback Site



Drawn	2003 8/19/95
Checked	7/27/01/05
Approved	
Date	

FILE 05 5 6C

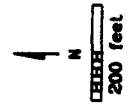
<p>OUS GROUNDWATER FLOW MODEL INITIAL HYDRAULIC CONDUCTIVITY ZONE</p>
<p>ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE</p>
<p>OUS WOMAN CREEK PRIORITY DRAINAGE</p>
<p>RPI/M REPORT</p>
<p>FIGURE 5-6C</p>



Legend

- N Flow
- Zone 1 (2.88x10⁻³) ft/day
- Zone 2 - (2.88x10⁻³) ft/day
- Zone 3 (2.59) ft/day
- Zone 4 - (34.58) ft/day

- Road
- Individual H sard u S balance Site



Drawn	<i>[Signature]</i> 8/9/95
Checked	<i>[Signature]</i> 8/9/95
Approved	Da
	Da

FILE OUS 3 6D

OUS GROUNDWATER FLOW MODEL INITIAL HYDRAULIC CONDUCTIVITY ZONES

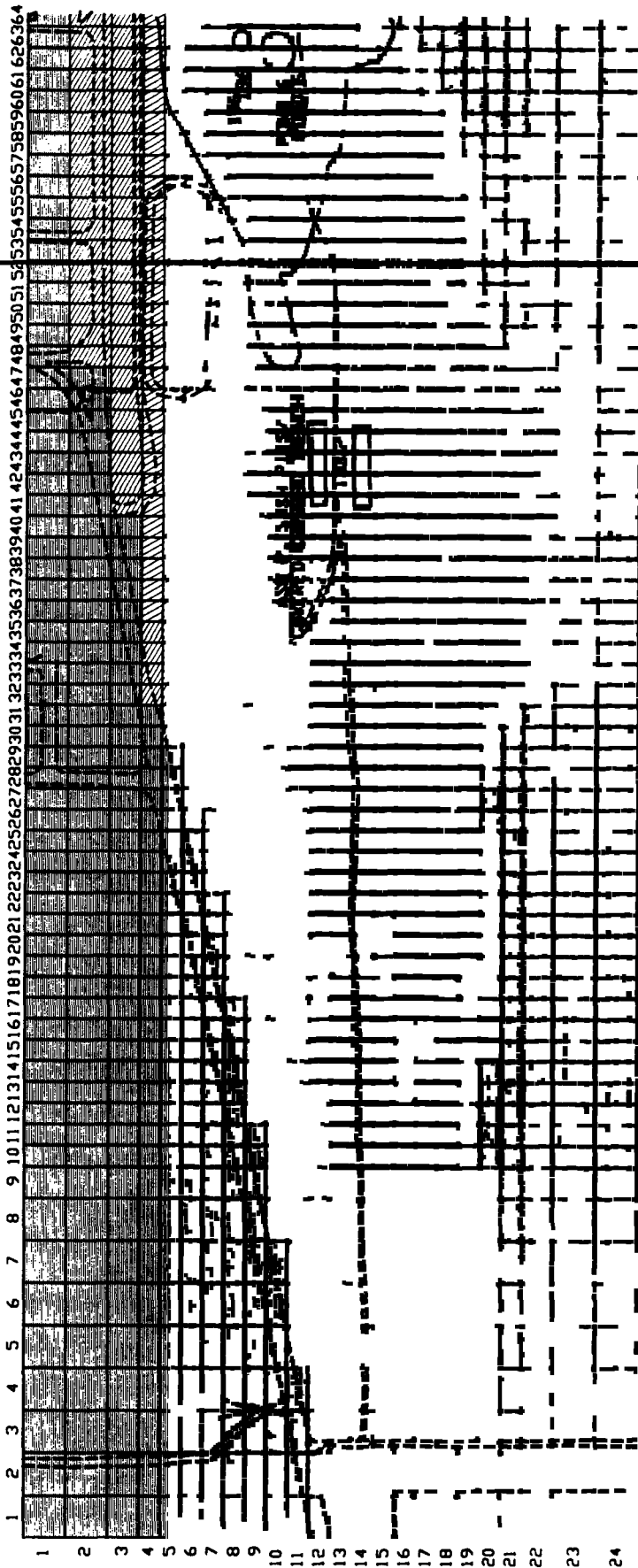
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-6D

Mat h
Li
F gu
5 78



Mat h
Li
F gu
5 78

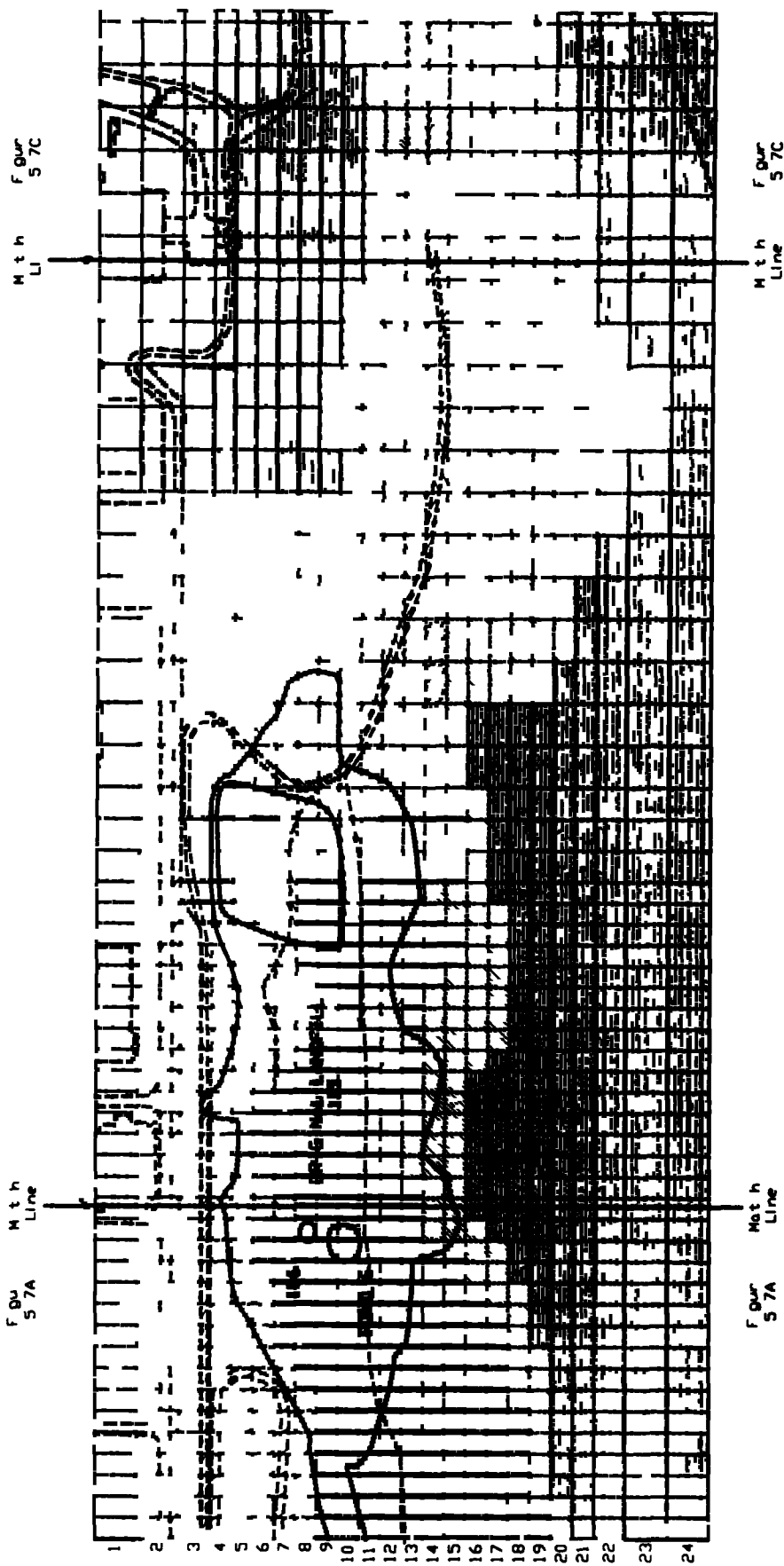
Legend

- N Flow
- Zone 1 = $(-5.2 \times 10^{-3}) (1.7 \times 10^{-3})$ ft/day
 - Zone 2 = (1.6×10^{-3}) ft/day
 - Zone 3 = (1.7×10^{-3}) ft/day
 - Zone 4 = (1.9×10^{-3}) ft/day
 - Zone 5 = (2.1×10^{-3}) ft/day
- Road
- Individual Hard as Site

N
200 feet

Dr. W.	8/19/95
Checked	7/20/95
Approved	
FILE OUS 5 7A.DWG	

OUS GROUNDWATER FLOW MODEL INITIAL RECHARGE ZONES
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS WOMAN CREEK PRIORITY DRAINAGE
RPI/RI REPORT
FIGURE 5-7A



Legend

- No Flow
- Zone 1 = $(-5.2 \times 10^{-3}) (1.7 \times 10^{-3})$ ft/day
- Zone 2 = (1.8×10^{-3}) ft/day
- Zone 3 = (1.7×10^{-3}) ft/day
- Zone 4 = (1.9×10^{-3}) ft/day
- Zone 5 = (2.1×10^{-3}) ft/day

- == Road
- Individual H sand
- S balance Site

N
200 feet

Drawn SAB 8/9/95
 Checked TJP 8-9-95
 Approved _____
 FILE OUS 5 7B DWG

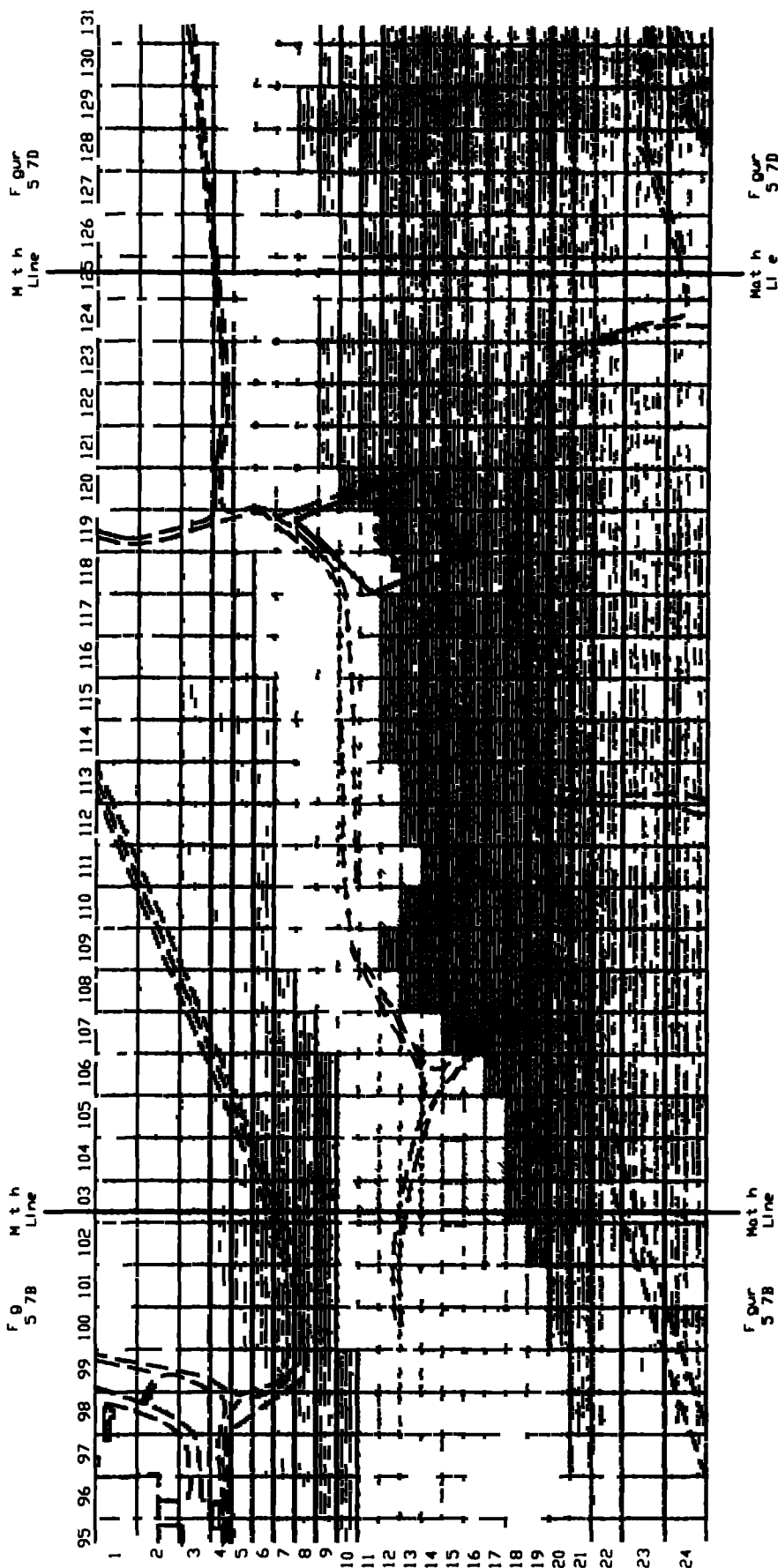
**OU5 GROUNDWATER
FLOW MODEL
INITIAL RECHARGE ZONES**

ROCKY PLATE ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/M REPORT

FIGURE 5-7B



Legend

- ☐ No Flow
- Zone 1 (52x10³) - (-17x10³) ft/day
- Zone 2 - (16 10³) ft/day
- Zone 3 (17 10³) ft/day
- Zone 4 - (19x10³) ft/day
- Zone 5 (21 10³) ft/day

Road
I divide al H zard u S balance Site

200 feet

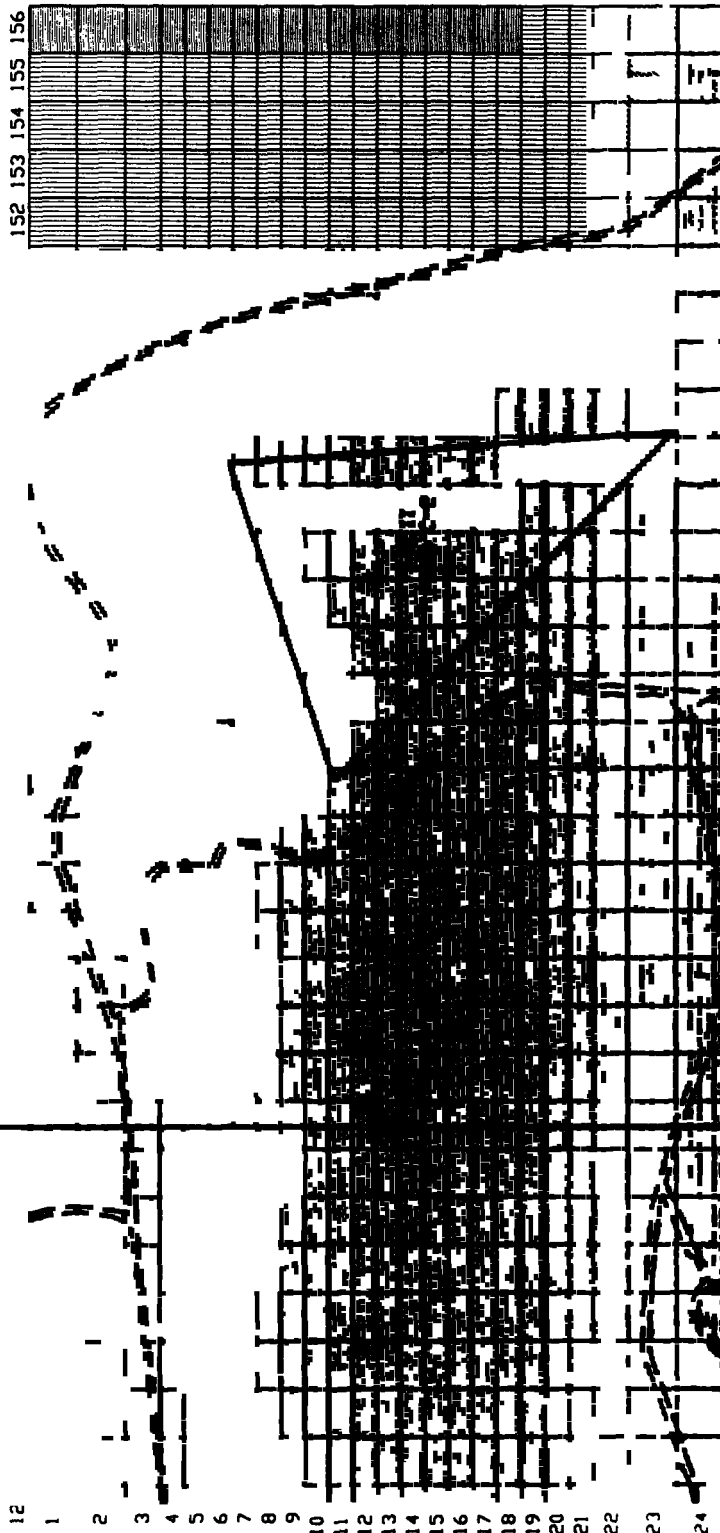
Dr on	8/9/95
Checked	8/9/95
Appr ved	D

FILE OUS 5 7C DVG

OU5 GROUNDWATER FLOW MODEL INITIAL RECHARGE ZONES
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OU5 WOMAN CREEK PRIORITY DRAINAGE
RFI/RI REPORT
FIGURE 5-7C

F Qu
5 7C

Mat h
Li



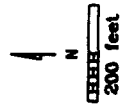
F Qu
5 7C

Mat h
Line

Legend

- No Flow
- Zone 1 = $(-5.2 \times 10^{-3}) - (1.7 \times 10^{-3})$ ft/day
- Zone 2 = (1.6×10^{-3}) ft/day
- Zone 3 = (1.7×10^{-3}) ft/day
- Zone 4 = (1.9×10^{-3}) ft/day
- Zone 5 = (2.1×10^{-3}) ft/day

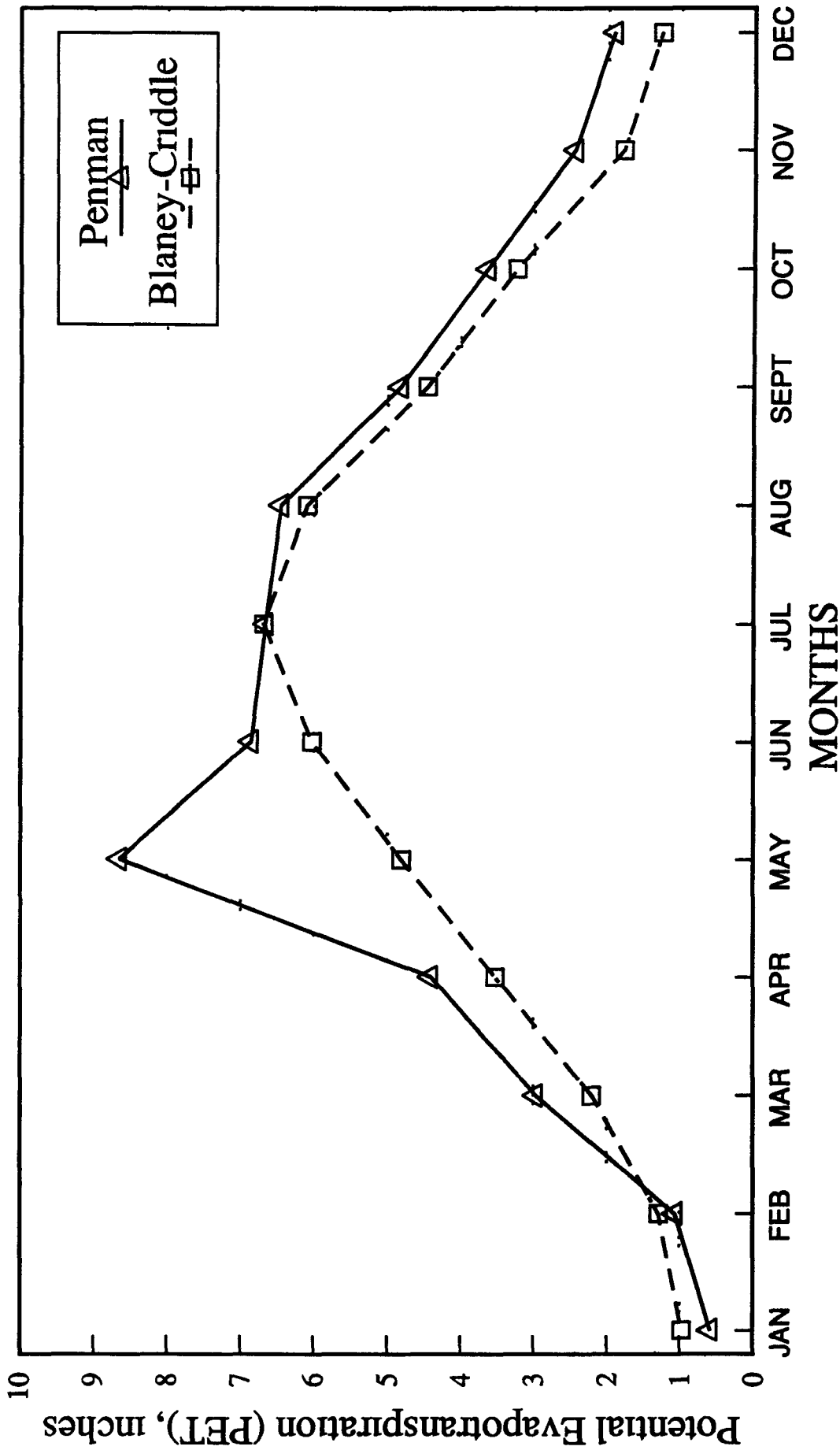
- Road
- Individual House
- Balance Site



Drawn	LAB 8/9/95
Checked	PAJ 8/9/95
Approved	
Date	

FILE QUS 5 7D.DWG

OU5 GROUNDWATER FLOW MODEL INITIAL RECHARGE ZONES	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
OU5 WOMAN CREEK PRIORITY DRAINAGE	
RPI/RE REPORT	
FIGURE 5-7D	



COMPARISON OF POTENTIAL
EVAPOTRANSPIRATION
CALCULATED BY PENMAN AND
BLANEY-CRIDDLE METHODS

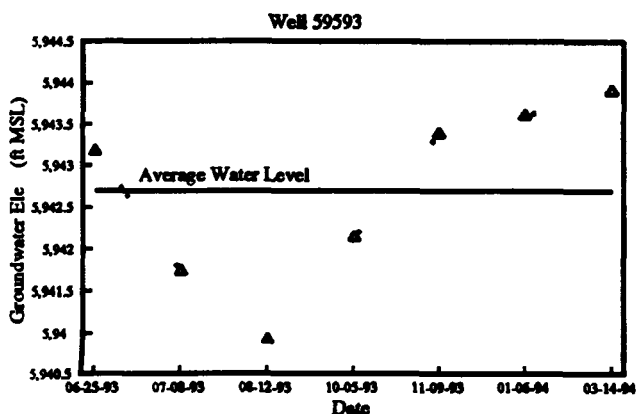
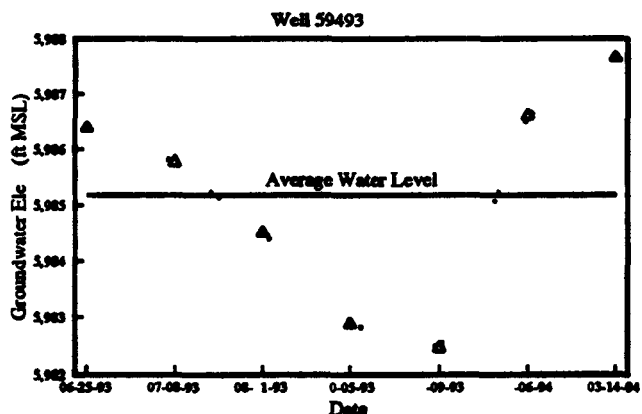
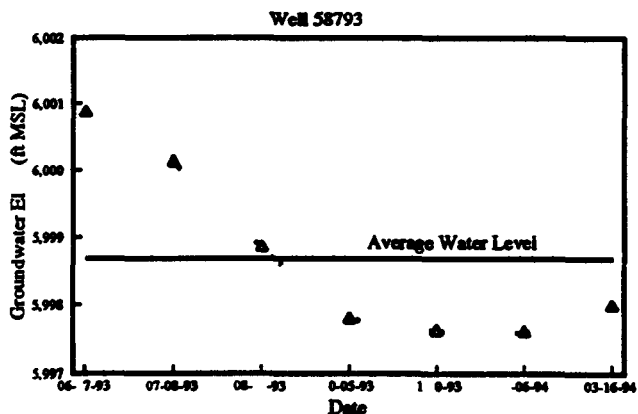
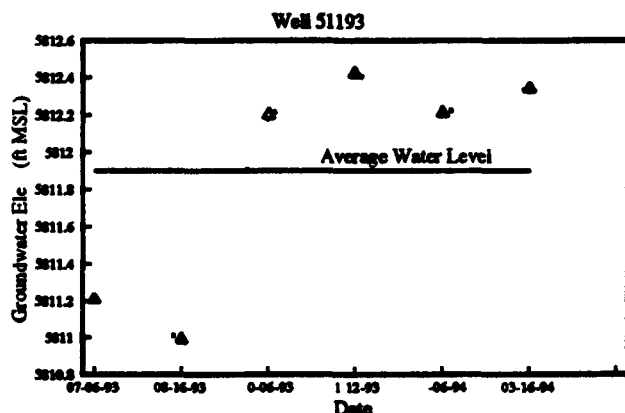
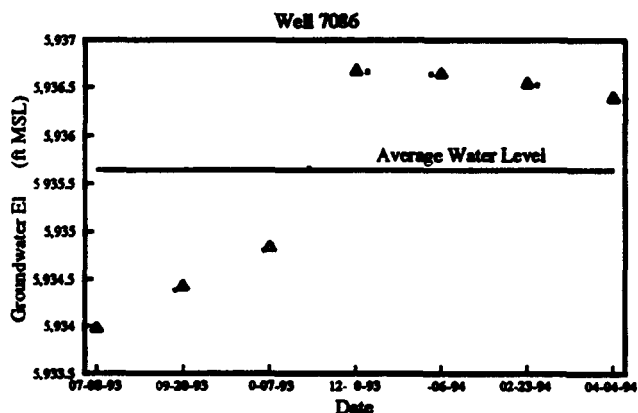
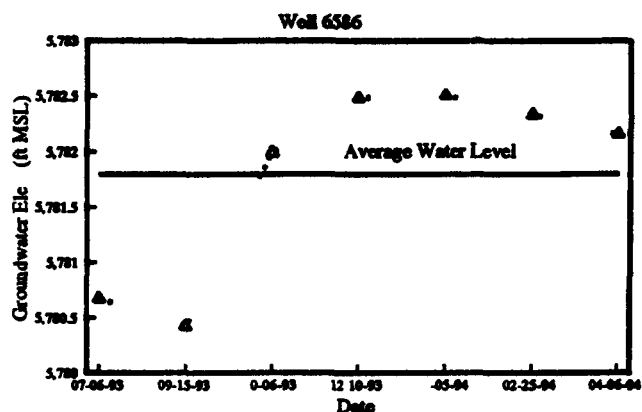
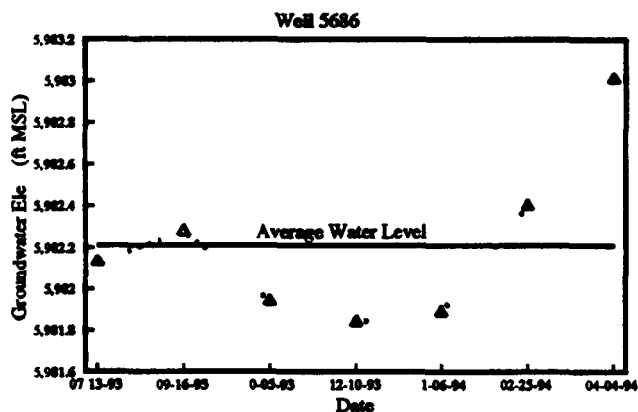
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	DATE
OCUS WOMAN CREEK PRIORITY DRAINAGE	DATE
REPORT	DATE
FIGURE 5-8	DATE

DRAWN *Pop 10/10/86*

CHECKED *John 10/10/86*

APPROVED *Wendy 10/10/86*

PLANNING



EXPLANATION

Measured Groundwater Elevation. ▲ ▲ ▲

**HYDROGRAPHS
OF
TARGET WELLS**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RFVRI REPORT

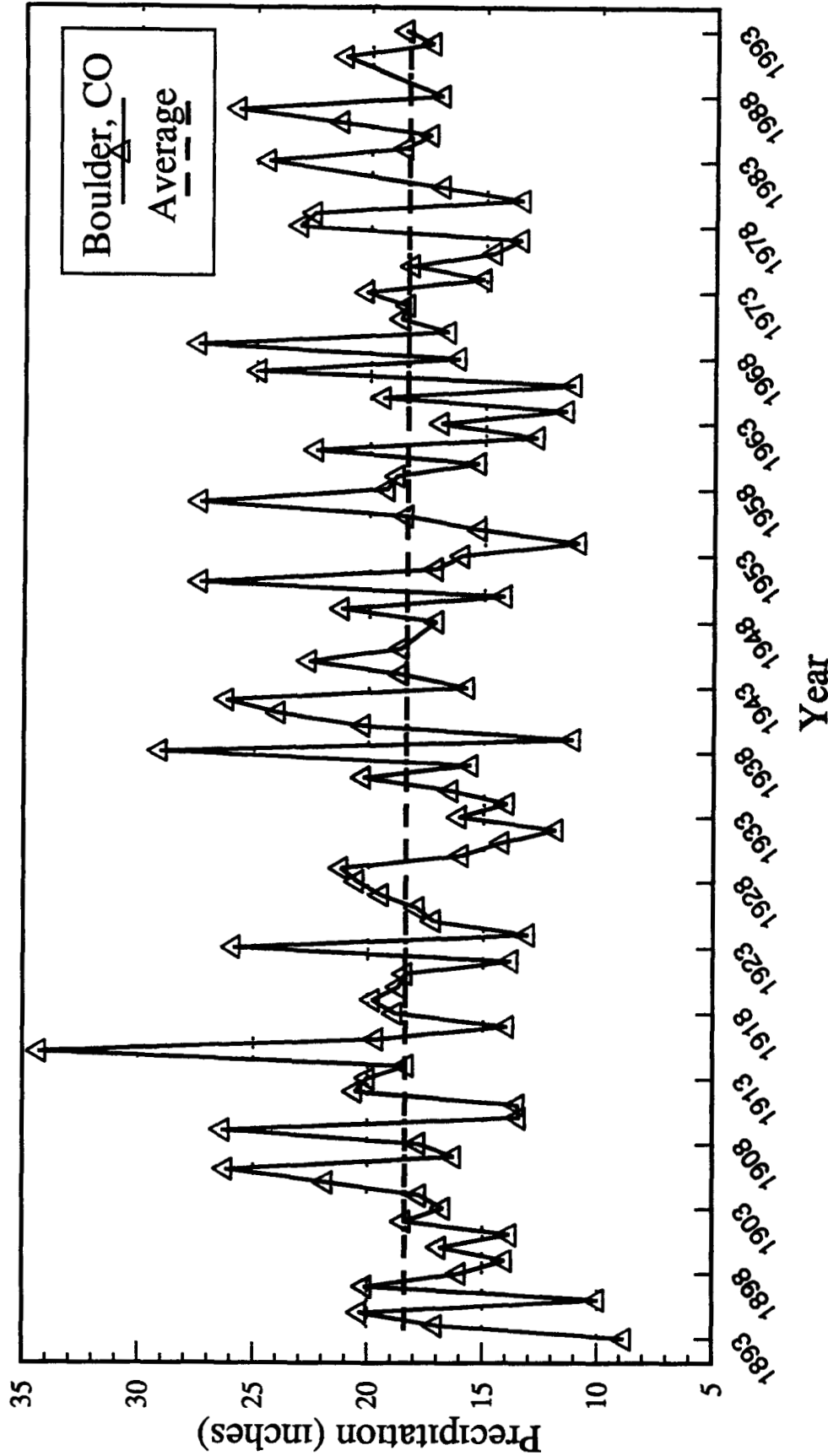
FIGURE 5-9

DRAWN 1026 7/21/95 DATE

CHECKED 78767h DATE

APPROVED _____ DATE

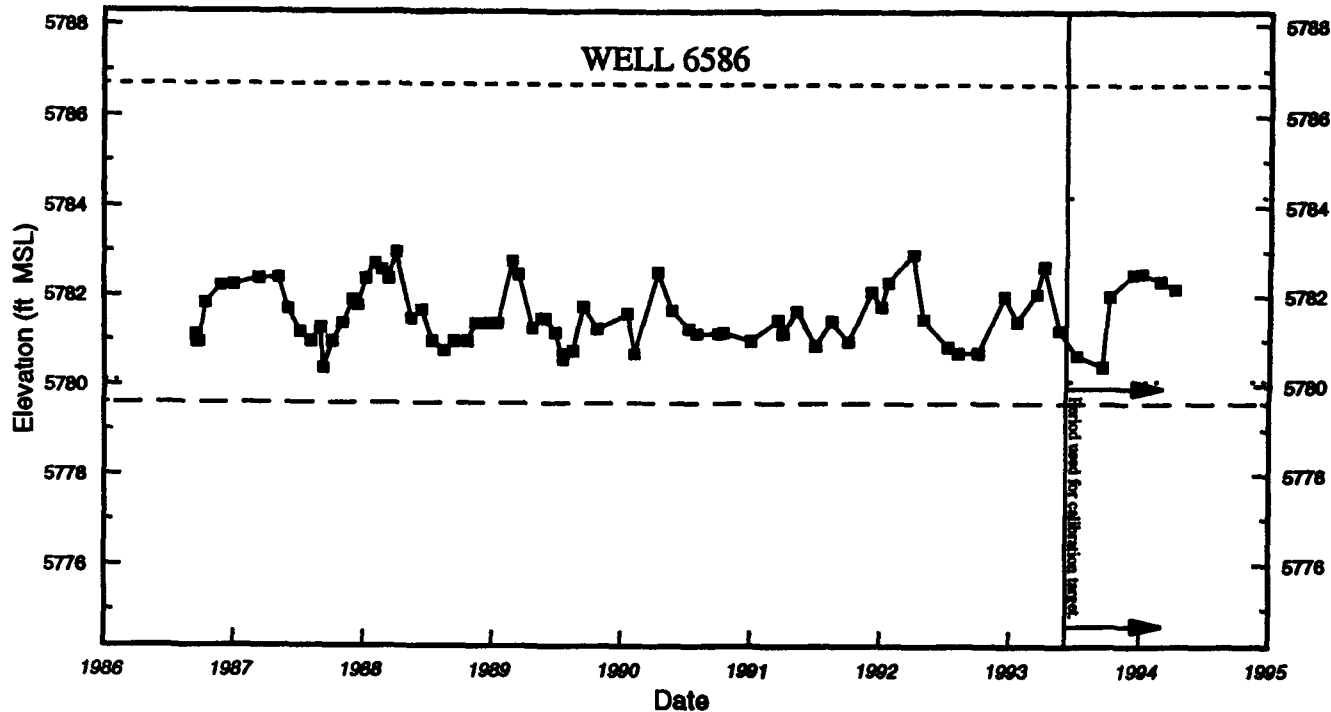
ES-9/DW



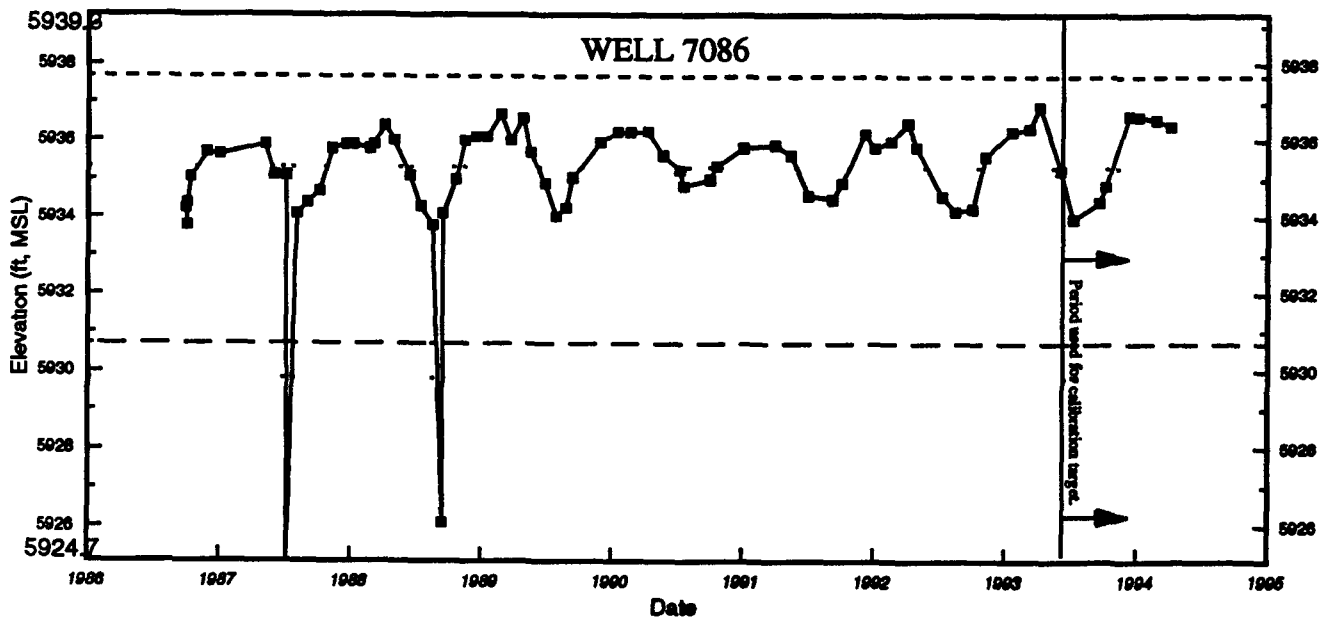
NOTE Average Precipitation at Boulder CO is 18.38 inches

PRECIPITATION AT
BOULDER, COLORADO

DRAWN	DATE	ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
CHECKED	DATE	COUS WOMAN CREEK PRIORITY DRAINAGE
APPROVED	DATE	REPORT REPORT
		FIGURE 5-10



Ground-Water Elevation Ground-Surface Elevation Top & Bottom of Screen Bedrock Elevation



Ground-Water Elevation Ground-Surface Elevation Top & Bottom of Screen Bedrock Elevation

NOTES The top and bottom lines of these hydrographs indicate the top of well casing and bottom of well elevations, respectively
Elevations plotted at Bottom of Well indicate a DRY condition.

HYDROGRAPHS OF WELLS 6586 AND 7086

DRAWN SDJ 1/27/95
DATE

CHECKED J. T. Hahn
DATE

APPROVED _____
DATE

FS-11.DRW

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-11

Figure
5 12B

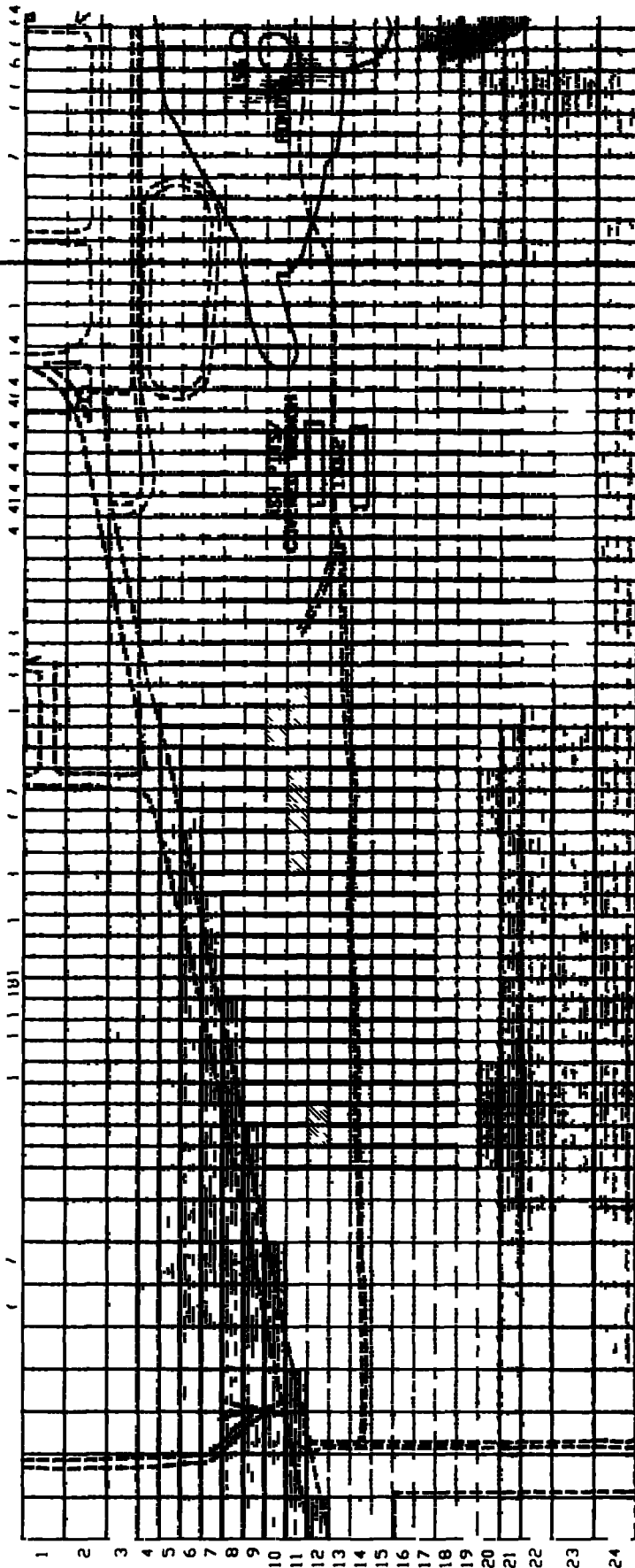


Figure
5 12B

Legend

- N Flow**
- Zone 1 - 0.1 ft/day
 - Zone 2 - 0.1 - 1 ft/day
 - Zone 3 - 1 - 10 ft/day
- Road**
- Individual Hazard us Subtance Site**

Dr on	8/7/95
Check d	8/8/95
Approved	
Date	

FILE OUS 512A.DWG

OU5 GROUNDWATER FLOW MODEL CALIBRATED HYDRAULIC CONDUCTIVITY ZONES

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-12A

Figure 5-12A

Figure 5-12C

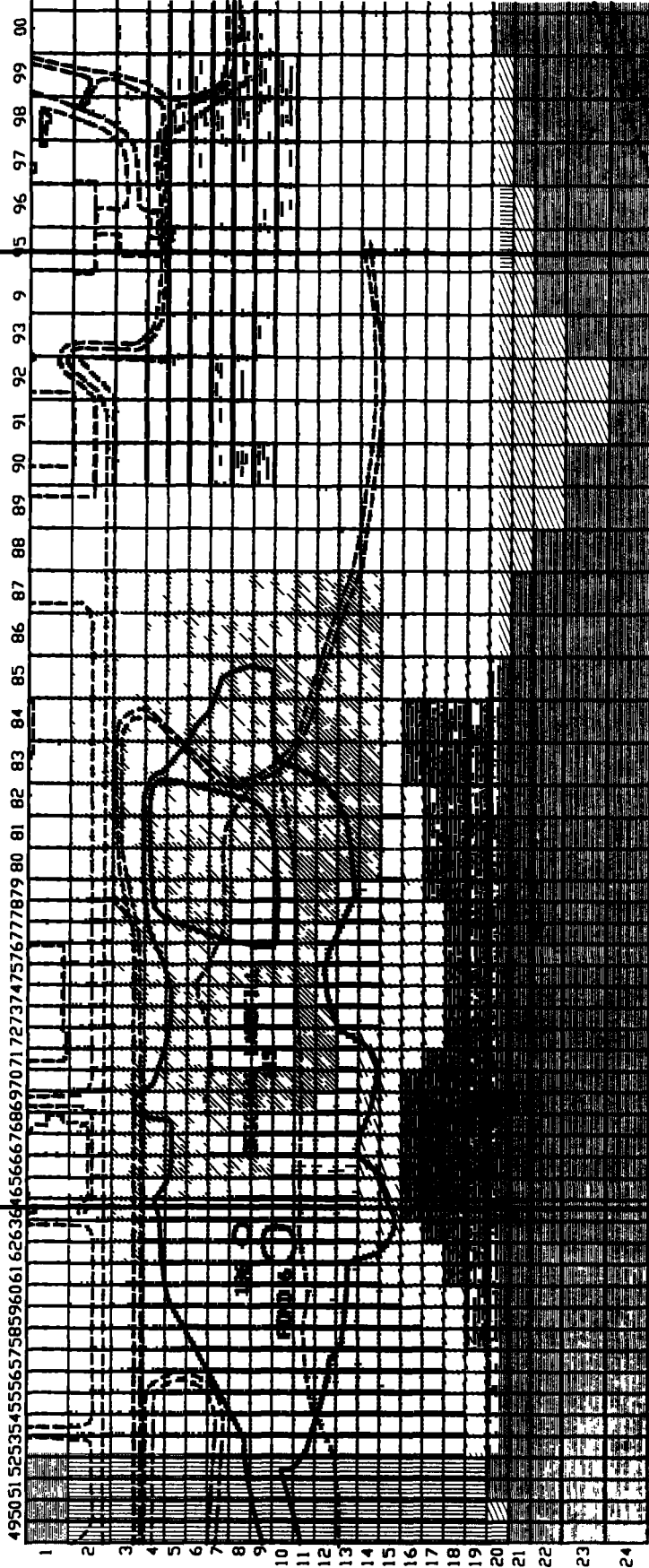


Figure 5-12A

Figure 5-12C

Legend

- N Flow**
- Zone 1 = 0.1 ft/day
 - Zone 2 = 1 ft/day
 - Zone 3 = 1 - 10 ft/day

Road

Individual Hazardous Substance Site

Drawn	8/9/95
Checked	8-9-95
Approved	
Date	

FILE 005 512B.DWG

OU5 GROUNDWATER FLOW MODEL CALIBRATED HYDRAULIC CONDUCTIVITY ZONES

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 WOMAN CREEK PRIORITY DRAINAGE

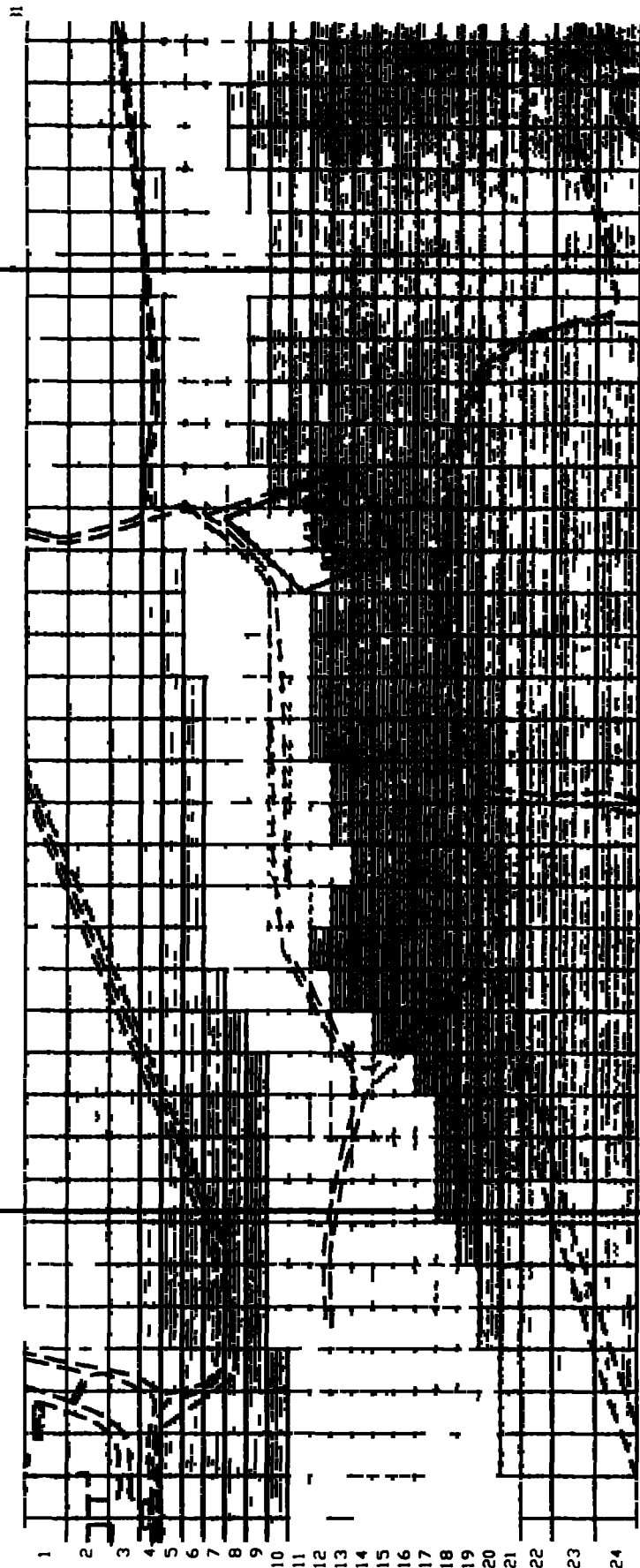
RPI/RI REPORT

FIGURE 5-12B

200 feet

Fig 5 12D

Fig 5 12B



Legend

- N Flow
- Zone 1 - 01 0.1 ft/day
- Zone 2 01 1 ft/day
- Zone 3 - 1 - 10 ft/day
- Road
- Individual Hazardous Site

200 feet

Dr. on LAB 8/9/95
 Checked 7/9/95
 Appr ed D
 Dat

FILE OUS 512C.DWG

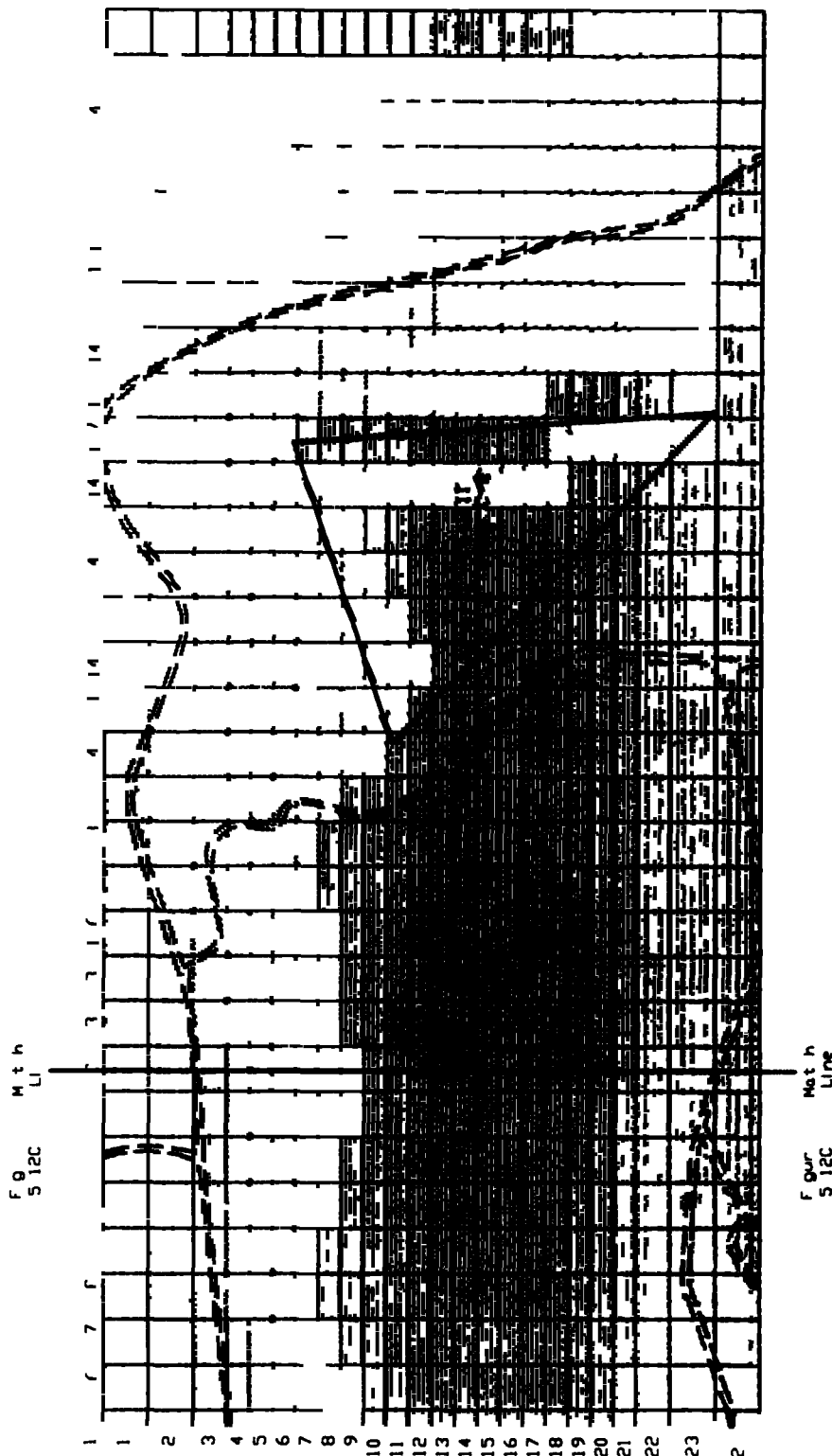
OU5 GROUNDWATER FLOW MODEL CALIBRATED HYDRAULIC CONDUCTIVITY ZONES

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

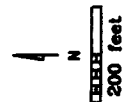
RPI/RI REPORT

FIGURE 5-12C



Legend

- N Flow
- Zone 1 01 - 0.1 ft/day
- Zone 2 0.1 - 1 ft/day
- Zone 3 1 - 10 ft/day
- Zone 4 10 - 100 ft/day
- Road
- Individual Hazard us Substance Site



Dr on	240 8/9/95
Checked	7/7 8/9/95
Approved	
Date	

FILE OUS 512D.DWG

OUS GROUNDWATER FLOW MODEL CALIBRATED HYDRAULIC CONDUCTIVITY ZONES

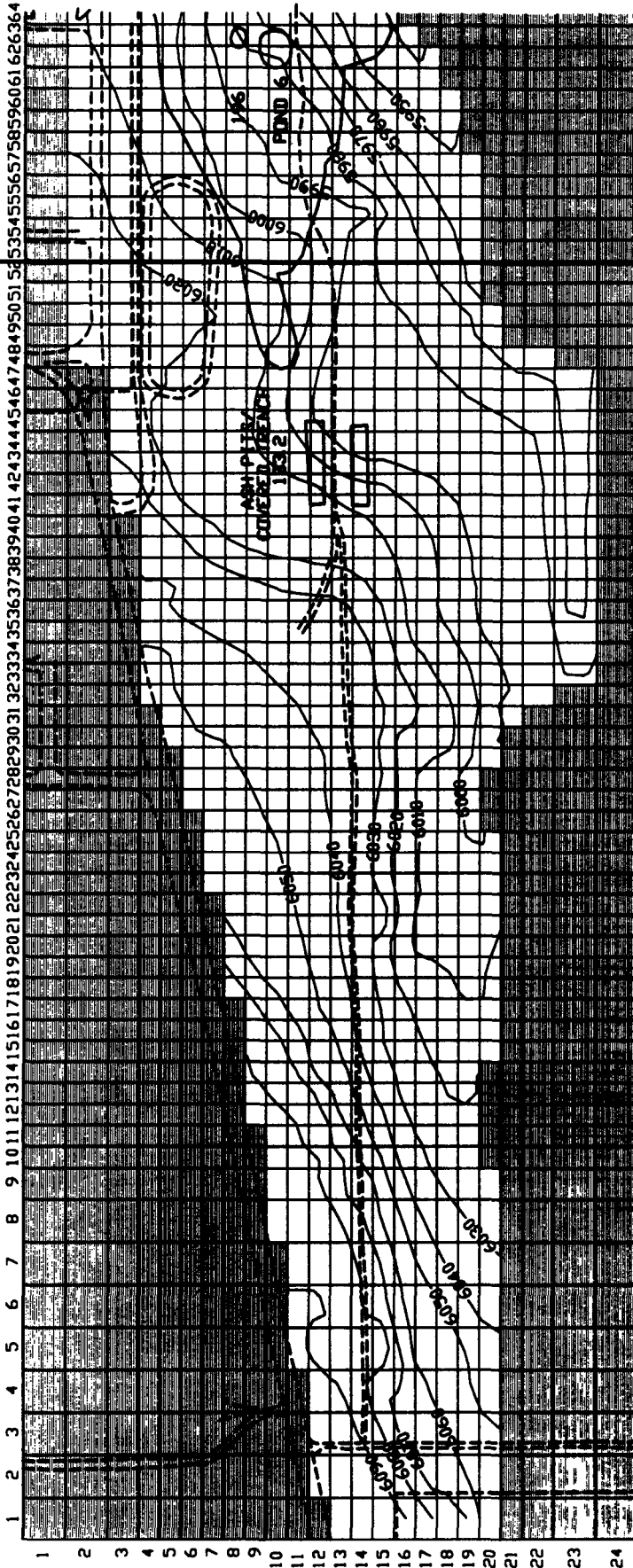
ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-12D

Mat h F Qu
LI 5 13B



Mat h F Qu
LI 5 13B

Legend

- Bedrock Elevation Contour 10
- Road
- Individual House
- Subtract

No Fl

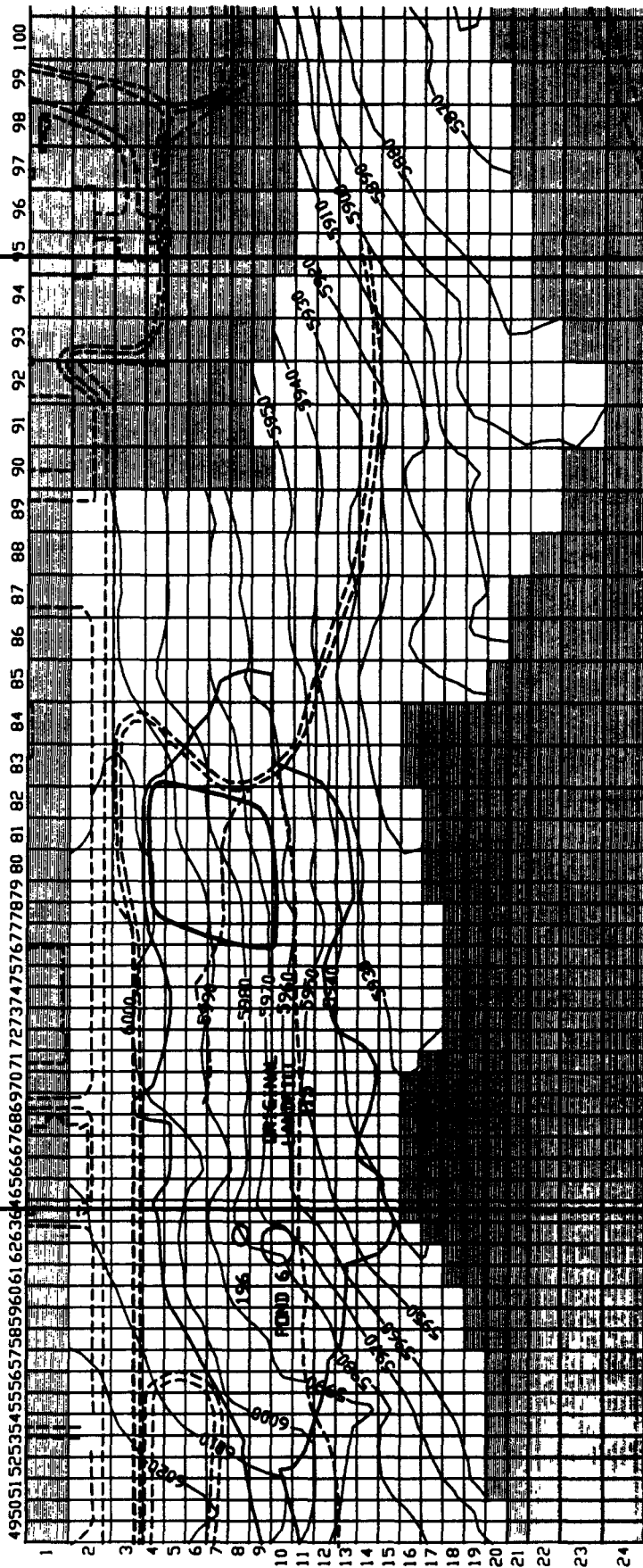
Drawn	2AR 8/9/95
Checked	7-7 8/15
Approved	

FILE QUS 513A.DWG

<p>QUS GROUNDWATER FLOW MODEL BEDROCK ELEVATIONS</p>	
<p>ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE</p>	
<p>QUS WOMAN CREEK PRIORITY DRAINAGE</p>	
<p>RPI/M REPORT</p>	
<p>FIGURE 5-13A</p>	

F Qu
S 13A

M t h
L i e
F Qu
S 13C



F Qu
S 13A

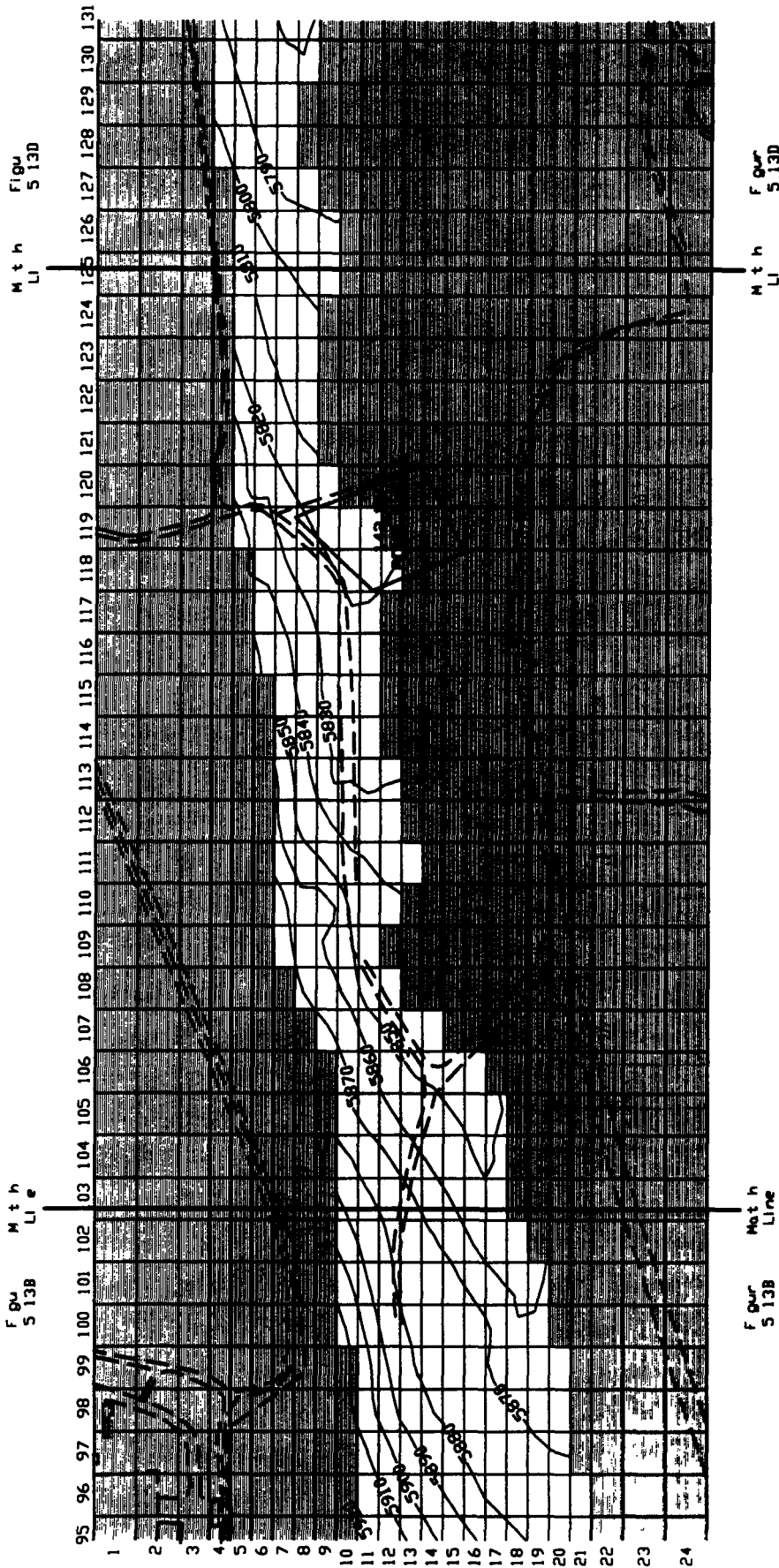
M t h
L i e
F Qu
S 13C

Legend

- No Flow
- Bedrock Elevation Contour 10
- Road
- Individual Hazardous Site

Drawn LAB 8/2/25
 Checked 727 8/19/25
 Approved _____
 FILE DUS S13B.DWG

<p>OU5 GROUNDWATER FLOW MODEL BEDROCK ELEVATIONS</p>	
<p>ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE</p>	
<p>OU5 WOMAN CREEK PRIORITY DRAINAGE</p>	
<p>RPT/IN REPORT</p>	
<p>FIGURE 6-13B</p>	



Legend

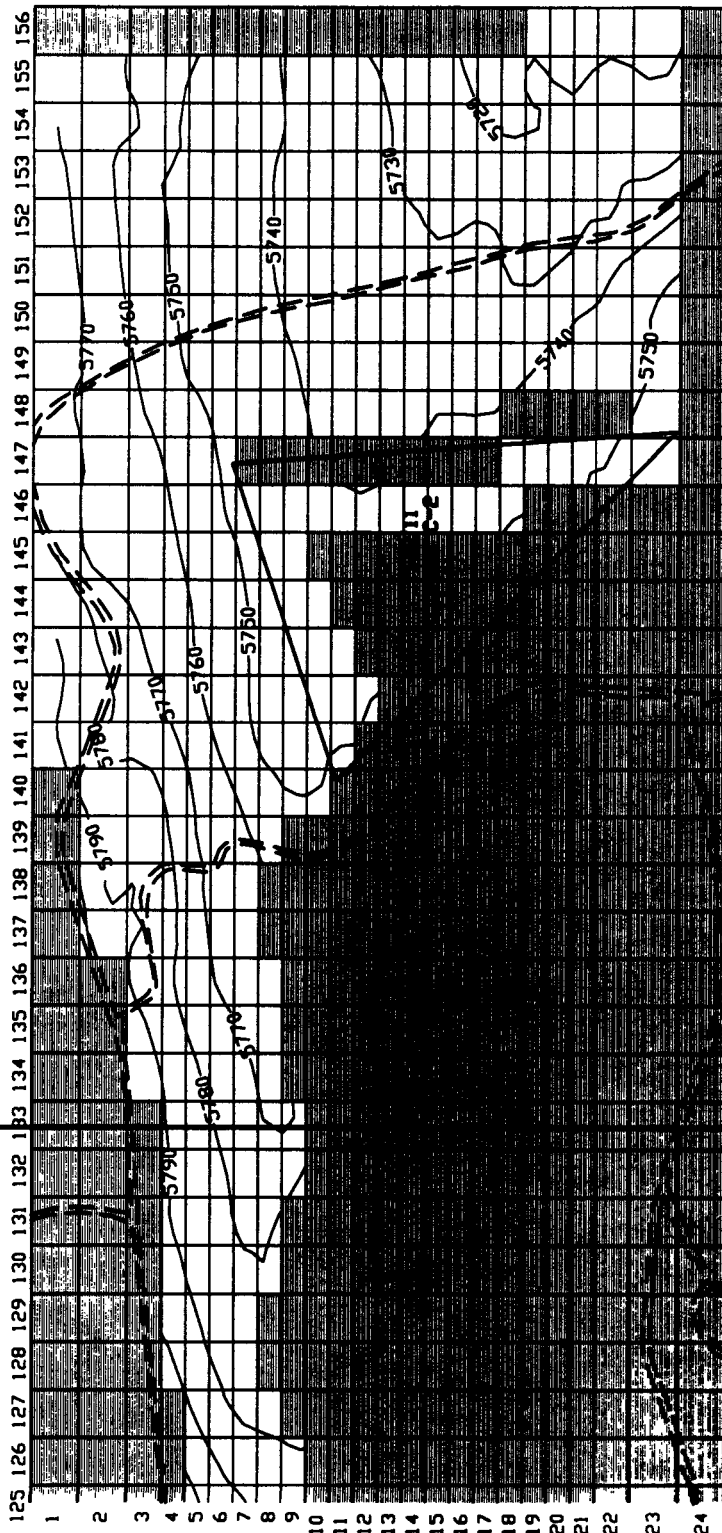
- No Flow
- Bedrock Elevatio
- Road
- Individual Hazardous Site

200 feet

Drawn	LAB 8/9/95
Checked	7/2/95
Approved	
Date	

FILE OUS 513C.DWG
OUS GROUNDWATER FLOW MODEL BEDROCK ELEVATIONS
ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS WOMAN CREEK PRIORITY DRAINAGE
RPI/RI REPORT
FIGURE 6-13C

F 94
S 13C
M t h
Line



F 94
S 13C
M t h
Line

Legend

- N P w
- Bedrock Elev ti n Contou 10
- Road
- Individual Hazard us S betance Site

200 feet

Dr wn	8/9/95
Checked	8-9-95
Approved	
FILE OUS 513D.DWG	

OUS GROUNDWATER FLOW MODEL BEDROCK ELEVATIONS
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS WOMAN CREEK PRIORITY DRAINAGE
RPI/RI REPORT
FIGURE 5-13D

North
Line
Four
514B



North
Line
Four
514B

Legend

Zone	Flow
Zone 1	(7 4296 10 ⁴) (2 4296 10) ft/day
Zone 2	(2 2857x10 ⁴) ft/day
Zone 3	(2 4296x10) ft/day
Zone 4	(2 7143x10 ⁴) ft/day
Zone 5	(3 0x10) ft/day

Road
Individual
Hazardous Site

North
Line
Four
514B
200 feet

Drawn	8/9/95
Checked	8/9/95
Approved	

FILE OUS 514A.DWG

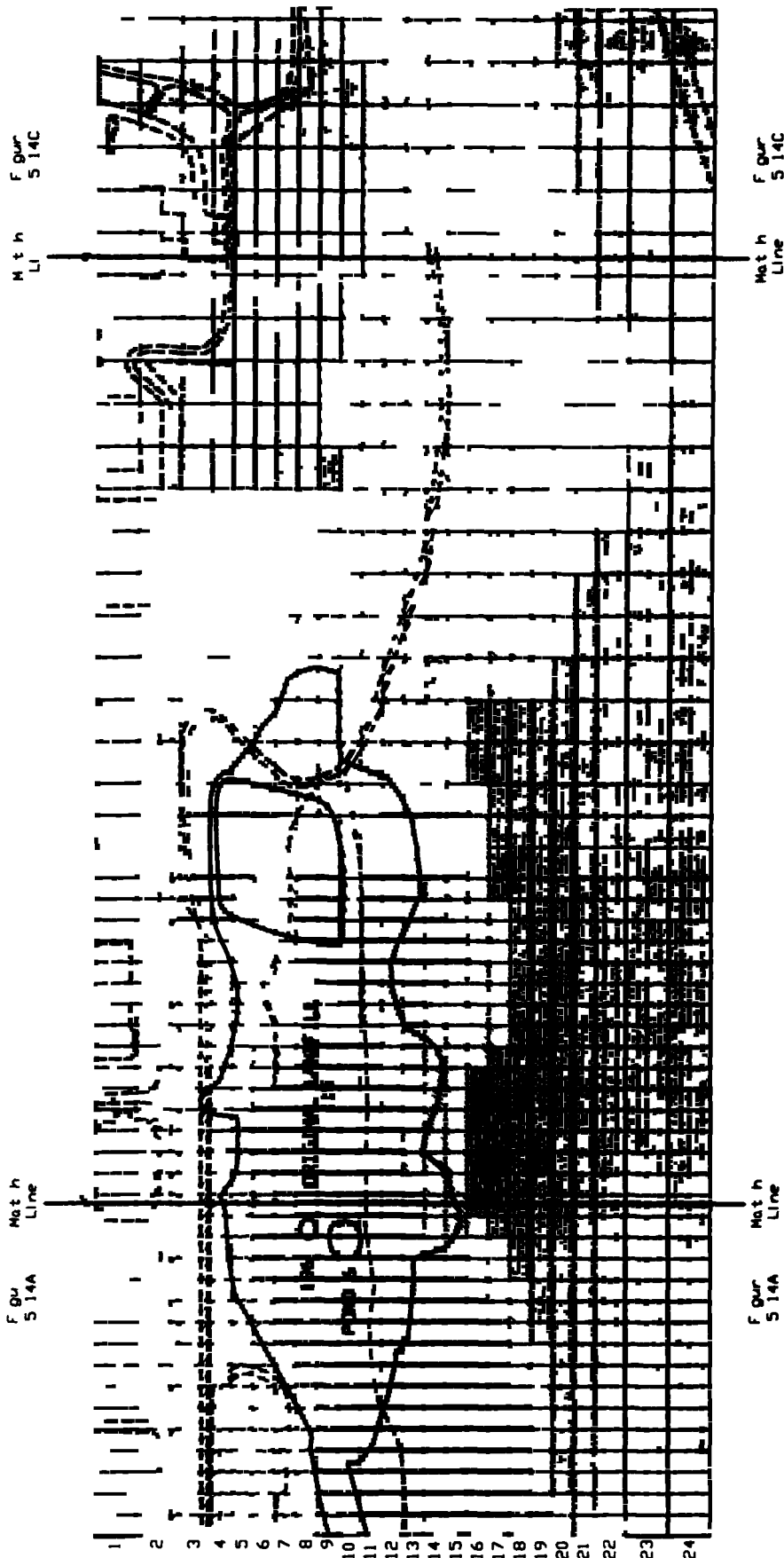
OUS GROUNDWATER FLOW MODEL CALIBRATED RECHARGE ZONES

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

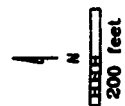
FIGURE 5-14A



Legend

- No Pl w
- Zon 1 = (7 4286 10) - (2 4286x10 ⁴) ft/day
- Zone 2 = (2 2867x10) ft/day
- Zone 3 = (2 4286x10 ⁴) ft/day
- Zone 4 = (2 7143x10) ft/day
- Zon 5 = (3 0x10 ⁴) ft/day

Road
 Indi id | H zard
 S balance Site



Dr wn	<i>8/19/95</i>
Checked	<i>8/19/95</i>
Approved	

FILE OUS 51 B.DWG

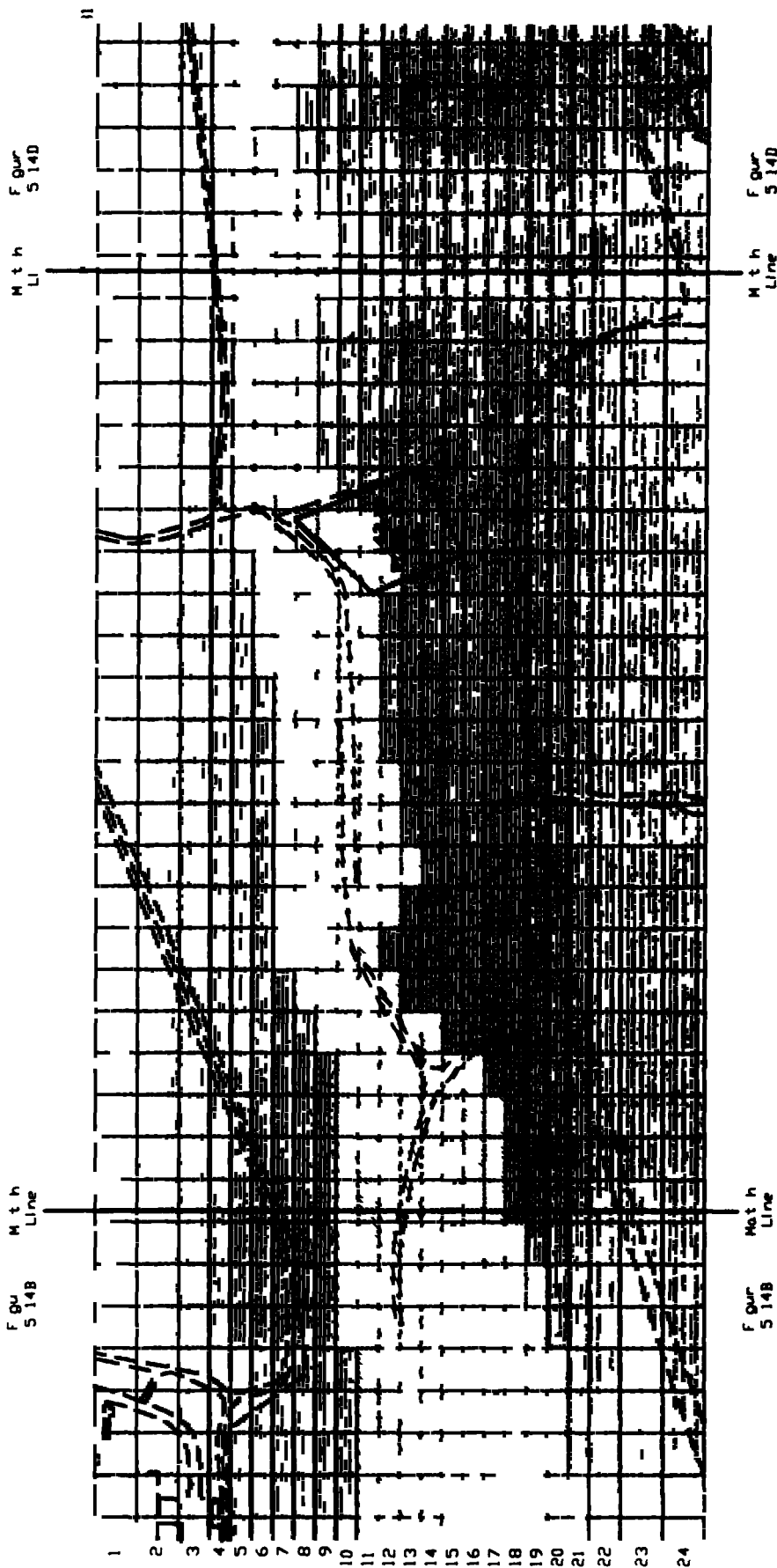
OU5 GROUNDWATER FLOW MODEL CALIBRATED RECHARGE ZONES

BOCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

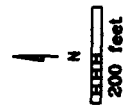
FIGURE 5-14B



Legend

- N P l w
- Zone 1 - (7 4286x10 ⁴) - (2 4286 10 ⁴) ft/day
- Zone 2 (2 2857x10) ft/day
- Zone 3 (2 4286x10) ft/day
- Zone 4 (2 7143x10) ft/day
- Zone 5 - (3 0x10) ft/d y

Road
Individual I H zard
S belanc Site



Dr wn	<i>[Signature]</i> 8/19/91
Checked	<i>[Signature]</i> 8-19-91
Approved	Date
	Dat

FILE OUS 514C DVG

OUS GROUNDWATER FLOW MODEL CALIBRATED RECHARGE ZONES

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/M REPORT

FIGURE 5-14C

Figure 5-14C

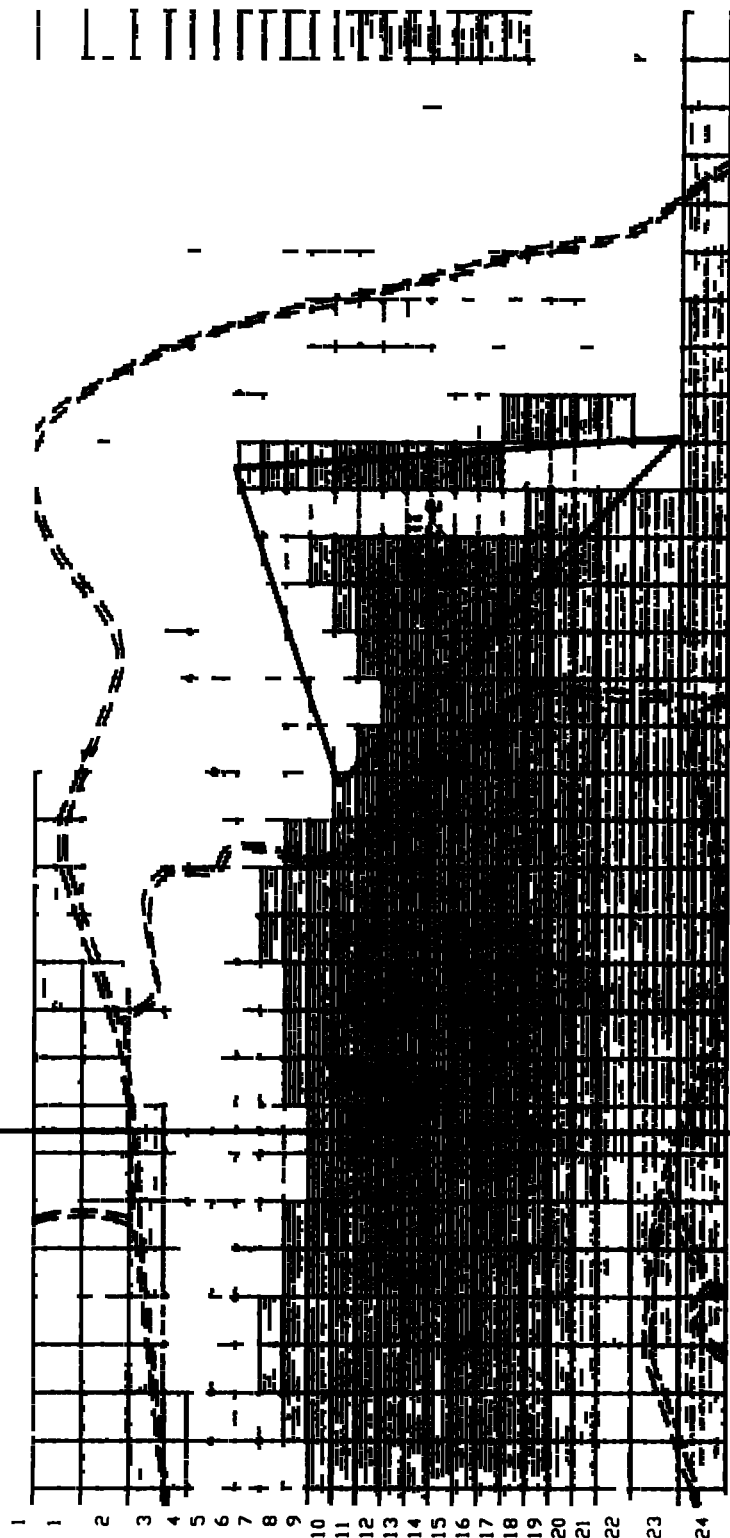


Figure 5-14C

Legend

- No Flow
- Zone 1 = (7 4286x10) - (2 4286 10 4) ft/day
- Zone 2 = (2 2807x10) ft/day
- Zone 3 = (2 4286x10) ft/day
- Zone 4 = (2 7143x10) ft/day
- Zone 5 = (3 0x10) ft/day

— Road
— Individual Hazardous Site

Drawn	<i>DBB 8/9/95</i>
Checked	<i>DBB 8/9/95</i>
Approved	
Date	

FILE OUS 514D.DWG

OU5 GROUNDWATER FLOW MODEL CALIBRATED RECHARGE ZONES

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

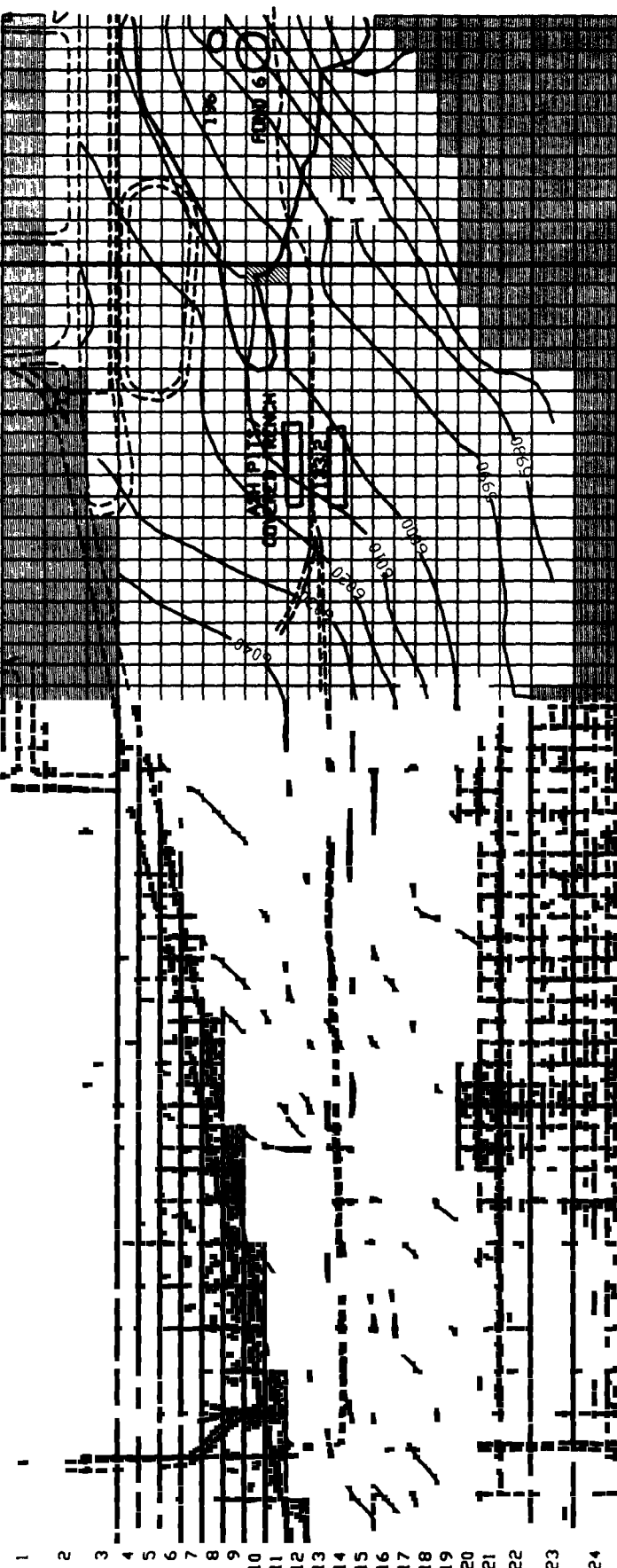
RPI/MI REPORT

FIGURE 5-14D

M t h
Line 5 158

32333435363738394041 42434445464748495051 52535455565758596061 626364

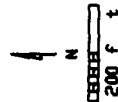
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24



M t h
Li 5 158

Legend

- No Fl
- Dry Ar a
- U te T bl Contour 10
- Road
- Indi dual Ho dous Sub t
- S t



Dr on 8/9/95
 Checked RJP
 Approved D
 Da

FILE OUS 315A.DWG

OUS GROUNDWATER FLOW MODEL SIMULATED WATER TABLE

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

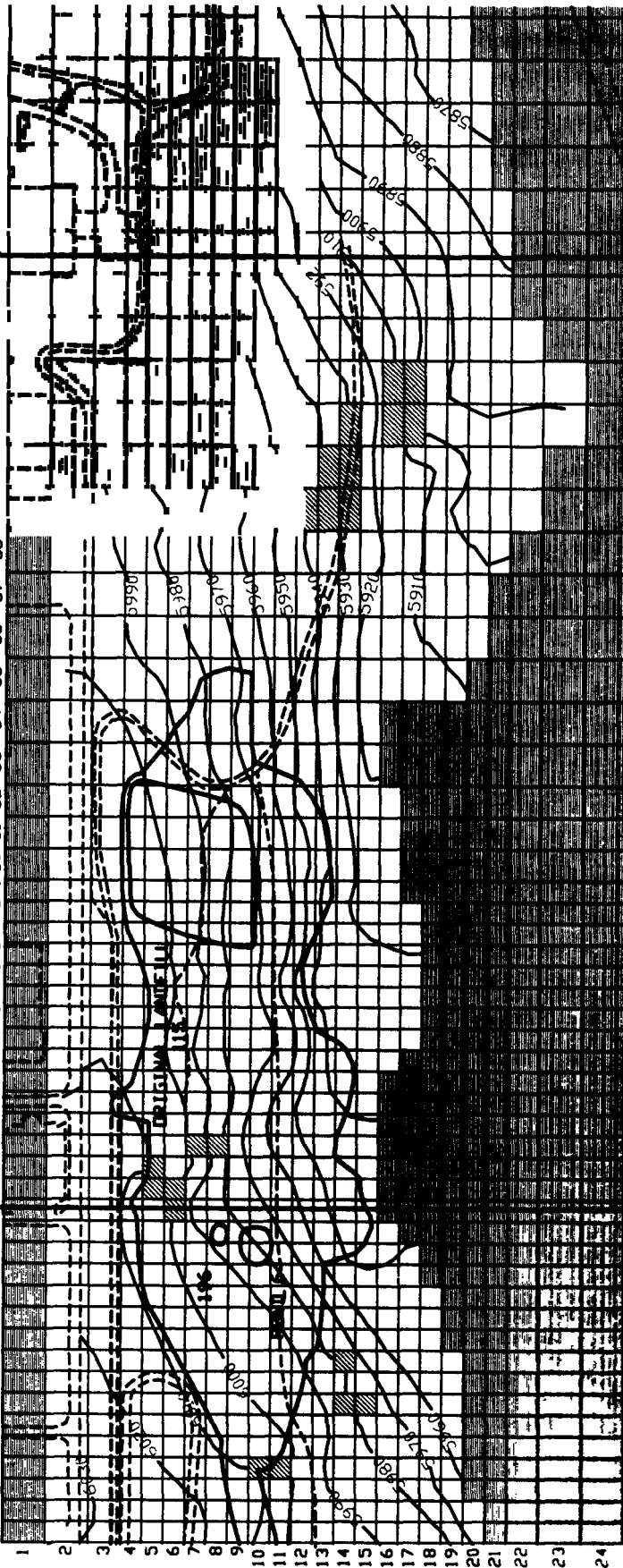
RPI/RI REPORT

FIGURE 5-18A

F Qu
5 15C

F Qu
5 15A

495051 525354 555657 585960 61 626364 656667 686970 71 727374 757677 7879 80 81 82 83 84 85 86 87 88



F Qu
5 15C

F Qu
5 15A

Legend

N Fl w
Dry Area

Water Table Contour
Road
1 divide 1 Hazardous Substance Site

200 feet

Drawn BAR 8/9/95
Checked BAR 8-5-95
Approved _____
Dat _____
Dat _____
FILE QUS 515B.DWG

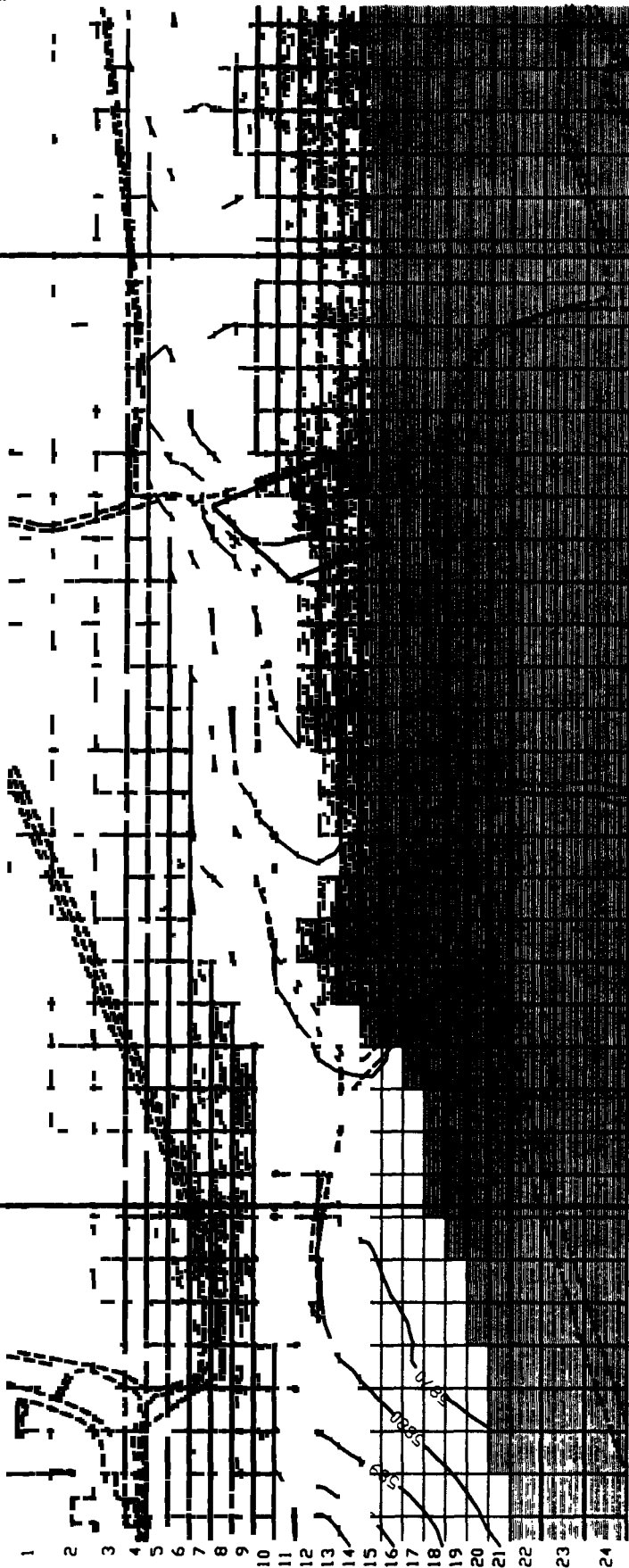
**QUS GROUNDWATER
FLOW MODEL
SIMULATED WATER TABLE**
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
QUS WOMAN CREEK PRIORITY DRAINAGE
RPI/M REPORT
FIGURE 6-15B

Math
Line
Four
S 15D

Math
Line
Four
S 15B

Math
Line
Four
S 15D

Math
Line
Four
S 15B

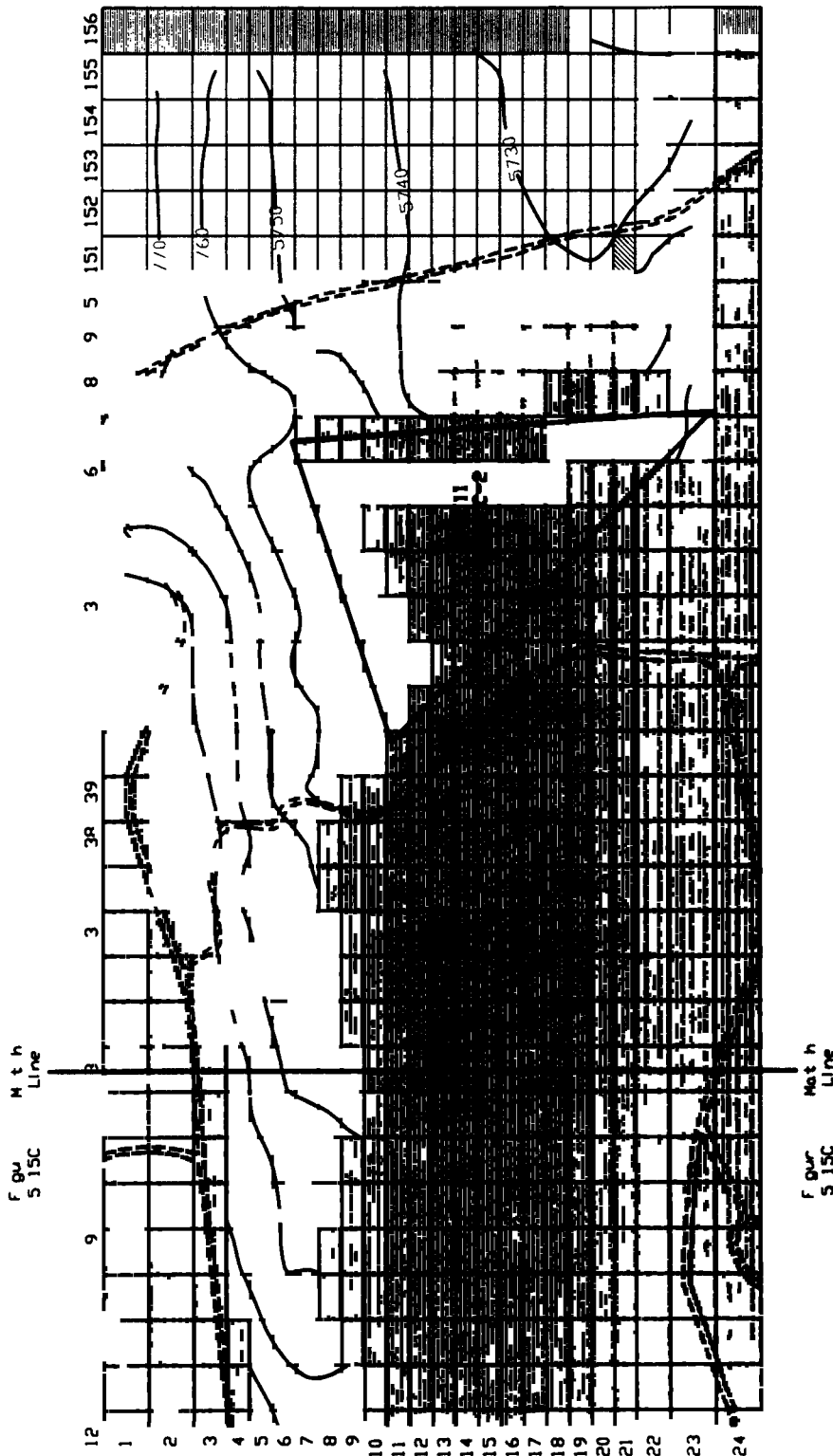


Legend

- Flow
- Dry Area
- Water Table Contour
- Road
- Individual Hazardous Substance Site

Drawn	NAME 8/9/95
Checked	DATE 8/9/95
Approved	DATE
FILE OUS 515C.DWG	

OUS GROUNDWATER FLOW MODEL SIMULATED WATER TABLE
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS WOMAN CREEK PRIORITY DRAINAGE
RPI/RI REPORT
FIGURE 5-15C



Legend

- N Flow
- W ler T ble Conto
- Road
- Individ l Hazardous S betance Site
- Dry Area

Drawn	NAU 8/9/95
Checked	7/27 0/9/95
Approved	

FILE OUS 315D.DWG

OUS GROUNDWATER FLOW MODEL SIMULATED WATER TABLE

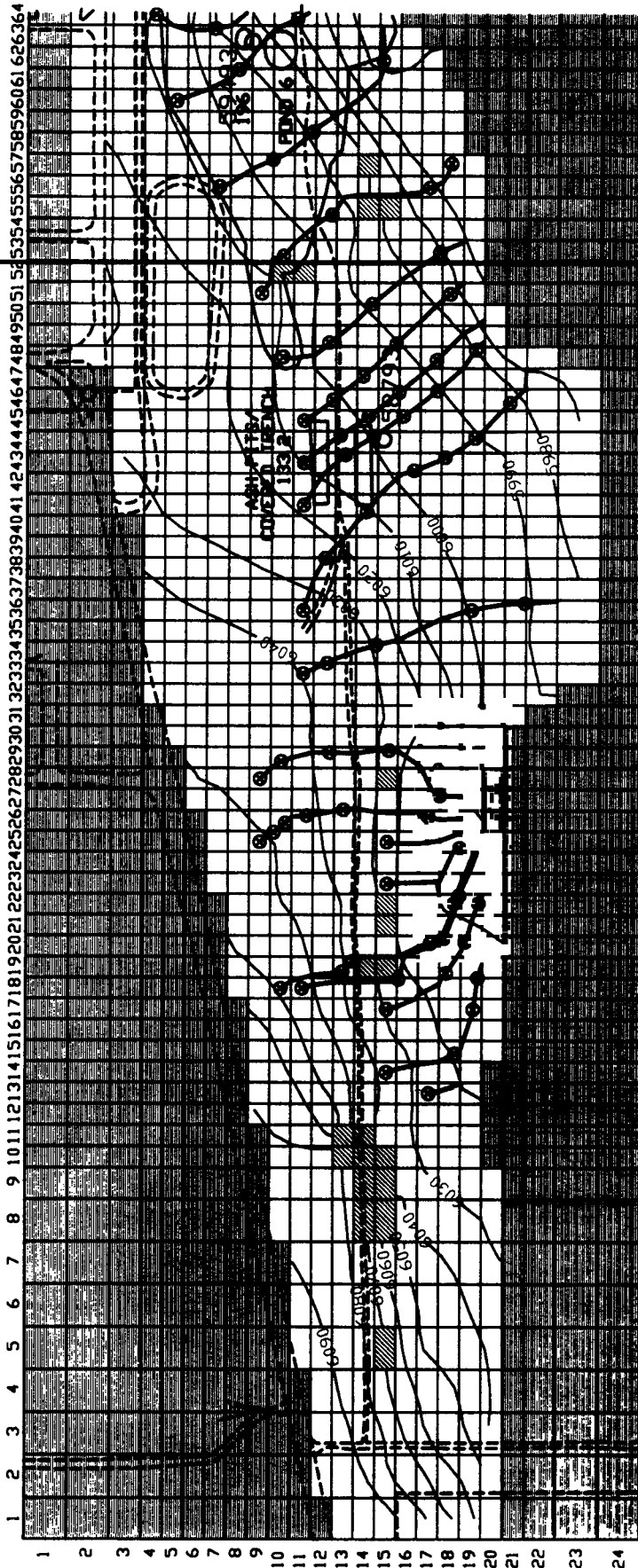
ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS WOMAN CREEK PRIORITY DRAINAGE

RPI/M REPORT

FIGURE 6-16D

M t h
L J
F Our
S 168



M t h
Line
F Our
S 168

Legend

- No Fl
Dry
- Particle Location (0.25 Y Inc et)
- Water Table Contour 10'
- Road
- Individual Horizontal Substanc St
- Monitoring Well

58793

Drawn	NAM 8/9/95
Checked	7/27 8/9/95
Approved	

FILE DUS 516A.DWG

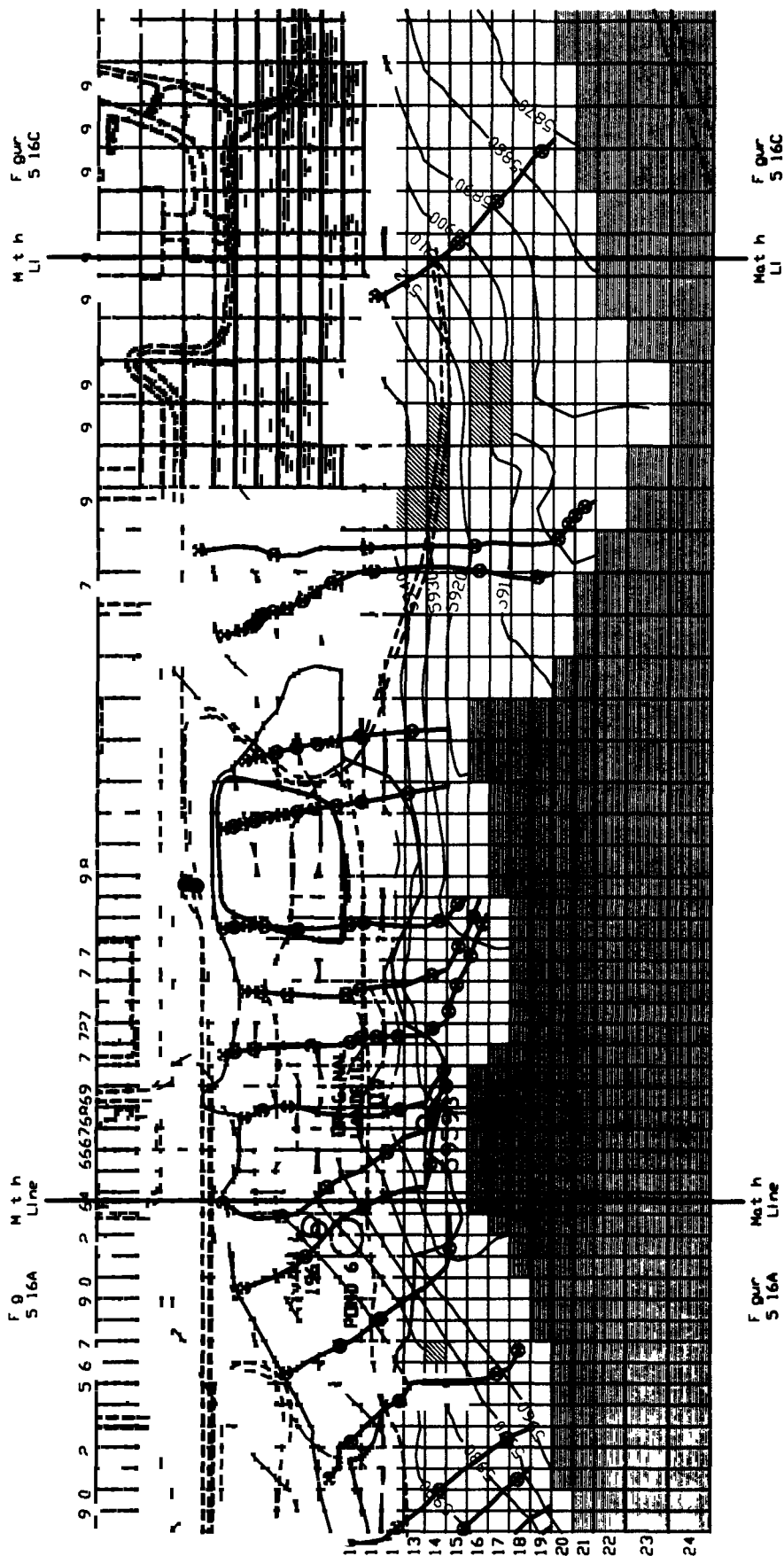
OU5 GROUNDWATER FLOW MODEL GRID PARTICLE TRACKING

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 WOMAN CREEK PRIORITY DRAINAGE

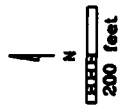
RFI/RI REPORT

FIGURE 5-16A



Legend

- No Flow
- Dry
- Particle Track
- Particle Location (0.25-Year In rem nt)
- Water Table Conto 10
- Road
- Individual Hazard us Subeta ce Site
- Monitoring W ll

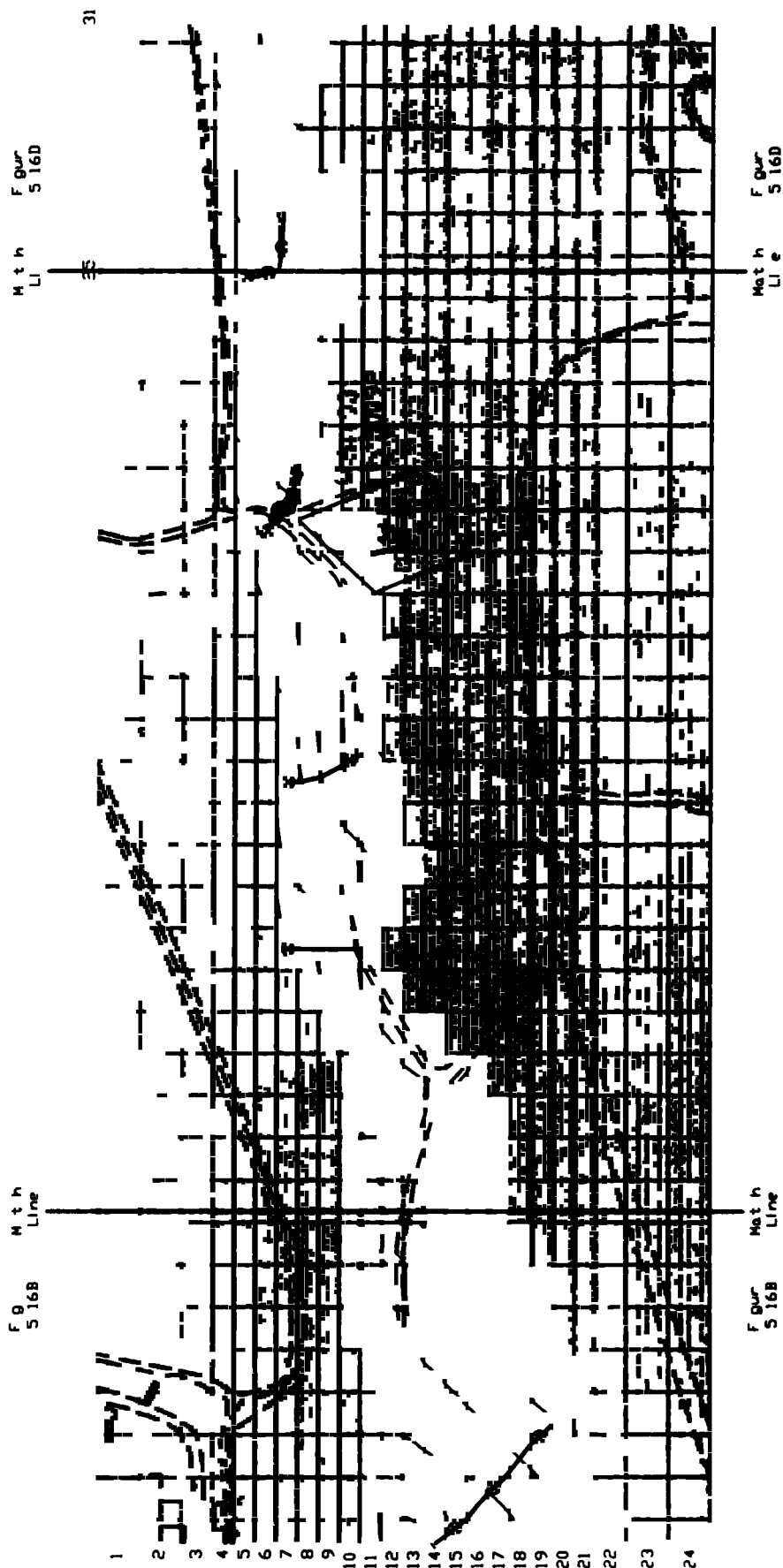


58793

Dr. W.	NAN 8/14/95	
Checked	R. J. 8/14/95	
Approved	Det	Det

FILE OUS 516B.DWG

OUS GROUNDWATER FLOW MODEL GRID PARTICLE TRACKING	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
OUS WOMAN CREEK PRIORITY DRAINAGE	
RPI/RI REPORT	
FIGURE 5-16B	

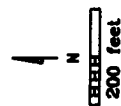


Legend

- N Flow
- Dry
- Particle Location (0.25-Year In rement)
- Water Table Contour 10
- Road
- Individual Hazard us Substance Site

58793

Monitoring Well



Drawn	NAM 8/9/95
Checked	8-9-95
Approved	
	0

FILE OUS S16C DWG

OU5 GROUNDWATER FLOW MODEL GRID PARTICLE TRACKING
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS WOMAN CREEK PRIORITY DRAINAGE
RFI/RI REPORT
FIGURE 5-10C

Figure 516C
North

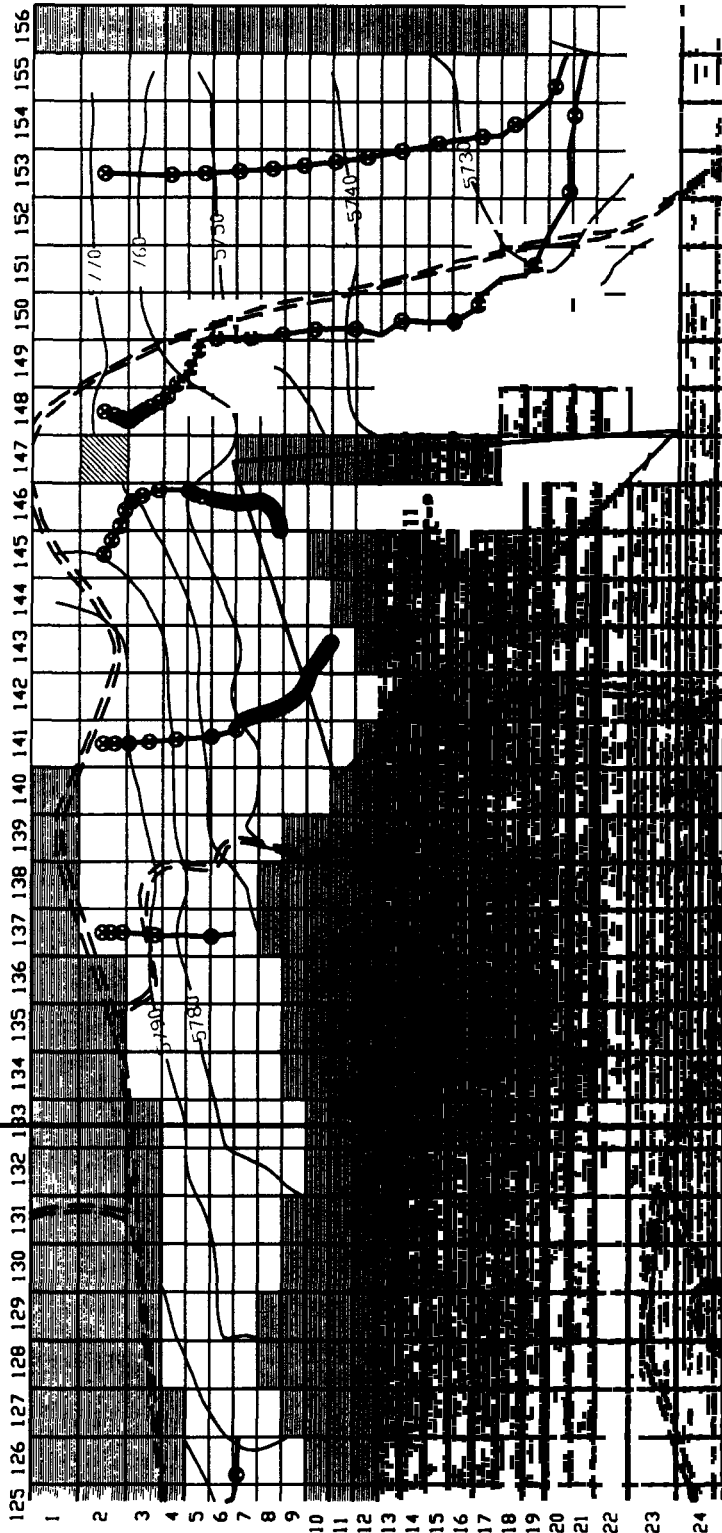
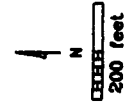


Figure 516C
North

Legend

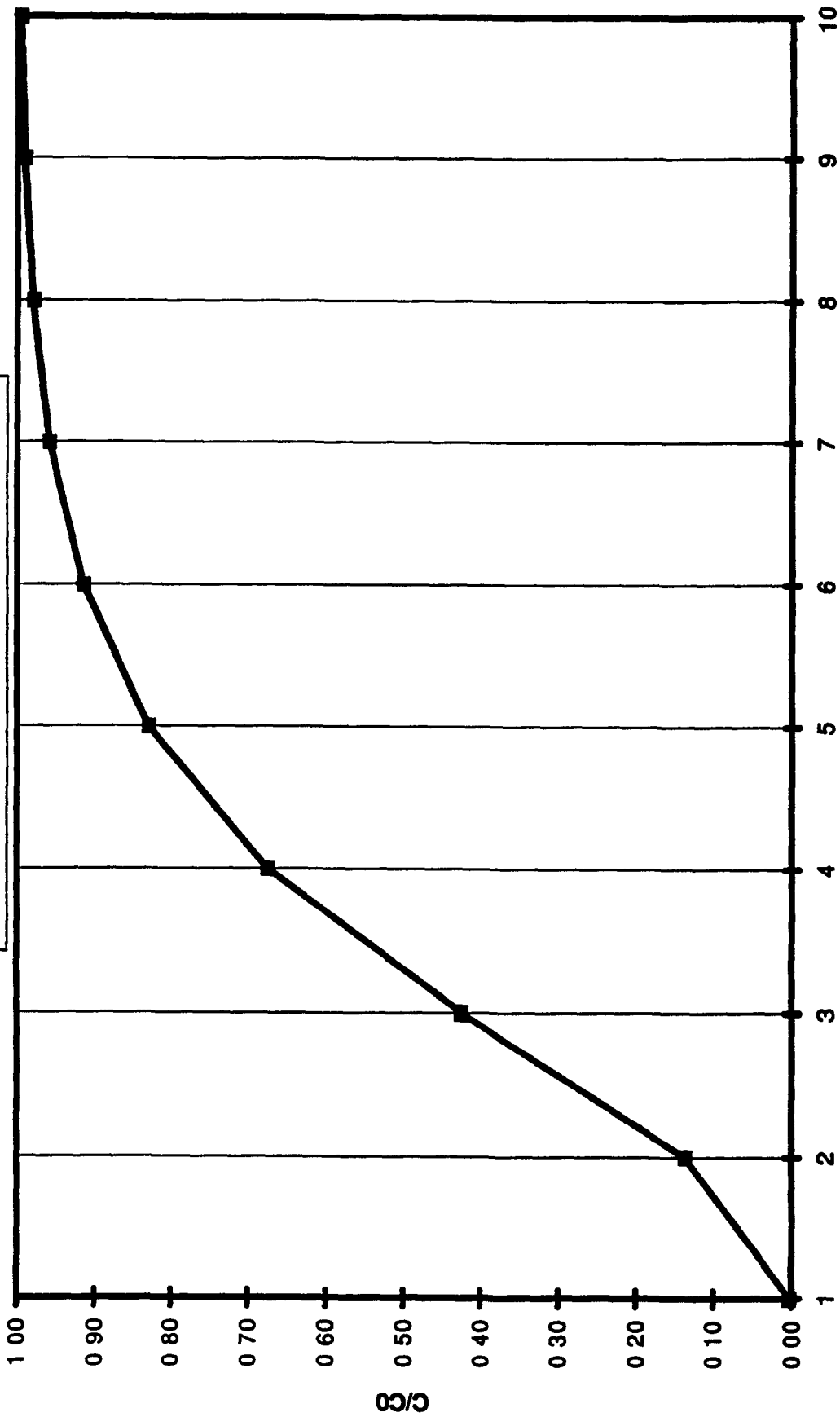
- Particle Track
- Particle Locati (0.25 Yea In rem t)
- Water Table Contour 10
- Road
- Individual Hazardous Substance Site



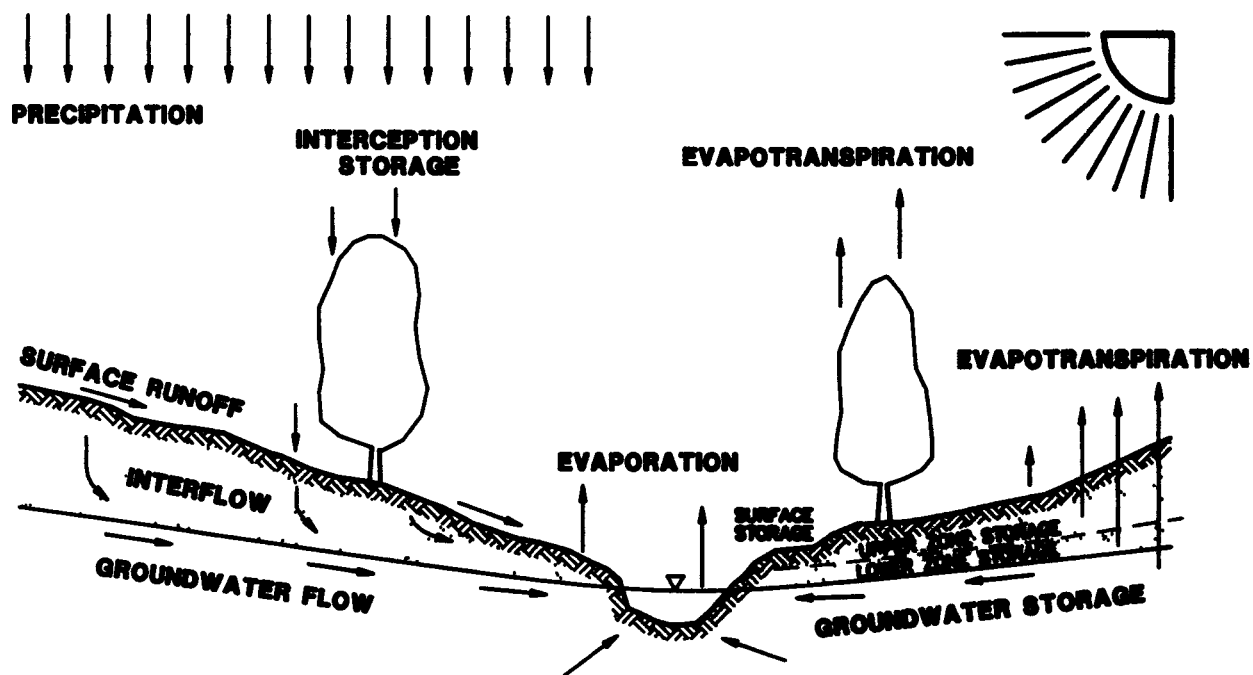
Drawn NAM 8/9/95
 Checked [Signature] Da 9-95
 Approved [Signature] Da 9-95
 FILE OUS 516D.DWG

OUS GROUNDWATER FLOW MODEL GRID PARTICLE TRACKING
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS WOMAN CREEK PRIORITY DRAINAGE
RFI/RI REPORT
FIGURE 5 16D

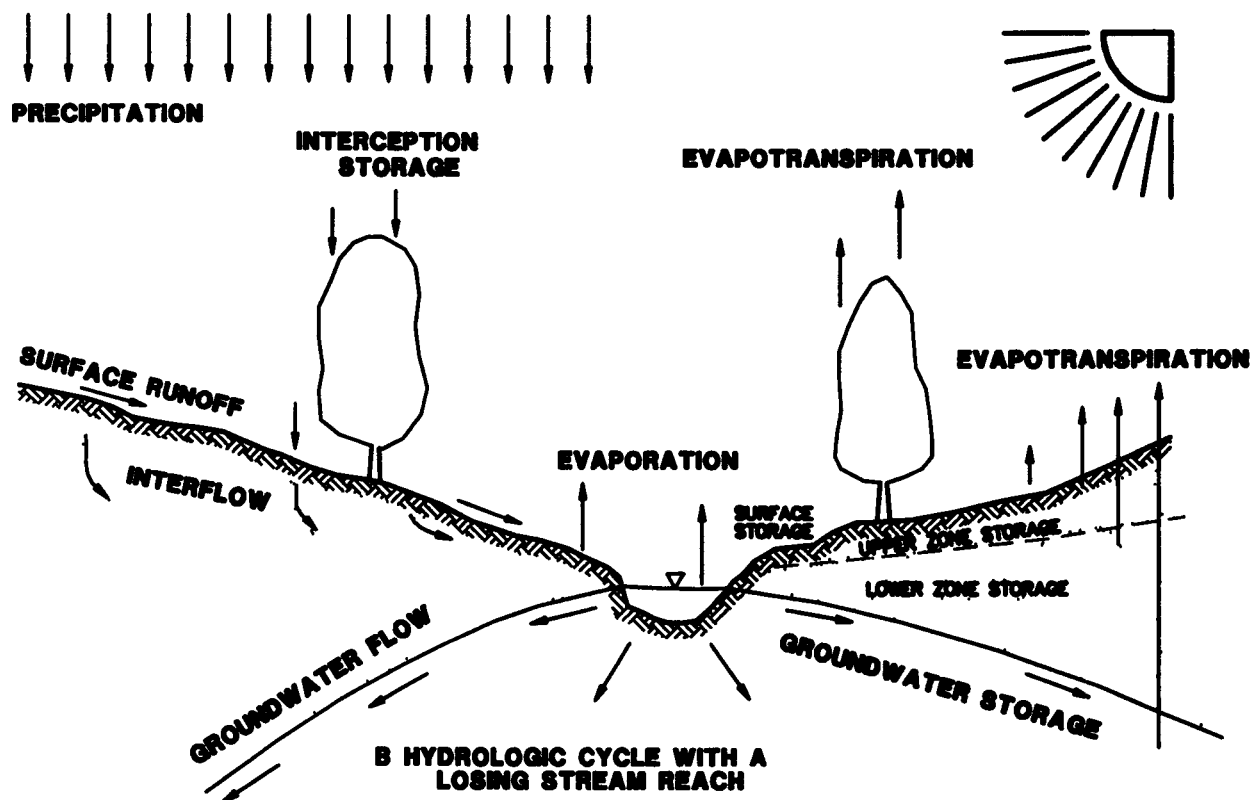
Retardation Factor = 1 Longitudinal Dispersivity = 1 foot



1 D ANALYTICAL SIMULATION OF CONTAMINANT TRANSPORT THROUGH THE VADOSE ZONE NORTH ASH PIT IHSS 133 2	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
OUS	WOMAN CREEK PRIORITY DRAINAGE
RF/R1 REPORT	
FIGURE 5-17	
DRAWN <i>204</i>	DATE <i>1/23/95</i>
CHECKED <i>789</i>	DATE <i>3/22/95</i>
APPROVED	DATE
ES:17.DRW	



A. HYDROLOGIC CYCLE WITH A GAINING STREAM REACH



B HYDROLOGIC CYCLE WITH A LOSING STREAM REACH

**HYDROLOGIC CYCLE WITH
GAINING AND LOSING
STREAM REACHES**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

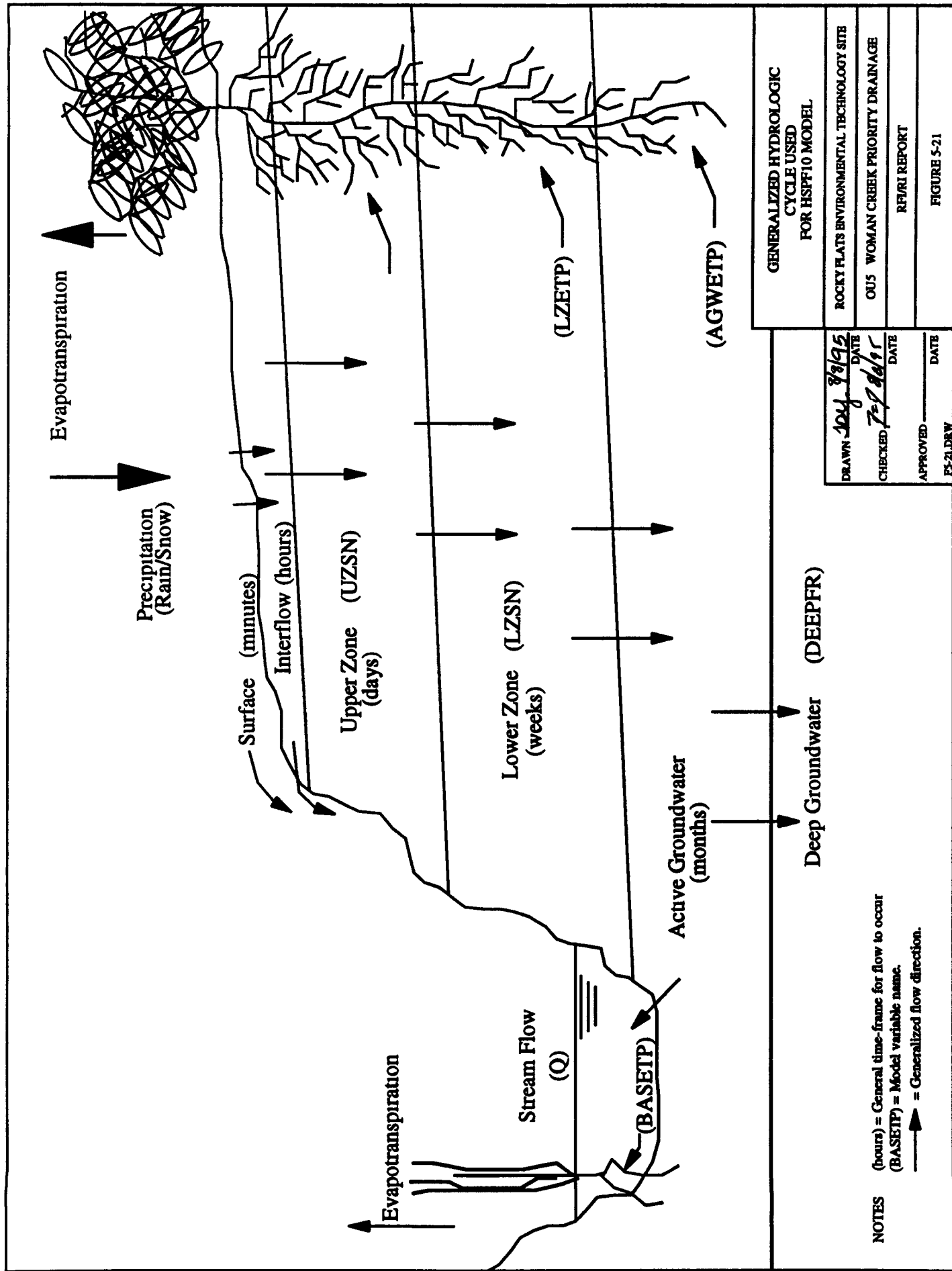
FIGURE 5-19

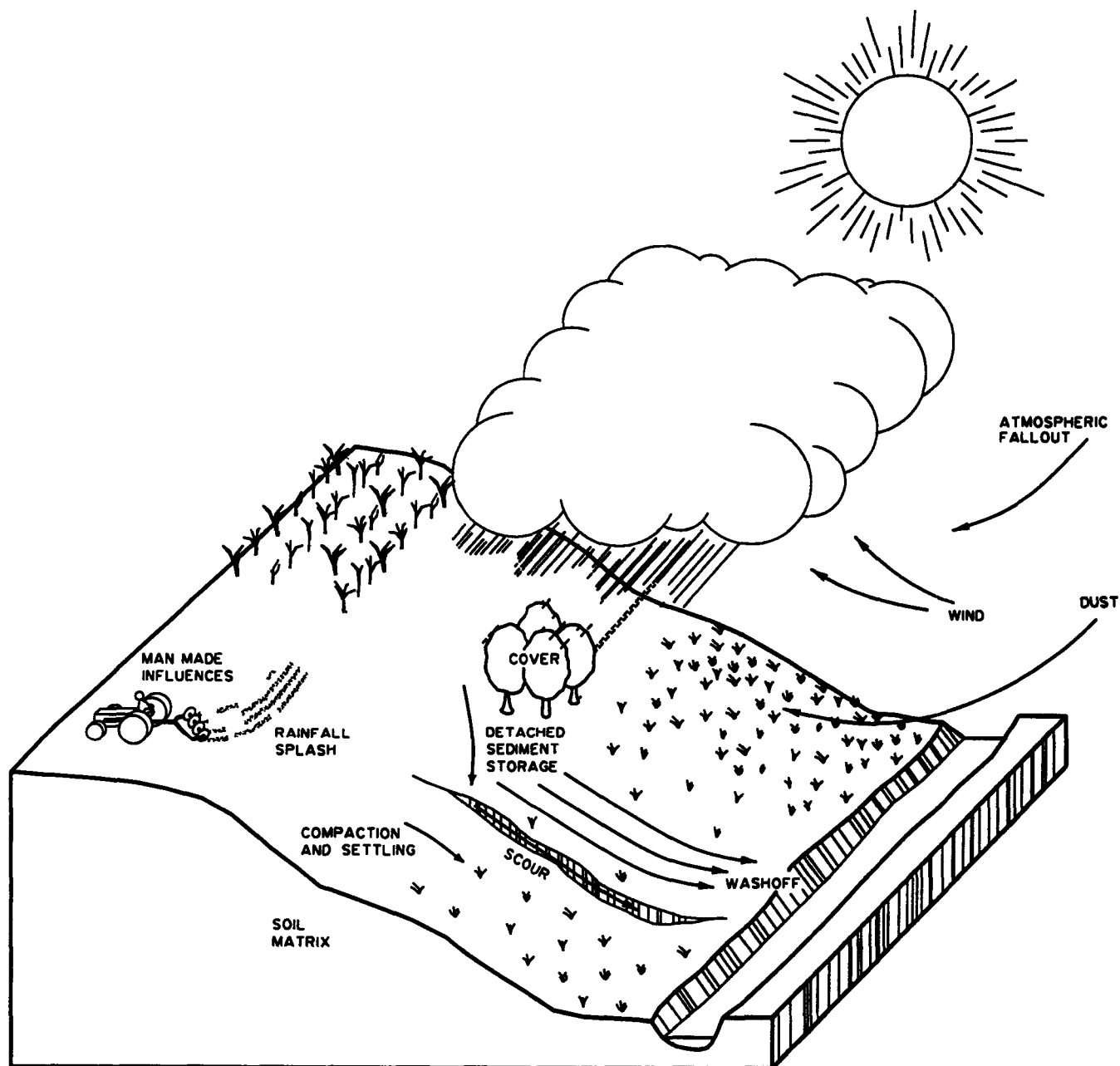
Draw	NAM	7/31/95
Checked	7-9	7/31/95
App oved		

FILE OU5-5-19 DWG

Source Modified From Bicknell
and Others (1993)

Lower Zone
Storage





Source Bicknell and Others (1993)

Drawn NAM 8/9/95 Date
 Checked 7-9/95 Date
 App oved _____ Date

FILE OU5 5 21DWG

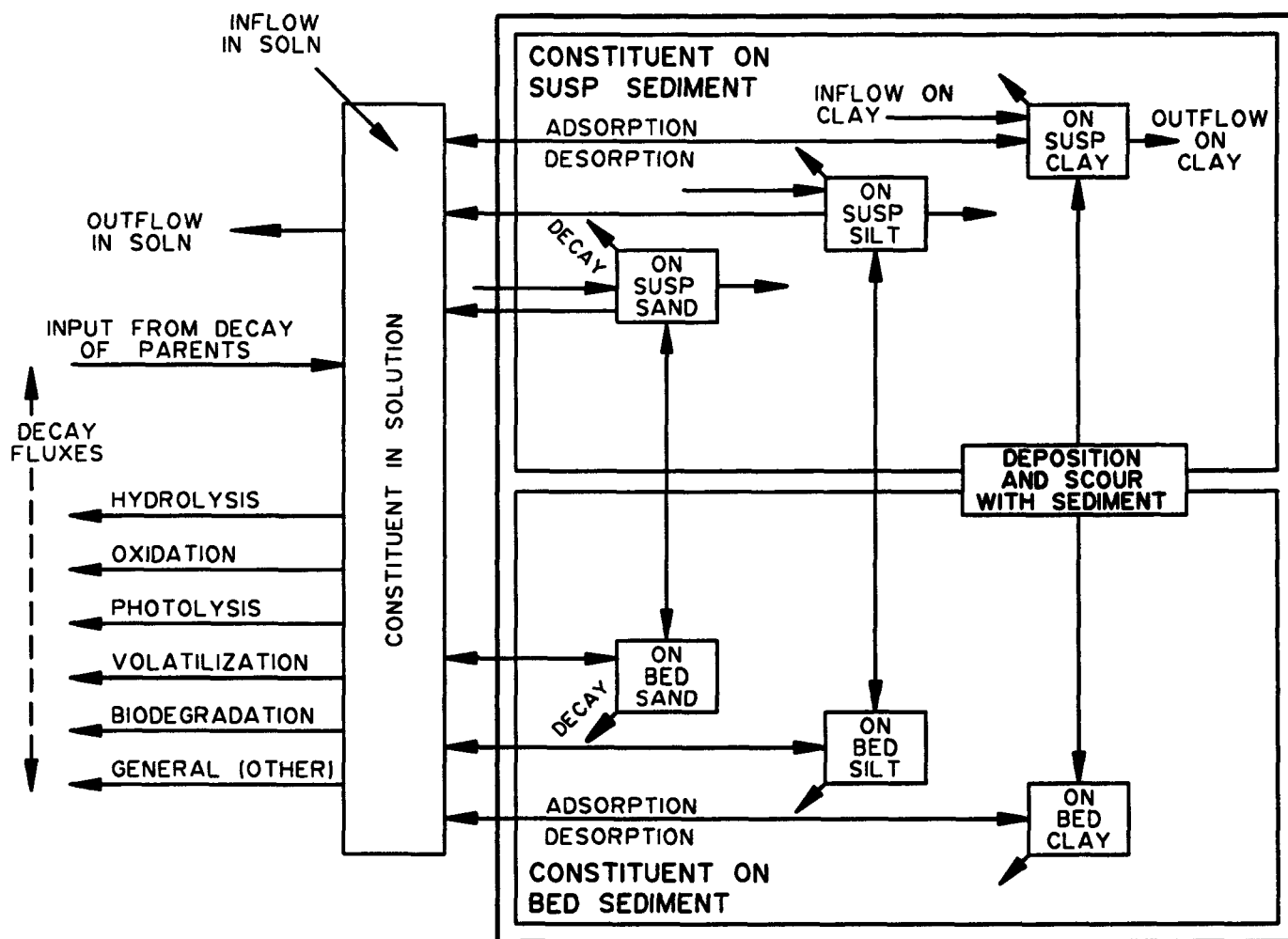
SOIL-EROSION PROCESSES USED IN HSPF10

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-22



POLLUTANT-FATE MECHANISMS MODELED IN HSPF10

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

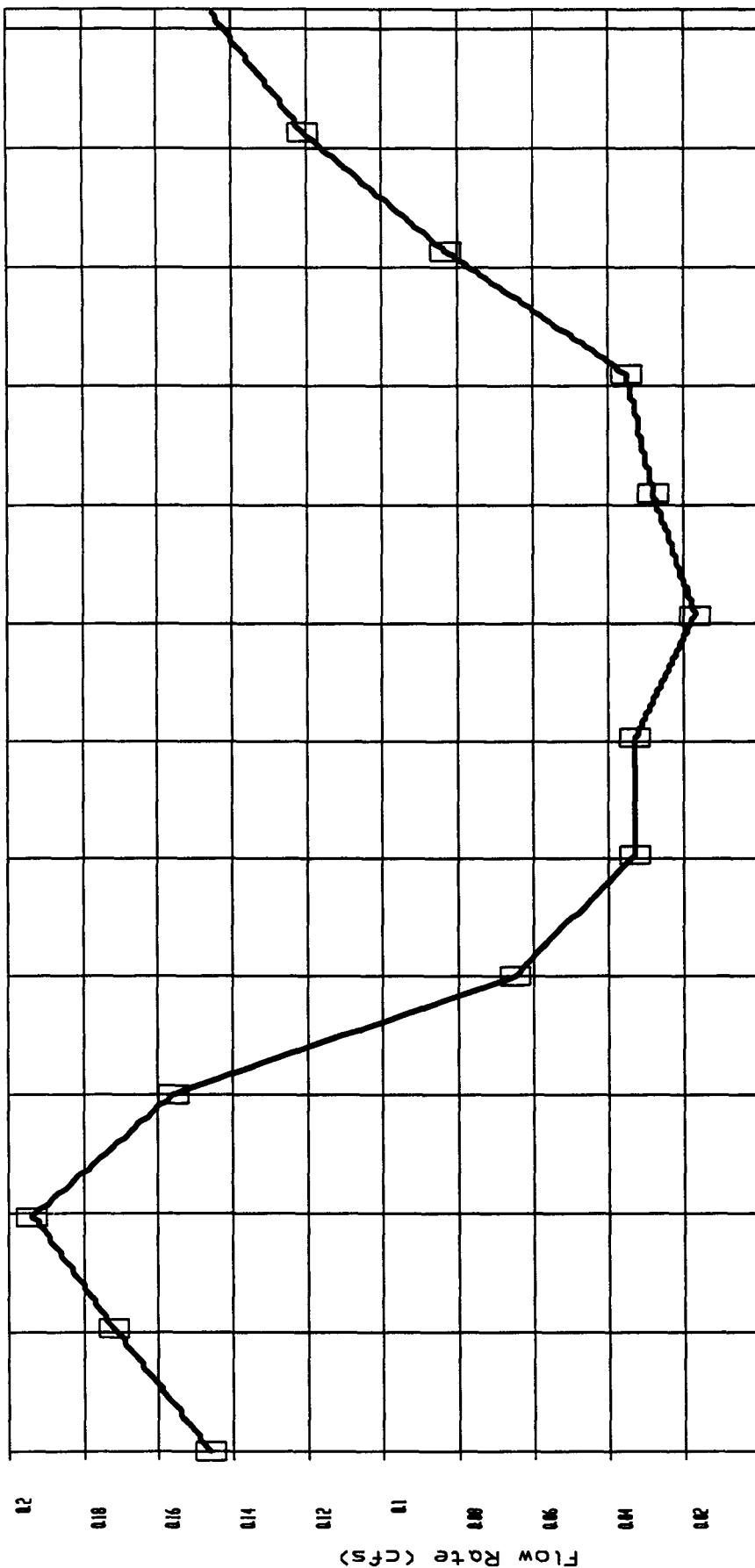
RFI/RI REPORT

FIGURE 5-23

Draw NAM 7/31/95
Date
Checked 7/31/95
Date
App oved _____
Date

Source Bicknell and Others (1993)

FILE OU5 5 23 DWG



Date

ANTELOPE SPRING CREEK GROUNDWATER INFLOW

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-25

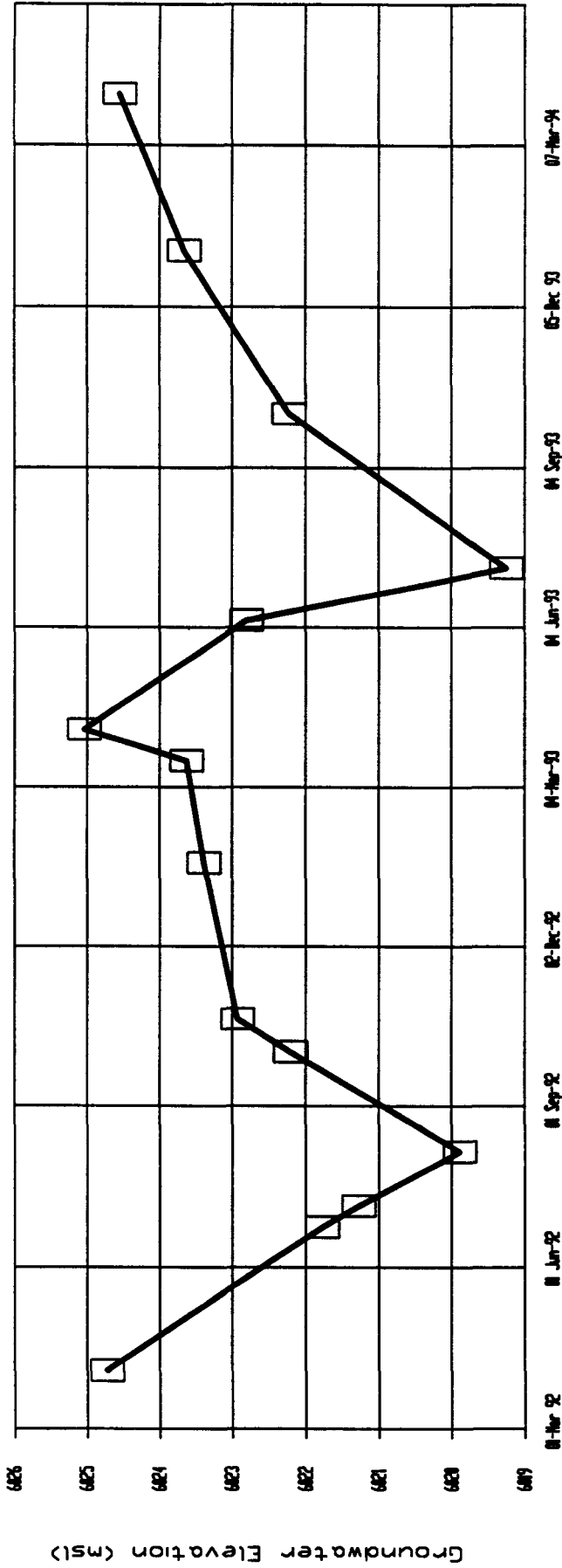
Drawn NAM 7/31/95

Checked 7-9 7/31/95

Approved

Date

FILE OU5 5 25 DWG



Date

HYDROGRAPH of WELL 1989 near Antelope Spring Creek

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-26A

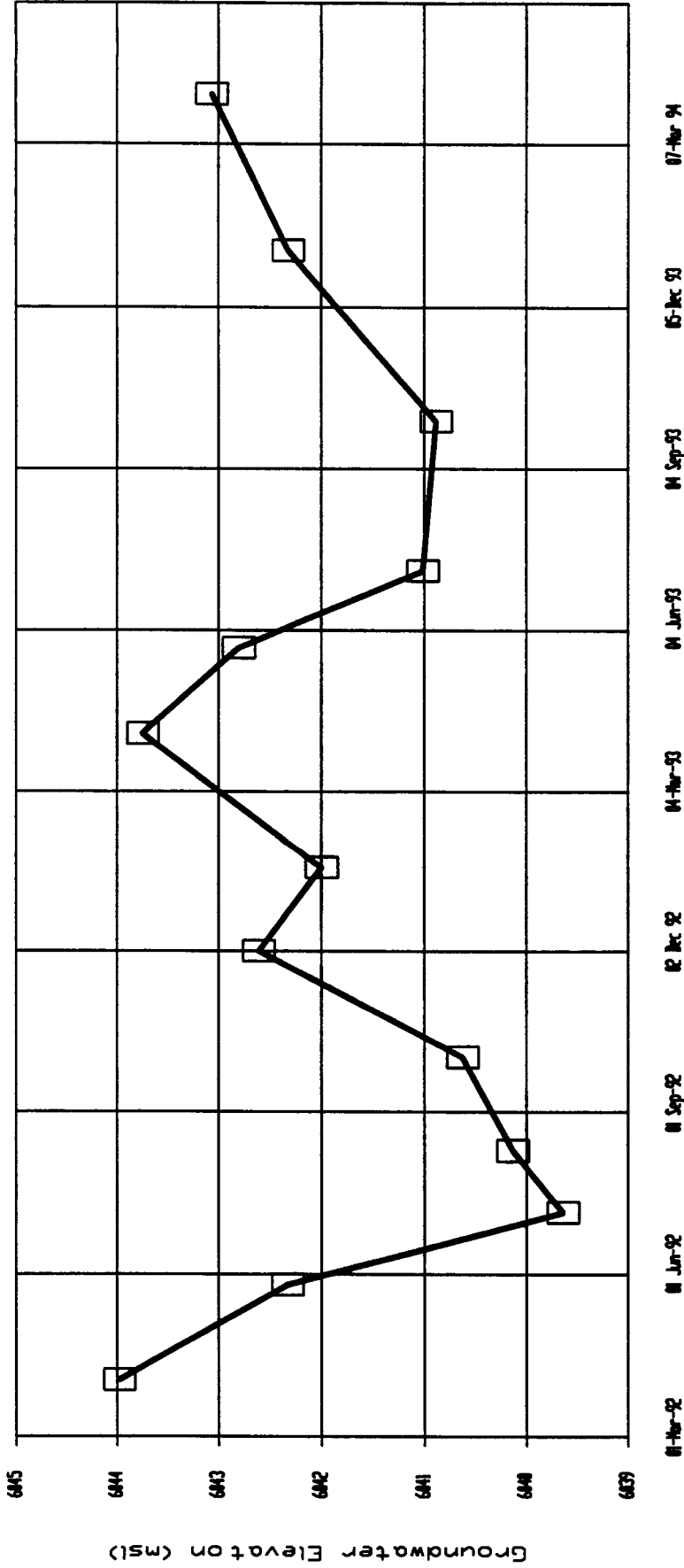
Drawn NAM 8/1/95

Checked REP 8/2/95

Approved REP 8/2/95

Date

FILE OU5 526a DVG



Date

HYDROGRAPH of WELL 2689 NEAR WOMAN CREEK

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

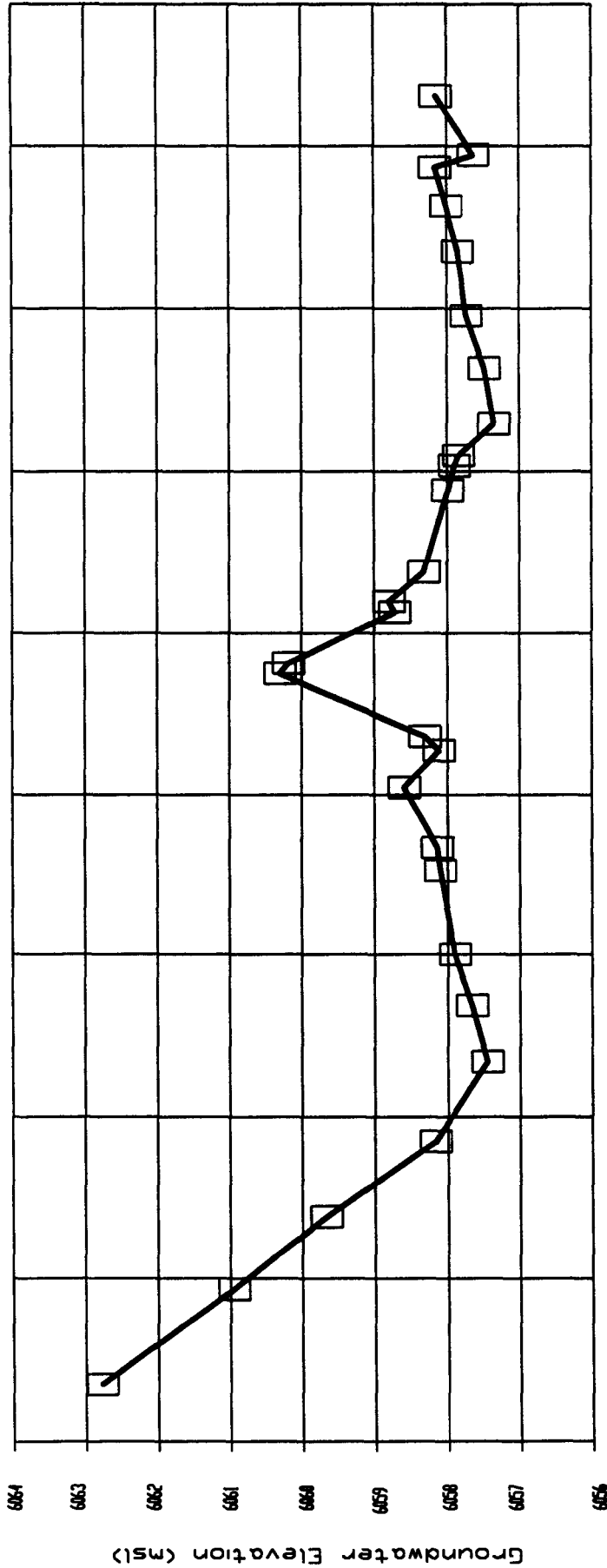
OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-26B

Drawn	NAM 8/9/95	Date	
Checked	JEJ 8/6/95	Date	
Approved		Date	

FILE OU5 526.DWG



01-Mar-92 01-Jun-92 01-Sep-92 01-Dec-92 01-Mar-93 01-Jun-93 01-Sep-93 01-Dec-93 01-Mar-94

Date

HYDROGRAPH of WELL 5386 NEAR SOUTH WOMAN CREEK

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-26C

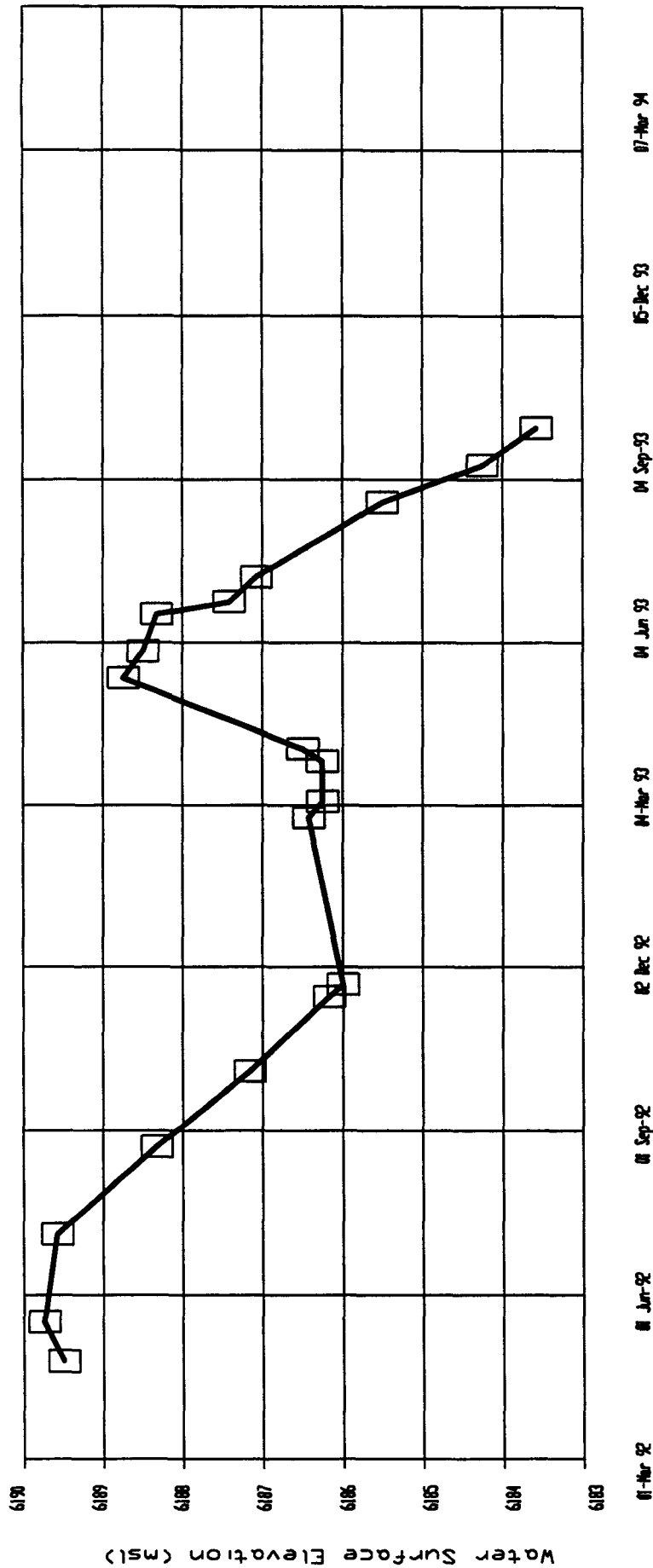
Drawn NAM 8/9/95

Checked 1/31/95

App oved 1/31/95

Date

FILE OU5 526C DVG



Date

HYDROGRAPH of ROCKY FLATS LAKE WATER SURFACE

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-27

Drawn NTM 7/31/95

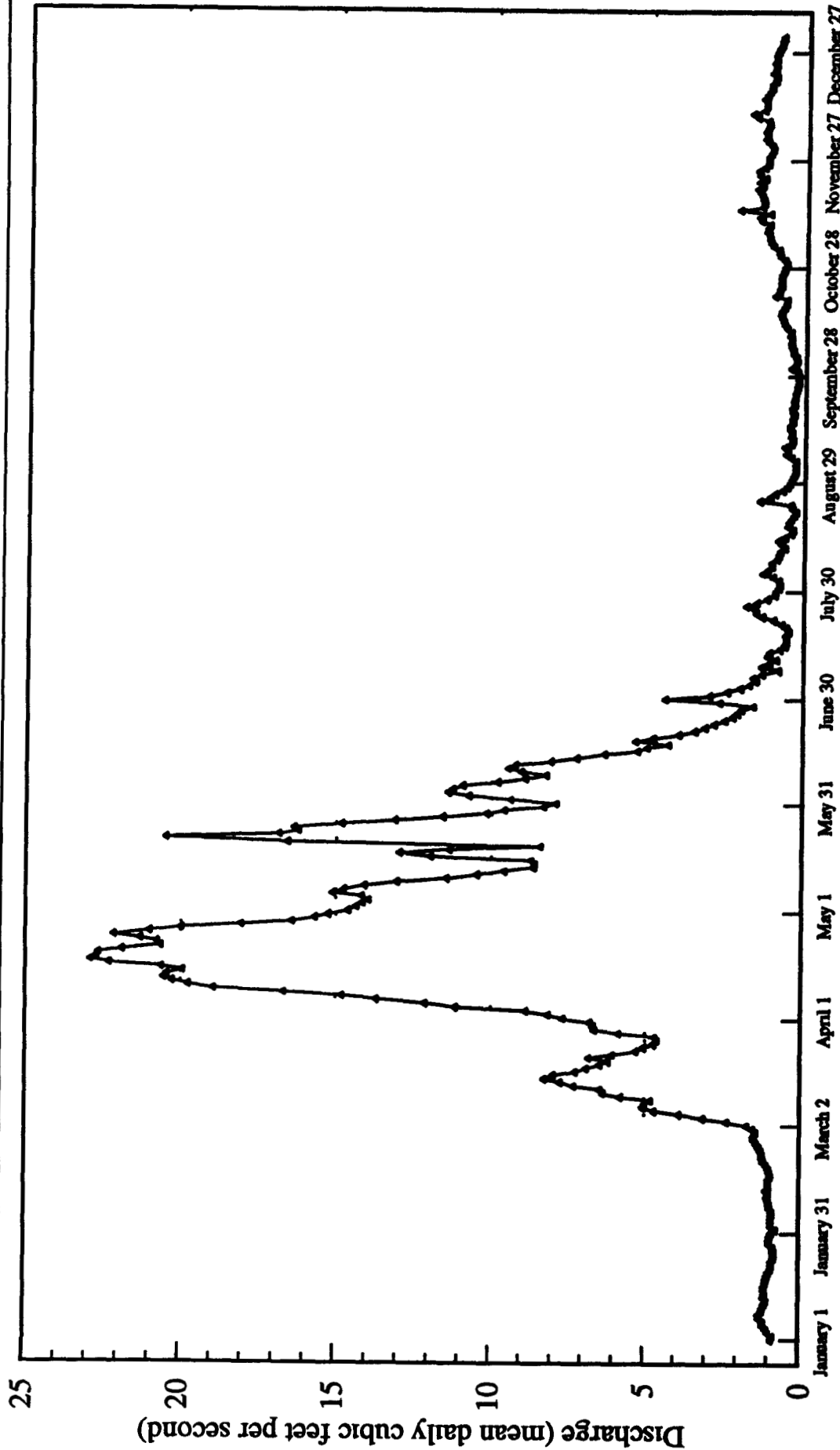
Checked 7/27/95

Approved 7/27/95

Date

Date

FILE OUS 527 DWG



MEAN DAILY DISCHARGE IN COAL CREEK AT PLAINVIEW

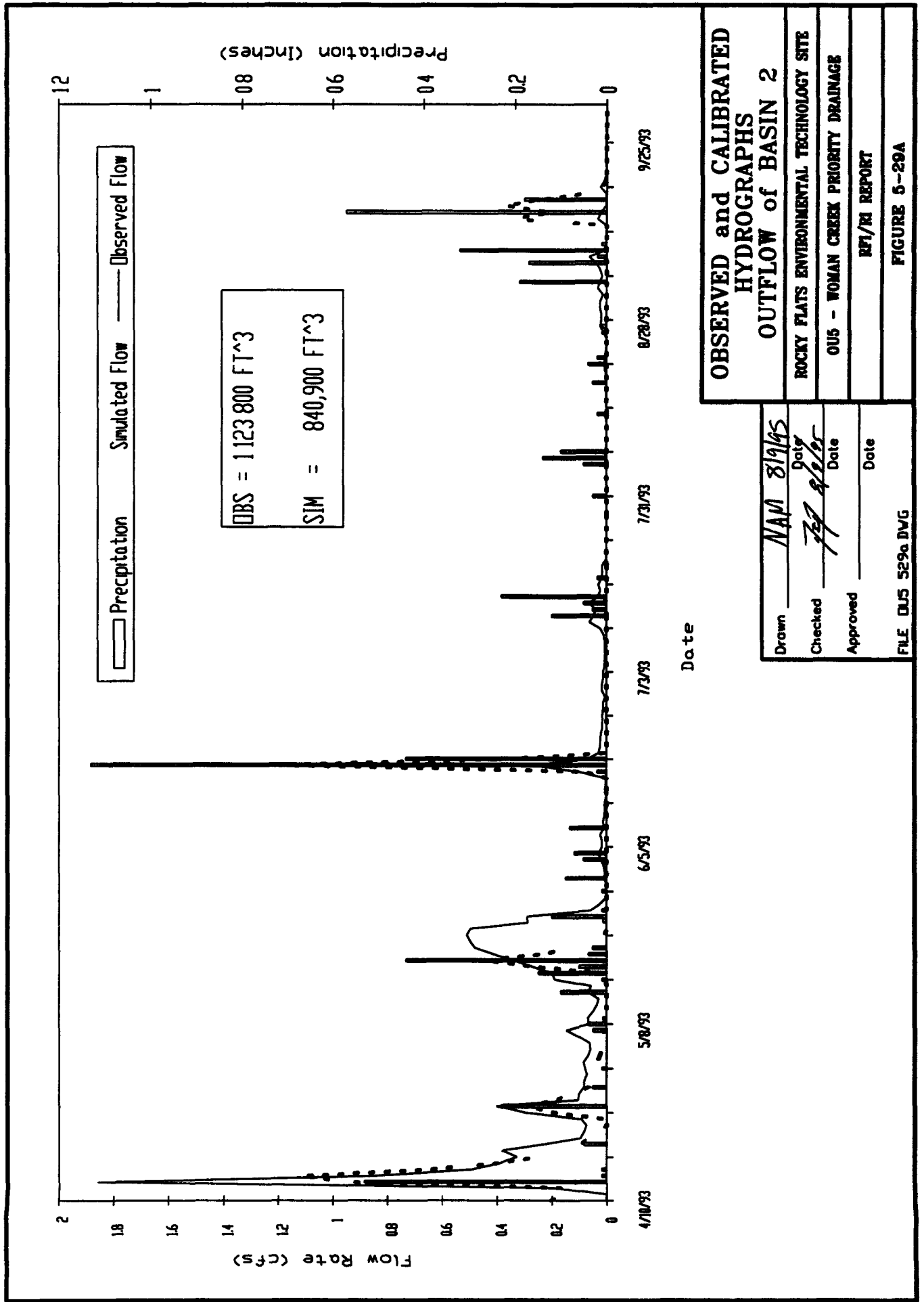
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	DATE
OUS WOMAN CREEK PRIORITY DRAINAGE	DATE
RF/RJ REPORT	DATE
FIGURE 5-28	DATE

DRAWN *Ray Jones*

CHECKED *Ray Jones*

APPROVED

ES-28.DRW

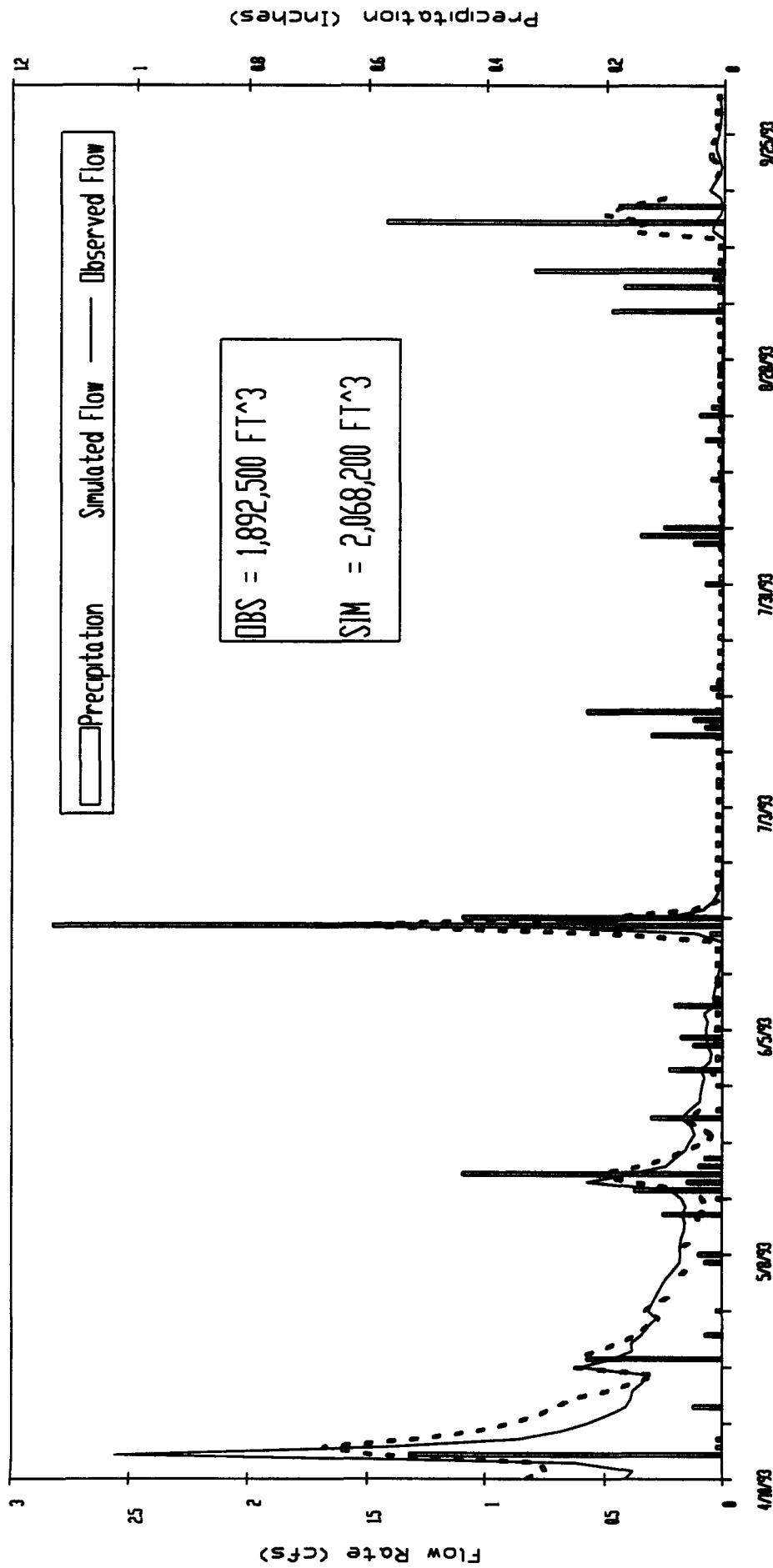


**OBSERVED and CALIBRATED
HYDROGRAPHS
OUTFLOW of BASIN 2**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS - WOMAN CREEK PRIORITY DRAINAGE
RFI/RI REPORT
FIGURE 5-29A

Drawn	NAM 8/19/95
Checked	7/27/95
Approved	
Date	

FILE OUS 529a.DWG



Date

Drawn NAM 8/19/95 Date
 Checked FE 8/26/95 Date
 Approved _____ Date

OBSERVED and CALIBRATED HYDROGRAPHS OUTFLOW of BASIN 4

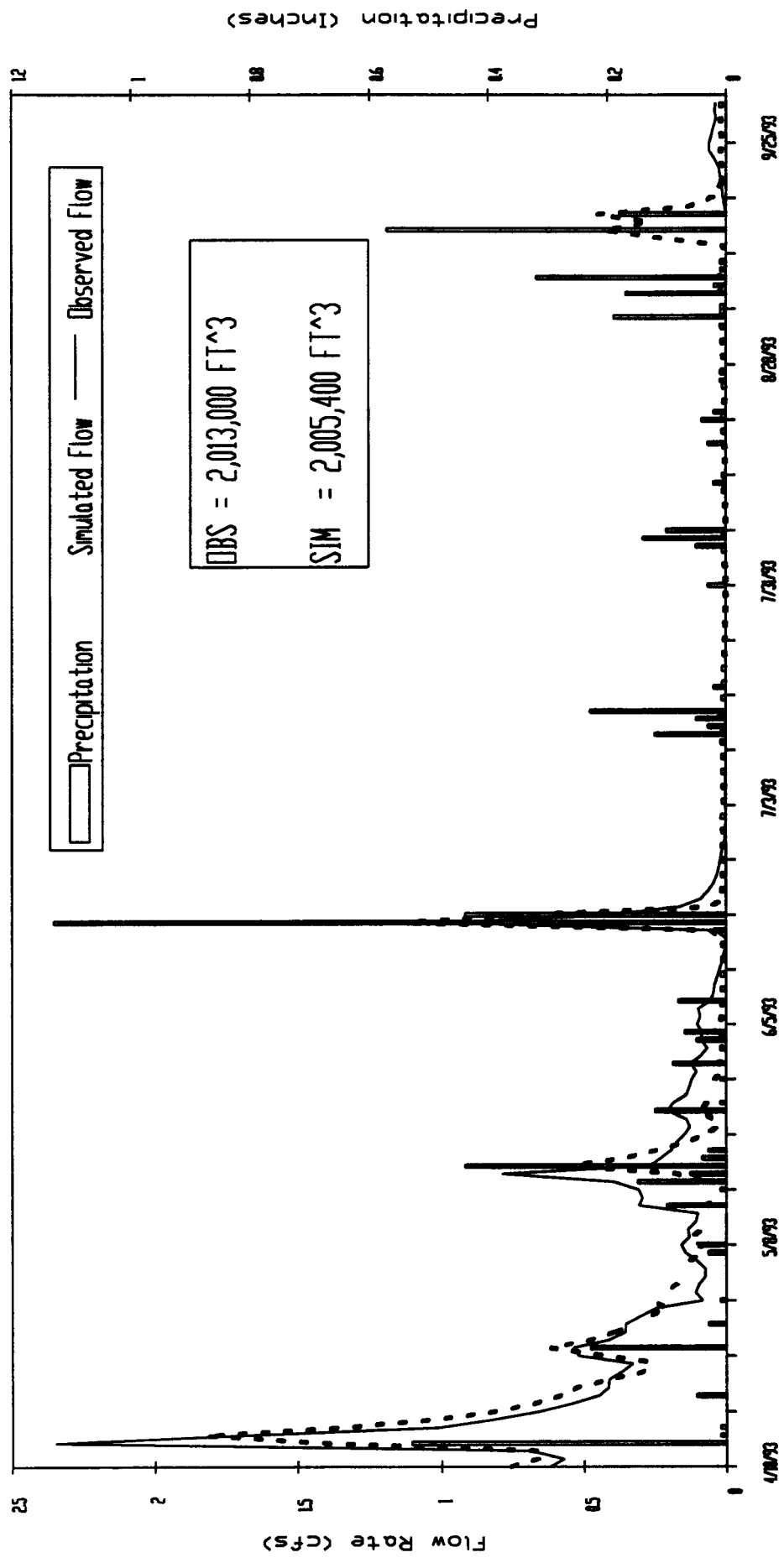
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-29B

FILE OUS 529B DVG



Date

**OBSERVED and CALIBRATED
HYDROGRAPHS
OUTFLOW of BASIN 5**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

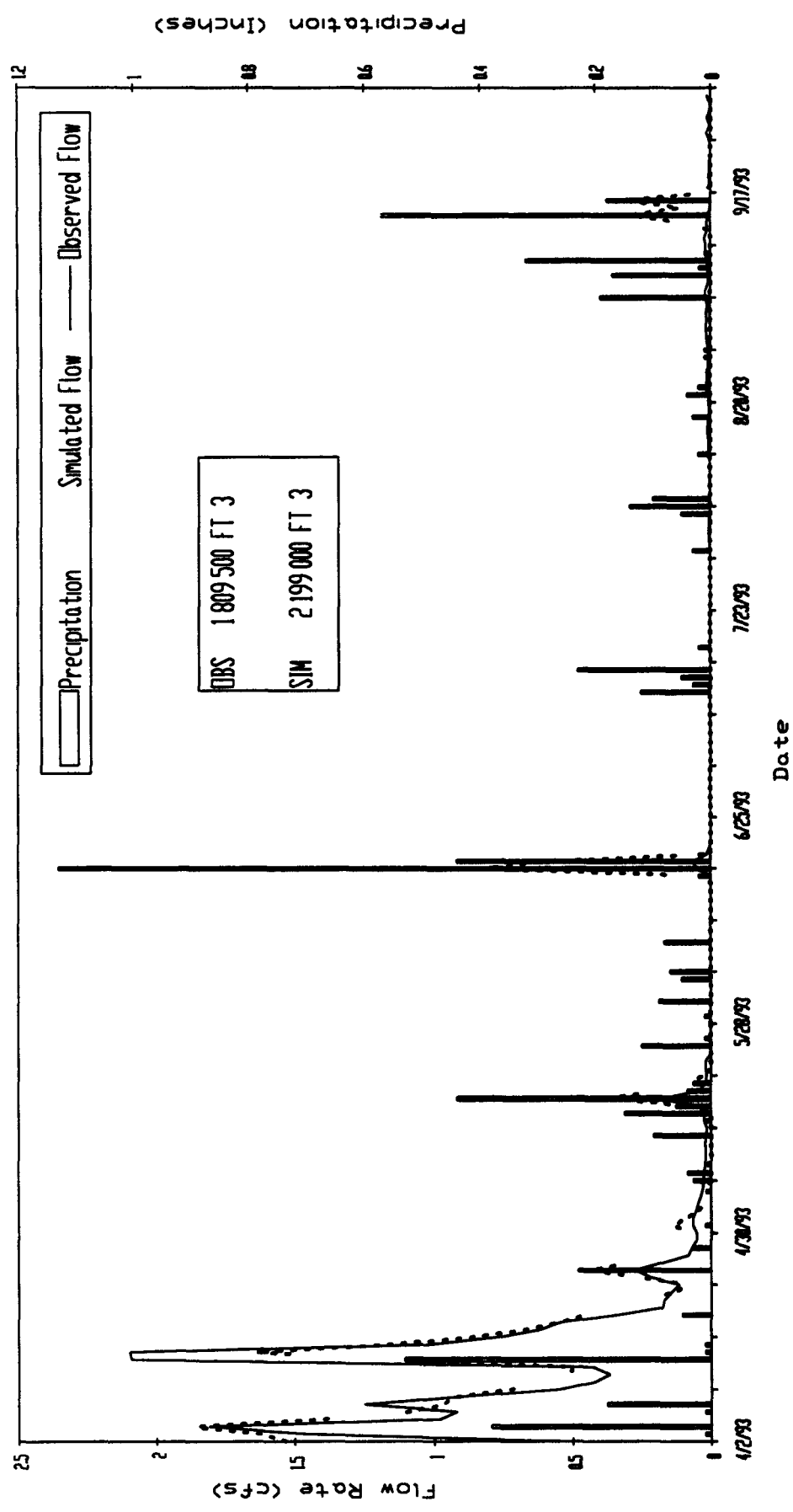
OUS - WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-29C

Drawn	NAM/8/93	Date	
Checked	<i>[Signature]</i>	Date	
Approved		Date	

FILE OUS 529C.DWG



**OBSERVED and CALIBRATED
HYDROGRAPHS
OUTFLOW of BASIN 6**

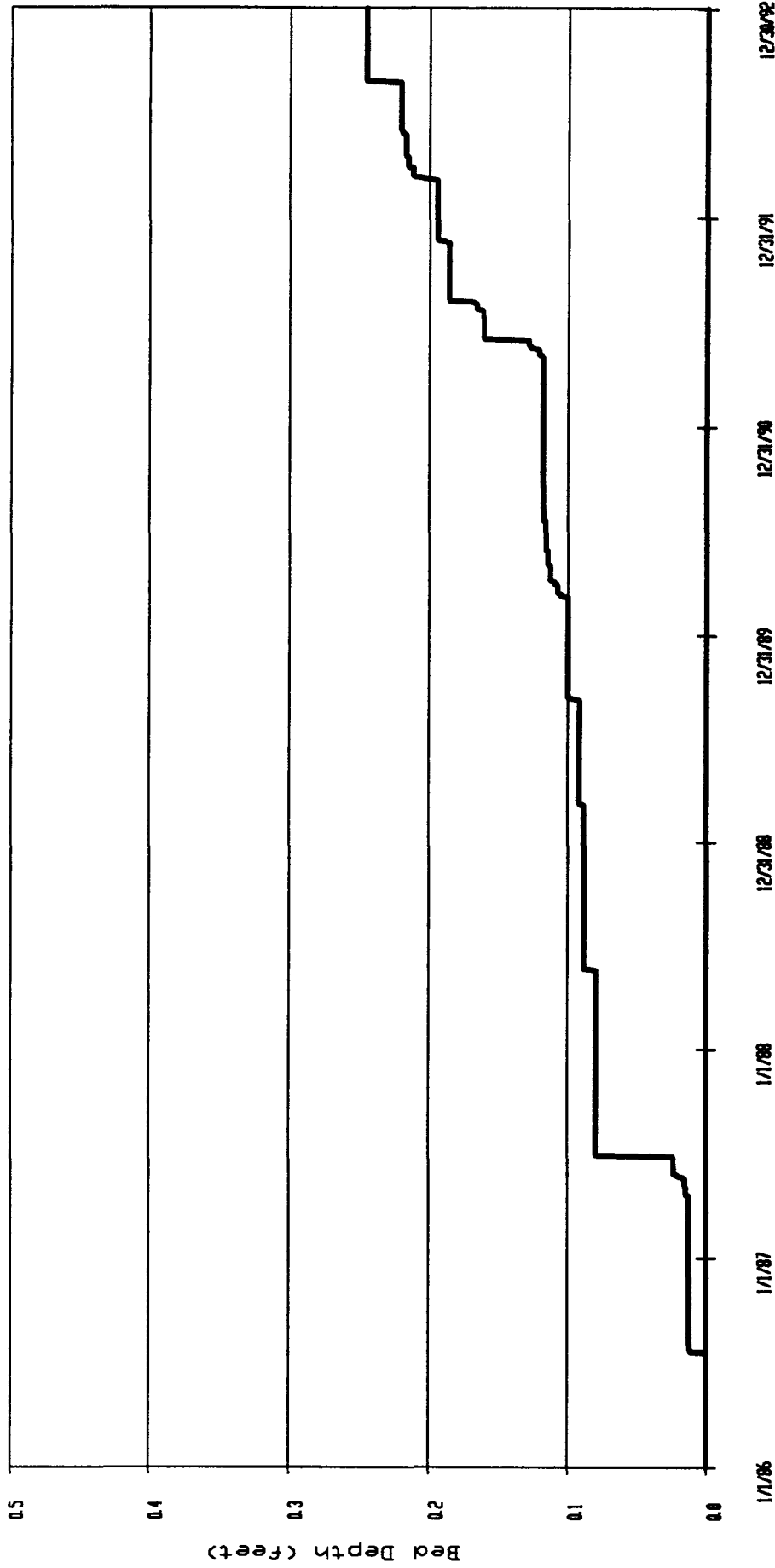
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-29D

Drawn	NAH/SLP	Date	8/2/93
Checked	727	Date	8/2/93
Approved		Date	
FILE OUS-S29D.DWG			

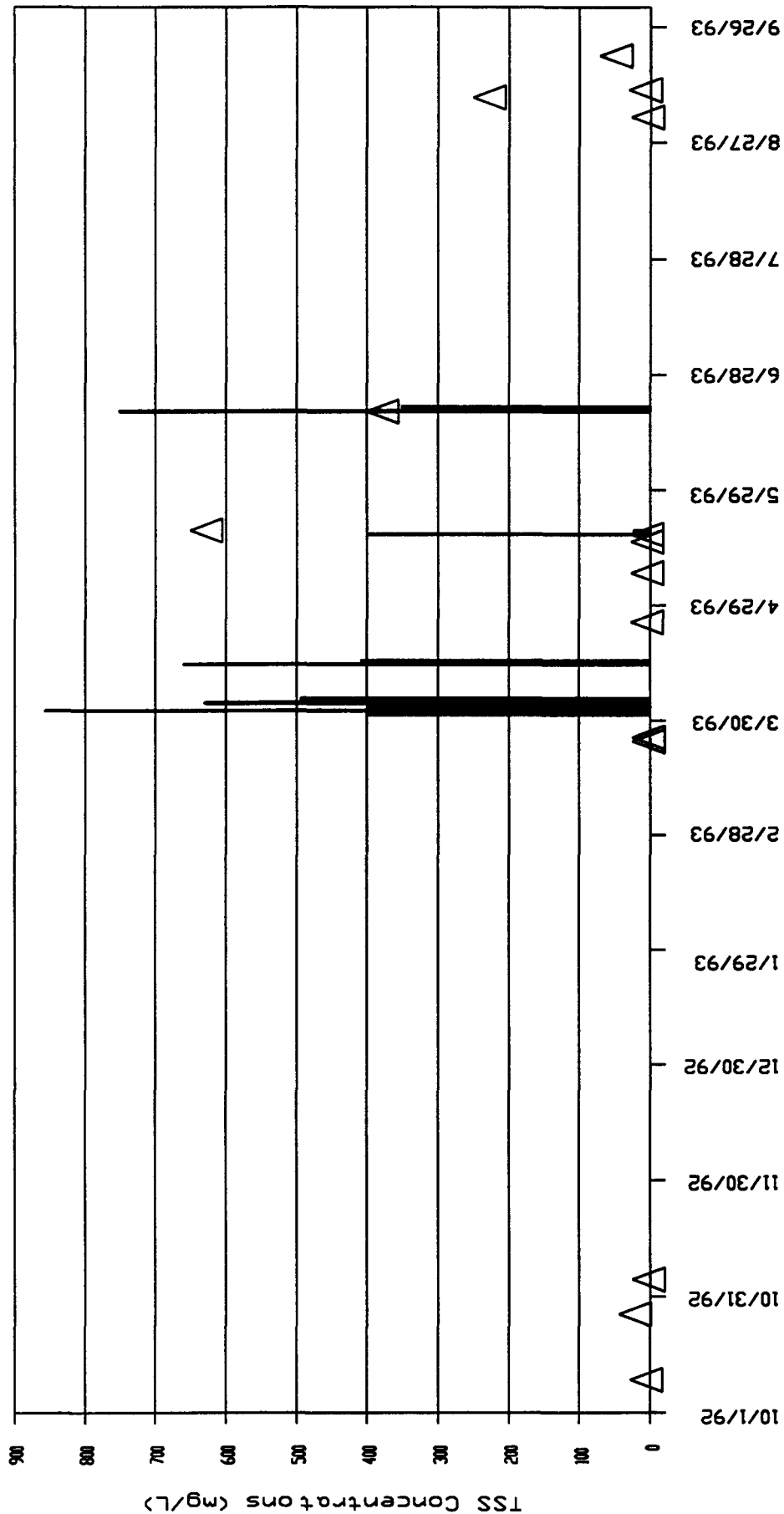


— Sediment Depth

7-YEAR CALIBRATION OF POND C-1 BOTTOM-SEDIMENT DEPOSITION

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OJ5 - WOMAN CREEK PRIORITY DRAINAGE
RPT/RI REPORT
FIGURE 5-30

Drawn	NAM 7/3/93	Date
Checked	REP 7/31/95	Date
Approved		Date
FILE OJ5 5 30 DVG		



Date

REACH 2

OBSERVED and CALIBRATED TOTAL SUSPENDED SEDIMENT

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-31A

Drawn MM 8/93

Checked 7/28/93

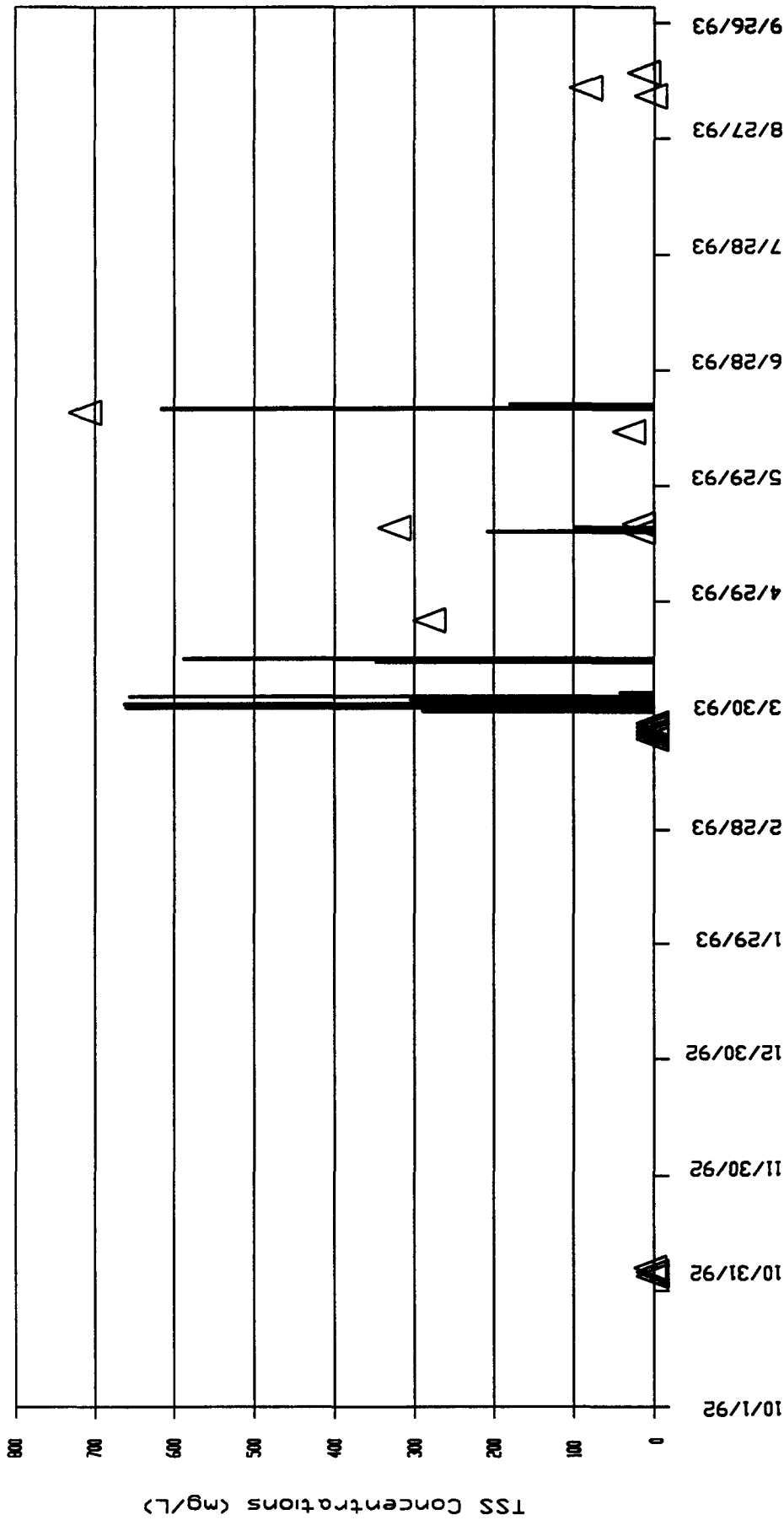
Approved 7/28/93

Date

FILE OUS-531A.DWG

□ CALIBRATED TSS

△ OBSERVED TSS



REACH 3 OBSERVED and CALIBRATED TOTAL SUSPENDED SEDIMENT

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS - WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-31B

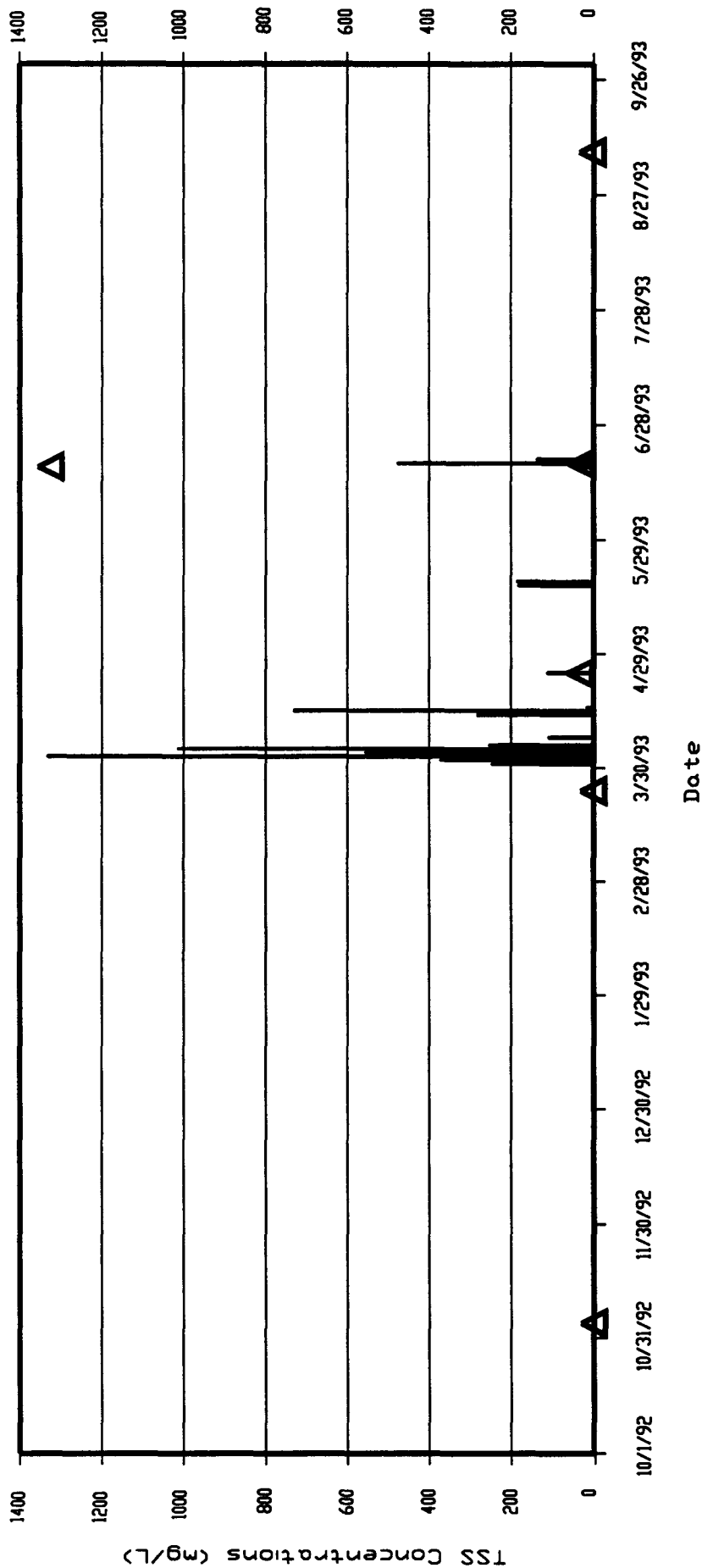
Date

Drawn NAM 8/19/95

Checked 7/27/95

Approved 7/27/95

FILE OUS S31B.DWG



☐ CALIBRATED TSS
☒ OBSERVED TSS

REACH 4

**OBSERVED and CALIBRATED
TOTAL SUSPENDED SEDIMENT**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

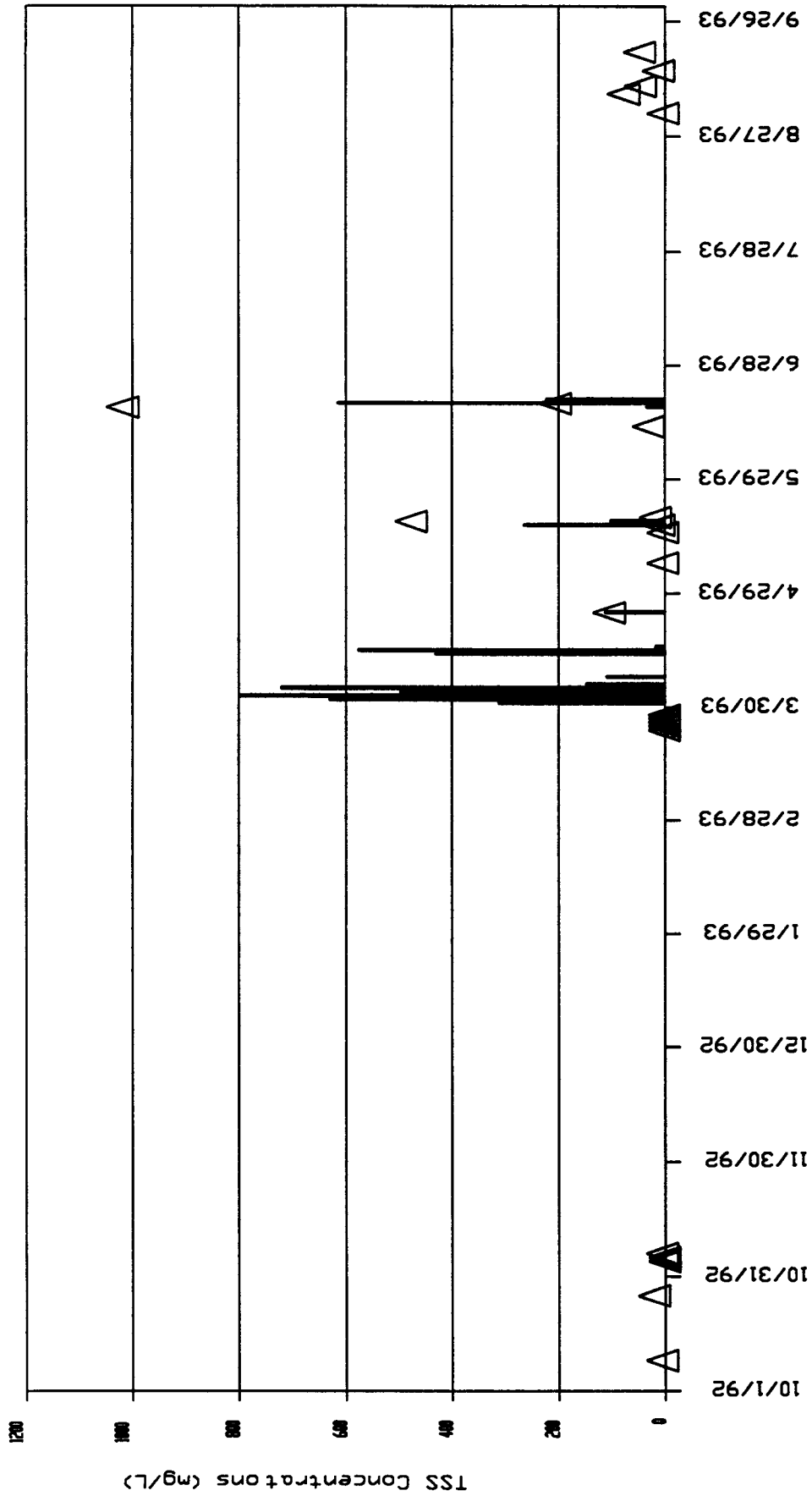
FIGURE 5-31C

Drawn NAM 8/9/95 Date 8/9/95

Checked TE/9/95 Date 9/9/95

Approved _____ Date _____

FILE OU5-531C DVG



**REACHES 2 through 4 MEAN
OBSERVED and CALIBRATED
TOTAL SUSPENDED SEDIMENT**

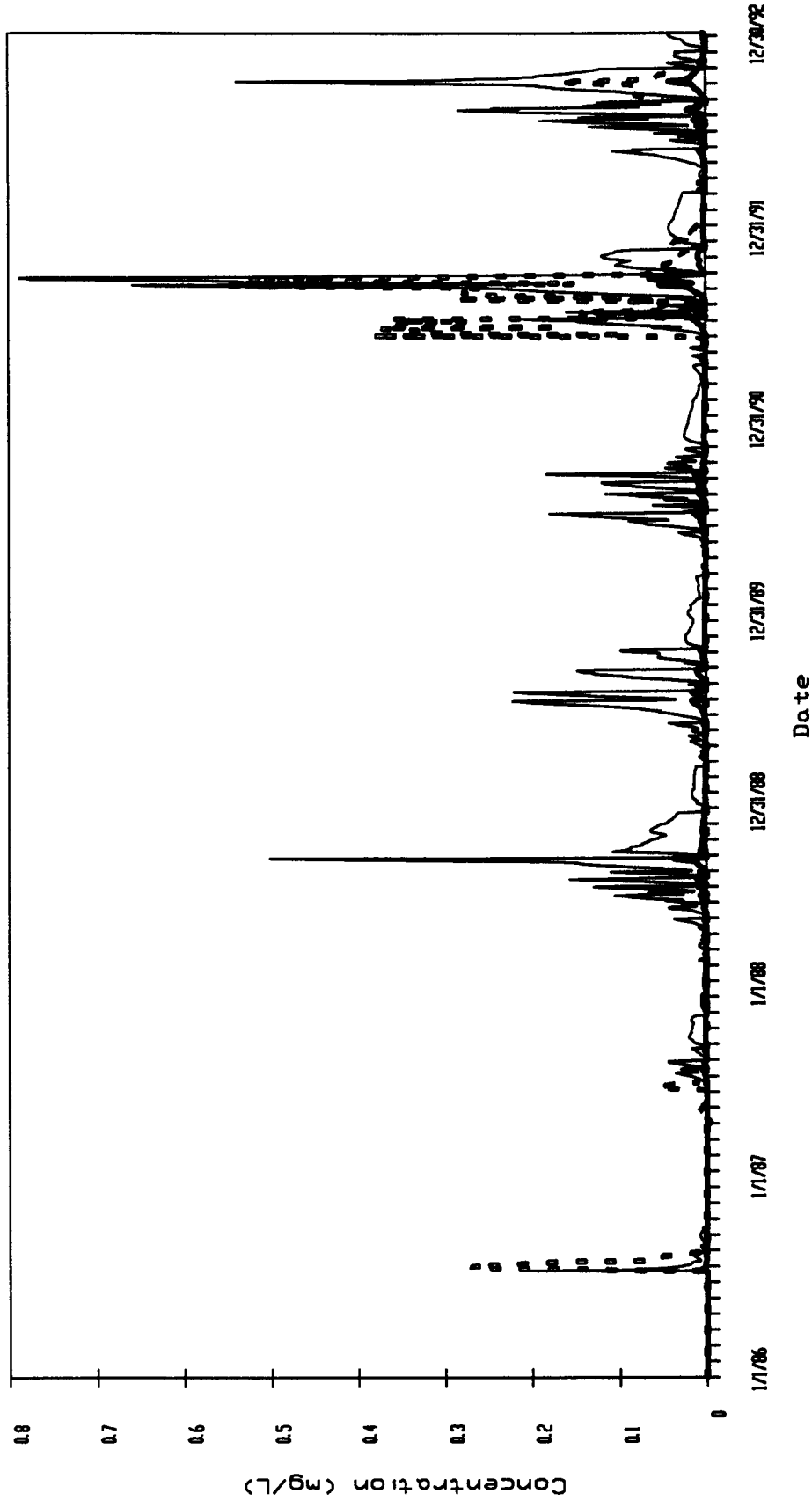
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS - WOMAN CREEK PRIORITY DRAINAGE
RPT/RI REPORT
FIGURE 5-31D

Date

Drawn	NAH	8/9/95
Checked	<i>[Signature]</i>	8/9/95
Approved		

☐ MEAN CALIBRATED TSS

☐ MEAN OBSERVED TSS



**GROUP 1 CALIBRATION
QUALITY OF POND C-1
WATER COLUMN**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-32A1

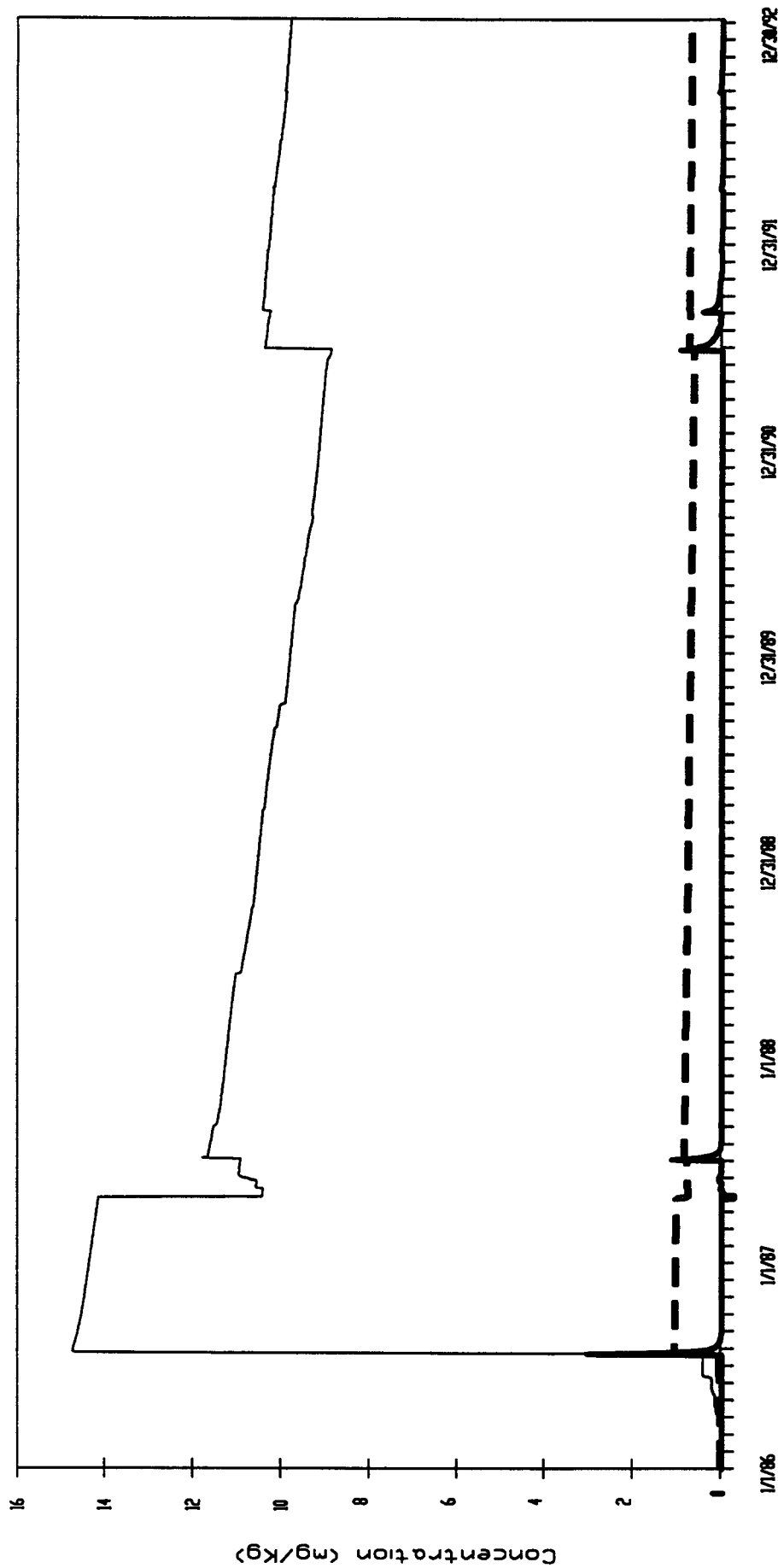
Drawn NAM 7/31/95 Date

Checked 7/29 7/31/95 Date

Approved _____ Date

FILE DU5532A1 DWG

— BARIUM
— LITHIUM
□ □ □ STRONTIUM



— BARIUM
 - - - LITHIUM
 ... STRONTIUM

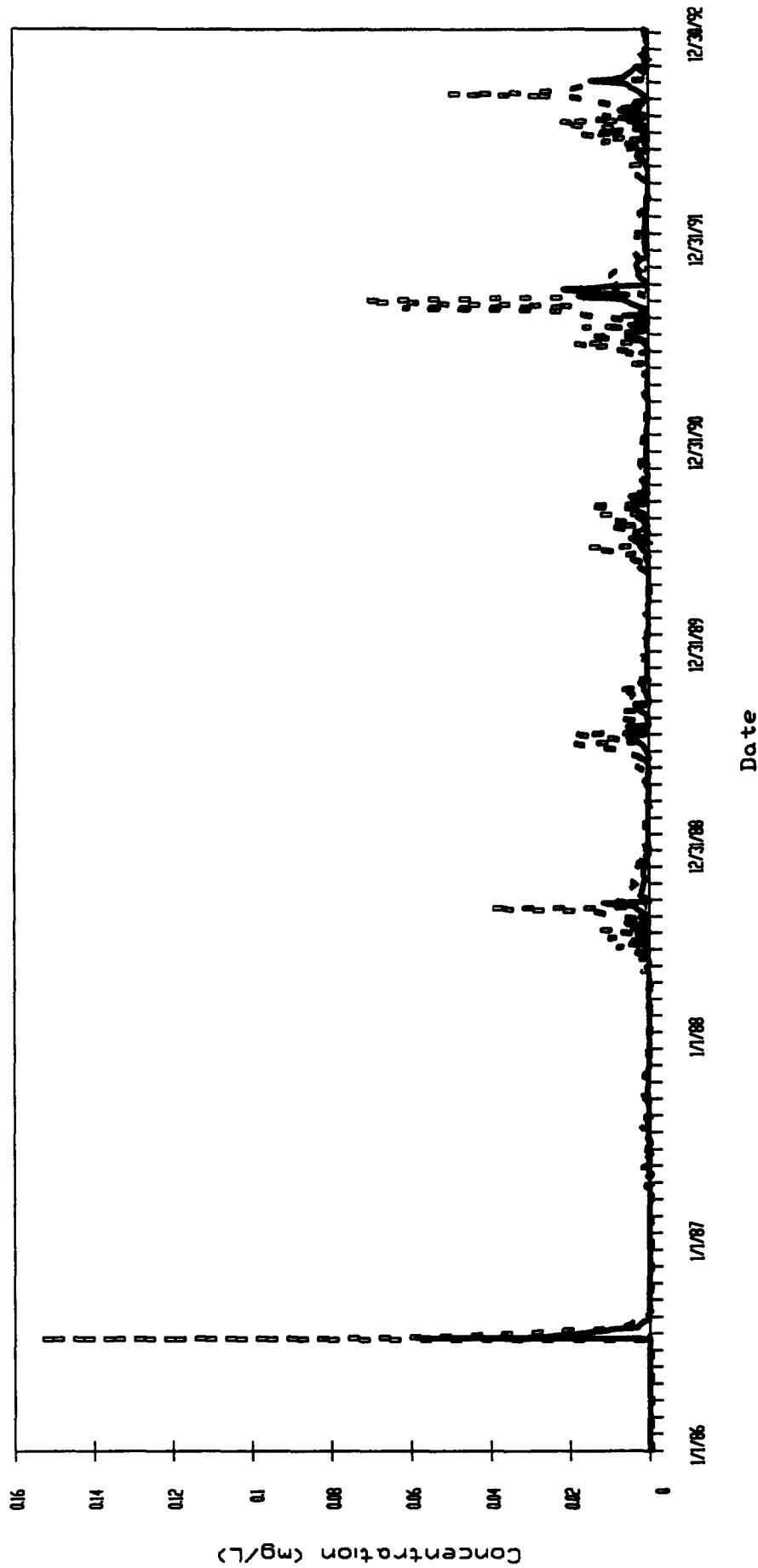
GROUP 1 CALIBRATION
 QUALITY of POND C-1
 BOTTOM - SEDIMENT

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
 OUS - WOMAN CREEK PRIORITY DRAINAGE
 RFI/RI REPORT

FIGURE 5-32A2

Drawn NAAM 8/19/95 Date
 Checked 7/29/95 Date
 Approved _____ Date

FILE OUS532A2 DVG



GROUP 2 CALIBRATION QUALITY OF POND C-1 WATER COLUMN

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

FIGURE 5-32B1

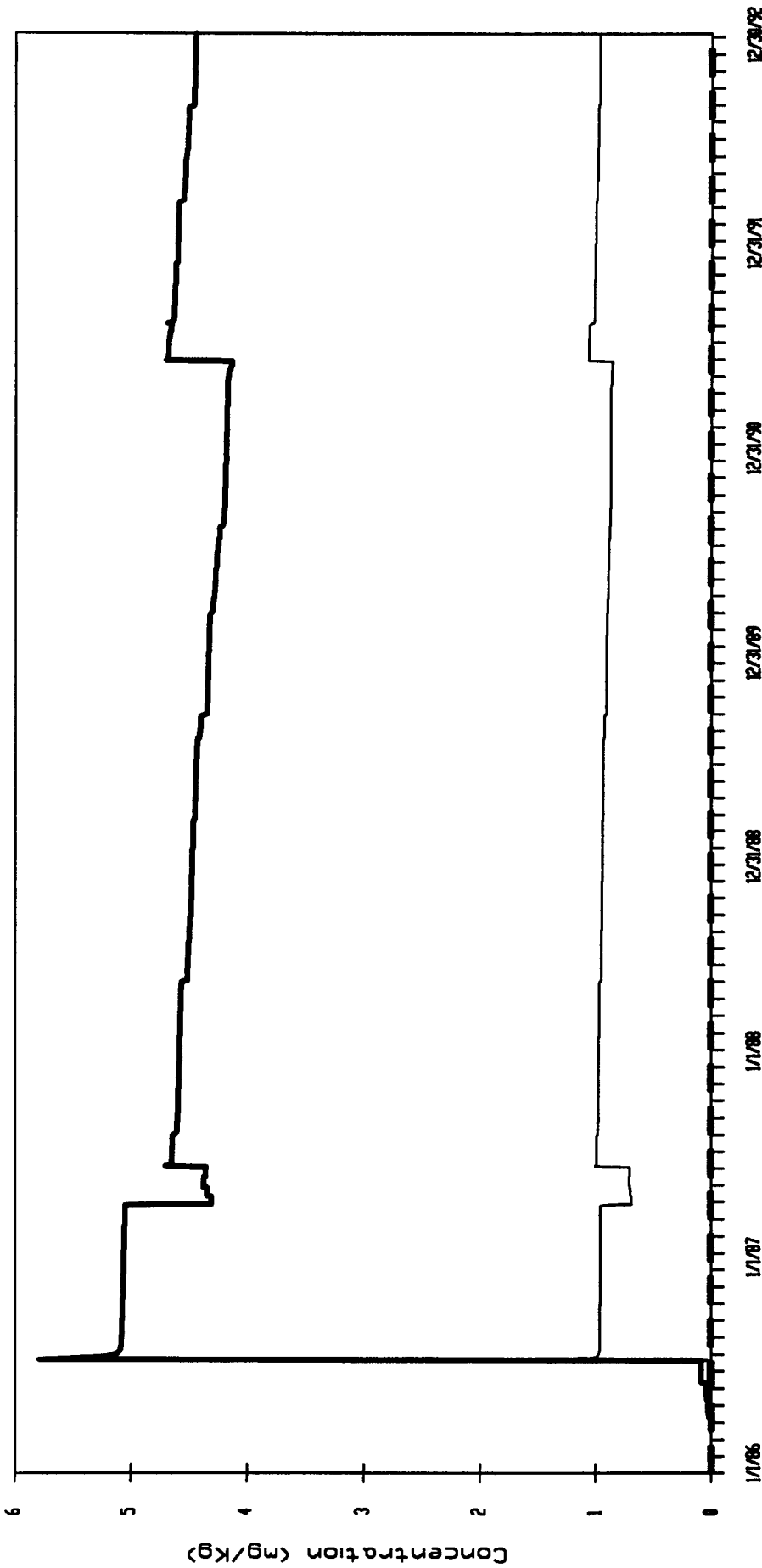
Drawn ADA 8/9/95 Date

Checked 7/9/95 Date

Approved _____ Date

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Date

GROUP 2 CALIBRATION QUALITY of POND C-1 BOTTOM-SEDIMENT

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 5-32B2

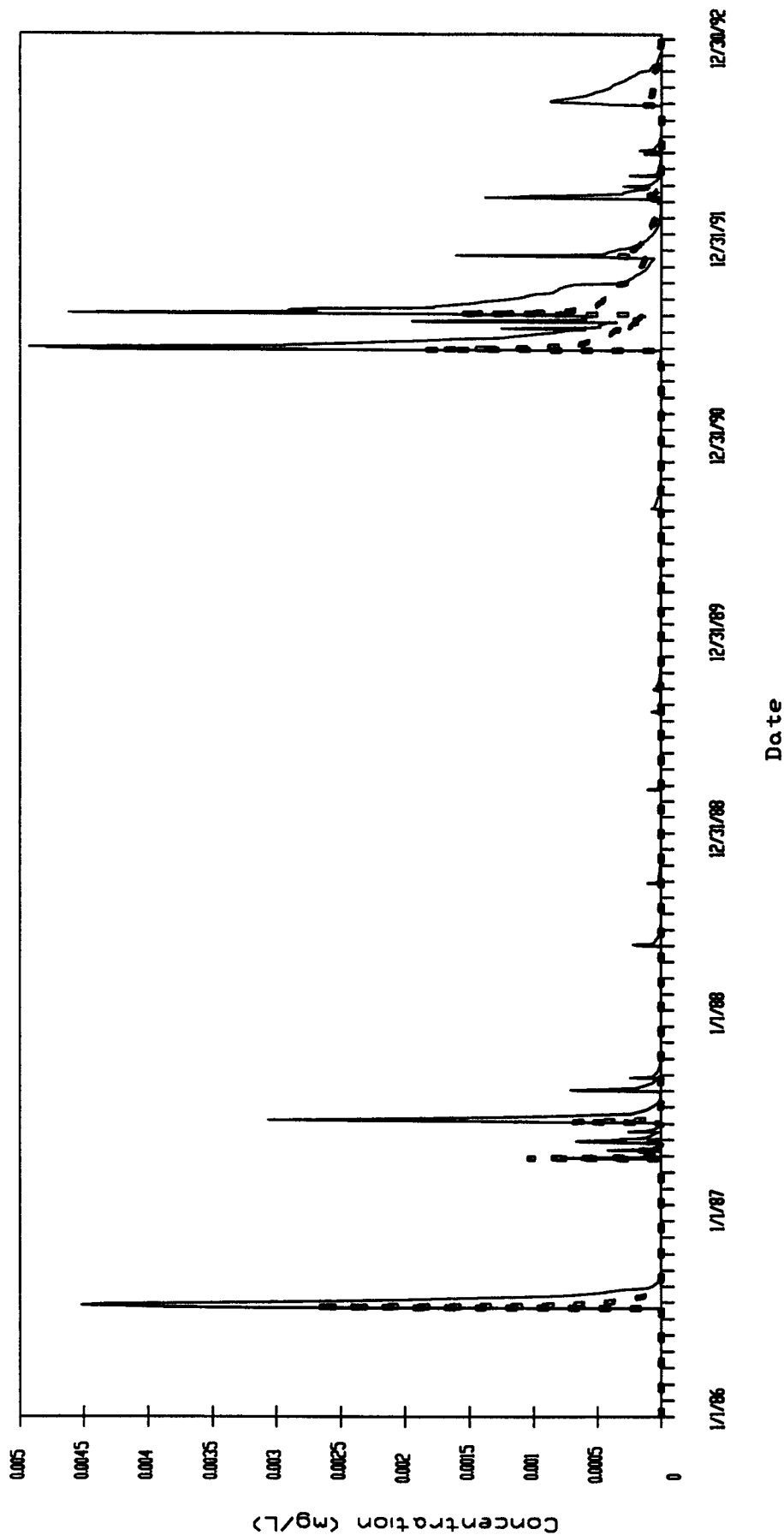
Drawn NAM 8/9/95

Checked *[Signature]* Date 8/2/95

Approved *[Signature]* Date

Date

FILE D:\5532B2.DWG



GROUP 3 CALIBRATION QUALITY OF POND C-1 WATER COLUMN

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

0105 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-32C1

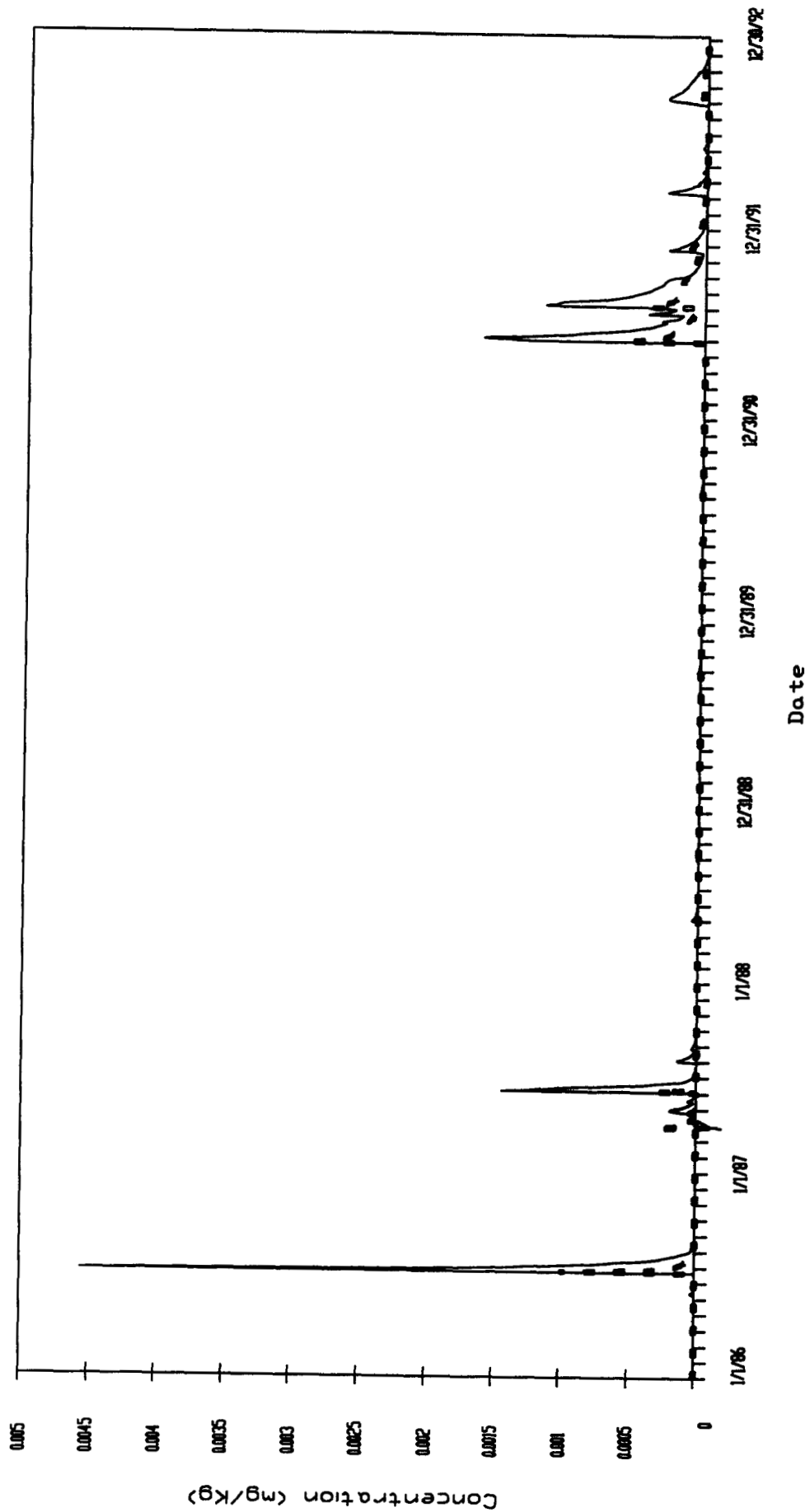
Drawn NAM 8/9/95

Checked [Signature] Date 8/9/95

Approved [Signature] Date 8/9/95

Date

FILE 0105532C1.DWG



**GROUP 3 CALIBRATION
QUALITY OF POND C-1
BOTTOM--SEDIMENT**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

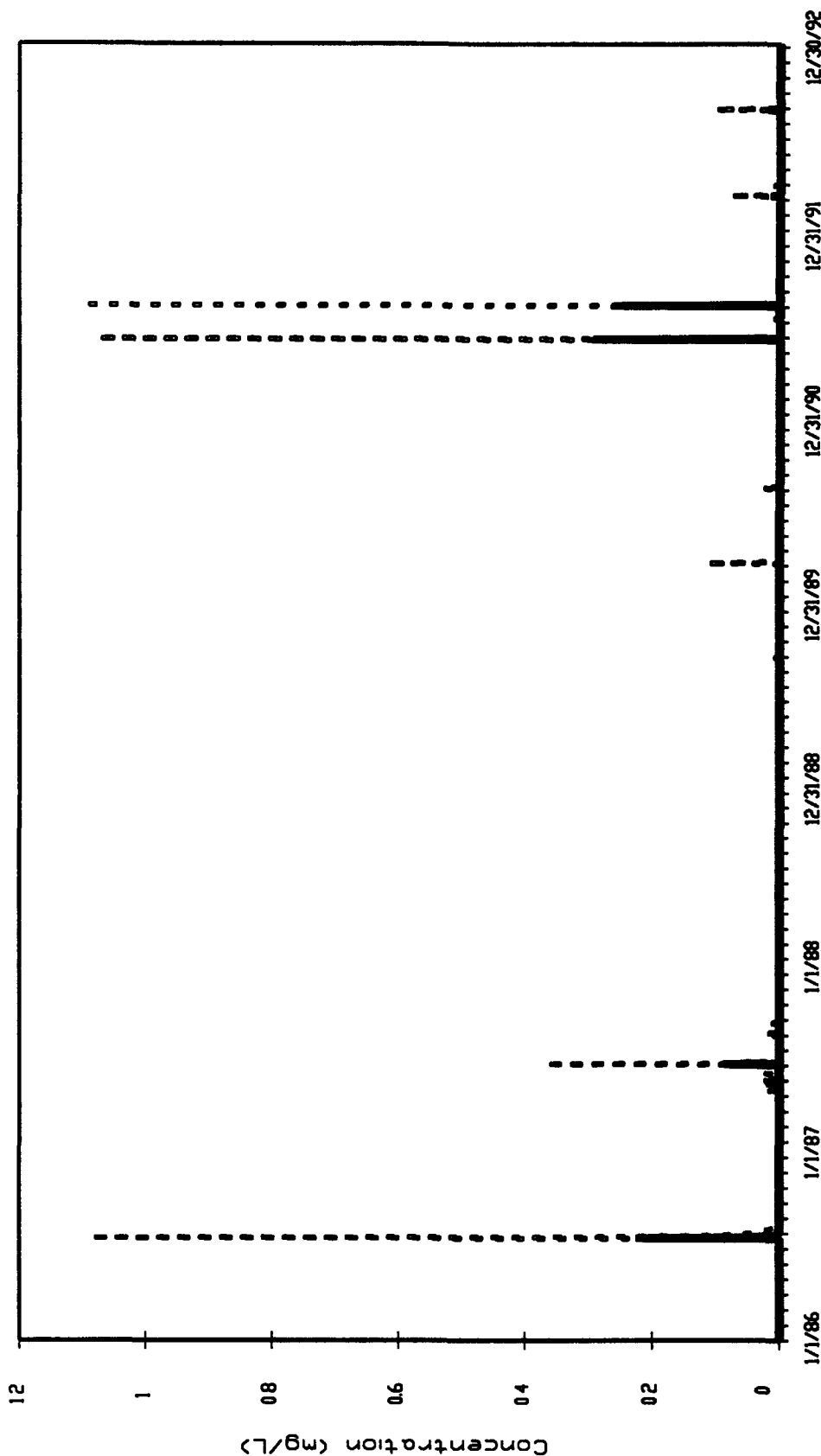
FIGURE 5-32C2

Drawn MAN 8/6/95 Date

Checked [Signature] Date

Approved [Signature] Date

FILE OUS532C2 DVG



GROUP 4 CALIBRATION QUALITY OF POND C-1 WATER COLUMN

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 - WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 5-32D1

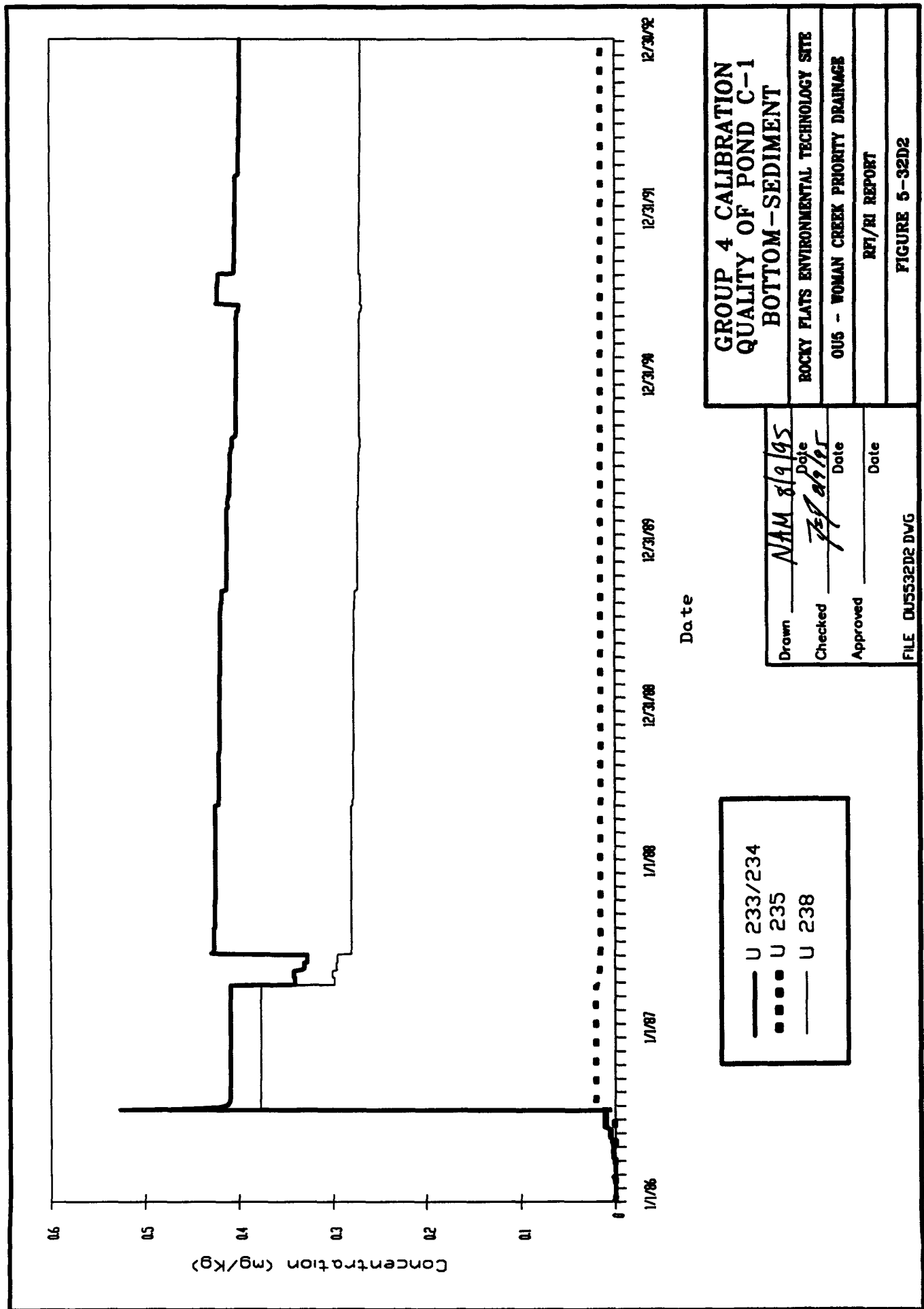
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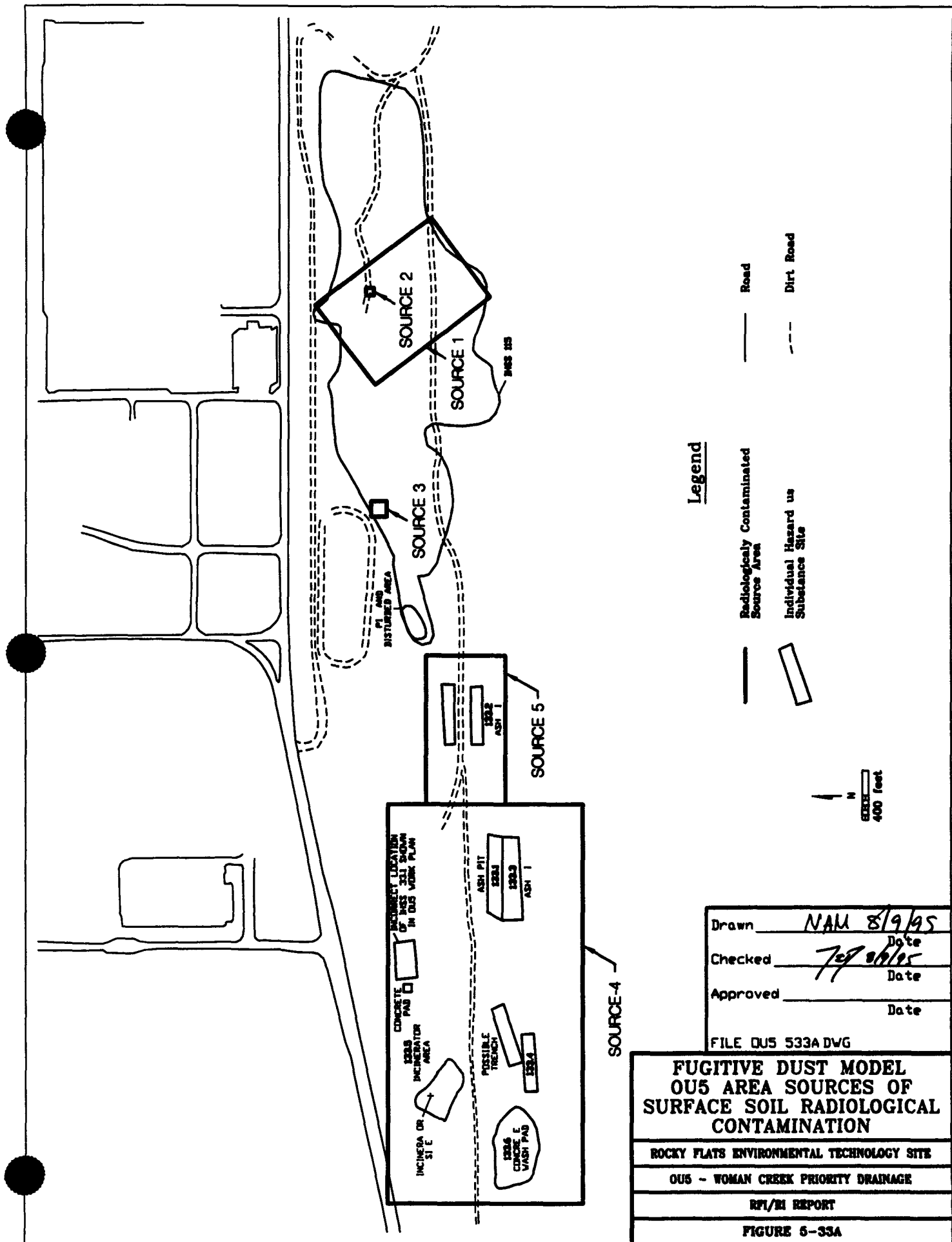
Checked 7/27/95 Date

Approved _____ Date

FILE OU5532D1 DVG

— U 233/234
- - - U 235
... U 238





Drawn NAM 8/9/95 Date
 Checked 7/29/95 Date
 Approved _____ Date

FILE OUS 533A DWG

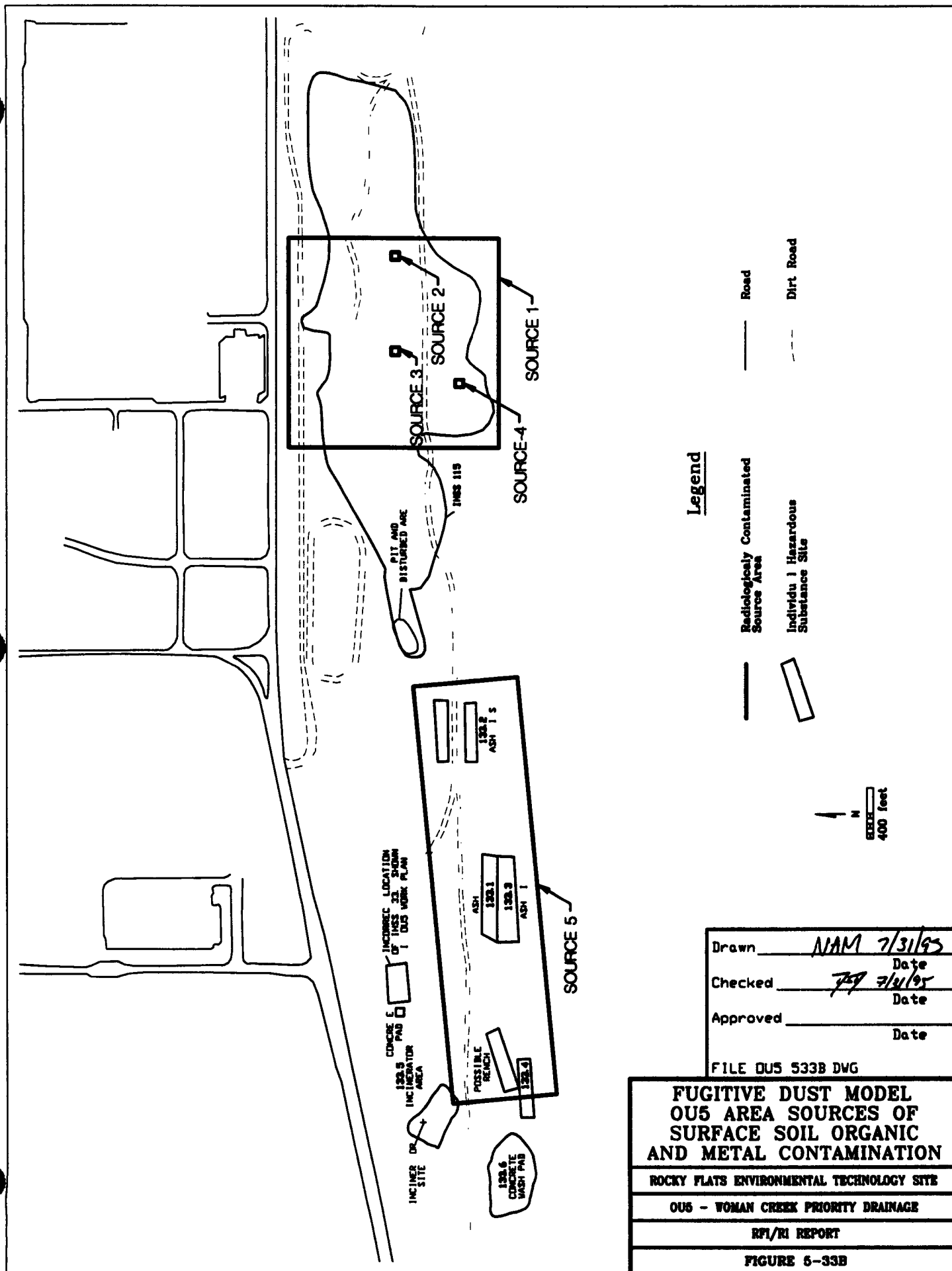
**FUGITIVE DUST MODEL
 OUS AREA SOURCES OF
 SURFACE SOIL RADIOLOGICAL
 CONTAMINATION**

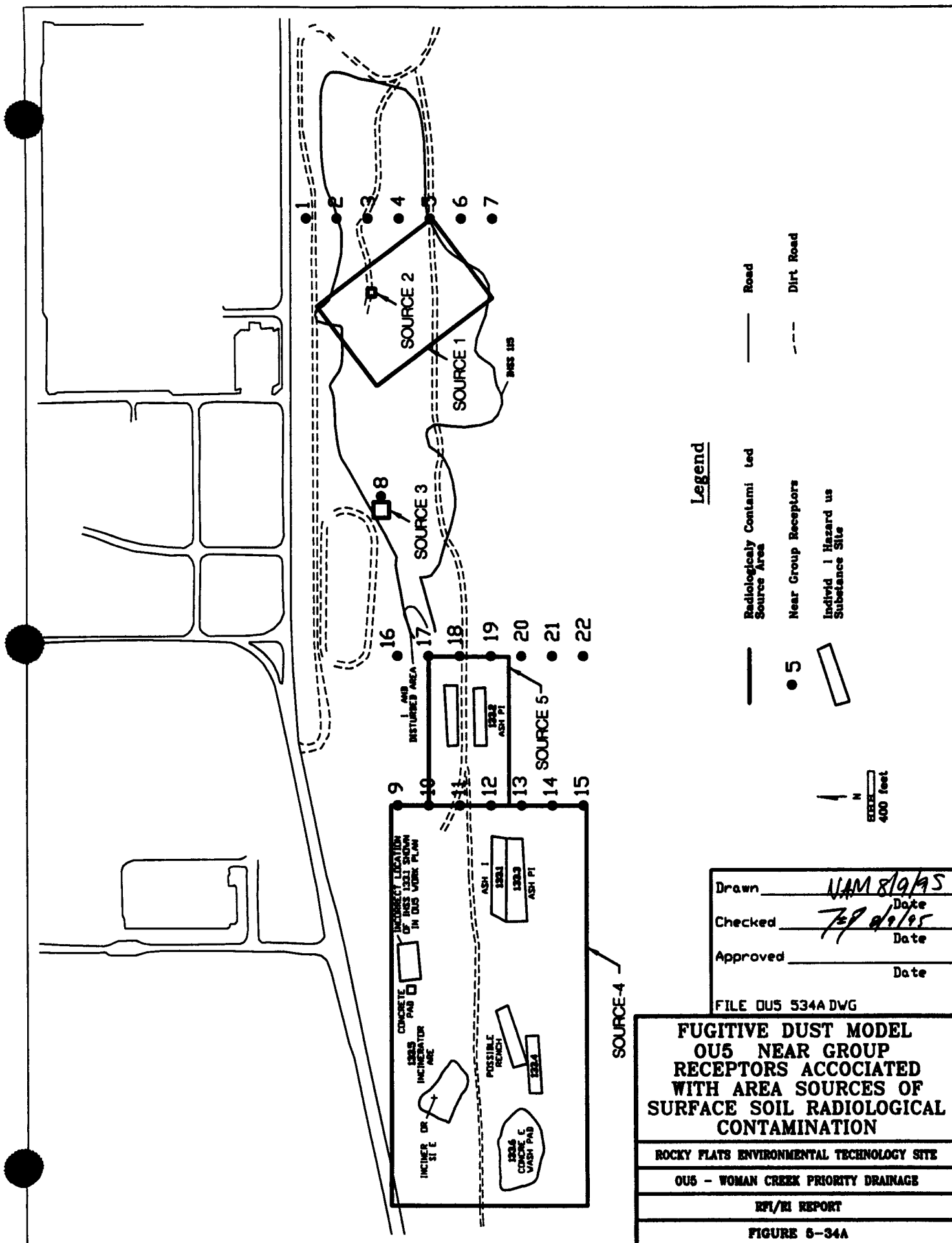
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

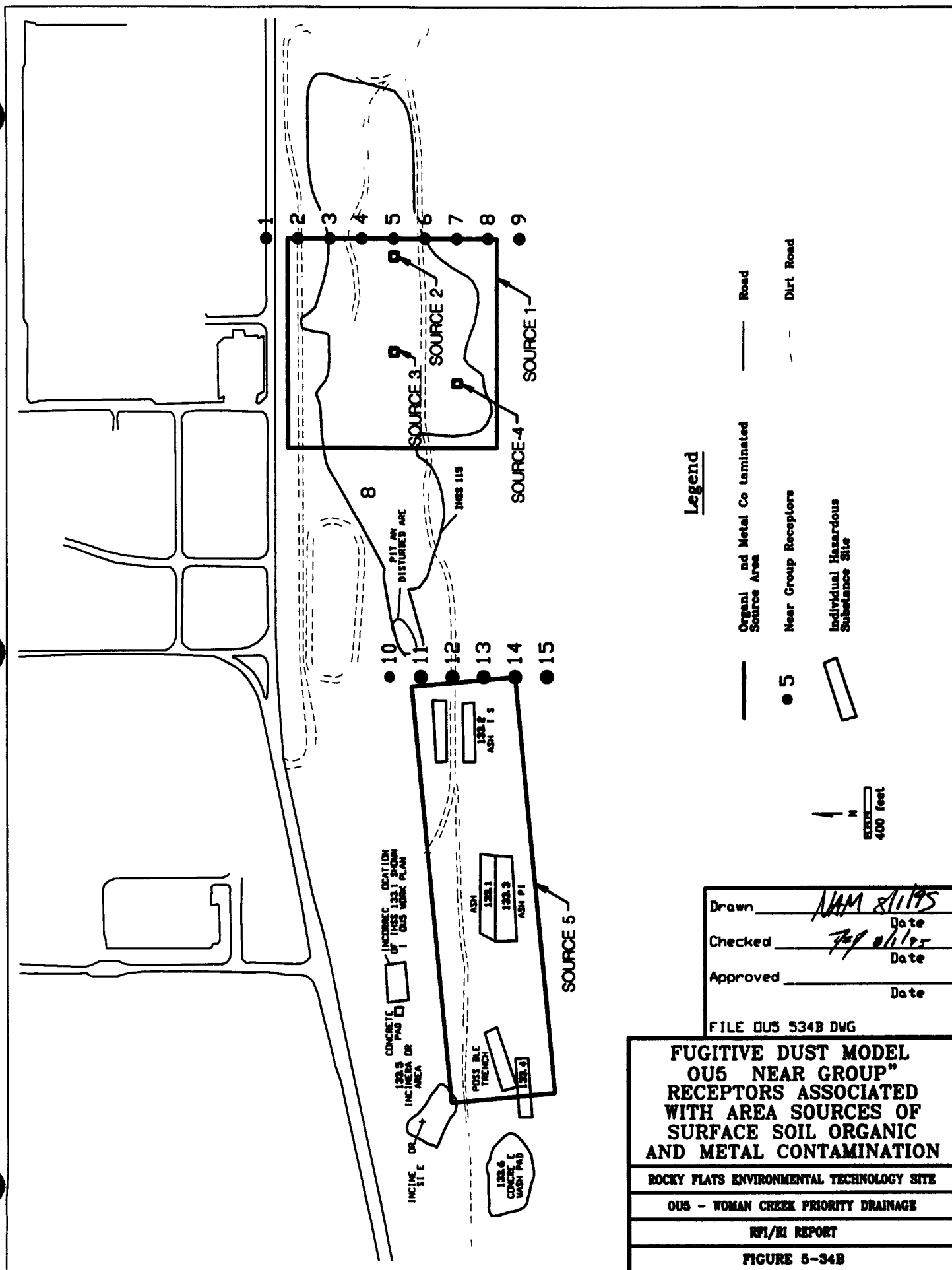
OUS - WOMAN CREEK PRIORITY DRAINAGE

RPI/BI REPORT

FIGURE 5-33A







Drawn	<i>AM 8/1/95</i>	Date
Checked	<i>For Miller</i>	Date
Approved		Date

FILE OUS 534B DWG

FUGITIVE DUST MODEL OUS NEAR GROUP RECEPTORS ASSOCIATED WITH AREA SOURCES OF SURFACE SOIL ORGANIC AND METAL CONTAMINATION
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS - WOMAN CREEK PRIORITY DRAINAGE
RFI/RI REPORT
FIGURE 5-34B

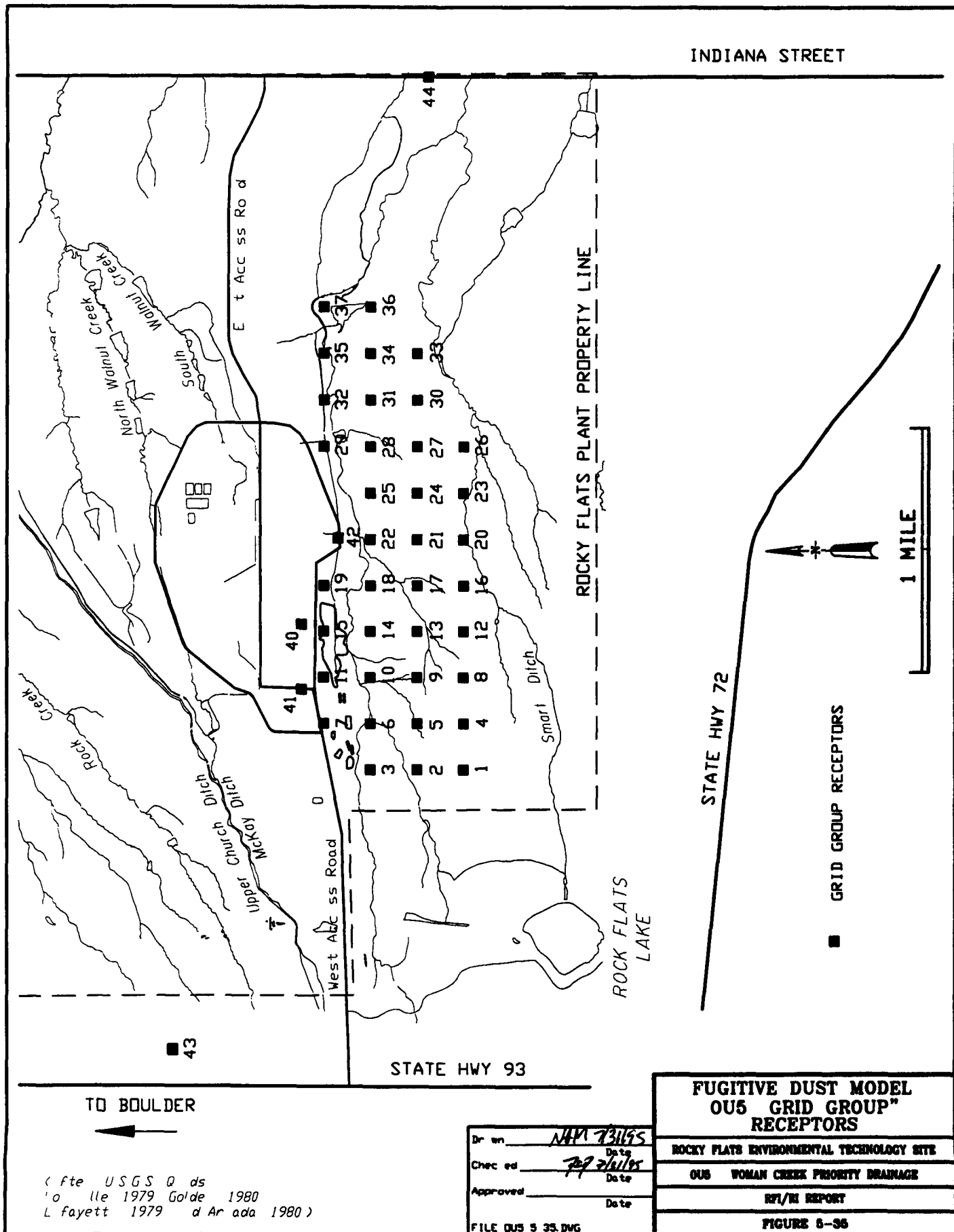


Table 5 1

Initial Recharge Rates OU 5 Groundwater Flow Model

Zone	Vegetation Type	Initial Recharge Rate	
		ft/day	in/yr
1	Riparian Woodland	5 2E-03	22 76
2	Short Upland Shrub	3 0E-03	13 04
3	Open Water	2 7E 03	11 65
4	Tall Marsh Bottom Land Shrub	2 3E-03	10 26
5	Wet Meadow Short Marsh	1 7E-03	7 48
6	Mesic Mixed Grassland Short Grassland	1 6E 03	7 17
7	Reclaimed Grassland	1 6E 03	7 17
8	Xeric Mixed Grassland	1 9E-03	8 50
9	Disturbed Area/Barren Lands/Annual Grass/Forb	2 1E 03	9 39

Table 5 2**Monthly Precipitation at Rocky Flats Plant**

Year	Month	Rain and Snowmelt Inches
1993	May	1 13
1993	June	1 79
1993	July	0 48
1993	August	0 42
1993	September	1 58
1993	October	1 41
1993	November	1 27
1993	December	0 35
1994	January	0 45
1994	February	0 77
1994	March	1 05
1994	April	4 03
Total		14 73

From EG&G Monthly Environmental Monitoring Report,
Rocky Flats Plant Reports May ER 4180110 219 through
April 1994 ER-4180110 222

Table 5 3
Estimated Consumptive Use Rates OU 5 Groundwater Flow Model

Zone No	Plant Subcommunity	K	Consumptive-Use F	Uc	Soil Moisture Correction	Corrected Uc	Dominant Plants	Basis for K
Community	Xeric Zone							
323	Xeric Mixed Grassland	0 70	26 95973308	18 87	0 33	6 23	narrow leaf sedge blue gramma Kentucky blue grass sage	Shultz 1976 sage brush
Community	Mesic Zone							
322	Mesic Mixed Grassland	0 85	26 95973308	22 92	0 33	7 56	western wheatgrass	USDA 1970 small grains
324	Reclaimed Grassland	0 85	26 95973308	22 92	0 33	7 56	smooth brome wheat grasses sweet clover	USDA 1970 small grains
410	Disturbed Area Annual Grass/Forb	0 85	26 95973308	22 92	0 33	7 56	annual sunflower sweet clover	USDA 1970 Ladono Whitecover
420	Disturbed Area Barren Lands	0 60	26 95973308	16 18	0 33	5 34	roads	Less than sage brush
Community	Hydric Zone							
110	Riparian Woodland	1 35	26 95973308	36 40	1 03	37 49	cottonwoods willows	Shultz 1976 cottonwood willows
220	Short Upland Shrub (Snowberry)	1 00	26 95973308	26 96	1 03	27 77	snowberry canada bluegrass	Shultz 1976 small willows
10	Wet Meadow (Grasses)	0 80	26 95973308	21 57	1 03	22 21	prairie shortgrass sedges	Shultz 1976 light vegetation
30	Tall Marsh (Cattails)	0 90	26 95973308	24 26	1 03	24 99	cattails, bulrushes	Shultz 1976 seeped areas
40	Open Water	0 95	26 95973308	25 61	1 03	26 38	impoundments	Shultz 1976 water surfaces

Notes

- 1 Zone numbers refer to DOE (1992c)
- 2 Calculated from Uc=K F
- 3 F = Consumptive Use Factor sum of the monthly consumptive use factors for each month during the growing season May 15 September 30 1993

Table 5-4

**Calibration Results Primary Target Wells
OU 5 Groundwater Flow Model**

<u>Well</u>	<u>X_Grid</u>	<u>Y_Grid</u>	<u>Column</u>	<u>Row</u>	<u>Observed</u>	<u>Calculated</u>	<u>(CAL -OBS)</u>
5686	2220	1308	36	23	5982.3	5982	-0.25
6586	9501	469	132	7	5781.7	5782	0.23242
7086	4003	859	72	15	5935.6	5935.3	-0.2666
51193	8379	575	120	9	5812	5812	-0.02002
58793	2605	838	44	15	5998.7	5998.9	0.26855
59493	3536	526	63	9	5985.2	5985.3	0.10449
59593	3786	773	68	13	5942.7	5943	0.26563

Number of Active Observation Points = 7

Mean of Residuals = 0.047782

Standard Deviation of Residuals (SDEV) = 0.232957

Mean of Absolute Residuals (MA) = 201102

Root Mean Squared Residuals (RMS) = 0.220905

Correlation Coefficient = 0.999997

Table 5-5
Calibration Results Secondary Wells and Wellpoints
OU 5 Groundwater Flow Model

Well	X_Gnd	Y_Gnd	Column	Row	Observed	Calculated	(CAL OBS)
5886	5435	1266	91	23	5891.6	5891.5	-0.1001
6886	5582	1196	92	22	5886.7	5887.2	0.45654
5786	3572	791	63	14	5947	5948.4	1.356
6486	7610	678	113	12	5833.4	5834.3	0.84912
59093	1327	999.8	19	18	6010	6012.2	2.1162
59393	3489	794.8	62	14	5947.2	5951.2	3.9731
59793	4128	797.4	75	14	5932.1	5934.6	2.4805
63093	1751	992.8	27	18	5998.7	6005.2	6.4565
59993	4132	799.9	75	14	5935.3	5934.3	-0.94678
60293	3847	753.9	69	13	5942.4	5942.2	-0.27393
60593	2973	673.7	51	11	6002	6000.9	1.1235
60693	2896	664.9	50	11	6008.1	6001.6	-6.54
60893	3585	506.7	64	8	5985.1	5983	2.0303
62593	1457	730.4	21	13	6043.6	6040.9	2.7148
62693	1926	723	31	12	6037.9	6037.9	7.76E-02
62793	4304	803	78	14	5935.6	5930.4	5.2026
62893	4700	385.9	83	6	5994	5991.8	2.1597
63593	2603	836.2	44	15	5997.3	5999.1	1.7725
63693	2608	848	44	15	5996.9	5998.5	1.6641
63793	2611	835.4	44	15	5998.3	5998.9	0.63037
63893	3536	521.9	63	8	5982.3	5985.6	3.3853
63993	3115	528.4	54	9	6001.4	6004.7	3.3301
64093	3124	532.1	54	9	6002.4	6004.1	1.7188
51293	314.8	1103	4	20	6041	6040.5	-0.5
51393	1057	1036	13	19	6020	6020.1	0.12646
51693	2102	1203	34	22	5986	5989	2.9878
52193	2102	1105	34	20	5998	5998.4	1.5933
53993	7058	736	107	13	5848	5848	0
54093	7052	708.1	107	12	5849	5848.6	-0.35449
54193	7046	681	107	12	5857	5851.3	5.6982
54693	9123	412.8	128	6	5792	5793.2	1.2485
51493	1717	1067	26	19	6000.7	6000.5	-0.2002
51593	2102	1290	34	23	5985.7	5986.2	0.47461
51793	2104	1184	34	22	5989.6	5990.5	0.87109
51893	2105	1165	34	21	5993.6	5992	1.6172
51993	2103	1145	34	21	5994.3	5993.5	-0.771
52093	2103	1125	34	20	5998.4	5996	1.4038
52593	2671	1314	45	23	5970.9	5970	-0.8999
52693	3505	808.2	62	14	5946.2	5949	2.8433
52793	4003	908.4	72	16	5935.1	5935	-6.49E-02
52893	4002	831.8	72	15	5936.4	5935.7	-0.74121
52993	4002	787.4	72	14	5936.7	5937	0.2959
53093	4005	755.9	72	13	5937.7	5939.2	1.4707
53293	4004	692.9	72	12	5956.2	5956.6	0.396
53393	4736	850.2	84	15	5916	5917.5	1.5
53493	5174	1154	88	21	5898.8	5899.5	0.7002
53593	5950	1127	96	21	5875.3	5876.8	1.4502
54393	7034	640.9	107	11	5858.6	5855	-3.5596
54493	7025	607.7	107	10	5863.6	999.99	dry cell
54793	9876	506.1	135	8	5773	5773	0

Number of Active Observation Points 49

Mean of Residuals (M) 0.1220504

Standard Deviation of Residuals (SDEV) 2.378982

Mean of Absolute Residuals (MA) 1.696468

Root Mean Squared Residuals (RMS) 2.357743

Correlation Coefficient 0.9993236

Probability of U Correlation 0

Table 5-6**Hydraulic Conductivities
OU 5 Groundwater Flow Model**

Zone	Hydraulic Conductivity ft/day	Effective Porosity	Zone	Hydraulic Conductivity ft/day	Effective Porosity
1	1 43E 02	0 01	14	5 14E-01	0 03
2	3 57E 02	0 01	15	6 29E 01	0 03
3	5 29E 02	0 01	16	8 23E-01	0 04
4	7 14E 02	0 01	17	8 57E 01	0 04
5	7 40E 02	0 01	18	9 29E-01	0 04
6	1 57E 01	0 01	19	1 00E+00	0 04
7	1 65E 01	0 01	20	2 86E+00	0 12
8	2 27E-01	0 01	21	4 94E+00	0 15
9	2 86E 01	0 01	22	7 14E+00	0 18
10	3 57E 01	0 02	23	1 00E+01	0 18
11	3 70E 01	0 02	24	1 43E+01	0 18
12	4 29E 01	0 02	25	2 86E+01	0 19
13	5 00E-01	0 03			

Table 5 7

**Recharges Rates from Calibration
of OU 5 Groundwater Model**

Zone	Recharge Rate (Feet per Day)
1	0 000742856
2	0 000442857
3	0 000385714
4	0 000342857
5	0 000242857
6	0 000228571
7	0 000242857
8	0 000271428
9	0 0003

Table 5 8

**Volumetric Budget
OU 5 Groundwater Flow Model**

<hr/>		
Inflow	Cubic Feet/Day	
	From Constant Head Cells =	15 556
	Recharge =	8 920
	Total Inflow =	24 476
Outflow	Cubic Feet/Day	
	To Constant Head Cells =	22 670
	Negative Recharge (phreatophytes) =	1 852 8
	Total Outflow =	24 522
Inflow	Outflow	Cubic Feet/Day
		-46 502
Percent Discrepancy		-0 19
<hr/>		

Table 5 9
Summary of Screening for Target Well Selection
OU 5 Solute Transport Model

Well Number	Chemical of Concern	Units	Background Mean	Mean Plus 2 St Dev	Well Maximum	Mean	Target Well?
50092	Aluminum	ug/l	72.24	231.57	9	9	No
	Americium-241	pCi/l	0.02	0.1	NA	NA	No
	Barium	ug/l	84.23	154.76	156	156	Yes
	Beryllium	ug/l	2.33	5.1	0.5	0.5	No
	Manganese	ug/l	22.91	128.92	0.5	0.5	No
	Plutonium-239/240	pCi/l	0.01	0.01	NA	NA	No
	Radium-226	pCi/l	0.26	0.48	0.55	0.47	Yes
	Uranium-233/234	pCi/l	6.1	19.08	5.9	5.16	No
	Uranium-235	pCi/l	0.23	0.65	0.39	0.33	No
	Uranium-238	pCi/l	4.31	13.65	3.5	3.19	No
51193	Vanadium	ug/l	13.03	45.06	NA	NA	No
	Aluminum	ug/l	72.24	231.57	100	41.4	No
	Americium-241	pCi/l	0.02	0.1	0.004	0.002	No
	Barium	ug/l	84.23	154.76	257	236.63	Yes
	Beryllium	ug/l	2.33	5.1	2.5	1.5	No
	Manganese	ug/l	22.91	128.92	3005	2900	Yes
	Plutonium-239/240	pCi/l	0.01	0.01	0.0005	-0.002	No
	Radium-226	pCi/l	0.26	0.48	NA	NA	No
	Uranium-233/234	pCi/l	6.1	19.08	0.49	0.36	No
	Uranium-235	pCi/l	0.23	0.65	0.09	0.06	No
58793	Uranium-238	pCi/l	4.31	13.65	0.59	0.34	No
	Vanadium	ug/l	13.03	45.06	25	13.5	No
	Aluminum	ug/l	72.24	231.57	100	73.33	No
	Americium-241	pCi/l	0.02	0.1	0.018	0.008	No
	Barium	ug/l	84.23	154.76	156	155	Yes
	Beryllium	ug/l	2.33	5.1	2.5	1.83	No
	Manganese	ug/l	22.91	128.92	515	490.67	Yes
	Plutonium-239/240	pCi/l	0.01	0.01	0.002	0.001	No
	Radium-226	pCi/l	0.26	0.48	0.55	0.55	Yes
	Uranium-233/234	pCi/l	6.1	19.08	0.87	0.55	No
59493	Uranium-235	pCi/l	0.23	0.65	0.04	0.01	No
	Uranium-238	pCi/l	4.31	13.65	1.1	0.67	No
	Vanadium	ug/l	13.03	45.06	25	17.5	No
	Aluminum	ug/l	72.24	231.57	100	43	No
	Americium-241	pCi/l	0.02	0.1	0.005	0.001	No
	Barium	ug/l	84.23	154.76	647	486.67	Yes
	Beryllium	ug/l	2.33	5.1	2.5	1.17	No
	Manganese	ug/l	22.91	128.92	10500	6130	Yes
	Plutonium-239/240	pCi/l	0.01	0.01	0.002	0.002	No
	Radium-226	pCi/l	0.26	0.48	1.03	1.03	Yes
59593	Uranium-233/234	pCi/l	6.1	19.08	2.1	1.99	No
	Uranium-235	pCi/l	0.23	0.65	0.16	0.08	No
	Uranium-238	pCi/l	4.31	13.65	1.9	1.72	No
	Vanadium	ug/l	13.03	45.06	25	11.03	No
	Aluminum	ug/l	72.24	231.57	37.7	22.23	No
	Americium-241	pCi/l	0.02	0.1	0.006	0.006	No
	Barium	ug/l	84.23	154.76	139	121	No
	Beryllium	ug/l	2.33	5.1	0.5	0.5	No
	Manganese	ug/l	22.91	128.92	761	575.67	Yes
	Plutonium-239/240	pCi/l	0.01	0.01	0.001	0.001	No
59593	Radium-226	pCi/l	0.26	0.48	0.56	0.56	Yes
	Uranium-233/234	pCi/l	6.1	19.08	3.5	2.57	No
	Uranium-235	pCi/l	0.23	0.65	0.37	0.2	No
	Uranium-238	pCi/l	4.31	13.65	3.6	2.23	No
	Vanadium	ug/l	13.03	45.06	2.5	2.17	No

Table 5 10
Target Concentrations OU 5 Solute Transport Model

Constituent	Well Number	Background Mean Concentration (BM)	Well Mean Concentration (WM)	Target Concentration (BM WM)
Barium in ug/l	50092	84 23	156	71 77
	51193	84 23	236 63	152 40
	58793	84 23	155	70 77
	59493	84 23	486 67	402 44
	59593	84 23	121	36 77
Manganese in ug/l	51193	22 91	2 900	2 877 09
	58793	22 91	490 67	467 76
	59493	22 91	6 130	6 107 09
	59593	22 91	575 67	552 76
Radium 226 in pCi/l	50092	0 26	0 47	0 21
	58793	0 26	0 55	0 29
	59493	0 26	1 03	0 77
	59593	0 26	0 56	0 30

Table 5 11
Calibration Results OU 5 Solute Transport Models

Chemical of Concern	Well Number	Target Concentration ug/l and pCi/l	Computed Concentration ug/l and pCi/l	Distribution Coefficient ml/g	Source Concentration ug/l and pCi/l
Barium	58793	70 77	72 39	0 624	2912 5
	59493	402 44	402 43	0 624	47859
	59593	NA	171 6	0 624	47859
	51193	152 4	152 4	0 624	152 49
	50092	71 77	71 77	0 624	93 868
Manganese	58793	467 76	510 1	3 059	291030
	59493	6107 09	6113 8	3 059	973180
	59593	552 76	558 1	3 059	973180
	51193	2877 09	2877 09	3 059	3663
	50092	NA	NA	NA	NA
Radium 226	58793	0 29	29 79	0 687	12 679
	59493	0 77	76 54	0 687	106 72
	59593	0 3	35 25	0 687	106 72
	51193	NA	NA	NA	NA
	50092	0 21	0 21	0 687	0 29345

Table 5-12
Thirty Year Future Concentrations at Woman Creek
OU 5 Groundwater Modeling

Constituent	Location of Greatest 30 Year Concentration		Greatest Thirty Year Concentration pCi/L or ug/L
	Column	Row	
Radium 226	120	11	0.27
Barium	70	15	93
Manganese	120	9	3451

Table 5-13
Worst-Case Future Concentrations at Woman Creek
OU 5 Groundwater Modeling

Constituent	Location of Worst Case Concentration		Steady State Concentration pCi/L or ug/L	Uncertainty Ratio	Worst-Case Concentration pCi/L or ug/L
	Column	Row			
Radium 226	49	20	0.26	10	2.6
Barium	70	15	93	1.71	159
Manganese	49	20	5911	1.1	6517

Table 5-14
Geometric Properties of HSPF10 Sub-Basins and Stream Reaches

Sub Basin	Calibration Basin Area (Acres)	Simulation Basin Area (Acres)	Reach Length (Feet)	Comments
Basin 1	364 2	364 2	None	Located west of South Boulder Diversion Canal (SBDC)
Basin 2	301 0	301 0	5 801	Extends eastward to the west boundary of RFETS (GS05)
Basin 3	494 4	557 8	5 961	Extends eastward to the confluence with Antelope Spring Creek
Basin 4	51 3	97 2	1 806	Extends eastward to GS17 (inflow to Pond C 1)
Basin 5	50 1	82 3	1 033	Extends through Pond C 1 to GS07 (outflow of Pond C 1)
Basin 6	603 4	643 9	10 392	Extends eastward to Indiana Street (GS02)
Totals	1 864 4	2 046 4	24 993	

Table 5 15
Monthly and Annual Precipitation at Rocky Flats Environmental Technology Site (inches)

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
1971						0.22	1.11	0.35	3.17	0.55	0.15	0.40	
1972	0.93	0.08	0.83	1.58	0.97	0.95	1.59	2.47	1.42	0.91	2.00	1.05	14.78
1973	1.05	0.15	2.04	4.73	4.71	0.66	1.53	0.54	2.74	0.65	1.30	1.48	21.58
1974	1.12	1.11	0.89	3.05	0.08	1.99	1.00	0.22	1.41	1.91	1.15	0.38	14.31
1975	0.38	0.84	1.42	1.31	3.73	1.11	0.83	1.22	0.80	0.68	0.85	0.21	13.38
1976	0.13	0.04	0.34	2.16	1.93	0.90	1.53	1.46	4.49	0.66	0.21	0.10	13.95
1977	0.06	0.47	0.08	1.80	0.46	1.13	2.73	1.04	0.12	0.40	0.34	0.09	8.72
1978	0.35	0.33											
1979													
1980													
1981													
1982													
1983	0.02	0.11	4.64	2.21	3.97	2.76	2.10	3.46	0.01	0.34	2.47	0.42	22.59
1984	0.36	0.65	0.84	1.42	0.56	0.91	0.77	1.69	0.16	3.68	0.00	0.28	11.32
1985	0.41	0.77	0.64	1.61	2.32	1.73	3.38	0.11	1.24	0.00	1.26	0.08	14.23
1986	0.06	0.33	0.00	2.68	2.23	2.03	1.46	1.58	0.84	0.98	0.38	1.26	15.03
1987	0.43	1.19	1.35	0.91	2.40	5.72	0.57	2.09	0.64	1.06	1.10	0.71	18.17
1988	0.27	0.55	1.10	1.22	2.20	0.95	1.66	1.60	1.36	0.09	0.40	0.54	11.94
1989	0.53	0.11	0.21	0.51	2.20	0.02	1.74	1.90	2.69	0.39	0.11	0.31	10.72
1990	0.28	0.17	2.16	1.33	1.82	0.12	3.16	1.41	2.00	0.80	0.64	0.02	13.91
1991	0.19	0.04	0.41	1.50	3.77	2.30	2.47	2.45	0.84	0.31	1.72	0.17	16.17
1992	0.31	0.00	3.37	0.53	1.51	2.21	1.10	2.97	0.00	0.59	1.00	0.11	13.70
1993	0.03	0.27	1.52	1.45	1.13	1.79	0.48	0.42	1.58	1.41	1.27	0.35	11.70
1994	0.45	0.77	1.05	4.03	1.37	1.12	0.4	1.5	0.68	0.96	1.08	0.16	13.57
Median	0.35	0.33	0.97	1.54	1.93	1.13	1.53	1.54	1.04	0.67	1.04	0.30	13.93
Mean	0.39	0.46	1.27	1.90	2.00	1.51	1.56	1.50	1.38	0.86	0.95	0.43	14.43
Std Dev	0.33	0.39	1.19	1.12	1.36	1.28	0.88	0.93	1.19	0.82	0.67	0.42	3.50
Maximum	1.12	1.19	4.64	4.73	4.71	5.72	3.38	3.46	4.49	3.68	2.47	1.48	22.59
Minimum	0.02	0.00	0.00	0.51	0.00	0.02	0.40	0.11	0.00	0.00	0.00	0.02	8.72
N	18	18	17	17	18	18	18	18	18	18	18	18	17

No published data found for this time period

Table 5-16
Summary of Chemicals of Concern by Medium

Group	Chemical of Concern	Surface Soil	Ground Water	Surface Water	Pond Sediment	Stream Sediment
Metals						
1	Barium		X	X		
	Lithium			X		
	Strontium			X		
2	Copper	X				X
	Mercury	X			X	X
	Zinc				X	X
Radionuclides						
3	Americium 241		X	X	X	X
	Plutonium 239/240		X		X	X
4	Uranium 233/234	X	X	X	X	
	Uranium 235	X	X		X	
	Uranium-238	X	X	X	X	

Source DOE 1995a

Table 5-17

**OU5 Surface-Water Gauge Stations (GS)
for Woman Creek Drainage Basin**

Site	Purpose/Location ¹⁾	Equipment	Flow Equation ²⁾
GS05	West boundary of RFETS on Woman Creek	9 Parshall Flume Flow Recorder	$CFS = 3.1667(FT^{1.5128})$
GS06	West boundary of RFETS on South Woman Creek	9 Parshall Flume Flow Recorder	$CFS = 3.1667(FT^{1.5128})$
GS17	Flow into Pond C 1 and seepage from SID	9 Parshall Flume Flow Recorder	$CFS = 3.1667(FT^{1.5128})$
GS07	Discharge from Pond C 1	9 Parshall Flume 90° V Notch Weir Flow Recorder	$CFS = 3.1667(FT^{1.5128})$
GS01	Indiana Street	Rated Culvert 43 X 78 CMP Flow Recorder	$CFS = 11.05(FT^3) + 30.87(FT^4) + 26.63(FT^5) + 10.35(FT^6) + 0.22(FT^7) + 0.00019$
GS02	Indiana Street	Rated Culvert 36 CMP Flow Recorder	$CFS = 0.08067(FT^3) + 5.0093(FT^4) + 1.0656(FT^5)$

NOTES

1) Locations are shown on Figure 5.3.2.2

2) Source EG&G 1994d

CMP = corrugated metal pipe CFS = cubic feet per second FT = feet (depth of flow)

Table 5 18

Woman Creek Observed Total Suspended Sediment (TSS) Concentrations

Date	Sample Location	Concentration (mg/L)				
		Reach 2	Reach 3	Reach 4	Reach 5	Reach 6
10/9/92	GS05	5				
10/26/92	GS05 GS07	21			10	
11/4/92	SW107 SW506 SW040 SW033 SW034 SW501 SW029 SW026	2 2	2 2 5	2	5 5	2
3/24/93	SW107 SW127 SW040 SW041 SW506 SW033 SW034 SW501 SW029 SW026	2 2	2 2 2 2 2	2	17	2
4/13/93	GS07 GS01 GS02				15	2 44
4/24/93	GS05 GS16 GS17	4	281	33		
5/7/93	GS05	4				
5/15/93	GS05	4				

Table 5 18 (Continued)

Date	Sample Location	Concentration (mg/L)				
		Reach 2	Reach 3	Reach 4	Reach 5	Reach 6
5/17/93	GS05	4				
	GS06	628				
	GS18		19			
	GS16		325			
	GS18		19			
6/12/93	GS16		31			
6/17/93	GS16		713			
	GS18		49			
	GS17			1326		
	GS02					10
6/18/93	GS06	378				
	GS17			32		
	GS14					7
9/2/93	GS05	4				
9/7/93	GS05	4				
	GS05	228				
	GS16		5			
	GS17			4		
9/9/93	GS06	8				
	GS16		85			
9/13/93	GS16		13			
9/18/93	GS05	48				

Table 5-19
OUS HSPF10 Model Water Quality Partition Coefficients and Other Values ¹⁾

COC	Partition Coefficients (ml/g) pH range 5 - 9			1/2 life T (yr)	1st Order Decay Coeff 693/T
	Sand (<10% clay) ²⁾	Silt (10-30% clay) ²⁾	Clay (>30% clay) ²⁾		
Barium	530 0	2800 0	16000 0		
Copper	41 9	92 2	336		
Lithium	0 0	0 2	0 8		
Mercury	322 0	580 0	5280 0		
Strontium	24 3	100 0	124 0		
Zinc	12 7	939 0	1460 0		
Am ₂₄₁	82 0	200 0	1000 0	458	1 5x10 ⁻³
PU _{239/240}	10 0	100 0	250 0	2 41x10 ⁴ /6 57x10 ³	2 9x10 ⁻⁵ /1 1x10 ⁻⁴
U _{233/234}	0 0	50 0	500 0	1 59x10 ⁵ /2 45x10 ⁵	4 0x10 ⁻⁹ /2 8x10 ⁻⁸
U ₂₃₅	0 0	50 0	500 0	7 0x10 ⁶	9 8x10 ⁻¹⁰
U ₂₃₈	0 0	50 0	500 0	4 47x10 ⁶	1 55x10 ⁻¹⁰

1) Source D L Streng and S R Peterson 1989

2) Estimated values based on values given for soil composition with the given total weight percent of clay organic matter and iron and aluminum oxyhydroxides

TABLE 5-20
Woman Creek Water-Budget Calibration Results ¹⁾

Location	Mass Volume (cubic feet)		Percent Difference
	Observed	Simulated	
GS05 (Basin 2)	1 123 800	840 900	-0 25
GS17 (Basin 4)	1 892 500	2 068 200	0 09
GS07 (Basin 5)	2 013 000	2 005 400	-0 00
GS02 (Basin 6)	1 809 500	2 199 000	0 22
Mean Results	1 709 700 00	1 778 375 00	0 04

1) Calibration period April 1993 through September 1993

Table 5 21
Comparison of Observed and Simulated Calibration Results
for Pond C 1 Water Column Quality¹⁾

Constituents (COCs)	Observed (OC Concentrations)	7 Year simulation results			7 Year Results as % of Observed		
		Median	Mean	Maximum	Median	Mean	Maximum
Group 1 (mg/L)	Reach 5						
Barium	0 0900	0 0110	0 0344	0 7880	12 22%	38 22%	875 56%
Lithium	0 0060	0 0008	0 0026	0 0650	13 17%	43 33%	1083 33%
Strontium	0 2750	0 0000	0 0161	0 5480	0 01%	5 85%	199 27%
Group 2 (mg/L)	Reach 5						
Copper	0 0030	0 0003	0 0010	0 0588	9 63%	34 11%	1961 06%
Mercury	0 0000	0 0000	0 0000	0 0003	NA	NA	NA
Zinc	0 0070	0 0010	0 0034	0 1562	14 40%	49 13%	2231 59 /
Group 3 (pCi/L)	Reach 5						
Americium 241	0 0040	0 0009	0 0012	0 0056	22 43%	30 31%	140 45%
Plutonium 239/240	0 0010	0 0000	0 0000	0 0043	0 10%	0 94%	434 58%
Group 4 (pCi/L)	Reach 5						
Uranium 233/234	0 9000	0 0239	0 0288	0 2940	2 66%	3 20%	32 67%
Uranium 235	NA	0 0000	0 0000	0 0160	NA	NA	NA
Uranium 238	0 6000	0 0002	0 0019	0 8750	0 03%	0 32%	145 83%
Mean					8.29%	22.82%	789.37%

- 1) Simulation period is 1986 through 1992 (7 years)
- 2) Observed (OC) concentrations are composite values from OUS field sampling data.
- 3) Simulation source terms were calculated with the SLD in place

Table 5 22
Comparison of Observed and Simulated Calibration Results
for Pond C 1 and Woman Creek Bottom Sediment Quality ¹⁾

Group 1 (ng/Kg)	Constituents (COCs)	Observed COC Concentrations	7 Year Simulated		30 Year Extrapolated		Simulated Residual	7 Year w/ SID results as % of observed	30 Year w/ SID results as % of observed
			Residuals	Residuals	Residuals	Residuals			
Group 1 (ng/Kg)	Reach 5								
	Barium	NA	9 800	41 993	1 850	77 687	NA	NA	NA
	Lithium	NA	0 680	2 914	1 860	5 420	NA	NA	NA
	Strontium	NA	0 017	0 073	1 800	0 131	NA	NA	NA
Group 2 (ng/Kg)	Reach 5								
	Copper	0 2430	0 865	3 707	2 077	7 698	355 97%	3168 09%	3168 09%
	Mercury	1 3310	NA	NA	NA	NA	NA	NA	NA
	Zinc	0 7590	4 160	17 826	1 800	32 086	548 09%	4227 42%	4227 42%
Group 3 (ng/Kg)	Reach 4								
	Copper	14 5000	0 955	4 092	2 077	8 499	6 59%	58 62%	58 62%
	Mercury	0 1000	NA	NA	NA	NA	NA	NA	NA
	Zinc	44 2000	4 470	19 154	1 800	34 477	10 11%	78 00%	78 00%
Group 4 (pCu/gm)	Reach 3								
	Copper	9 3900	1 256	5 382	2 077	11 178	13 38%	119 05%	119 05%
	Mercury	0 1100	NA	NA	NA	NA	NA	NA	NA
	Zinc	35 0000	5 660	24 253	1 800	43 656	16 17%	124 73%	124 73%
Group 5 (pCu/gm)	Reach 5								
	Americium-241	0 1030	0 0000	0 0001	1 7650	0 0002	0 02%	0 15%	0 15%
	Plutonium-239/240	0 6840	0 0001	0 0003	1 9180	0 0005	0 01%	0 07%	0 07%
Group 6 (pCu/gm)	Reach 4								
	Americium-241	0 0000	0 0003	0 0015	1 7650	0 0026	4 25%	32 14%	32 14%
	Plutonium-239/240	0 0390	0 0015	0 0064	1 9180	0 0123	3 85%	31 61%	31 61%
Group 7 (pCu/gm)	Reach 3								
	Americium-241	0 0061	0 0002	0 0010	1 7650	0 0018	3 93%	29 76%	29 76%
	Plutonium-239/240	0 0071	0 0013	0 0056	1 9180	0 0107	18 31%	150 48%	150 48%
Group 8 (pCu/gm)	Reach 5								
	Uranium-233/234	2 0090	0 260	1 114	6 771	7 544	12 45%	361 11%	361 11%
	Uranium-235	0 0920	0 010	0 043	24 362	1 044	10 87%	1134 69%	1134 69%
	Uranium-238	1 7620	0 380	1 628	23 919	38 947	21 57%	2210 40%	2210 40%
Mean								68.37%	781.75%

1) Simulated values for 1986 through 1992 (7 year)
2) Observed COC concentrations are compared to estimated values for sampling data.
3) Simulated values were calculated with the SID program.
4) If the calculated concentration is less than the area with the SID is included

Table 5 23A
Statistical Summary of Group 1, 30 Year Simulation
Water Column Quality

Reach 3

	Barium (mg/L)		Lithium (mg/L)		Strontium (mg/L)	
	mean	median	mean	median	mean	median
Mean	0 0001	0	0 000008	0	0 00001	0
Standard Error	0 000004	0	0 000000	0	0 000007	0
Median	0 0001	0	0 000009	0	0 0001	0
Mode	n/a	0	n/a	0	n/a	0
Standard Deviation	0 0000	0	0 000002	0	0 00004	0
Sample Variance	0 000000	0	0 000000	0	0 000000	0
Kurtosis	0 687	n/a	0 686	n/a	0 591	n/a
Skewness	-0 565	n/a	-0 564	n/a	0 366	n/a
Range	0 0001	0	0 000005	0	0 0002	0
Minimum	0 0001	0	0 000005	0	0 00006	0
Maximum	0 0002	0	0 00001	0	0 0002	0
Sum	0 003	0	0 0002	0	0 004	0
Count	29	29	29	29	29	29
Confidence Level (95%)	0 000008	n/a	0 000001	n/a	0 00001	n/a

Reach 4

	Barium (mg/L)		Lithium (mg/L)		Strontium (mg/L)	
	mean	median	mean	median	mean	median
Mean	0 000001	0	0 000002	0	0 000003	0
Standard Error	0 000001	0	0 000000	0	0 000003	0
Median	0 00003	0	0 000002	0	0 00005	0
Mode	n/a	0	n/a	0	n/a	0
Standard Deviation	0 000006	0	0 000000	0	0 00001	0
Sample Variance	0 000000	0	0 000000	0	0 000000	0
Kurtosis	0 244	n/a	0 236	n/a	1 38	n/a
Skewness	-0 065	n/a	0 059	n/a	0 848	n/a
Range	0 00002	0	0 000002	0	0 00007	0
Minimum	0 00002	0	0 000001	0	0 00002	0
Maximum	0 00004	0	0 000003	0	0 00009	0
Sum	0 001	0	0 00006	0	0 001	0
Count	29	29	29	29	29	29
Confidence Level (95%)	0 000002	n/a	0 000000	n/a	0 000005	n/a

Table 5 23A (Continued)

Reach 5

	Barium (mg/L)		Lithium (mg/L)		Strontium (mg/L)	
	mean	median	mean	median	mean	median
Mean	0.234	0.118	0.031	0.010	0.062	0.020
Standard Error	0.009	0.007	0.002	0.001	0.005	0.002
Median	0.226	0.113	0.029	0.009	0.079	0.018
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	0.050	0.036	0.010	0.003	0.024	0.012
Sample Variance	0.002	0.001	0.0001	0.00001	0.001	0.0001
Kurtosis	2.01	3.07	1.29	3.35	0.123	3.05
Skewness	1.26	1.49	1.26	1.65	0.561	1.42
Range	0.220	0.170	0.042	0.016	0.104	0.057
Minimum	0.162	0.063	0.018	0.005	0.044	0.003
Maximum	0.383	0.233	0.059	0.021	0.148	0.060
Sum	6.79	3.43	0.892	0.278	2.39	0.577
Count	29	29	29	29	29	29
Confidence Level (95%)	0.018	0.013	0.004	0.001	0.009	0.004

Reach 6

	Barium (mg/L)		Lithium (mg/L)		Strontium (mg/L)	
	mean	median	mean	median	mean	median
Mean	0.719	0.009	0.119	0.001	0.024	0.002
Standard Error	0.164	0.001	0.027	0.0001	0.056	0.0002
Median	0.498	0.008	0.085	0.001	0.056	0.001
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	0.884	0.003	0.145	0.0003	0.302	0.001
Sample Variance	0.782	0.00001	0.021	0.00000	0.091	0.00000
Kurtosis	17.8	3.14	11.7	3.53	25.6	3.84
Skewness	3.92	1.59	3.19	1.73	4.94	1.56
Range	4.74	0.014	0.719	0.001	1.66	0.005
Minimum	0.103	0.005	0.013	0.0003	0.013	0.0002
Maximum	4.84	0.018	0.732	0.002	1.67	0.005
Sum	20.9	0.264	3.45	0.021	4.14	0.048
Count	29	29	29	29	29	29
Confidence Level (95%)	0.322	0.001	0.053	0.0001	0.110	0.0004

Table 5 23B
Statistical Summary of Group 1, 30-Year Simulation
Sediment Associated Quality

Reach 3

	Barium (mg/KG)		Lithium (mg/KG)		Strontium (mg/KG)	
	mean	median	mean	median	mean	median
Mean	17.3	17.6	1.22	1.25	1.27	1.06
Standard Error	0.125	0.113	0.009	0.008	0.051	0.048
Median	17.4	17.7	1.2	1.3	1.2	1.1
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	0.674	0.610	0.048	0.043	0.275	0.261
Sample Variance	0.455	0.372	0.002	0.002	0.076	0.068
Kurtosis	1.0	0.719	1.0	0.710	0.031	0.028
Skewness	0.065	0.234	0.065	0.238	0.777	0.073
Range	2.4	2.2	0.167	0.157	0.997	1.1
Minimum	16.2	16.6	1.1	1.2	0.883	0.500
Maximum	18.5	18.8	1.3	1.3	1.9	1.6
Sum	501	511	35.4	36.1	36.9	30.8
Count	29	29	29	29	29	29
Confidence Level (95%)	0.245	0.222	0.017	0.016	0.100	0.095

Reach 4

	Barium (mg/KG)		Lithium (mg/KG)		Strontium (mg/KG)	
	mean	median	mean	median	mean	median
Mean	14.4	14.4	0.999	1.02	1.50	1.40
Standard Error	0.118	0.100	0.008	0.007	0.042	0.045
Median	14.2	14.4	1.00	1.02	1.47	1.40
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	0.637	0.537	0.045	0.038	0.224	0.242
Sample Variance	0.405	0.289	0.002	0.001	0.050	0.058
Kurtosis	-0.144	-0.672	0.156	-0.678	-0.039	0.049
Skewness	-0.081	-0.148	0.081	-0.138	0.602	-0.072
Range	2.64	1.95	0.187	0.137	0.865	1.02
Minimum	12.6	13.4	0.894	0.948	1.14	0.884
Maximum	15.3	15.3	1.08	1.09	2.01	1.90
Sum	410	419	29.0	29.6	43.6	40.7
Count	29	29	29	29	29	29
Confidence Level (95%)	0.232	0.196	0.016	0.014	0.081	0.088

Table 5 23B (Continued)

Reach 5

	Barium (mg/KG)		Lithium (mg/KG)		Strontium (mg/KG)	
	mean	median	mean	median	mean	median
Mean	15.4	15.7	0.699	0.684	0.085	0.026
Standard Error	0.281	0.343	0.009	0.012	0.005	0.003
Median	15.0	15.1	0.699	0.678	0.085	0.023
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	1.51	1.85	0.046	0.063	0.026	0.016
Sample Variance	2.29	3.42	0.002	0.004	0.001	0.000
Kurtosis	2.62	3.68	1.05	0.065	0.336	3.41
Skewness	1.40	1.72	0.031	0.016	0.588	1.48
Range	7.07	8.80	0.170	0.270	0.114	0.079
Minimum	13.2	13.2	0.612	0.541	0.049	0.003
Maximum	20.3	22.0	0.783	0.811	0.163	0.082
Sum	448	456	20.3	19.8	2.64	0.756
Count	29	29	29	29	29	29
Confidence Level (95%)	0.550	0.673	0.017	0.023	0.010	0.006

Reach 6

	Barium (mg/KG)		Lithium (mg/KG)		Strontium (mg/KG)	
	mean	median	mean	median	mean	median
Mean	9.90	9.97	0.699	0.704	0.510	0.419
Standard Error	0.075	0.065	0.005	0.005	0.022	0.016
Median	9.90	9.97	0.699	0.704	0.510	0.419
Mode	n/a	10.0	n/a	n/a	n/a	n/a
Standard Deviation	0.402	0.348	0.029	0.025	0.118	0.087
Sample Variance	0.162	0.121	0.001	0.001	0.014	0.008
Kurtosis	0.078	-0.045	0.024	0.007	-0.977	0.859
Skewness	-0.799	-0.410	-0.825	-0.431	0.450	0.862
Range	1.40	1.42	0.103	0.102	0.394	0.351
Minimum	8.93	9.07	0.627	0.639	0.378	0.295
Maximum	10.3	10.5	0.730	0.742	0.771	0.646
Sum	285	287	20.1	20.2	15.9	12.4
Count	29	29	29	29	29	29
Confidence Level (95%)	0.146	0.127	0.011	0.009	0.043	0.032

Table 5 24A
Statistical Summary of Group 2 30 Year Simulation
Water Column Quality

Reach 3

	Copper (ug/L)		Mercury (ug/L)		Zinc (ug/L)	
	mean	median	mean	median	mean	median
Mean	0 088	0	0 000000	0	0 000005	0
Standard Error	0 004	0	0 000000	0	0 000000	0
Median	0 088	0	0 000000	0	0 000005	0
Mode	n/a	0	n/a	0	n/a	0
Standard Deviation	0 022	0	0 000000	0	0 000009	0
Sample Variance	0 0005	0	0 000000	0	0 000000	0
Kurtosis	0 274	n/a	0 701	n/a	-0 675	n/a
Skewness	0 685	n/a	-0 577	n/a	-0 574	n/a
Range	0 075	0	0 000000	0	0 00003	0
Minimum	0 056	0	0 000000	0	0 00003	0
Maximum	0 131	0	0 000000	0	0 00006	0
Sum	2 54	0	0 000002	0	0 001	0
Count	29	29	29	29	29	29
Confidence Level (95%)	0 008	n/a	0 000000	n/a	0 000003	n/a

Reach 4

	Copper (ug/L)		Mercury (ug/L)		Zinc (ug/L)	
	mean	median	mean	median	mean	median
Mean	0 027	0	0 000000	0	0 000000	0
Standard Error	0 001	0	0 000000	0	0 000000	0
Median	0 027	0	0 000000	0	0 000001	0
Mode	n/a	0	n/a	0	n/a	0
Standard Deviation	0 007	0	0 000000	0	0 000002	0
Sample Variance	0 00005	0	0 000000	0	0 000000	0
Kurtosis	-0 481	n/a	0 106	n/a	0 024	n/a
Skewness	0 626	n/a	0 077	n/a	-0 014	n/a
Range	0 024	0	0 000000	0	0 000009	0
Minimum	0 017	0	0 000000	0	0 000006	0
Maximum	0 041	0	0 000000	0	0 00002	0
Sum	0 801	0	0 000000	0	0 000303	0
Count	29	29	29	29	29	29
Confidence Level (95%)	0 003	n/a	0 000000	n/a	0 000001	n/a

Table 5 24A (Continued)

Reach 5

	Copper (ug/L)		Mercury (ug/L)		Zinc (ug/L)	
	mean	median	mean	median	mean	median
Mean	25.1	9.17	0.00006	0.00002	0.044	0.016
Standard Error	1.75	0.651	0.00000	0.00000	0.003	0.001
Median	25.3	9.18	0.00005	0.00002	0.044	0.015
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	9.40	3.51	0.00002	0.00001	0.017	0.006
Sample Variance	88.3	12.3	0.00000	0.00000	0.0003	0.00004
Kurtosis	0.387	0.428	2.67	4.94	2.52	4.74
Skewness	0.404	0.275	1.53	1.96	1.50	1.92
Range	40.2	15.5	0.00009	0.00004	0.075	0.031
Minimum	8.83	2.60	0.00003	0.00001	0.027	0.007
Maximum	49.0	18.1	0.00012	0.00005	0.102	0.038
Sum	728	266	0.002	0.001	1.40	0.451
Count	29	29	29	29	29	29
Confidence Level (95%)	3.42	1.28	0.00001	0.00000	0.006	0.002

Reach 6

	Copper (ug/L)		Mercury (ug/L)		Zinc (ug/L)	
	mean	median	mean	median	mean	median
Mean	82.6	0.688	0.000	0.000	0.134	0.001
Standard Error	15.3	0.049	0.000	0.000	0.037	0.000
Median	65.4	0.696	0.000	0.000	0.134	0.001
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	82.6	0.266	0.0002	0.0000	0.198	0.001
Sample Variance	6.823	0.071	0.0000	0.0000	0.039	0.000
Kurtosis	12.5	0.333	11.0	4.79	10.8	4.54
Skewness	3.14	0.296	3.08	1.95	3.06	1.90
Range	428	1.15	0.001	0.000	0.980	0.002
Minimum	11.3	0.203	0.00002	0.00000	0.018	0.001
Maximum	439	1.35	0.001	0.000	0.998	0.003
Sum	2.394	20.0	0.006	0.000	5.03	0.035
Count	29	29	29	29	29	29
Confidence Level (95%)	30.1	0.097	0.0001	0.00000	0.072	0.0002

Table 5 24B
Statistical Summary of Group 2, 30-Year Simulation
Sediment Associated Quality

Reach 3

	Copper (mg/KG)		Mercury (mg/KG)		Zinc (mg/KG)	
	mean	median	mean	median	mean	median
Mean	101 010	91 483	0 004	0 004	3 43	3 88
Standard Error	1 549	1 667	0 000	0 000	0 087	0 097
Median	101 574	92 800	0 004	0 005	3 40	3 96
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	8 339	8 977	0 001	0 001	0 469	0 522
Sample Variance	69 546 829	80 592 166	0 000	0 000	0 220	0 272
Kurtosis	0 30	1 23	0 357	1 12	-0 146	1 17
Skewness	0 19	0 20	0 023	-0 036	-0 065	-0 151
Range	33 123	28 216	0 002	0 002	1 90	1 85
Minimum	84 959	76 084	0 003	0 003	2 43	3 01
Maximum	118 083	104 300	0 005	0 006	4 33	4 86
Sum	2 929 281	2 652 994	0 115	0 130	99 4	112
Count	29	29	29	29	29	29
Confidence Level (95%)	3 035	3 267	0 0002	0 0002	0 171	0 190

Reach 4

	Copper (mg/KG)		Mercury (mg/KG)		Zinc (mg/KG)	
	mean	median	mean	median	mean	median
Mean	15 918	13 547	0 004	0 004	3 41	3 63
Standard Error	326	236	0 0001	0 0001	0 051	0 059
Median	15 918	13 547	0 004	0 004	3 41	3 63
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	1 754	1 271	0 0004	0 0005	0 275	0 319
Sample Variance	3 075 998	1 614 545	0 0000	0 0000	0 075	0 102
Kurtosis	-0 963	1 77	0 236	1 130	-0 410	1 13
Skewness	0 271	1 12	0 183	-0 509	0 249	-0 552
Range	6 576	5 828	0 002	0 002	1 04	1 53
Minimum	13 082	12,039	0 003	0 003	2 85	2 75
Maximum	19 658	17 867	0 005	0 005	3 89	4 27
Sum	470 593	403 546	0 112	0 121	98 4	106
Count	29	29	29	29	29	29
Confidence Level (95%)	638	462	0 0001	0 0002	0 100	0 116

Table 5 24B (Continued)

Reach 5

	Copper (mg/KG)		Mercury (mg/KG)		Zinc (mg/KG)	
	mean	median	mean	median	mean	median
Mean	1 001	992	0.003	0.004	2.324	3.19
Standard Error	66.0	68.6	0.000	0.000	0.056	0.059
Median	986	968	0.003	0.004	2.77	3.16
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	355	370	0.000	0.001	0.301	0.316
Sample Variance	126 159	136 546	0.000	0.000	0.091	0.100
Kurtosis	0.591	0.115	0.655	-0.928	0.580	-0.663
Skewness	0.260	0.720	0.683	0.264	0.638	0.328
Range	1 307	1 315	0.002	0.002	1.32	1.19
Minimum	381	507	0.003	0.003	2.34	2.58
Maximum	1 688	1 822	0.005	0.005	3.66	3.77
Sum	29 039	28 760	0.101	0.113	82.3	92.4
Count	29	29	29	29	29	29
Confidence Level (95%)	129	134	0.0002	0.0002	0.110	0.115

Reach 6

	Copper (mg/KG)		Mercury (mg/KG)		Zinc (mg/KG)	
	mean	median	mean	median	mean	median
Mean	11 245	8 338	0.002	0.002	1.53	2.02
Standard Error	283	287	0.0000	0.0001	0.033	0.032
Median	11 627	8 115	0.002	0.002	1.85	2.00
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	1 524	1 546	0.0003	0.0003	0.176	0.170
Sample Variance	2 322,356	2 391 057	0.0000	0.0000	0.031	0.029
Kurtosis	-0.411	20.4	-0.826	-0.821	-0.550	-0.686
Skewness	-0.335	4.19	0.178	0.143	0.123	0.168
Range	5 901	8 800	0.001	0.001	0.698	0.660
Minimum	7 933	6 973	0.001	0.001	1.51	1.69
Maximum	13 834	15 773	0.002	0.002	2.21	2.35
Sum	326 025	241 801	0.051	0.055	52.7	58.5
Count	29	29	29	29	29	29
Confidence Level (95%)	555	563	0.0001	0.0001	0.064	0.062

Table 5 25A
Statistical Summary of Group 3, 30 Year Simulation
Water Column Quality

Reach 3

	Am241 (pCi/L)		Pu239/240 (pCi/L)	
	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>
Mean	0 0002	0	0.00004	0
Standard Error	0 0000	0	0 00000	0
Median	0 0002	0	0 00004	0
Mode	n/a	0	n/a	0
Standard Deviation	0 00005	0	0 00001	0
Sample Variance	0 00000	0	0 00000	0
Kurtosis	0 308	n/a	-0 658	n/a
Skewness	0 684	n/a	0 573	n/a
Range	0 0002	0	0 00002	0
Minimum	0 0001	0	0 00002	0
Maximum	0 0003	0	0 00005	0
Sum	0 006	0	0 001	0
Count	29	29	29	29
Confidence Level (95%)	0 00002	n/a	0 00000	n/a

Reach 4

	Am241 (pCi/L)		Pu239/240 (pCi/L)	
	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>
Mean	0.00004	0	0.00000	0
Standard Error	0 00000	0	0 000000	0
Median	0 00004	0	0 000009	0
Mode	n/a	0	n/a	0
Standard Deviation	0 00001	0	0 000002	0
Sample Variance	0 00000	0	0 000000	0
Kurtosis	0 353	n/a	-0 217	n/a
Skewness	0 633	n/a	-0 156	n/a
Range	0 00004	0	0 000008	0
Minimum	0 00003	0	0 000005	0
Maximum	0 00007	0	0 00001	0
Sum	0 001	0	0 0003	0
Count	29	29	29	29
Confidence Level (95%)	0 000004	n/a	0 000001	n/a

Table 5 25A (Continued)

Reach 5

	Am241 (pCi/L)		Pu239/240 (pCi/L)	
	mean	median	mean	median
Mean	0.134	0.047	0.005	0.002
Standard Error	0.002	0.001	0.000	0.000
Median	0.134	0.046	0.005	0.002
Mode	n/a	n/a	n/a	n/a
Standard Deviation	0.010	0.003	0.002	0.001
Sample Variance	0.000	0.000	0.000	0.000
Kurtosis	0.190	-0.121	3.31	8.79
Skewness	0.087	0.074	1.70	2.70
Range	0.042	0.013	0.009	0.004
Minimum	0.113	0.040	0.003	0.001
Maximum	0.155	0.053	0.012	0.005
Sum	3.88	1.35	0.159	0.050
Count	29	29	29	29
Confidence Level (95%)	0.004	0.001	0.001	0.000

Reach 6

	Am241 (pCi/L)		Pu239/240 (pCi/L)	
	mean	median	mean	median
Mean	0.519	0.004	0.004	0.000
Standard Error	0.119	0.000	0.004	0.000
Median	0.360	0.004	0.015	0.000
Mode	n/a	n/a	n/a	n/a
Standard Deviation	0.640	0.000	0.022	0.000
Sample Variance	0.409	0.0000	0.0005	0.0000
Kurtosis	18.7	0.145	10.2	8.87
Skewness	4.05	0.110	2.97	2.73
Range	3.47	0.001	0.106	0.000
Minimum	0.068	0.003	0.002	0.000
Maximum	3.54	0.004	0.108	0.000
Sum	15.0	0.104	0.568	0.004
Count	29	29	29	29
Confidence Level (95%)	0.233	0.000	0.008	0.000

Table 5 25B
Statistical Summary of Group 3 30 Year Simulation
Sediment Associated Quality

Reach 3

	Am241 (pCi/g)		Pu239/240 (pCi/g)	
	mean	median	mean	median
Mean	0 184	0 167	0.003	0.003
Standard Error	0 003	0 003	0 000	0 000
Median	0 185	0 169	0 003	0 003
Mode	n/a	n/a	n/a	n/a
Standard Deviation	0 015	0 016	0 000	0 000
Sample Variance	0 000	0 000	0 000	0 000
Kurtosis	-0 299	1 226	-0 041	1 24
Skewness	-0 201	-0 200	0 131	0
Range	0 060	0 051	0 002	0 001
Minimum	0 155	0 139	0 002	0 003
Maximum	0 215	0 190	0 004	0 004
Sum	5 34	4 85	0 083	0 094
Count	29	29	29	29
Confidence Level (95%)	0 005	0 006	0 000	0 000

Reach 4

	Am241 (pCi/g)		Pu239/240 (pCi/g)	
	mean	median	mean	median
Mean	0 012	0 010	0 003	0 004
Standard Error	0 000	0 000	0 000	0 000
Median	0 012	0 010	0 003	0 004
Mode	n/a	n/a	n/a	n/a
Standard Deviation	0 002	0 002	0 000	0 000
Sample Variance	0 000	0 000	0 000	0 000
Kurtosis	7 15	5 92	0 278	0 015
Skewness	2 02	1 97	-0 665	-0 392
Range	0 012	0 008	0 001	0 001
Minimum	0 009	0 009	0 003	0 003
Maximum	0 021	0 017	0 004	0 004
Sum	0 361	0 304	0 100	0 108
Count	29	29	29	29
Confidence Level (95%)	0 001	0 001	0 000	0 000

Table 5 25B (Continued)

Reach 5

	Am241 (pCi/g)		Pu239/240 (pCi/g)	
	mean	median	mean	median
Mean	0 150	0 132	0 000	0 000
Standard Error	0 003	0 003	0 000	0 000
Median	0 151	0 134	0 003	0 003
Mode	n/a	n/a	n/a	n/a
Standard Deviation	0 015	0 014	0 0003	0 0003
Sample Variance	0 0002	0 0002	0 0000	0 0000
Kurtosis	0 107	0 754	0 514	-0 840
Skewness	0 549	0 169	0 673	0 083
Range	0 064	0 051	0 001	0 001
Minimum	0 111	0 105	0 002	0 003
Maximum	0 174	0 156	0 003	0 004
Sum	4 35	3 82	0 079	0 088
Count	29	29	29	29
Confidence Level (95%)	0 006	0 005	0 0001	0 0001

Reach 6

	Am241 (pCi/g)		Pu239/240 (pCi/g)	
	mean	median	mean	median
Mean	0 135	0 100	0 000	0 000
Standard Error	0 003	0 004	0 000	0 000
Median	0 140	0 097	0 002	0 002
Mode	n/a	n/a	n/a	n/a
Standard Deviation	0 018	0 020	0 000	0 000
Sample Variance	0 000	0 000	0 000	0 000
Kurtosis	0 413	21 526	0 447	0 534
Skewness	0 332	4 354	0 175	0 076
Range	0 071	0 111	0 001	0 001
Minimum	0 095	0 084	0 001	0 002
Maximum	0 166	0 195	0 002	0 002
Sum	3 91	2 89	0 051	0 055
Count	29	29	29	29
Confidence Level (95%)	0 007	0 007	0 000	0 000

Table 5 26A
Statistical Summary of Group 4, 30-Year Simulation
Water Column Quality

Reach 3

	U233/234 (pCi/L)		U235 (pCi/L)		U238 (pCi/L)	
	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>
Mean	0 010	0	0 002	0	0 104	0
Standard Error	0 0003	0	0 0001	0	0 004	0
Median	0 010	0	0 002	0	0 109	0
Mode	n/a	0	n/a	0	n/a	0
Standard Deviation	0 002	0	0 0004	0	0 019	0
Sample Variance	0 0000	0	0 0000	0	0 0004	0
Kurtosis	0 734	n/a	0 734	n/a	-0 734	n/a
Skewness	-0 555	n/a	0 555	n/a	-0 555	n/a
Range	0 006	0	0 001	0	0 066	0
Minimum	0 006	0	0 001	0	0 065	0
Maximum	0 012	0	0 002	0	0 132	0
Sum	0 286	0	0 056	0	3 02	0
Count	29	29	29	29	29	29
Confidence Level (95%)	0 001	n/a	0 0001	n/a	0 007	n/a

Reach 4

	U233/234 (pCi/L)		U235 (pCi/L)		U238 (pCi/L)	
	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>
Mean	0 000	0	0 0003	0	0 019	0
Standard Error	0 000	0	0 0000	0	0 001	0
Median	0 002	0	0 0004	0	0 019	0
Mode	n/a	0	n/a	0	n/a	0
Standard Deviation	0 0004	0	0 0001	0	0 004	0
Sample Variance	0 00000	0	0 00000	0	0 00002	0
Kurtosis	-0 109	n/a	0 110	n/a	0 110	n/a
Skewness	-0 035	n/a	0 036	n/a	-0 036	n/a
Range	0 002	0	0 0003	0	0 016	0
Minimum	0 001	0	0 0002	0	0 012	0
Maximum	0 003	0	0 0005	0	0 028	0
Sum	0 052	0	0 010	0	0 543	0
Count	29	29	29	29	29	29
Confidence Level (95%)	0 0001	n/a	0 00003	n/a	0 001	n/a

Table 5 26A (Continued)

Reach 5

	U233/234 (pCi/L)		U235 (pCi/L)		U238 (pCi/L)	
	mean	median	mean	median	mean	median
Mean	3.91	1.38	0.260	0.080	13.6	4.26
Standard Error	0.082	0.026	0.018	0.006	0.976	0.368
Median	3.82	1.35	0.250	0.076	13.0	3.95
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	0.442	0.141	0.095	0.031	5.26	1.98
Sample Variance	0.195	0.020	0.009	0.001	27.6	3.94
Kurtosis	0.859	0.256	2.51	3.71	3.54	4.91
Skewness	1.11	0.520	1.49	1.59	1.69	1.99
Range	1.69	0.588	0.415	0.147	23.8	9.21
Minimum	3.37	1.12	0.141	0.035	7.44	2.05
Maximum	5.06	1.71	0.555	0.182	31.2	11.3
Sum	113	40.0	7.53	2.32	395	124
Count	29	29	29	29	29	29
Confidence Level (95%)	0.161	0.051	0.034	0.011	1.91	0.722

Reach 6

	U233/234 (pCi/L)		U235 (pCi/L)		U238 (pCi/L)	
	mean	median	mean	median	mean	median
Mean	10.2	0.104	0.938	0.006	37.9	0.922
Standard Error	3.09	0.002	0.197	0.000	10.5	0.029
Median	10.2	0.103	0.707	0.006	37.9	0.293
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	16.7	0.011	1.06	0.002	56.8	0.155
Sample Variance	278	0.0001	1.12	0.0000	3226	0.024
Kurtosis	16.8	1.57	9.50	3.86	11.1	5.33
Skewness	3.76	0.723	2.91	1.68	3.10	2.14
Range	89.3	0.052	5.10	0.012	281	0.734
Minimum	2.10	0.083	0.094	0.002	5.30	0.139
Maximum	91.4	0.135	5.20	0.014	287	0.873
Sum	424	3.02	27.2	0.176	1430	9.33
Count	29	29	29	29	29	29
Confidence Level (95%)	6.06	0.004	0.386	0.001	20.7	0.056

Table 5 26B
Statistical Summary of Group 4 30 Year Simulation
Sediment Associated Quality

Reach 3		U233/234 (pCIVG)		U235 (pCIVG)		U238 (pCIVG)	
		<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>		
Mean		1 50	1.53	0 294	0.300	15 8	16.1
Standard Error		0 011	0 010	0 002	0 002	0 114	0 104
Median		1 51	1 54	0 296	0 302	15 9	16 2
Mode		n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation		0 058	0 053	0 011	0 010	0 615	0 560
Sample Variance		0 003	0 003	0 000	0 000	0 379	0 314
Kurtosis		1 04	0 726	1 04	0 73	1 04	0 726
Skewness		0 063	0 236	0 063	-0 236	0 063	0 236
Range		0 204	0 193	0 040	0 038	2 15	2 03
Minimum		1 40	1 44	0 275	0 282	14 8	15 1
Maximum		1 61	1 63	0 315	0 320	16 9	17 2
Sum		43 4	44 3	8 53	8 70	458	467
Count		29	29	29	29	29	29
Confidence Level (95%)		0 021	0 019	0 004	0 004	0 224	0 204

Reach 4		U233/234 (pCIVG)		U235 (pCIVG)		U238 (pCIVG)	
		<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>		
Mean		1.22	1.26	0.240	0.247	12.9	13.3
Standard Error		0 012	0 012	0 002	0 002	0 130	0 131
Median		1 23	1 27	0 242	0 249	13 0	13 3
Mode		n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation		0 067	0 067	0 013	0 013	0 701	0 706
Sample Variance		0 004	0 004	0 000	0 000	0 492	0 498
Kurtosis		-0 72	-0 066	0 72	-0 07	-0 72	0 066
Skewness		-0 033	0 054	0 033	0 054	-0 033	0 054
Range		0 256	0 278	0 050	0 055	2 69	2 93
Minimum		1 10	1 13	0 215	0 222	11 6	11 9
Maximum		1 35	1 41	0 266	0 276	14 3	14 8
Sum		35 5	36 5	6 96	7 16	374	385
Count		29	29	29	29	29	29
Confidence Level (95%)		0 024	0 024	0 005	0 005	0 255	0 257

Table 5 26B (Continued)

Reach 5

	U233/234 (pCIVG)		U235 (pCIVG)		U238 (pCIVG)	
	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>		
Mean	3.65	3.35	0.128	0.143	6.86	7.70
Standard Error	0.048	0.044	0.002	0.002	0.116	0.108
Median	3.69	3.37	0.128	0.145	6.86	7.77
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	0.260	0.234	0.012	0.011	0.627	0.583
Sample Variance	0.067	0.055	0.000	0.000	0.393	0.340
Kurtosis	0.007	0.689	0.594	-0.244	0.551	0.264
Skewness	-0.548	-0.196	0.492	-0.254	0.482	0.268
Range	1.06	0.848	0.052	0.045	2.77	2.39
Minimum	2.99	2.90	0.108	0.120	5.80	6.42
Maximum	4.06	3.75	0.160	0.164	8.57	8.81
Sum	106	97.0	3.71	4.16	199	223
Count	29	29	29	29	29	29
Confidence Level (95%)	0.094	0.085	0.004	0.004	0.228	0.212

Reach 6

	U233/234 (pCIVG)		U235 (pCIVG)		U238 (pCIVG)	
	<i>mean</i>	<i>median</i>	<i>mean</i>	<i>median</i>		
Mean	0.866	0.861	0.167	0.170	9.05	9.07
Standard Error	0.007	0.006	0.001	0.001	0.069	0.059
Median	0.866	0.869	0.169	0.170	9.05	9.11
Mode	n/a	n/a	n/a	n/a	n/a	n/a
Standard Deviation	0.037	0.030	0.007	0.006	0.369	0.319
Sample Variance	0.001	0.001	0.000	0.000	0.136	0.102
Kurtosis	0.016	-0.001	0.028	-0.024	0.028	-0.024
Skewness	-0.797	-0.432	0.835	-0.425	-0.835	0.424
Range	0.134	0.125	0.024	0.025	1.30	1.32
Minimum	0.775	0.790	0.152	0.155	8.14	8.32
Maximum	0.91	0.915	0.176	0.180	9.44	9.64
Sum	25.0	25.0	4.85	4.90	260	263
Count	29	29	29	29	29	29
Confidence Level (95%)	0.013	0.011	0.003	0.002	0.134	0.116

Table 5-27A

Fugitive Dust Model OU 5 Area Sources for Radionuclides

Source number	x coordinate of center (meters)	y coordinate of center (meters)	x dimension of rectangle (meters)	y dimension of rectangle (meters)	height of emission (meters)	angle of rotation	No of samples	Radionuclide levels (pCi/g)				
								Am 241	Pu 239/240	U 233/234	U 235	U 238
1	24 958 40	14 569 32	142 28	97 45	0	52 76	18	0 023	0 096	12 322	2 505	106 938
2	24 967 69	14 601 44	7 62	7 62	0	0	1	0 19 (0)	0 13 (0)	2 800	670	38 000
3	24 754 33	14 492 30	15 24	15 24	0	0	1	0 084	0 009	200	46	2 000
4	24 265 27	14 487 14	392 88	192 02	0	0	17 22	0 02	0 06	7 19	0 39	27 23
5	24 535 63	14 506 80	147 84	78 94	0	0	17 22	0 02	0 06	7 19	0 39	27 23

Source of sample results DOE 1994a RFEDS

Table 5-27B

Fugitive Dust Model OU 5 Area Sources for Organic Chemicals of Concern

Source number	x coordinate of center (meters)	y-coordinate of center (meters)	x dimension of rectangle (meters)	y dimension of rectangle (meters)	height of emission (meters)	angle of rotation	No of samples	Arochlor 1254	Contaminant levels (ug/g)			
									Benzo(a) anthracene	Benzo(b) fluoranthene	Benzo(a) pyrene	
1	24925 23	14569 03	201 17	201 17	0	0	15 36	7 13E 01	6 75E 01	7 57E 01	5 20E 01	
2	25009	14568	7 62	7 62	0	0	0-1	0	4 50E01	4 90E01	4 30E01	
3	24917	14568	7 62	7 62	0	0	0-1	0	0	0	0	
4	24887	14507	7 62	7 62	0	0	0-1	0	0	0	0	
5	24398 17	14482 19	402 34	100 58	0	5 36	0 9	0	0	6 92E 03	8 28E 02	

Source of sample results DOE 1994a RFEDS

Table 5-27B (Continued)

Source number	x coordinate of center (meters)	y coordinate of center (meters)	x dimension of rectangle (meters)	y dimension of rectangle (meters)	height of emission (meters)	angle of rotation	No of samples	Contaminant levels (ug/g)				
								Dibenzo (a h) anthracene	Fluor anthene	Indeno (1 2 3 c d) pyrene	Pyrene	
1	24 925 23	14 569 03	201 17	201 17	0	0	15 36	2 71E 01	8 37E 01	3 00E 01	1 02E00	
2	25 009	14 568	7 62	7 62	0	0	0 1	7 00E00	1 40E02	3 2E01	1 20E02	
3	24 917	14 568	7 62	7 62	0	0	0-1	1 10E00	1 20E01	3 10E00	0	
4	24 887	14 507	7 62	7 62	0	0	0 1	0	0	0	0	
5	24 398 17	14 482 19	402 34	100 58	0	5 36	0 9	1 11E 02	8 10E 02	1 161E 02	9 40E 02	

Source of sample results DOE 1994a RFEDS

Table 5-27C

Fugitive Dust Model OU 5 Area Sources for Metals Chemicals of Concern

Source number	x coordinate of center (meters)	y-coordinate of center (meters)	x dimension of rectangle (meters)	y dimension of rectangle (meters)	height of emission (meters)	angle of rotation	No of sample s	Contaminant levels (mg/g)			
								Copper	Mercury	Silver	
1	24925 23	14569 03	201 17	201 17	0	0	20 36	3 15E 02	1 32E 04	1 05E 03	
2	25009	14568	7 62	7 62	0	0	0 1	0	0	0	
3	24917	14568	7 62	7 62	0	0	0-1	0	0	0	
4	24887	14507	7 62	7 62	0	0	0-1	0	0	1 26E 02	
5	24398 17	14482 19	402 34	100 58	0	5 36	10	1 62E 02	7 10E 05	1 53E 03	

Source of sample results DOE 1994a RFEDS

Table 5 28

**Fugitive Dust Model OU 5 Source Input Parameters
Particle Size Distributions and Densities**

Particle size class	Grain size distribution (Percent finer by weight)	Particle size distribution (Fraction within 100 μm range)	Particle density (g/cm^3)
$\leq 10 \mu\text{m}$	19	0.500	1.385
$\leq 30 \mu\text{m}$	28	0.237	
$\leq 100 \mu\text{m}$	38	0.263	

Source DOE 1994a

Table 5 29**Fugitive Dust Model OU 5 Source Multipliers and
Orders of Magnitude of Output Results**

Radionuclide Constituent	Source multiplier	Order of magnitude of output results (pCi/m ³ for concentration pCi/m ² s for deposition)
Uranium 233/234	E+01	E 07
Uranium 235	E+01	E 07
Uranium 238	E 01	E 05

Organic Constituent	Source multiplier	Order of magnitude of output results (ug/m ³ for concentration ug/m ² s for deposition)
Aroclor 1254	E+03	E 09
Benzo(a)anthracene	E+03	E 09
Benzo(a)pyrene	E+03	E 09
Benzo(b)fluoranthene	E+03	E 09
Dibenzo(a h)anthracene	E+03	E 09
Fluoranthene	E+03	E 09
Indeno(1 2 3 c d)pyrene	E+03	E 09
Pyrene	E+03	E 09

Metal Constituent	Source multiplier	Order of magnitude of output results (mg/m ³ for concentration mg/m ² s for deposition)
Copper	E+03	E 09
Mercury	E+05	E 11
Silver	E+05	E 11

Table 5 30

Fugitive Dust Model Determination of Card 14A Input Parameters for Americium 241

Wind erosion potential equation $P(u) = 58(u - u_1)^2 / 25(u - u_1)$ where friction velocity $u = 0.062 \times 10\text{-m wind speed } u$ threshold friction velocity $u_1 = 1.17 \text{ m/s}$				Coefficients in wind erosion potential equation $P(u)$	
				0 222952	50 1462
Divide coefficients in $P(u)$ equation by 3 600 s/hr to obtain coefficients for hourly emission rate equation, E_{PM}				Coefficients in fugitive particulate matter emission rate equation E_{PM}	
				6 19311E 05	1 39295E 02
Multiply coefficients in E_{PM} equation by a selected multiplier (Table GM 5 5 3) for Am 241 1 00E+04				Coefficients in fugitive particulate matter emission rate equation E_{PM}	
				6 19311E 01	1 39295E+02
Coefficients in contaminant emission rate equation $E_{cont m i}$ Card 14A coefficients					
Source number	Americium 241 concentration in soil (pCi/g)	G_1	G_2	G_3	
1	2 30E 02	1 42442E 02	4 38574E 01	3 20379E+00	
2	0 00E+00	0 00000E+00	0 00000E+00	0 00000E+00	
3	8 40E 02	5 20221E 02	1 60175E+00	1 17008E+01	
4	2 00E 02	1 23862E 02	3 81369E 01	2 78590E+00	
5	2 00E 02	1 23862E 02	3 81369E 01	2 78590E+00	

Table 5-31A**Fugitive Dust Model Near Group Receptors for
Area Sources of Radionuclides**

Receptor number	Description	x-coordinate (meters)	y-coordinate (meters)
1	East of Sources 1 & 2	25 040 30	14 666 03
2	East of Sources 1 & 2	25 040 30	14 635 55
3	East of Sources 1 & 2	25 040 30	14 605 07
4	East of Sources 1 & 2	25 040 30	14 574 59
5	East of Sources 1 & 2	25 040 30	14 544 11
6	East of Sources 1 & 2	25 040 30	14 513 63
7	East of Sources 1 & 2	25 040 30	14 483 15
8	East of Source 3	24 767 90	14 592 64
9	East of Source 4	24 461 94	14 576 85
10	East of Source 4	24 461 94	14 546 37
11	East of Source 4	24 461 94	14 515 89
12	East of Source 4	24 461 94	14 485 41
13	East of Source 4	24 461 94	14 454 93
14	East of Source 4	24 461 94	14 424 45
15	East of Source 4	24 461 94	14 393 97
16	East of Source 5	24 601 01	14 576 85
17	East of Source 5	24 601 01	14 546 37
18	East of Source 5	24 601 01	14 515 89
19	East of Source 5	24 601 01	14 485 41
20	East of Source 5	24 601 01	14 454 93
21	East of Source 5	24 601 01	14 424 45
22	East of Source 5	24 601 01	14 393 97
23	OU5 Sampler 102	23 781 61	14 580 18
24	OU5 Sampler 100	25 131 49	14 537 28
25	OU5 Sampler 101	24 642 66	14 489 62

Table 5-31B**Fugitive Dust Model Near Group Receptors For
Area Sources of Organic and Metal Constituents**

Receptor number	Description	x coordinate (meters)	y coordinate (meters)
1	East of Sources 1 2 3&4	25 026 81	14 690 37
2	East of Sources 1 2 3&4	25 026 81	14 659 89
3	East of Sources 1 2 3&4	25 026 81	14 629 41
4	East of Sources 1 2 3&4	25 026 81	14 598 93
5	East of Sources 1 2 3&4	25 026 81	14 568 45
6	East of Sources 1 2 3&4	25 026 81	14 537 97
7	East of Sources 1 2 3&4	25 026 81	14 507 49
8	East of Sources 1 2 3&4	25 026 81	14 477 01
9	East of Sources 1 2 3&4	25 026 81	14 446 53
10	East of Source 5	24 603 15	14 572 82
11	East of Source 5	24 603 15	14 542 34
12	East of Source 5	24 603 15	14 511 86
13	East of Source 5	24 603 15	14 481 38
14	East of Source 5	24 603 15	14 450 90
15	East of Source 5	24,603 15	14,420 42

Table 5-31C**Fugitive Dust Model OU 5 "Grid Group Receptors**

Receptor number	Description	x coordinate (meters)	y-coordinate (meters)
1	Grid receptor	24 079	13 716
2	Grid receptor	24 079	14 021
3	Grid receptor	24 079	14 326
4	Grid receptor	24 384	13 716
5	Grid receptor	24 384	14 021
6	Grid receptor	24 384	14 326
7	Grid receptor	24 384	14 630
8	Grid receptor	24 689	13 716
9	Grid receptor	24 689	14 021
10	Grid receptor	24 689	14 326
11	Grid receptor	24 689	14 630
12	Grid receptor	24 994	13 716
13	Grid receptor	24 994	14 021
14	Grid receptor	24 994	14 326
15	Grid receptor	24 994	14 630
16	Grid receptor	25 298	13 716
17	Grid receptor	25 298	14 021
18	Grid receptor	25 298	14 326
19	Grid receptor	25 298	14 630
20	Grid receptor	25 603	13 716
21	Grid receptor	25 603	14 021
22	Grid receptor (maximum AOC3 receptor)	25 603	14 326
23	Grid receptor	25 908	13 716
24	Grid receptor	25 908	14 201
25	Grid receptor	25 908	14 326
26	Grid receptor	26 213	13 716
27	Grid receptor	26 213	14 201
28	Grid receptor	26 213	14 326

Table 5 31C (Continued)

29	Grd receptor	26 213	14 630
30	Grd receptor	26 518	14 021
31	Grd receptor	26 518	14 326
32	Grd receptor	26 518	14 630
33	Grd receptor	26 822	14 021
34	Grd receptor	26 822	14 326
35	Grd receptor	26 822	14 630
36	Grd receptor	27 127	14 326
37	Grd receptor	27 127	14 630
40	RAAMP sampler 13	25 039 05	14 700 44
41	RAAMP sampler 14	24 608 47	14 774 94
42	RAAMP sampler 23	25 611 67	14 536 11
43	RAAMP sampler 32	22 250	15 621
44	RAAMP sampler 38	28 624 85	13,949 07

Table 5 32

**Comparison of OU 5 Ambient Air Data with
Fugitive Dust Model Results**

OU5 Sample r	Ambient data +/- error (pCi/m ³)	FDM value (pCi/m ³)
Americium 241		
S102	1 80E 05+/- 0 48E 05	0
S101	1 68E 05+/- 0 56E 05	1 69E 07
S100	1 14E 05+/- 0 37E 05	9 43E 09
Plutonium 239/240		
S102	9 53E 07+/- 7 04E 07	0
S101	1 27E 06+/- 1 23E 06	5 34E 07
S100	0+/- 7 19E 07	3 60E 08
Uranium 233/234		
S102	5 50E 05+/- 2 77E 05	0
S101	8 06E 05+/- 2 75E 05	6 48E 05
S100	9 06E 05+/- 3 02E 05	1 31E 05
Uranium 235		
S102	2 98E 06+/- 6 01E 06	0
S101	5 06E 06+/- 6 67E 06	5 32E 06
S100	5 83E 06+/- 6 74E 06	2 83E 06
Uranium 238		
S102	5 95E 05+/- 2 86E 05	0
S101	7 51E 05+/- 2 59E 05	3 06E 04
S100	7 06E 05+/- 2 58E 05	1 51E 04

Notes

See text Section 5 3 3 5 Verification Ambient data represent the period December 30 1992 through January 26 1993 FDM values represent the period January 1 1993 through January 31 1993

Table 5 33A

Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum Annual (1990) Averages
Radionuclides

Receptor	Uranium 233/234	Uranium 235	Uranium 238
Maximum AOC1 exposure	6 56E-05	1 55E-05	8 78E 04
Maximum AOC2 exposure	6 05E-05	8 28E 06	3 58E-04
Maximum AOC3 exposure	3 65E-06	4 80E-07	2 52E 05

Receptor	Uranium 233/234	Uranium 235	Uranium 238
Maximum AOC1 exposure	4 45E-06	1 06E 06	5 98E 05
Maximum AOC2 exposure	4 54E-06	6 46E-07	2 79E-05
Maximum AOC3 exposure	1 57E-07	2 11E-08	1 11E-06

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits AOC3 is Woman Creek drainage

Table 5-33B

Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum Annual (1990) Averages
Organic Chemicals of Concern

Receptor	Annual average ambient air concentration (ug/m ³)			
	Aroclor 1254	Benzo(a)anthracene	Benzo(b)fluoranthene	Benzo(a)pyrene
Maximum AOC1 exposure	3 78E-06	1 74E-05	1 89E-05	1 60E 05
Maximum AOC2 exposure	0	0	4 00E-08	4 86E-07
Maximum AOC3 exposure	1 61E 07	1 65E-07	1 85E-07	1 41E 07
Receptor	Annual average deposition (ug/m ² s)			
	Aroclor 1254	Benzo(a)anthracene	Benzo(b)fluoranthene	Benzo(a)pyrene
Maximum AOC1 exposure	2 82E-07	1 38E-06	1 05E-06	1 28E 06
Maximum AOC2 exposure	0	0	2 08E-09	3 51E 08
Maximum AOC3 exposure	7 41E-09	7 61E-09	8 54E-09	6 48E-09

Table 5-33B (Continued)

Receptor	Annual average ambient air concentration (ug/m ³)			
	Dibenzo(a h)anthracene	Fluoranthene	Indeno(1 2 3 c d)pyrene	Pyrene
Maximum AOC1 exposure	3 51E 06	4 82E 05	1 15E 05	4 27E 05
Maximum AOC2 exposure	6 50E 08	4 72E 07	9 45E 08	5 59E 07
Maximum AOC3 exposure	6 47E 08	2 43E 07	7 95E 08	2 77E 07

Receptor	Annual average deposition (ug/m ² s)			
	Dibenzo(a h)anthracene	Fluoranthene	Indeno(1 2 3 c d)pyrene	Pyrene
Maximum AOC1 exposure	2 74E 07	3 87E-06	6 36E 07	3 42E 06
Maximum AOC2 exposure	4 68E-09	3 40E-08	4 90E-09	4 03E 08
Maximum AOC3 exposure	2 98E-09	1 12E-08	3 67E-09	1 28E 08

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits AOC3 is Woman Creek drainage

Table 5-33C

**Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum Annual (1990) Averages
Metals Chemicals of Concern**

Receptor	Annual average ambient air concentration (mg/m ³)		
	Copper	Mercury	Silver
Maximum AOC1 exposure	1 70E-07	7 17E 12	5 74E 11
Maximum AOC2 exposure	9 57E 08	4 17E 12	0
Maximum AOC3 exposure	9 49E-09	4 03E 11	2 44E 10

Receptor	Annual average deposition (mg/m ² s)		
	Copper	Mercury	Silver
Maximum AOC1 exposure	1 26E 08	5 3E 13	4 27E 12
Maximum AOC2 exposure	6 90E-09	3 0E 13	0
Maximum AOC3 exposure	4 29E 10	1 82E 12	1 12E 11

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits
AOC3 is Woman Creek drainage

Table 5-34A

**Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum 1990 24 Hour Averages
Radionuclides**

Receptor	Uranium 233/234	Uranium 235	Uranium 238
Maximum AOC1 exposure	2 27E-02	5 41E-03	3 06E 01
Maximum AOC2 exposure	1 86E-02	2 58E 03	1 11E-01
Maximum AOC3 exposure	1 21E-03	1 65E 04	8 63E-03

Receptor	Uranium 233/234	Uranium 235	Uranium 238
Maximum AOC1 exposure	1 54E-03	3 68E 04	2 08E-02
Maximum AOC2 exposure	1 38E-03	1 99E-04	8 56E-03
Maximum AOC3 exposure	5 10E-05	7 14E-06	3 72E-04

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits AOC3 is Woman Creek drainage

Table 5 34B

**Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum 1990 24 Hour Averages
Organic Chemicals of Concern**

Receptor	24 hour average ambient air concentration (ug/m ³)			
	Aroclor 1254	Benzo(a)anthracene	Benzo(b)fluoranthene	Benzo(a)pyrene
Maximum AOC1 exposure	1 18E-03	5 01E-03	5 46E-03	4 60E 03
Maximum AOC2 exposure	0	0	1 26E-05	1 53E-04
Maximum AOC3 exposure	5 65E-05	5 79E-05	6 51E-05	4 92E 05
Receptor	24 hour average deposition (ug/m ² s)			
	Aroclor 1254	Benzo(a)anthracene	Benzo(b)fluoranthene	Benzo(a)pyrene
Maximum AOC1 exposure	8 73E-05	3 92E 04	2 96E 04	3 61E 04
Maximum AOC2 exposure	0	0	6 44E-07	1 09E 05
Maximum AOC3 exposure	2 57E-06	2 64E-06	2 97E-06	2 23E-06

Table 5-34B (Continued)

Receptor	24 hour average ambient air concentration (ug/m)			
	Dibenzo(a h)anthracene	Fluoranthene	Indeno(1 2 3 c d)pyrene	Pyrene
Maximum AOC1 exposure	1 03E-03	1 37E-02	3 28E-03	1 22E 02
Maximum AOC2 exposure	2 04E-05	1 49E-04	2 96E 05	1 75E 04
Maximum AOC3 exposure	2 27E-05	8 51E-05	2 79E 05	9 70E 05

Receptor	24 hour average deposition (ug/m ² s)			
	Dibenzo(a h)anthracene	Fluoranthene	Indeno(1 2 3 c d)pyrene	Pyrene
Maximum AOC1 exposure	7 89E-05	1 09E-03	1 79E 04	9 62E-04
Maximum AOC2 exposure	1 46E-06	1 06E-05	1 51E-06	1 25E-05
Maximum AOC3 exposure	1 03E-06	3 88E-06	1 27E-06	4 41E-06

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits
AOC 3 is the Woman Creek drainage

Table 5-34C

**Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum 1990 24 Hour Averages
Metals Chemicals of Concern**

24 hour average ambient air concentration (mg/m ³)			
Receptor	Copper	Mercury	Silver
Maximum AOC1 exposure	5 31E-05	2 23E-09	1 80E-08
Maximum AOC2 exposure	3 00E-05	1 31E-09	0
Maximum AOC3 exposure	3 25E-06	1 38E-08	8 66E-08
24 hour average deposition (mg/m ² s)			
Receptor	Copper	Mercury	Silver
Maximum AOC1 exposure	3 90E-06	1 64E 10	1 32E-09
Maximum AOC2 exposure	2 14E-06	9 35E 11	0
Maximum AOC3 exposure	1 45E-07	6 13E 10	3 90E-09

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits
AOC 3 is the Woman Creek drainage

Table 5-35A

Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum 1990 1 Hour Averages
Radionuclides

Receptor	Uranium 233/234	Uranium 235	Uranium 238
Maximum AOC1 exposure	1 78E-01	4 26E-02	2 41E00
Maximum AOC2 exposure	6 96E-02	9 51E-03	4 07E 01
Maximum AOC3 exposure	4 89E-03	7 93E-04	4 32E-02

Receptor	Uranium 233/234	Uranium 235	Uranium 238
Maximum AOC1 exposure	1 22E-02	2 92E-03	1 66E-01
Maximum AOC2 exposure	5 25E-03	7 49E-04	3 21E-02
Maximum AOC3 exposure	2 13E-04	3 63E-05	1 98E 03

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits AOC3 is Woman Creek drainage

Table 5 35B

Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum 1990 1 Hour Averages
Organic Chemicals of Concern

Receptor	1 hour average ambient air concentration (ug/m ³)			
	Aroclor 1254	Benzo(a)anthracene	Benzo(b)fluoranthene	Benzo(a)pyrene
Maximum AOC1 exposure	5 58E-03	2 18E-02	2 37E-02	2 02E-02
Maximum AOC2 exposure	0	0	4 73E 05	5 70E 04
Maximum AOC3 exposure	3 57E-04	3 94E-04	4 40E-04	3 14E-04
Receptor	1-hour average deposition (ug/m ² s)			
	Aroclor 1254	Benzo(a)anthracene	Benzo(b)fluoranthene	Benzo(a)pyrene
Maximum AOC1 exposure	4 35E-04	1 76E-03	1 35E-03	1 63E 03
Maximum AOC2 exposure	0	0	2 51E-06	4 16E-05
Maximum AOC3 exposure	1 65E-05	1 82E-05	2 03E-05	1 45E-05

Table 5-35B (Continued)

Receptor	1 hour average ambient air concentration (ug/m ³)			
	Dibenzo(a h)anthracene	Fluoranthene	Indeno(1 2 3 c d)pyrene	Pyrene
Maximum AOC1 exposure	4 28E-03	6 11E-02	1 45E 02	5 39E 02
Maximum AOC2 exposure	7 62E-05	5 55E-04	1 11E-04	6 50E-04
Maximum AOC3 exposure	1 45E-03	6 05E-04	1 93E-04	6 60E-04
Receptor	1 hour average deposition (ug/m ² s)			
	Dibenzo(a h)anthracene	Fluoranthene	Indeno(1 2 3 c d)pyrene	Pyrene
Maximum AOC1 exposure	3 40E-04	4 99E-03	8 27E-04	4 39E 03
Maximum AOC2 exposure	5 56E-06	4 05E-05	5 88E-06	4 74E-05
Maximum AOC3 exposure	6 70E-06	2 80E-05	8 91E-06	3 05E-05

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits
AOC 3 is the Woman Creek drainage

Table 5-35C

**Fugitive Dust Model Results for Selected OU 5 Receptors
Maximum 1990 1 Hour Averages
Metals Chemicals of Concern**

Receptor	1 hour average ambient air concentration (mg/m ³)		
	Copper	Mercury	Silver
Maximum AOC1 exposure	2 46E-04	1 03E 08	8 24E 08
Maximum AOC2 exposure	1 12E-04	4 88E-09	0
Maximum AOC3 exposure	1 59E-05	6 70E-08	5 32E-07

Receptor	1 hour average deposition (mg/m ² s)		
	Copper	Mercury	Silver
Maximum AOC1 exposure	1 92E-05	8 06E 10	6 42E 09
Maximum AOC2 exposure	8 15E-06	3 56E 10	0
Maximum AOC3 exposure	7 34E-07	3 08E-09	2 45E-08

Note Area of Concern 1 (AOC1) is IHSS 115 the old landfill AOC2 is IHSS 133 the ash pits
AOC 3 is the Woman Creek drainage

Table 5-36

Indoor Air Model Input Data Requirements

Johnson Ettinger Equations Symbol Building Characteristic	Units	Range of Values Commercial Office Building
Building size	m ²	557 (464-650)
Basement size	m ²	373 (311-436)
A _B = area of building basement floor and walls below grade	m ²	562 (483-639)
V = building volume	m ³	1 359 (1 113 1 586)
ACH = building air changes per hour	dimensionless	0 5 (0 04 1 5)
Q _{bdg} = building ventilation rate	m ³ /hr	24 000 (680)
X _{crack} = total floor/wall seam perimeter distance	cm	7 730 (7 057-8 350)
Z _{crack} = depth of crack below surface	cm	244
r _{crack} = width of crack	cm	1 9
ΔP = building pressure difference relative to ambient pressure	Pa (10 g/cm s ²)	1 (1 10)
k _v = soil permeability to vapor flow	darcy (10 ⁻⁸ cm ²)	10 (0 01 100)

Sources DOE 1994b EPA, 1992a Johnson and Ettinger 1991 Nihiser pers comm 1993

Table 5-37

**Maximum Concentrations of VOCs
Identified in the IHSS 115 Soil-Gas Survey**

Constituent	Maximum Concentration ($\mu\text{g/L}$)
tetrachloroethene (PCE) (tetrachloroethylene perchloroethylene)	7 6
1 1 1 trichloroethane (TCA)	13 0
trichloroethene (TCE) (trichloroethylene)	28 0

Source DOE 1994a

Table 5-38**Vapor Viscosities of VOCs
Identified in IHSS 115 Soil-Gas Survey**

Constituent	Vapor Viscosity (g/cm s) at temperature
tetrachloroethene (PCE) (tetrachloroethylene perchloroethylene)	0 01932 at 15°C 0 00798 at 30°C
1 1 1 trichloroethane (TCA)	0 00566 at 20°C 0 00532 at 25°C
trichloroethene (TCE) (trichloroethylene)	0 00903 at 15°C 0 00725 at 30°C

Source Dean 1992

Table 5-39

**Results of Indoor Air Modeling for
OU 5 Human Health Risk Assessment**

Constituent	Concentration in Basement Area ($\mu\text{g}/\text{m}^3$)
	Commercial Office Building
tetrachloroethene (PCE) (tetrachloroethylene perchlorethylene)	0 018 (0 0056 0 25)
1 1 1 trichloroethane (TCA)	0 067 (0 021 0 92)
trichloroethene (TCE) (trichloroethylene)	0 23 (0 071 3 2)

6 0 HUMAN HEALTH RISK ASSESSMENT

The human health risk assessment (HHRA) for OU 5 is summarized in this section. The HHRA represents a portion of the BRA associated with the RFI/RI. This section presents the methodology and results of the HHRA.

6 1 INTRODUCTION

6 1 1 Purpose

The purpose of the OU 5 HHRA is to develop a quantitative description and assessment of the human health risks posed by the COCs at OU 5. This HHRA is incorporated in its entirety as part of the BRA for OU 5. The resulting analysis of the human health risks posed by OU 5 responds to and fulfills the requirements of Attachment 2, Section VII D, Interagency Agreement. These agreements among DOE, EPA, and CDPHE require an analysis acceptable to both EPA and CDPHE. Pursuant to this requirement, the method of evaluation is consistent with the EPA RAGS (EPA, 1989).

6 1 2 Scope

This HHRA contains a variety of information pertinent to potential human health risks associated with OU 5. COCs are identified and an exposure assessment links the COCs to potentially exposed receptors through current or future land uses and the associated exposures. COC intakes are calculated, compared with EPA guidance, and potential health risks are estimated. Uncertainty analysis is then performed on the evaluations and results are documented.

6 1 3 Delineation of OU 5 Contaminant Source Areas

A source area is defined as an IHSS or group of IHSSs where concentrations or activities of potential chemicals of concern (PCOCs) in any medium exceed an upper bound estimate of the background range. The upper bound estimate of the background range for metals and radionuclides is defined as the background mean plus two standard deviations. All detected organics are considered to be above background levels.

Six OU 5 source areas were agreed to by EPA CDPHE and DOE and are listed below and generally coincide with the OU 5 IHSSs with the exception of IHSS 209. IHSS 209 is not considered a source area because only calcium exceeded the criterion of the mean plus two standard deviations. In addition, calcium is an essential nutrient with no applicable or relevant and appropriate requirements (ARARs) available. The six physical areas are largely determined by the extent of the potential contamination and are

- (1) IHSS 115/196 Source Area. This source area includes the area of IHSS 115 (the Original Landfill) and IHSS 196 (the Filter Backwash Pond). It also includes the additional area of a small margin around IHSS 115 to include associated data points.
- (2) IHSS 133 Source Area. This source area includes the area encompassing all of the 133 IHSSs. This includes the Ash Pits (IHSS 133 1, 133 2, 133 3, and 133 4), the Incinerator (IHSS 133 5), and the Concrete Wash Pad (IHSS 133 6).
- (3) Surface Disturbance South of IHSS 133 Source Area. This source area is located approximately 1000 feet south of the ash pits (IHSS 133) and includes areas of former excavations and associated surface soil sampling locations.
- (4) SID and Pond C 2 Source Area. This source area includes the SID up to the Original Landfill (IHSS 115) boundary and the C 2 pond (IHSS 142 11). The SID terminates into Pond C 2.
- (5) Surface Disturbance West of IHSS 209 Source Area. This source area includes the Surface Disturbance area located approximately 1150 feet west of IHSS 209.
- (6) Woman Creek and Pond C 1 Source Area. This source area includes Woman Creek to the west boundary of the OU 5 study area and the C 1 pond (IHSS 142 10) located along the Woman Creek drainage.

6.1.4 Determination of OU 5 Areas of Concern

AOCs are defined as one or several source areas that are in close proximity and can be evaluated as a unit in the HHRA. Of the six source areas identified in OU 5, the IHSS 115/196 Source Area and the IHSS 133 Source Area are generally physically separated and are treated individually as AOCs. The SID and Pond C 2 Source Area and the Woman Creek and Pond C 1 Source Areas are interrelated and are treated together as one AOC.

The source area south of IHSS 133 did not exceed the CDPHE risk based conservative screen criterion and therefore is not considered an AOC. The source area west of IHSS 209 slightly exceeded the CDPHE conservative screen criterion due to plutonium 239/240 in one surface soil sample. The remaining samples are significantly less than the risk based concentration (RBC) and subsequent sampling was not able to reproduce the plutonium 239/240 concentration that exceeded the CDPHE conservative screen

Because the criterion was only slightly exceeded and due to a single sample of one PCOC this source area is not identified as an AOC

In summary the OU 5 AOCs are shown in Figure 6.1 and are identified as

- AOC number 1 is identical to the IHSS 115/196 Source Area
- AOC number 2 is identical to the IHSS 133 Source Area
- AOC number 3 contains the SID Pond C 1 and Pond C 2 and Woman Creek Source Areas

6.1.5 Chapter Organization

This HHRA is divided into nine sections. Section 6.1 provides a brief introduction, purpose, scope, OU description, data aggregation, and report organization. It also identifies the OU 5 source areas and AOCs. Section 6.2 presents the COC methodology and its application in the identification and selection of COCs. Section 6.3 provides a description of how scenarios and pathways are identified and selected for quantitative analysis. It discusses each current and future land use and potential receptors that could be exposed to the COCs in the context of the land uses. Section 6.4 presents pathway specific information such as intake equations, modeling data and exposure factors and concentrations and resulting receptor intakes. Section 6.5 presents the COC toxicity information including carcinogenic and noncarcinogenic effects. Section 6.6 provides the methodology and application of combining the results of the exposure assessment and the toxicity assessment. It includes the numerical estimates by scenario and receptor of potential health effects and the OU 5 uncertainty analysis. Section 6.7 presents a summary of the entire HHRA.

6.2 CHEMICALS OF CONCERN IDENTIFICATION

The HHRA evaluates potential human health risks for applicable receptors under current and potential future land use conditions, assuming no remedial action takes place at OU 5. COCs are metals or radionuclides whose concentration or activity statistically exceeds background concentrations or activities, and organic compounds that are not naturally occurring but that could pose a human health risk under the assumed exposure conditions. COCs are identified on an OU wide basis for each medium (e.g., groundwater and soil) through which exposure to chemicals could occur. The identification of COCs will

also help focus the efforts of environmental transport modeling description of the nature and extent of contamination and remedy selection

6 2 1 Selection Process for Chemicals of Concern

COCs are selected at OU 5 for surface soil subsurface soil groundwater surface water seep water pond sediment, seep sediment and stream sediment. These media were sampled during the Phase I RFI/RI in accordance with the OU 5 Work Plan as amended (DOE 1992a) COCs are identified on an OU wide basis by pooling analytical results for samples collected from the various sampling locations for each medium

The process for selection of COCs is shown in Figure 6 2 and includes the following elements

- evaluation of data
- comparison to background concentrations
- application of professional judgement
- elimination of essential nutrients and major ions
- evaluation of detection frequency
- concentration/toxicity screen
- evaluation of risk based concentrations for infrequently detected analytes and identification of special-case COCs

6 2 2 Evaluation of Data

The preliminary step in the process for selection of COCs is the evaluation of analytical data for samples collected from each environmental medium Analytical data from environmental samples collected during the OU 5 field sampling program and the sitewide sampling programs were used to characterize potential contamination at OU 5 The samples used in this evaluation were collected between October 1992 and November 1993 however sampling is ongoing as data gaps are identified. The number of samples sampling locations and other features of the sampling and analytical program are discussed in the OU 5 Work Plan (DOE 1992a) various TMs and summarized in TM15 (DOE 1994a) Samples were collected from the following media

- surface soil
- subsurface soil
- groundwater
- surface water
- seep water
- pond sediment
- seep sediment
- stream sediment

The data set is described in Appendix A of TM11 (DOE 1995a) and was used to determine the OU 5 PCOCs. These data are also described in Section 4.0. The COC selection process is intended to identify the chief environmental constituents in each medium that could have adverse impacts on public health. The risk assessment focuses on OU 5 constituents that are potentially significant health hazards. Inorganic constituents whose concentrations are below background levels or that are essential nutrients or major ions are excluded from the risk assessment. Organic constituents that would contribute insignificantly to overall risk are identified and discussed in DOE (1995a) but are not included in this quantitative risk assessment.

6.2.3 Comparison to Background Concentrations

The evaluation of analytical data for the development of PCOCs is presented in TM11 (DOE 1995a). Analytical results for metals and radionuclides were compared to background levels derived from data for subsurface soils, groundwater, seeps/springs, and stream sediments reported in the BGCR (DOE 1993a) and from background surface soil samples collected in the Rock Creek area during the 1991 OU 1 Phase III investigation and the 1993 OU 2 Phase II investigation. Metals and radionuclides whose concentrations did not statistically exceed background levels were eliminated from further consideration as PCOCs.

TM11 (DOE 1995a) presents the background comparison methodology in detail and contains summary tables of statistical results for metals and radionuclides in all media. Organic constituents were assumed to be anthropogenic in origin and are not attributable to background; therefore, any organic constituent detected is initially considered a PCOC.

6 2 4 Application of Professional Judgment

The spatial and temporal distribution and the pattern of geochemical characteristics of certain metals and radionuclides identified as being above background levels were carefully evaluated using professional judgement to support a conclusion as to whether these constituents were likely to be naturally occurring or due to environmental contamination. The evaluation and professional judgment are briefly described here and in more detail in TM11 (DOE 1995a) which contains discussions of professional judgement as it was applied to each medium.

Based on the known histories of the OU 5 IHSSs as well as the operational history of the Site, none of the radionuclides identified as PCOCs are eliminated through this process. The primary radionuclides identified as PCOCs, americium 241, plutonium 239/240, and the uranium isotopes, are expected as site contaminants. Much of the spatial and temporal distribution and geochemical characteristics of certain metals in each of the environmental media applicable to OU 5 is based on the information presented in TM15 (DOE 1994a).

6 2 5 Elimination of Essential Nutrients and Major Ions

Calcium, iron, magnesium, potassium, and sodium were eliminated from further consideration as COCs because these constituents are essential nutrients, occur naturally in the environment, and are toxic only at very high doses (EPA 1994d). Anions in groundwater (other than nitrate) were not evaluated. The elimination of essential nutrients and major cations and anions is applied to all applicable media in OU 5.

6 2 6 Evaluation of Detection Frequency

PCOCs that were detected at a frequency of greater than five percent were considered potential OU wide COCs. These chemicals were included in concentration/toxicity screens to identify chemicals that could contribute significantly to total risk. Analytes detected at or less than five percent frequency are not considered characteristic of OU wide contamination and the potential for exposure is low. Maximum concentrations of infrequently detected organic constituents and metals were compared to risk based concentrations (1000 X RBC) to identify isolated or highly localized occurrences of high concentrations (i.e., hot spots) that could pose a health risk if routine exposure were to occur as discussed in Section

6 2 8 Chemicals that exceeded the RBC comparison would have been retained as special-case COCs for evaluation in the risk assessment however none of the OU 5 PCOCs exceeded their respective threshold and therefore no special case COCs were retained Because DOE Order 5400.1 (DOE 1990) stipulates the use of all data (except for rejected data) for radionuclides negative values were used as reported and radionuclides were considered to be detected at 100 percent frequency

6 2 7 Concentration/Toxicity Screen

COCs in each medium were selected using separate concentration/toxicity screens for noncarcinogens, carcinogens, and radionuclides. The screens included inorganics that were detected at concentrations or activities greater than background levels and at greater than five percent frequency, and organic chemicals that were detected at greater than five percent frequency. The purpose of applying the screen is to focus the risk assessment on the chief contributors to potential risk. To perform the screen, each PCOC in a medium is scored according to its maximum detected concentration and toxicity to obtain a risk factor. The risk factor for noncarcinogenic effects is the maximum detected concentration divided by the EPA reference dose (RfD) for that analyte. The risk factor for carcinogenic effects (and for radionuclides) is the maximum detected concentration (or activity) multiplied by the EPA cancer slope factor (CSF) for that chemical (or radionuclide). The chemical specific risk factors are summed to calculate total risk factors for the noncarcinogenic and carcinogenic (radioactive and nonradioactive) PCOCs in each medium. The ratio of the risk factor for each PCOC to the total risk factor is called a risk index; the risk index approximates the relative risk associated with each PCOC in the medium. Separate concentration/toxicity screens were performed for carcinogenic and noncarcinogenic effects of organic chemicals and metals and for carcinogenic effects of radionuclides. Several chemicals have both noncarcinogenic and carcinogenic effects and are included in both concentration/toxicity screens. The results of the concentration/toxicity screens are presented in Tables 6.1 through 6.20.

Each PCOC that comprised less than one percent of the total risk factor was not considered a COC for evaluation in the quantitative risk assessment. This approach reduces the number of chemicals to be carried through a risk assessment. However, the approach is conservative (i.e., health protective) because it retains some chemicals that contribute as little as one percent of the total potential risk in that medium. In most cases, only a few chemicals contribute the majority of potential risk in each medium.

TM11 (DOE 1995a) identifies specific toxicity factors for each PCOC and how the factors were used to determine the OU 5 COCs. The toxicity factors that were used in TM11 DOE (1995a) were also used to estimate human health effects in the HHRA.

6.2.8 Evaluation of Risk Based Concentrations for Infrequently Detected Analytes and Identification of Special-Case COCs

As discussed in Section 6.2.6, analytes detected infrequently (in less than five percent of all samples in the medium) are not considered characteristic of OU wide contamination and the potential for exposure is low. These constituents were further screened to include any infrequently detected analyte that could contribute significantly to risk if routine exposure to a hot spot were to occur. In this analysis, maximum measured concentrations were compared to screening levels equivalent to 1000 times RBCs (DOE 1995a). Any infrequently detected analyte measured at a concentration greater than 1000 times the respective RBC would have been identified as representing a potential health risk if exposure were to occur and included in the list of special case COCs for evaluation in the HHRA. Tables 6.21 through 6.24 present the RBC comparisons. As shown by these tables, no special-case COCs were identified by the RBC comparisons. Table 6.25 presents a summary of OU 5 COCs by medium.

6.3 IDENTIFICATION OF SCENARIOS AND PATHWAYS

Potential exposure scenarios and pathways are identified using existing and potential future land uses. The RME is defined as the highest exposure that is reasonably expected to occur at a site according to the EPA's concept of RME (EPA 1989). The term "potential" is used as a reasonable chance of occurrence within the context of the RME scenario. Using this approach, potential exposure routes are evaluated using a CSM. In the CSM, exposure pathways are evaluated by their potential contribution to exposure and classified as significant, insignificant, and negligible or incomplete. Significant pathways are potentially complete pathways that involve relatively direct exposure or only moderately reduced concentrations due to contaminant fate and transport. Insignificant pathways are potentially complete pathways that are expected to result in exposure concentrations one or more orders of magnitude lower than significant exposure pathways. Negligible pathways are potentially complete pathways where either direct exposure is expected to be negligible or fate and transport is expected to reduce contaminant concentrations by several orders of magnitude or more in comparison to significant exposure pathways.

Incomplete pathways are those where the exposure to the potential receptor is expected to be blocked or incomplete. Both significant and insignificant pathways will be evaluated quantitatively.

This section discusses current and future land uses, potential human receptors, and associated scenarios and pathways.

6.3.1 Current and Future Land Use

In general, current land use surrounding the Site includes open space, agricultural, residential, office, gravel mining, and commercial/industrial. Table 6.26 summarizes the current patterns of land use at OU 5 and near the Site; the table also identifies potential future land use. Future land use scenarios are identified as improbable (scenarios that are unlikely to occur) or credible (scenarios that could reasonably occur or are expected to occur). Current and future land uses, both offsite and onsite (OU 5), are discussed in more detail in TM11 DOE (1995b).

Current activities within OU 5 consist of environmental investigations, monitoring, cleanup, and routine security surveillance. The Site operations and maintenance activities are not conducted within OU 5. Future onsite residential and agricultural development is inconsistent with land use plans for the area (RFETS 1995). Future land use would more likely involve industrial complexes at the developed portions of the Site and open space uses in the buffer zone. The portions of OU 5 with suitable topography will also be evaluated further for construction of and subsequent use of an office complex. Thus, onsite use of office facilities and designation of the buffer zone as an ecological preserve and/or open space were considered to be credible future land use scenarios for OU 5 and are consistent with the recommendations of the Rocky Flats Future Site Use Working Group (RFETS 1995).

6.3.2 Evaluation of Potential Human Receptors

Current and future human population groups on and near the site are potential candidates for evaluation (i.e., receptors) based on their likelihood of exposure to site-related COCs. EPA guidance does not require an exhaustive assessment of every potential receptor and exposure scenario (EPA 1992). Rather, the highest potential exposures that are reasonably expected to occur should be evaluated, along with an

assessment of any associated uncertainty (EPA 1989) However all potential receptors have been identified and evaluated to ensure that important exposure pathways or receptors were not overlooked

Potential human receptors on and near the OU 5 study area are current and future residents current and future onsite workers future onsite ecological researchers and future open space receptors (DOE 1995b)

Current and future residents include OU 5 onsite and offsite residential receptors The current and future offsite residential receptor potentially receives exposures of contaminants from the entire plant site and not just OU 5 Because OU 5 contributes only a portion of the potential exposures to this receptor the current and future offsite resident will not be evaluated further in the OU 5 HHRA (DOE 1995b) Future onsite residential development is also inconsistent with future land use plans therefore a future onsite residential receptor will not be evaluated further in the OU 5 HHRA (RFETS 1995)

Current and future OU 5 onsite workers include current onsite security personnel future office complex workers and future construction workers It is assumed that the current onsite security workers will continue to provide security services to the OU 5 study area and that most of the security work will continue to be performed from patrol vehicles Also to be conservative the site specific exposure factors for a current onsite industrial worker will be used for the current onsite security worker Because some OU 5 locations may be suitable for an office complex a future office worker and a future construction worker to build the complex will be evaluated in the OU 5 HHRA

Because it is credible that the OU 5 study area may be preserved as an ecological reserve or as open space a future onsite ecological researcher and a future onsite open space receptor will be evaluated in the OU 5 HHRA

A CSM (Figure 6 3) was used to evaluate potential exposure routes The CSM documents each potential exposure by potential contribution to each human receptor The exposure is classified as significant insignificant, and negligible or incomplete

6 3 3 Receptor Locations and Exposure Areas

For HHRA's conducted at the Site onsite exposures will be evaluated in separate AOCs identified in the OU. A discussion of the OU 5 AOCs is in Section 6 1 4 Determination of OU 5 Areas of Concern. Grids are typically placed over each AOC to define the areas in which a potential receptor can reasonably be expected to come in contact with COCs. Default grid sizes are 10 acres for a residential receptor, 30 acres for an industrial or office worker, and 50 acres for an ecological researcher or open space recreational user. However, the largest AOC identified at OU 5 is AOC 2 with 24.5 acres, and the chosen grid size should be appropriate for the potential receptors. Because a residential receptor is not appropriate, as discussed in Section 6 3 2, the next largest grid size is 30 acres, which is larger than any of the three OU 5 AOCs. Therefore, all applicable receptors will be assessed on an AOC wide basis. This results in calculating and using 95 percent upper confidence limit (UCL) exposure concentrations on an AOC wide basis and using AOC wide modeling results to calculate potential health effects for each applicable receptor in each AOC.

Using chemical sampling data and fate and transport modeling, as appropriate, the exposure point concentrations and activities are used to quantitatively evaluate chemical intakes for potential receptors. Table 6 27 identifies current and future receptors and potentially complete pathways as associated with specific AOCs. Details regarding the selection of the five receptors and their associated pathways can be found in TM12 DOE (1995b).

6 4 EXPOSURE ASSESSMENT

Pathway specific exposures or intakes are quantified through the use of intake equations, exposure parameters, and exposure concentrations. Intake equations are pathway specific, whereas exposure parameters and exposure concentrations are both scenario specific and pathway specific. Depending on the pathway, exposure concentrations may be statistically derived directly from field investigation data, or may be modeled using fate and transport models or estimation techniques. This section first presents exposure concentrations and modeling, followed by exposure factors, intake equations, and then the resulting intakes.

6 4 1 Exposure Concentrations and Modeling

Where appropriate measured chemical specific concentrations in surface soil subsurface soil groundwater seep water and seep sediment were used to calculate 95% UCLs. The method used to calculate 95% UCLs is consistent with the EPA guidance *Calculating the Concentration Term for Risk Assessment* (EPA 1994a). Concentrations of COCs suspended in air were estimated using an air dispersion model (Fugitive Dust Model) and are discussed in detail in Section 5 3 3. Groundwater and surface water modeling are discussed in Section 5 3 1 and Section 5 3 2 respectively. Concentrations for each COC have been calculated separately for each of the three AOCs and are used to calculate separate intakes. Tables 6 28 through 6 30 present chemical specific concentrations in AOC1 AOC2 and AOC3 that were used to calculate OU 5 intakes.

Concentrations for each COC to be used in the risk assessment were calculated using the method consistent with EPA's *Calculating the Concentration Term for Risk Assessment*, (EPA 1994a). Where numerous groundwater and surface water samples were taken at the same sampling location over a period of time these concentrations were averaged and then the averages were used in the equations to calculate the respective 95% UCLs. Also based on EPA guidance (EPA 1992c) all UCLs were calculated assuming lognormal distributions of the data populations. The specific cases where this approach was not appropriate are discussed below.

The groundwater sample sizes in AOC1 were small and large variations in concentrations were noted. Therefore the calculated 95% UCLs were not appropriate and maximum measured concentrations were conservatively used. Sample sizes for seep water and seep sediments in AOC1 were also small and not appropriate for calculating 95% UCLs therefore maximum concentrations were used.

Only one well in AOC2 was available for sampling of groundwater resulting in a small sample size. Therefore calculating a 95% UCL was not appropriate and the maximum concentrations were used. Sample sizes for seep water and seep sediments in AOC2 were also small and were not appropriate for calculating 95% UCLs therefore maximum concentrations were used.

Two wells in AOC3 were available for sampling groundwater and there was a small sample size therefore calculating 95% UCLs was not appropriate and maximum concentrations were used. Stream sediment

Two wells in AOC3 were available for sampling groundwater and there was a small sample size therefore calculating 95% UCLs was not appropriate and maximum concentrations were used. Stream sediment samples of americium 241 and plutonium 239/240 were small and therefore the 95% UCL concentrations are not appropriate. For these two COCs in AOC3 stream sediment the maximum concentrations were used.

6.4.2 Exposure Factors and Intake Equations

The Rocky Flats Site Specific Exposure Factors for Quantitative Human Health Risk Assessment were used in the intake equations and are found in Appendix M. The appropriate exposure factors and chemical concentrations are incorporated into the intake equations in Sections 6.4.2.1 through 6.4.2.6 to calculate respective receptor COC intakes.

6.4.2.1 Incidental Ingestion of Soil, Sediment, and Dust

Receptor intakes may result from incidental ingestion of COCs in soil, sediment, and dust. The following equation is used to calculate the intake:

$$\text{Intake (mg/kg day)} = \frac{CS \times IR \times CF \times FI \times ME \times EF \times ED}{BW \times AT}$$

Where

CS	= Chemical concentration in soil, sediment or dust (mg/kg or pCi/g)
IR	= Ingestion rate (mg/day)
CF	= Conversion factor (10^{-6} kg/mg)
ME	= Matrix effect in GI tract (unitless)
FI	= Fraction ingested from contaminated source (unitless)
EF	= Exposure frequency (days/year)
ED	= Exposure duration (years)
BW	= Body weight (kg)
AT	= Averaging time (days)

For calculation of radionuclide intakes, the concentration is expressed in pCi/g and the expression is not divided by body weight and averaging time. The intake for radionuclides is expressed in pCi. The chemical specific matrix effects are found in Table 6.3.1.

6 4 2 2 Inhalation of Airborne Contaminants

Airborne contaminants associated with complete pathways at OU 5 are in the particulate form. Dermal absorption of contaminants that may be in the vapor phase is considered to be negligible in proportion to inhalation intakes and therefore is disregarded in accordance with RAGS (EPA 1989a). The following equation is used to estimate inhalation intakes:

$$\text{Intake (mg/kg day)} = \frac{\text{CA} \times \text{IR} \times \text{RF} \times \text{RDF} \times \text{ET} \times \text{EF} \times \text{ED}}{\text{BW} \times \text{AT}}$$

Where

CA	= Contaminant concentration in air (mg/m ³ or pCi/m ³)
IR	= Inhalation rate (m ³ /hour)
RF	= Respirable fraction (unitless)
RDF	= Respiratory deposition factor (unitless)
ET	= Exposure time (hours/day)
EF	= Exposure frequency (days/year)
ED	= Exposure duration (years)
BW	= Body weight (kg)
AT	= Averaging time (days)

For calculation of intakes from inhalation of particulates, only the fraction of the particulate concentration in air that is considered to be respirable (<10 μm) is evaluated. Air dispersion modeling performed for OU 5 considered particle size and therefore the air concentrations are the respirable particulates only. The respirable fraction parameter for inhalation of airborne contaminants at OU 5 is therefore always 1.0. The respiratory model developed by the International Commission on Radiological Protection indicates that particles with sizes above 10 μm are relatively unimportant contributors to internal dose (NCRP 1985). For calculation of radionuclide intakes, the concentration is expressed in pCi/m³ and the expression is not divided by body weight and averaging time. The intake for radionuclides is expressed in pCi.

6 4 2 3 Dermal Contact with Soil and Sediments

The exposure from dermal contact with organic chemicals in soil and sediments is calculated using the following equation which results in an estimate of the absorbed dose (i.e., intake) not the amount of

chemical in contact with the skin Exposure from dermal contact with metals and radionuclides was not estimated due to the low rate of absorption of these constituents

$$\text{Absorbed Dose (mg/kg day)} = \frac{\text{CS} \times \text{CF} \times \text{SA} \times \text{FC} \times \text{AF} \times \text{ABS} \times \text{EF} \times \text{ED}}{\text{BW} \times \text{AT}}$$

Where

CS	= Chemical concentration in soil or sediment (mg/kg)
CF	= Conversion factor (10^{-6} kg/mg)
SA	= Skin surface area available for contact (cm /event)
FC	= Fraction contacted from contaminated source (unitless)
AF	= Soil to skin adherence factor (mg/cm ²)
ABS	= Skin absorption factor (unitless)
EF	= Exposure frequency (events/year)
ED	= Exposure duration (years)
BW	= Body weight (kg)
AT	= Averaging time (days)

6 4 2 4 Ingestion of Surface Water and Suspended Sediment

The equation used to calculate intake from ingestion of contaminated water is presented below

$$\text{Intake (mg/kg day)} = \frac{\text{CW} \times \text{IR} \times \text{ER} \times \text{EF} \times \text{ED}}{\text{BW} \times \text{AT}}$$

Where

CW	= Chemical concentration in water (mg/liter or pCi/liter)
IR	= Inhalation rate (liter/hour)
ER	= Exposure rate (hours/day)
EF	= Exposure frequency (days/year)
ED	= Exposure duration (years)
BW	= Body weight (kg)
AT	= Averaging time (days)

For calculation of radionuclide intakes the concentration is expressed in pCi/liter and the expression is not divided by body weight and averaging time The intake for radionuclides is expressed in pCi

6 4 2 5 Dermal Contact with Surface Water

The equation used for dermal contact with chemicals in surface water is presented below. This equation calculates the actual absorbed dose (i.e., intake versus the amount of chemical that comes in contact with the skin).

$$\text{Absorbed Dose (mg/kg day)} = \frac{\text{CW} \times \text{CF} \times \text{SA} \times \text{PC} \times \text{ET} \times \text{EF} \times \text{ED}}{\text{BW} \times \text{AT}}$$

Where

- CW = Chemical concentration in water (mg/liter)
- CF = Volumetric conversion factor for water (1 liter/100 cm³)
- SA = Skin surface area available for contact (cm²)
- PC = Chemical specific dermal permeability constant (cm/hour)
- ET = Exposure time (hours/day)
- EF = Exposure frequency (days/year)
- ED = Exposure duration (years)
- BW = Body weight (kg)
- AT = Averaging time (days)

The chemical specific dermal permeability constants are found in Table 6-31. Exposure from dermal contact with metals and radionuclides was not estimated due to the low rate of absorption of these constituents.

6 4 2 6 External Radiation Exposure

Radionuclide intakes for external exposure are calculated using the following equation:

$$\text{Intake (pCi/g Year)} = C \times EF \times ED \times (1/\text{Se}) \times \text{Te}$$

Where

- C = Isotope activity (pCi/g)
- EF = Exposure frequency ratio (unitless)
- ED = Exposure duration (years)
- Se = Gamma shielding factor (unitless)
- Te = Gamma exposure factor (unitless)

6 4 3 **Calculated Intakes**

In accordance with EPA guidance calculations are conducted for both central tendency (CT) and RME values for receptor intakes (EPA 1994a). The Rocky Flats site specific exposure factors in Appendix M contain both RME and CT values and were used to calculate intakes. Tables 6-32 through 6-41 document the RME and CT carcinogenic chemical intakes for receptors in AOC1. Tables 6-42 through 6-51 document the RME and CT carcinogenic chemical intakes for AOC2 and Tables 6-52 through 6-55 document the RME and CT carcinogenic chemical intakes for applicable receptors in AOC3. RME and CT noncarcinogenic chemical intakes for receptors in AOC1 are found in Tables 6-56 through 6-67. Tables 6-68 through 6-79 document the RME and CT noncarcinogenic chemical intakes for AOC2 and Tables 6-80 through 6-85 document the RME and CT noncarcinogenic chemical intakes for receptors at AOC3.

6 5 **TOXICITY ASSESSMENT**

Toxicity values are used to characterize potential risk and health effects and this section documents the toxicity constants for the OU 5 COCs. The toxicity constants used in this risk assessment were obtained from several sources but the primary source of information was EPA's Integrated Risk Information System (IRIS) database (EPA 1994c). IRIS contains only those toxicity values that have been verified by EPA's Carcinogenic Risk Assessment Verification Endeavor (CRAVE) Work Groups. The IRIS database is updated monthly and per RAGS (EPA 1989) supersedes all other sources of toxicity information. If the necessary data are not available in IRIS, EPA's most recent issue of Health Effects Assessment Summary Tables (HEAST) is used (EPA 1994b). The HEAST tables are published annually and updated approximately two times per year. HEAST contains a comprehensive listing of provisional risk assessment information that has undergone review and has the concurrence of individual EPA Program Offices but has not had enough review to be recognized as high quality agency wide consensus information (EPA 1994b). Additional sources of information used in this risk assessment include the EPA Environmental Criteria and Assessment Office (ECAO) and guidance from EPA toxicologists.

The COCs identified in TM11 (DOE 1995a) have verified toxicity values available from IRIS or HEAST except for the chemicals that are documented in EG&G Rocky Flats Inc. memo 94 RF 11283 (EG&G 1993c). Table 6-30 provides a summary of the OU 5 COCs and their respective toxicity information that

was used for the risk characterization. Additional detail and references for toxicity values can be found in TM11 (DOE 1995a) and the OU 5 toxicity letter (EG&G 1993c).

The following four sections discuss toxicity assessments specific to noncarcinogenic and carcinogenic chemicals.

6.5.1 Toxicity Assessment for Noncarcinogenic Effects

Potential noncarcinogenic effects will be evaluated in the risk characterization by comparing daily intakes with chronic RfDs developed by EPA. This section provides a definition of an RfD and discusses how it is applied in the risk assessment.

A chronic RfD is an estimate (with uncertainty spanning perhaps an order of magnitude) of the daily exposure that can be incurred during a lifetime without an appreciable risk of a noncancer effect being incurred in human populations, including sensitive subgroups (EPA 1989). The RfD is based on the assumption that thresholds exist for noncarcinogenic toxic effects (e.g., liver or kidney damage). RfDs are typically presented in units of mg/kg-day and are calculated by dividing a dose (representing a no observed adverse effect level or a lowest-observed adverse effect level) at which there are no significant measurable effects produced by an uncertainty or safety factor that typically ranges from 10 to 10,000. Thus, there should be no adverse effects associated with chronic daily intakes at or below the RfD value. Conversely, if chronic daily intakes exceed this threshold level, there is a potential that some adverse noncarcinogenic health effects might be observed in exposed individuals.

RfDs have been derived by EPA for both oral and inhalation exposures. However, in January 1991, EPA decided to replace inhalation RfDs with reference concentrations (RfCs). RfCs are expressed in terms of concentrations in air (mg/m^3) not in terms of dose or mg/kg-day. An RfC may be converted to a corresponding inhaled dose (mg/kg-day) by dividing by 70 kg (an estimated human body weight), multiplying by 20 m^3/day (an assumed human inhalation rate), and adjusting by an appropriate absorption factor (EPA 1994b).

6 5 2 Toxicity Assessment for Carcinogenic Effects

Potential carcinogenic risks are expressed as an estimated probability that an individual may develop cancer from lifetime exposure. This probability is based on projected intakes and chemical specific dose response data or Cancer Slope Factors (CSFs). CSFs and the estimated daily intake of a compound averaged over a lifetime of exposure are used to estimate the incremental risk of an individual exposed to that compound developing cancer. There are two classes of potential carcinogens: nonradioactive and radioactive chemicals. For the purposes of this toxicity assessment, each of these two classes of elements or compounds are discussed separately.

6 5 2 1 Toxicity Assessment for Nonradioactive Chemical Carcinogens

Evidence of chemical carcinogenicity originates primarily from two sources: lifetime studies with laboratory animals and human (epidemiological) studies. For most such chemical carcinogens, animal data from laboratory experiments represent the primary basis for the extrapolation. Effects from exposure to high (i.e., administered) doses are based on laboratory animal bioassay results, whereas effects associated with exposure to low doses of a chemical are generally estimated from mathematical models.

For these nonradioactive chemical carcinogens, EPA assumes a small number of molecular events can evoke changes in a single cell that can lead to uncontrolled cellular proliferation and tumor induction. This mechanism for carcinogenesis is referred to as stochastic, which means that there is theoretically no level of exposure to a given chemical carcinogen that does not pose a small, but finite, probability of generating a carcinogenic response. Because risk at low exposure levels cannot be measured directly, either in laboratory animals or human epidemiology studies, various mathematical models have been proposed to extrapolate from high to low doses.

Consistent with guidance in RAGS (EPA, 1989), PAHs that have been identified as COCs in OU 5 will not be quantitatively evaluated for dermal exposure. RAGS states: It is inappropriate to use the oral slope factor to evaluate the risks associated with dermal exposure to carcinogens such as benzo(a)pyrene, which cause skin cancer through a direct action at the point of application. RAGS also states: Generally only a qualitative assessment of risks from dermal exposure to these chemicals is possible. The PAHs in OU 5

are benzo(a)anthracene benzo(a)pyrene benzo(b)fluoranthene, dibenzo(a,h)anthracene fluoranthene indeno(1 2 3 cd)pyrene and pyrene

Uncertainties in the toxicity assessment for nonradioactive chemical carcinogens are dealt with by classifying each chemical into one of several groups according to the weight-of evidence from epidemiological studies and animal studies Table 6 86 presents specific definitions for weight of evidence

6 5 2 2 Toxicity Constants for Radioactive Chemicals

Extensive literature exists that describes the health effects of radionuclides on humans and animals Intensive research by national and international commissions has established universally accepted limits to which workers and the public may be exposed without clinically detectable effects This literature has resulted in EPA classifying all radioactive chemicals as Group A carcinogens because they emit ionizing radiation which, at high doses has been associated with increased cancer incidence in humans

A fundamental difference between the assessment of potential toxicity associated with exposure to radionuclide and nonradionuclide carcinogens is that CSFs for radionuclides are typically best estimates (mean or median values) rather than upper 95th percentile values Furthermore in the past, risk factors for radionuclides have generally been based on fatalities (i e the number of laboratory animals or people who actually died from cancer) whereas CSFs for nonradiological carcinogens are based on incidence (i e the number of lab animals or people who developed cancer) Finally the CSFs for radionuclides are expressed in different units [i e risk per pCi (pCi⁻¹) rather than mg/kg-day⁻¹]

6 6 RISK CHARACTERIZATION

Risk characterization involves estimating the magnitude of the potential adverse effects of COCs under study and summarizing risks to human health Risk characterization considers the nature and weight-of evidence supporting these risk estimates and the magnitude of uncertainty surrounding those estimates Risk characterization combines the results of the exposure and toxicity assessments to provide numerical estimates of health risk. These estimates are comparisons of exposure levels with RfDs or estimates of the lifetime cancer risk for a given intake The process of characterizing risk includes the following

- Calculating and characterizing cancer risk and potential noncarcinogenic effects
- Conducting qualitative uncertainty analysis and
- Conducting quantitative uncertainty analysis

6 6 1 Calculating and Characterizing Cancer Risk and Noncarcinogenic Effects

To quantify the human health risks the intakes are first calculated for each COC each applicable scenario and each AOC. The CT and RME intakes are calculated based on measured or modeled concentrations and using the methodology documented in the RAGS (EPA 1989) and discussed in Section 6 4 Exposure Assessment, and Section 6 4 3 Calculated Intakes. The specific intakes are then compared to the applicable chemical specific toxicological data discussed in Section 6 5 Toxicity Assessment, and presented in Table 6 41 to determine the potential CT and RME human health risks.

The potential human health risks from each COC are calculated to determine potential carcinogenic effects and to determine potential noncarcinogenic effects. Each of these calculations is discussed in the following sections.

6 6 1 1 Determining Carcinogenic Effects

The following calculations are used to determine carcinogenic effects by obtaining numerical estimates of lifetime cancer risks.

$$RISK = INTAKE \times CSF$$

Where

Risk = Potential lifetime excess cancer risk (unitless)
CSF = Cancer slope factor for chemicals (mg/kg-day)¹ or (pCi)¹
Intake = Chemical intake (mg/kg-day) or (pCi)

Section 6 4 3 Calculated Intakes identifies where specific estimated intakes for each receptor by AOC are found and Table 6 31 presents the CSFs for each applicable COC. Inhalation and ingestion CSFs were used with respective inhalation and ingestion intakes to estimate potential human health risks. The CSF is characterized as an upperbound estimate.

Cancer risks are summed separately across all potential nonradioactive and radioactive chemical carcinogens considered in the risk assessment using the following equation

$$RISK_T = \sum RISK_i$$

Where

$RISK_T$ = Total cancer risk expressed as a unitless probability

$RISK_i$ = Risk estimate for the i th contaminant

This equation is an approximation of the precise equation for combining risks to account for the probability of a receptor developing cancer as a consequence of exposure to two or more carcinogens. As stated in RAGS (EPA 1989) the difference between the precise equation and this approximation is negligible for total cancer risks less than 0.1. This risk summation assumes independence of action by the compounds involved. Some limitations are posed by this approach and are discussed in RAGS (EPA 1989).

Most models for low dose extrapolation produce quantitatively similar results in the range of observable data, but yield estimates that can vary by three or four orders of magnitude at lower doses. Animal bioassay data are not adequate to determine whether any of the competing models are better than the others. In addition, there is no evidence to indicate that the precision of low-dose risk estimates increases through the use of more sophisticated models. Thus, if a carcinogenic response occurs at the exposure level studied, it is assumed that a similar response will occur at all lower doses, unless evidence to the contrary exists.

Tables 6-87 through 6-96 document the risks calculated for AOC1 receptors using RME and CT exposure parameters. Tables 6-97 through 6-106 document risks calculated for AOC2 receptors using RME and CT exposure parameters, and Tables 6-107 through 6-110 document the risks calculated for AOC3 receptors using RME and CT parameters. These tables identify the total calculated risk by receptor, total receptor risk for each COC across all applicable pathways, and total receptor risk for each pathway for all applicable COCs. Point estimates of potential human health risk are discussed further in Section 6.6.2.

6 6 1 2 Determining Noncarcinogenic Effects

Potential health effects associated with exposure to individual noncarcinogenic compounds are evaluated by calculating hazard quotients. A hazard quotient (HQ) is the ratio of the intake rate to the RfD as follows:

$$HQ = \frac{INTAKE}{RfD}$$

Where

HQ = Noncancer hazard quotient
Intake = Chemical intake (mg/kg day)
RfD = Reference dose (mg/kg day)

Chronic RfDs are extracted from IRIS and HEAST and specific values are documented on Table 6 31. Similar to CSFs, the RfDs for inhalation and ingestion are used with respective inhalation and oral intakes.

Hazard Indices (HIs) are the summed hazard quotients for each chemical across the applicable pathways. When the HI exceeds unity, there may be concern for potential human health effects from exposure to noncarcinogenic chemicals. Obviously, any single chemical with an exposure level greater than its toxicity value will cause the HI to exceed unity; however, multiple chemical exposures can also cause the HI to exceed this threshold even if no single chemical exposure exceeds its respective RfD.

Tables 6 111 through 6 122 document the calculated RME and CT HQs and HIs for the applicable receptors in AOC1. Tables 6 123 through 6 134 document the calculated RME and CT HQs and HIs for the applicable receptors in AOC2. Tables 6-135 through 6 140 document the calculated RME and CT HQs and HIs for the applicable receptors in AOC3. The tables identify individual HQs by COC and pathway and provide total HIs by chemical and a total of all HIs by receptor. The point estimates of potential health effects that are documented on these tables are discussed in more detail in Section 6 6 2.

6 6 2 Point Estimates of Risk and Health Effects

Reasonable exposure pathways were evaluated in Section 6 3 Scenario and Pathway Identification, and the risks and HI values for the applicable COCs were summed across these pathways. Consistent with

EPA guidance (EPA 1992b) both RME and CT point estimates for lifetime cancer risk and potential noncarcinogenic health effects were calculated. Additionally, the total carcinogenic risks are documented separately for Class A, B, and C carcinogens as directed by RAGS (EPA 1989). An additional point of reference is provided by adding the total risks for the weight of evidence classifications to arrive at a conservative total risk for each receptor. These risks are expressed in the text using one significant figure per EPA guidance (EPA 1989). For greater detail, the risks estimated in Tables 6-87 through 6-140 are expressed in two significant figures. Noncarcinogenic health effects are expressed as HI values. First, the total HI values were calculated by summing HQ values by receptor without regard for the target organ affected. Because no HI exceeded or approached unity, it was not necessary to sum the HQ values according to target organ. The following sections discuss the results of RME and CT point estimates of lifetime cancer risk and potential noncarcinogenic health effects by receptor.

6.6.2.1 Future Construction Worker

The future construction worker is a potential receptor in AOC1 and AOC2. As discussed in Section 6.3 Scenario and Pathway Identification, the construction worker receptor is not an applicable receptor in AOC3. Total calculated RME risk for this receptor in AOC1 is $4\text{E-}07$ with ingestion of surface soil and exposure to external radiation being the driving pathways and with uranium 238 being the most significant COC (Table 6-87). The construction worker total CT risk in AOC1 is $2\text{E-}07$; the driving pathway is external radiation and uranium 238 is the most significant COC (Table 6-92). The total calculated RME risk for this receptor in AOC2 is $8\text{E-}08$ with ingestion of surface soil contributing the most risk and the most significant COC being uranium 238 (Table 6-97). The construction worker total CT risk in AOC2 is $3\text{E-}08$ with the external radiation pathway and uranium 238 contributing the greatest risk (Table 6-102).

Total RME HI calculated for the construction worker in AOC1 is $0.04\text{E-}02$ and the greatest pathway and COC respectively are ingestion of subsurface soil and Aroclor 1254 (Table 6-111). The total CT HI calculated for this receptor in AOC1 is 0.006 with the greatest contribution from ingestion of subsurface soil and from Aroclor 1254 (Table 6-117). Total RME HI calculated for this receptor in AOC2 is 0.01 with the greatest contributions coming from ingestion of subsurface soil and antimony (Table 6-123). Total CT HI calculated for the construction worker in AOC2 is 0.002 with ingestion of subsurface soil and antimony providing the greatest risk by pathway and COC respectively (Table 6-129).

6 6 2 2 Current Worker (Security Worker)

The current worker receptor is exposed to COCs in AOC1 and AOC2 and not in AOC3. Total RME risk for this receptor in AOC1 is $3E05$ with the greatest contributors being the external radiation pathway and uranium 238 (Table 6 88). The total CT risk for the current worker at AOC1 is $2E-06$ with a driving pathway of external radiation and uranium 238 contributing the most risk (Table 6 93). The total RME risk for this receptor in AOC2 is $4E-06$ with the external radiation pathway and uranium 238 contributing the most risk (Table 6 98). The total CT risk for the current worker in AOC2 is $3E-07$ with the greatest contributing pathway and COC of external radiation and uranium 238 respectively (Table 6 103).

The total RME HI for the current worker at AOC1 is $0.07E-02$ with the driving pathway being dermal absorption of surface soil and the most significant COC being Aroclor 1254 in surface soil (Table 6 112). The total CT HI for this receptor at AOC1 is $0.01E-02$ with dermal absorption the dominant pathway and Aroclor 1254 the dominant COC in soil (Table 6 118). The total RME HI for the current worker at AOC2 is $0.0005E-04$ with the driving pathway being ingestion of surface soil and the most significant COC being copper (Table 6 124). The total CT HI for this receptor at AOC2 is 0.00008 the respective driving pathway and COC are ingestion of surface soil and copper respectively (Table 6 130).

6 6 2 3 Future Ecological Researcher

The future ecological researcher is an applicable receptor in all three AOCs. The RME total risk for this receptor in AOC1 is $1E-06$. The driving pathway is exposure to external radiation and the most significant COC is uranium 238 (Table 6 89). The CT total risk for a future ecological researcher in AOC1 is $7E-07$ with the dominant pathway and COC being external radiation and uranium 238 respectively (Table 6-94). The RME total risk for this receptor in AOC2 is $2E-07$ and the driving pathway is exposure to external radiation and the most significant COC is uranium 238 (Table 6 99). The CT total risk for this receptor in AOC2 is $1E-07$ the respective dominant pathway and COC is external radiation exposure and uranium 238 (Table 6 104). The RME total risk for an ecological researcher in AOC3 is $2E-08$ with a driving pathway of ingestion of pond sediments and the most significant COC is plutonium 239/240 (Table 6 107). The CT total risk for this receptor in AOC3 is $6E-09$ with the respective dominant pathway and COC being ingestion of pond sediments and plutonium 239/240 (Table 6 109).

The RME total HI for the ecological researcher in AOC1 is 0.04 the dominant pathway is dermal absorption of surface soil and the most significant COC is Aroclor 1254 in surface soil (Table 6.113). The CT total HI for this receptor in AOC1 is 0.01 the driving pathway is ingestion of seep sediments and the dominant COC is Aroclor 1254 (Table 6.119). Total RME HI for this receptor in AOC2 is 0.02 with the respective dominant pathway and COC being ingestion of seep sediments and antimony (Table 6.125). The CT total HI for an ecological researcher in AOC2 is 0.004. The driving pathway is ingestion of seep sediments and the dominant COC is antimony (Table 6.131). The RME HI total for this receptor in AOC3 is 0.004 with the driving pathway being ingestion of stream sediments and the driving COC is mercury (Table 6.135). The CT total HI for an ecological researcher in AOC3 is 0.001. The respective dominant pathway and COC is ingestion of stream sediments and mercury (Table 6.138).

6.6.2.4 Future Office Worker

The future office worker is a potential receptor in AOC1 and AOC2 only. As discussed in Section 6.3 Scenario and Pathway Identification, the office worker receptor is not an applicable receptor in AOC3. The total RME risk for this receptor in AOC1 is 3×10^{-5} with the driving pathway being exposure to external radiation and the dominant COC being uranium 238 (Table 6.90). Total CT risk for a future office worker in AOC1 is 2×10^{-6} the respective dominant pathway and COC are external radiation and uranium 238 (Table 6.95). The total RME risk for this receptor in AOC2 is 4×10^{-6} the driving pathway is exposure to external radiation and the dominant COC is uranium 238 (Table 6.100). Total CT risk for this receptor in AOC2 is 3×10^{-7} and the respective dominant pathway and COC are exposure to external radiation and uranium 238 (Table 6.105).

The RME total HI for the future office worker in AOC1 is 0.05. The driving pathway is dermal absorption of surface soil and the dominant COC is Aroclor 1254 in surface soil (Table 6.114). CT total HI for this receptor in AOC1 is 0.007 with the dominant pathway and COC respectively being dermal absorption of surface soil and Aroclor 1254 in surface soil (Table 6.120). The total RME HI for a future office worker in AOC2 is 0.0005. The driving pathway is ingestion of surface soil and the most significant COC is copper (Table 6.126). Total CT HI for this receptor in AOC2 is 0.00004 with the driving pathway and COC respectively of ingestion of surface soil and copper (Table 6.132).

6 6 2 5 Future Open-Space User

Future open space users consist of both adults and children with complete pathways in all three AOCs. Total lifetime cancer risks are estimated for an open space user whereas noncancer hazard indices are calculated separately for adult and child receptors for the soil and sediment ingestion scenarios. The total RME risk for the open space user in AOC1 is $4\text{E-}06$ with respective dominant pathway and COC of exposure to external radiation and uranium 238 (Table 6 91). The total CT risk for this receptor is $4\text{E-}07$ with a driving pathway of external radiation exposure and uranium 238 being the most significant COC (Table 6 96). Total RME risk for this open space receptor in AOC2 is $6\text{E-}07$. The dominant pathway is exposure to external radiation and the dominant COC is uranium 238 (Table 6 101). Total CT risk for an open space user in AOC2 is $6\text{E-}08$ with external radiation exposure being the dominant pathway and uranium 238 the most significant COC (Table 6 106). Total RME risk for this receptor in AOC3 is $4\text{E-}08$. The dominant pathway and COC are ingestion of pond sediments and plutonium 239/240 respectively (Table 6 108). The CT total risk for this adult receptor is $2\text{E-}09$ with the driving pathway being ingestion of pond sediments and the driving COC being plutonium 239/240 (Table 6 110).

The total RME HI for the open space user in AOC1 is 0 01 with a driving pathway of dermal absorption and the most significant COC being Aroclor 1254 in surface soil (Table 6 115). The total RME HI for a child open space receptor in AOC1 is 0 04. The dominant pathway and COC are ingestion of seep sediments and antimony respectively (Table 6 116). The total CT HI for the adult receptor in AOC1 is 0 0009 and the driving pathway and COC are ingestion of seep sediments and antimony respectively (Table 6 121). The total CT HI for a child open space receptor in AOC1 is 0 007. The dominant pathway is ingestion of seep sediments and the most significant COC is antimony (Table 6 122).

The total RME HI for an adult open space receptor in AOC2 is 0 003 with respective dominant pathway and COC being ingestion of seep sediments and antimony (Table 6 127). Total RME HI for this child receptor in AOC2 is 0 03. The driving pathway is ingestion of seep sediments and the most significant COC is antimony (Table 6 128). Total CT HI for an adult receptor in AOC2 is 0 0006 with the dominant pathway being ingestion of seep sediments and antimony being the dominant COC (Table 6 133). The CT total HI for a child open space receptor in AOC2 is 0 005 with the driving pathway of ingestion of seep sediments and the driving COC is antimony (Table 6 134).

The total RME HI for an adult open space user in AOC3 is 0.0008 with respective dominant pathway and COC being ingestion of stream sediments and mercury (Table 6-136). Total RME HI for a child open space receptor in AOC3 is 0.007. The dominant pathway is ingestion of stream sediments and the dominant COC is mercury (Table 6-137). Total CT HI for the adult open space receptor in AOC3 is 0.0002. The driving pathway is ingestion of stream sediments and the most significant COC is mercury (Table 6-139). The CT total HI for the child open space receptor in AOC3 is 0.0004 with respective dominant pathway and COC being ingestion of stream sediments and mercury (Table 6-140).

6.6.3 Uncertainty Analysis

Analysis of uncertainty associated with risk estimates is an important part of the risk assessment process. EPA guidance (EPA 1992b) states that point estimates of risk do not fully convey the range of information considered and used in developing the assessment. The EPA has suggested the use of both RME and CT exposure scenarios in order to provide upper (conservative) and lower (less conservative) bounds on what the actual risk may be. This is an alternative method of portraying the uncertainty inherent in the risk estimates to performing a more time consuming and expensive probabilistic uncertainty analysis. The RME estimates are to be used for risk management decisions but a comparison to the CT estimates provides a good estimation of the uncertainty associated with the decisions. Quantitative probabilistic uncertainty analysis was not performed in this risk assessment. The range between the RME and CT risk estimates is a good indicator of the uncertainty inherent in the RME characterization. Uncertainties identified during the risk assessment process are discussed below.

During the risk assessment process there are essentially four stages of the analysis that can introduce uncertainties. These stages are data collection and evaluation, exposure assessment, toxicity assessment, and risk characterization. The uncertainties within the HHRA are driven by uncertainty in the site investigation data, the likelihood of hypothetical exposure scenarios, the transport models used to estimate concentrations at receptor locations, receptor intake parameters, and the toxicity values used to characterize risk. Uncertainties are also introduced in the risk assessment when exposure to several substances across multiple pathways are summed.

The following sections qualitatively discuss specific uncertainties introduced into the OU 5 HHRA. Table 6-141 summarizes the uncertainties and limitations in this HHRA.

6 6 3 1 POTENTIAL IMPACTS TO HHRA

As discussed in Section 2.2, impacts, if any, that result from the collection of additional data during the TM15 field investigation on the conclusions of the OU 5 HHRA must be assessed. This section discusses an assessment of potential impacts to the HHRA.

Tables 2.3 through 2.10 provide a summary of the results of the analyses of samples collected during the 15 field investigation and those collected during the investigation outlined in the OU 5 Work Plan (DOE 1992a). The information provided on these tables was discussed in Section 2.2 to assist in assessing whether the results of the TM15 field investigation impacted the conclusions of the HHRA. As discussed in Chapters 4.0 and 6.0, the data collected under the OU 5 Work Plan investigation were aggregated by each sample medium on an OU wide basis for comparison to background to identify PCOCs and subsequent COCs. TM11 COCs for HHRA (DOE 1995a) details the background comparison and PCOC and COC determinations. The purpose of this section is to compare the results of the sampling program for each environmental medium sampled under TM15 with the results of the OU 5 Work Plan investigation. It should be recognized that many of the samples collected during the TM15 field investigation were collected for purposes other than for the HHRA (e.g., for characterization of drummed cuttings and fluids). This assessment of the potential for impact to the conclusions of the HHRA was performed to ensure that the results of the HHRA represent the most conservative estimates of risk to human health.

Subsurface Soils Data for subsurface soil samples are provided in Tables 2.3, 2.4, and 2.5 for metals, radionuclides, and organic compounds, respectively. As indicated on Table 2.3, the mean concentration of the combined OU 5 subsurface soil data set (includes samples collected prior to and during the implementation of TM15) for several metals increased significantly relative to the mean concentration calculated previously for the HHRA using only those data collected prior to the implementation of TM15. A significant increase in concentrations could result in a metal that was not previously identified as a COC in being identified as a COC using the larger data set. The apparent increased concentrations of cesium, selenium, thallium, and tin can all be attributed to the increased reporting limits provided in RFEDS for the samples collected during the implementation of TM15 versus those reported for the pre-TM15 samples. Each of these metals was detected at relatively low frequencies; therefore, the increased

reporting limits cause the mean to be skewed toward higher concentrations (for non-detect results one half the reporting limit replaces the result for the calculation of statistics) This represents an apparent, rather than a real increase in concentrations

The mean concentration of lead also increased significantly from that reported previously In addition the maximum concentration of lead detected in subsurface soils increased from 935 mg/kg in the pre TM15 data to 5 200 mg/kg in a sample collected from one of the TDEM anomalies in the IHSS 133 area (Table 2 3) The concentrations of lead detected in subsurface soil samples from IHSS 115 collected during the TM15 field investigation are all within the range of background concentrations As discussed in Section 6 6 3 2 the close association of high lead concentrations with waste material identified during drilling in the ash pits (IHSS 133) indicates that the detected lead is not mobile in the soil or readily available for human intake and lead is not considered a significant contributor to the human health risk associated with OU 5

As indicated on Table 2 4 the mean activities of radionuclides in subsurface soils did not change appreciably from those calculated previously using only the pre TM15 data. The most significant increases in both mean and maximum activities occurred only for the uranium isotopes Each of these isotopes was identified as a COC in the OU 5 HHRA therefore an increase in concentrations would not result in a change in the list of COCs for subsurface soils The mean and maximum concentrations for these isotopes are the same magnitude as those used for the HHRA therefore the risk calculations would not change significantly

The following organic chemicals were detected in higher concentrations in subsurface soil samples collected during the implementation of TM15 than in subsurface soil samples collected prior to TM15 (Table 2 5) bis(2 ethylhexyl)phthalate bromoform, butylbenzyl phthalate chloroform, diethyl phthalate di n octyl phthalate and methylene chloride Of these compounds only bis(2 ethylhexyl)phthalate and methylene chloride were evaluated in the concentration/toxicity screening for the OU 5 HHRA (DOE 1995a) Butyl benzyl phthalate was evaluated by comparison to a risk based concentration (RBC) in DOE (1995a) None of these compounds were determined to be COCs for OU 5 in DOE (1995a)

In order to evaluate whether the concentrations of these organic chemicals detected in samples collected under the TM15 field investigation would impact the conclusions of the HHRA a comparison of the maximum concentration (both detects and nondetects) with the respective RBC was performed (Table 2 14) Although this comparison is usually performed only for those compounds that are detected at a frequency of less than 5 percent it is used here for all of these compounds regardless of detection frequency as an initial indicator of whether the results of the HHRA may need to be reevaluated

As indicated on Table 2 14 the maximum detected and nondetected concentrations for each of these organic chemicals in subsurface soils are significantly less than their respective RBC In addition for bis(2 ethylhexyl)phthalate and methylene chloride the percentage of total risk that would be associated with these chemicals at the maximum detected concentrations shown on Table 2 5 was recalculated for comparison to the concentration/toxicity screens presented in TM11 COCs for the HHRA (DOE 1995a) Even with the increased concentrations both chemicals still represent zero percent of the total risk factor noncarcinogenic and carcinogenic associated with subsurface soils

In summary the subsurface soil data collected during the TM15 field investigation do not indicate that the conclusions of the OU 5 TM11 COCs for the HHRA (DOE 1995a) need to be reevaluated to incorporate these data.

Groundwater. Tables 2 7 through 2 10 present summaries of data for groundwater samples collected during both the original OU 5 Work Plan investigation and during the TM15 field program The following discussions only include data from unfiltered samples (i e total results) for metals and radionuclides because only total concentrations are used in the HHRA

As shown on Table 2 7 the mean concentrations of most metals in the combined OU 5 data set decreased from those calculated for the HHRA using only the data collected under the OU 5 Work Plan investigation For those metals that were previously identified as being COCs this decrease in concentrations could potentially result in one or more of these constituents no longer being identified as a COC However inspection of the data provided on Table 2 7 indicates that, although the mean concentrations for these metals decreased the concentrations are still greater than the range of background concentrations Additionally for all of these metals the highest concentration detected was in samples collected during the original OU 5 Work Plan investigation Because the concentration/toxicity screens

performed to determine COCs for the HHRA use the maximum concentration for each constituent the inclusion of the additional data would not affect the identification of COCs

The mean concentrations of arsenic and thallium in the combined data set are slightly higher than those calculated for samples collected during the OU 5 Work Plan investigation As discussed above for subsurface soils an increase in concentrations has the potential to result in a constituent that was not identified as a COC previously in being identified as a COC using the larger data set. Although the mean concentration for arsenic increased arsenic concentrations in the samples collected during the TM15 investigation are within the range of concentrations reported from the previous sampling program Additionally the increased mean calculated for thallium is the result of the low frequency of detection and the increased reporting limit for this constituent.

As discussed above for total metals in groundwater the mean total activities of most radionuclides in the combined data set also decreased from those calculated using only samples collected during the OU 5 Work Plan investigation (Table 2 9) In all cases the mean activities of those radionuclides identified as COCs decreased slightly and the highest activities reported for OU 5 samples were from samples collected during the OU 5 Work Plan investigation Therefore it is unlikely that the slight decrease in mean activities would result in these radionuclides not being identified as PCOCs and subsequently as COCs using the larger data set

The mean activities for two radionuclides cesium 137 and tritium calculated using the combined data set increased from those calculated using only the data collected under the OU 5 Work Plan investigation Although the mean activities for these radionuclides increased the activities detected in both the OU 5 Work Plan investigation data and the TM15 data are well within the range of background concentrations

The data presented in Table 2 10 indicate that a large number of organic compounds were detected in samples collected during the TM15 field investigation that were either not detected or were detected at lower concentrations in samples from the OU 5 Work Plan investigation These compounds are identified in Table 2 15 with a comparison of the maximum detected and nondetected concentrations with the appropriate RBC The maximum detected and nondetected concentrations of most of these compounds do not exceed the residential groundwater RBC For those compounds where the maximum detected and/or nondetected concentrations exceed the RBC none of the concentrations exceed 1 000 times the RBC

Therefore according to the criterion used in the OU 5 TM11 COCs for the HHRA (DOE 1995a) these compounds would not be considered special case COCs

Three of the organic compounds included in Table 2 15 were evaluated in the concentration/toxicity screens for OU 5 (DOE 1995a) These compounds bis(2 ethylhexyl)phthalate di n butyl phthalate and naphthalene were not identified as COCs based on the data collected under the OU 5 Work Plan investigation The percentage of total risk that would be associated with these chemicals using the maximum detected concentrations shown on Table 2 10 was recalculated for comparison to the concentration/toxicity screens presented in TM11 OU 5 COCs for the HHRA (DOE 1995a) With the higher concentrations the percentage of total noncarcinogenic risk attributable to these compounds did not change from that reported in (DOE 1995a) The percentage of the total carcinogenic risk attributable to bis(2 ethylhexyl)phthalate increased from 0 03 percent to 0 07 percent Therefore even at the higher concentrations none of these compounds would be identified as COCs

In summary the groundwater data collected during the TM15 field investigation do not indicate that the conclusions of the OU 5 HHRA as presented in TM11 (DOE 1995a) need to be reevaluated to incorporate these data

Surface Soils The activities of americium 241 and plutonium 239/240 detected in the surface soil samples collected from IHSS 209 and the other surface disturbances during the TM15 field investigation were less than the maximum activities reported previously for surface soil samples from OU 5 The concentration/toxicity screens performed to identify COCs for the OU 5 HHRA were calculated using the highest activity reported for the samples collected under the OU 5 Work Plan investigation Because these concentration/toxicity screens did not identify americium 241 and plutonium 239/240 as COCs at that time (DOE 1995a) the inclusion of additional data with lower activities would not change this determination Therefore the surface soil data collected during the TM15 field investigation does not impact the conclusions of the HHRA presented in this chapter

6 6 3 2 Source Areas and Areas of Concern

In the Surface Disturbance South of the Ash Pits soil was the only medium in which PCOCs were detected These PCOCs consisted of two organic compounds and 26 inorganic compounds 5 of which

were radionuclides. The carcinogenic and noncarcinogenic ratio sums for this source area were calculated to be 0.82 and 0.45 respectively (DOE 1994). Because the ratio sums do not exceed one, this source area was not considered an AOC and was not evaluated further.

Similarly, in the Surface Disturbance West of IHSS 209 PCOCs were detected only in soil. The detected PCOCs consisted of three organic compounds and 25 inorganic compounds, 5 of which were radionuclides. The carcinogenic and noncarcinogenic ratio sums for this source area were calculated to be 2.2 and 0.42 respectively. The carcinogenic ratio sum exceeds one because a single sample of plutonium 239/240 was greater than its RBC. No other detected PCOC approached its respective RBC. A review of the data indicated that the maximum activity of plutonium 239/240 was 5.01 pCi/g and the RBC is 3.43 pCi/g. Subsequent sampling has not produced samples at this level of plutonium 239/240 activity and, in fact, has yielded results lower than the RBC of 3.43 pCi. As a result, it was determined that this source area does not contribute significantly to the risk associated with OU 5 and was not quantitatively evaluated as an AOC.

6.6.3.3 Discussion of Analytes

Nickel was detected in OU 5 soil; however, it was considered inappropriate to apply a CSF. The only forms of nickel known to be carcinogenic are nickel refinery dust and nickel subsulfide via the inhalation route (EPA 1994b). Based on historical evidence, the only indication of nickel use at the Site is in the form of nickel carbonyl. The limited toxicity information on nickel carbonyl indicates that it is a probable human carcinogen; however, there is inadequate data for human carcinogenicity. Therefore, no toxicity values (RfD/RfC or CSFs) are available for this form of nickel. Nickel carbonyl is also highly volatile at room temperature and readily decomposes in the presence of oxygen. Because of its physical properties and the fate and transport characteristics of nickel carbonyl, it is unlikely that any of this compound remains onsite after 20 years. Therefore, based on the research performed on this issue, nickel was not considered a significant contributor to OU 5 risk and was not evaluated as a carcinogenic chemical.

Lead was detected in surface soil, subsurface soil, and groundwater at OU 5. The maximum lead concentration was 129 mg/kg in surface soil, 935 mg/kg in subsurface soil, and 240 µg/L in groundwater. The levels of lead detected in surface soil and groundwater are well below the EPA screening level for lead in soil for residential land use of 400 ppm (EPA 1994e). The highest concentration of lead detected in

subsurface soil was 935 mg/kg however all of the highest concentrations were detected in samples taken from the boreholes drilled within the ash pits (IHSS 133 1 to IHSS 133 4) In all cases the samples with the highest concentrations were collected from intervals where waste materials were encountered during drilling This indicates that the detected lead is not mobile in the soil or readily available for human intake Based on the sampling data lead is not considered a significant contributor to the human health risk associated with OU 5

Arsenic was identified as a PCOC in groundwater pond sediment and stream sediment However process knowledge does not indicate that there was any large quantity or widespread use of arsenic at the Site An agency meeting was held on February 16 1995 specifically to discuss the background comparisons and application of professional judgement as applied to arsenic (DOE 1995b) As discussed and agreed to in that meeting arsenic can be screened out as a PCOC for these three media based on the results of the statistical tests and professional judgement Arsenic is considered to be within background concentrations and will not significantly contribute to the risk at OU 5

Seven PAHs were identified as COCs in either surface or subsurface soil The CSM identified several potential receptors that have a complete dermal pathway to these media however RAGS (EPA 1989) states It is inappropriate to use the oral slope factor to evaluate the risks associated with dermal exposure to carcinogens such as benzo(a)pyrene which cause skin cancer through a direct action at the point of application The PAHs that are COCs in OU 5 are benzo(a)anthracene benzo(a)pyrene benzo(b)fluoranthene dibenzo(a,h)anthracene fluoranthene Indeno(1 2 3 cd)pyrene and pyrene Dermal exposure to these PAHs has not been quantified however it does not appear that these chemicals contribute significantly to the overall risks to the receptors that would potentially have dermal contact with surface and subsurface soil

6.7 RADIATION DOSE CALCULATIONS

Total radiation doses for one year of exposure (expressed as total Effective Dose Equivalent [EDE] in mrem/year) were estimated for receptors exposed to radionuclides in soil air and other media by ingestion inhalation and external irradiation pathways The estimated doses are compared to DOE radiation standards for protection of public health also expressed in mrem/yr

6 7 1 Methodology

This section defines the terms used in estimating annual radiation doses explains how the doses are calculated and describes the national annual radiation protection standards that are used for comparison to the calculated doses

6 7 1 1 Definitions

Dose Terms

Absorbed Dose is the energy imparted to matter by ionizing radiation per unit mass of irradiated material at the place of interest in that material The absorbed dose is expressed in units of rad (or gray) (1 rad = 0 01 gray)

Committed Dose Equivalent is the predicted total dose equivalent to a tissue or organ over a 50-year period after a known intake of radionuclide into the body It does not include contributions from external dose Committed dose equivalent is expressed in units of rem (or sievert)

Committed Effective Dose Equivalent (CEDE) is the sum of the committed dose equivalents to various tissues in the body each multiplied by the appropriate weighting factor Committed effective dose equivalent is expressed in units of rem (or sievert)

Dose Equivalent is the product of absorbed dose in rad (or gray) in tissue and a quality factor Dose equivalent is expressed in units or rem (or sievert)

Effective Dose Equivalent (EDE) is the summation of the products of the dose equivalent received by specified tissues of the body and a tissue specific weighting factor This sum is a risk-equivalent value and can be used to estimate the health effects risk of the exposed individual The tissue specific weighting factor represents the fraction of the total health risk resulting from uniform whole body irradiation that would be contributed by the particular tissue The effective dose equivalent includes the committed effective dose equivalent from internal deposition of radionuclides and the effective dose equivalent due

to penetrating radiation from sources external to the body Effective dose equivalent is expressed in units or rem (or sievert)

Weighting Factor is tissue specific and represents the fraction of the total health risk resulting from uniform whole body irradiation that could be contributed to that particular tissue The weighting factors recommended by the ICRP (Publication 26) and used here are

<u>Organ or Tissue</u>	<u>Weighting Factor</u>
Gonads	0.25
Breasts	0.15
Red Bone Marrow	0.12
Lungs	0.12
Thyroid	0.03
Bone Surfaces	0.03
Remainder ¹	0.30

¹ Remainder means the five other organs with the highest dose (e.g. liver, kidney, spleen, thymus, adrenal, pancreas, stomach, small intestine, or upper and lower large intestine, but excluding skin, lens of the eye, and extremities) The weighting factor for each of these organs is 0.06

Quality Factor is the principal modifying factor used to calculate the dose equivalent from the absorbed dose For the purposes of the Order, the following quality factors, which are taken from DOE 5480.11, are to be used

<u>Radiation Type</u>	<u>Quality Factor</u>
X rays, gamma rays, positrons, and electrons (including tritium)	1
Neutrons <10 keV	3
Neutrons >10 keV Protons and single charged particles of unknown energy with rest mass > one atomic mass unit	10
Alpha Particles Multiple charged particles (and particles of unknown energy)	20

* For neutrons of known energies, the more detailed quality factors given in DOE 5480.11 may be used

Radioactivity means the property or characteristic of radioactive material to spontaneously disintegrate with the emission of energy in the form of radiation. The unit of radioactivity is the curie (or becquerel).

6.7.2 Calculating Annual Radiation Doses

Annual radiation doses were determined by selecting dose conversion factors and calculating the radionuclide intake for each receptor and pathway. The annual EDE was then calculated.

6.7.2.1 Selection of Dose Conversion Factors

Radionuclide specific dose conversion factors for the CEDE were used in the calculation of EDEs for the ingestion and inhalation routes of exposure. Radionuclide specific dose conversion factors for the EDEs were used for the external irradiation route of exposure. These values were obtained from EPA's

Limiting Values of Radionuclide Intake and Air Concentration and Dose Conversion Factors for Inhalation, Submersion, and Ingestion (EPA 1988d) for the inhalation and ingestion route of exposure and from the External Exposure to Radionuclides in Air, Water, and Soil (EPA 1993a).

For some radionuclides, dose conversion factors (DCF) vary based on the chemical species (e.g., oxidation state or mineralized form) of the radionuclide. Differences in DCFs for the ingestion route of exposure reflect differences in fractional uptake (f_1) of radionuclide species from the small intestine to blood. Less soluble radionuclide forms have smaller DCFs than more soluble forms because the less soluble forms are absorbed to a lesser degree from the gastrointestinal tract into the bloodstream (EPA 1988d). Since the form of radionuclide is not known, the most conservative (or greatest f_1) was used for the most conservative estimate of radionuclide intake via ingestion. Table 6-144 lists the fractional uptakes and ingestion DCFs (in Sv/Bq) for each radionuclide of concern.

DCFs for the inhalation route of exposure also vary based on the chemical species of the radionuclide. The different DCFs reflect the difference in the rates that radionuclide species are cleared from the lungs. Lung clearance rates are classified as days (D), weeks (W), or years (Y). In general, less soluble forms of the radionuclide are cleared from the lungs more slowly than more soluble forms. Once again, the species of each radionuclide of concern is not known, so the most conservative lung clearance class was used in order to determine radionuclide intake via inhalation. Table 6-144 lists the most conservative lung clearance class and corresponding inhalation DCF (in Sv/Bq) for each radionuclide of concern. A check

was performed to ensure that the f value and the lung clearance class were compatible and that the combination gave the highest combined ingestion and inhalation CEDE

For the external irradiation route of exposure the DCF is the annual EDE received (mrem/yr) from exposure to radiation from each radionuclide present external to the body. The radiation field is assumed to be equal to the radiation level at a distance of 1 meter (m) above the ground surface. The DCFs for external radiation exposure from surface soil were taken from an EPA report (EPA 1993a) and are listed in terms of mrem/year per $\mu\text{Ci}/\text{gram}$ in Table 6 144

6 7 2 2 Ingestion and Inhalation Routes of Exposure

For the inhalation and ingestion routes of exposure annual intake of radionuclides expressed in pCi/yr is first calculated using the following equation

$$\text{Intake (pCi/year)} = C \times IR \times EF$$

Where

C = Activity concentration at the exposure point (pCi/g pCi/L or pCi/m³)

IR = Intake rate (mg/day L/day m³/day)

EF = Exposure frequency (days/year)

Exposure factors used in calculating annual radionuclide intake for specific receptors and pathways are identical to the exposure factors used in the intake equations in Sections 6 4 2 1 through 6 4 2 6. The annual intake of each radionuclide in pCi/year is multiplied by the CEDE DCF (mrem/pCi or Sv/Bq) from Table 6 144 to estimate the CEDE for one year (mrem/year)

6 7 2 3 External Irradiation

For the external irradiation route of exposure a concentration in soil (pCi yr/gram) is calculated using the following equation

$$AC \left(\frac{\text{pCi-yr}}{\text{gram}} \right) = C \times ED \times EF_r \times (1 - Se) \times Te$$

Where

C	= Mass activity concentration at the exposure point (pCi/g soil)
ED	= Exposure Duration (1 year)
EF	= Exposure frequency ratio (unitless)
Se	= Gamma shielding factor (unitless)
Te	= Gamma exposure factor (unitless)

The concentration of each radionuclide in soil (in pCi year/gram) is multiplied by the dose conversion factor for external radiation (mrem/year per pCi/gram) (Table 6 144) to estimate the annual EDE (mrem) for each radionuclide

6 7 2 4 Estimating Annual Radiation Dose

The sum of CEDEs from all radionuclides taken into the body in a year added to the EDEs for all radionuclides external to the body is compared to radiation protection standards which also reflect this sum

Annual radiation doses were estimated for all receptors and exposure areas The results are summarized (Tables 6 145 through 6 146) and compared to radiation protection standards in the following sections

6 7 3 Radiation Protection Standards

DOE Order 5480 11 Radiation Protection for Occupational Workers limits radiation exposure of radiological workers to 50 mSv/year (5 000 mrem/yr) DOE order 5400 5 Radiation Protection of the Public and the Environment, limits the annual radiation dose limit for members of the public to 1 mSv/year (100 mrem/year) for all routes of exposure The occupational limit for general employees (i e those not considered to be radiological workers) may be 100 mrem/year to 5 000 mrem/year depending on employment circumstances However general employees who have not completed Radiological Worker I or II Training are not permitted unescorted access to any area in which they are expected to receive doses in excess of 100 mrem in one year General employees who have not received Radiological Worker I or II Training are not normally expected to exceed 100 mrem in a year These values are for radiation doses received in addition to that from natural background radiation (U S average background radiation is approximately 300 mrem/year NCRP 1987) and that received from routine medical treatments (U S

average is approximately 50 mrem/year (NCRP 1987). Background levels in the Denver area are estimated to range from 350 to 700 mrem/year; these levels are higher than the national average because of high levels of radium, thorium, and radon in native rock and soils and because cosmic radiation exposure increases with increased altitude (NCRP 1987).

6.7.4 Point Estimates of Annual Radiation Dose

Annual radiation doses in terms of mrem/year were calculated for onsite receptors in AOC1, AOC2, and AOC3. Results are summarized in Tables 6-145 through 6-147.

6.7.4.1 Future Construction Worker

Radionuclide exposure pathways evaluated for the current worker were

- Ingestion of surface soil
- Ingestion of subsurface soil
- Inhalation of airborne particle
- External irradiation from subsurface soil

The future construction worker is a potential receptor in AOC1 and AOC2. As discussed in Section 6.6.2.1, the construction worker receptor is not a receptor in AOC3. The total annual radiation dose for the construction worker in AOC1 is 7.1×10^{-2} mrem/year for the CT exposure condition and 3.6×10^{-1} mrem/year for the reasonable maximum exposure (RME) conditions (Table 6-145). The total annual radiation dose for the construction worker in AOC2 is 3.1×10^{-2} mrem/year for the average (CT) exposure condition and 1.3×10^{-1} mrem/year for the RME condition (Table 6-146). These values are below the DOE limits for radiological workers (5,000 mrem/year) and members of the public (100 rem/year).

6.7.4.2 Current Worker (Security Worker)

Radionuclide exposure pathways evaluated for the current worker were

- Ingestion of surface soil
- Inhalation of airborne particles
- External irradiation from surface soil

The future construction worker is a potential receptor in AOC1 and AOC2 and not in AOC3. The total annual dose for the current worker in AOC1 is 1.8×10^{-1} mrem/year for the CT exposure conditions and 5.4×10^{-1} mrem/year for the RME conditions (Table 6-145). The total annual radiation dose for the current worker in AOC2 is 3.2×10^{-2} mrem/year for the average (CT) exposure condition and 9.9×10^{-2} mrem/year for the RME condition (Table 6-146). These values are below the DOE limits for radiological workers ($5,000$ mrem/year) and members of the public (100 rem/year).

6.7.4.3 Future Ecological Researcher

The future ecological researcher is an applicable pathway for all AOCs. However, AOC3 pathway varied from AOC1 and AOC2 pathways due to the unique nature of AOC3.

Radionuclide exposure pathways evaluated for the ecological researcher in AOC1 and AOC2 were

- Ingestion of surface soil
- Inhalation of airborne particles
- Ingestion of seep sediments
- External irradiation from surface soil

Radionuclide exposure pathways for the ecological researcher in AOC3 were

- Ingestion of pond sediments
- Ingestion of stream sediments
- Ingestion of surface water

The total annual dose for the future ecological researcher in AOC1 is 1.9×10^{-1} mrem/year for the CT exposure conditions and 2.6×10^{-1} mrem/year for the RME conditions (Table 6-145). The total annual radiation dose for the ecological researcher in AOC2 is 6.2×10^{-2} mrem/year for the average (CT) exposure condition and 5.9×10^{-2} mrem/year for the RME condition (Table 6-146). The total annual dose for AOC3 was estimated as 4.1×10^{-2} mrem/yr for the CT conditions and 1.3×10^{-1} mrem/year for the RME conditions. These values are below the DOE limits for radiological workers ($5,000$ mrem/year) and members of the public (100 rem/year).

6 7 4 4 **Future Office Worker**

The future office worker is a potential receptor in only AOC1 and AOC2. The office worker is not an applicable receptor in AOC3. Radionuclide exposure pathways for the office worker were the same as for the current worker. The total annual dose for the office worker in AOC1 is 1.6×10^{-1} mrem/year for the CT exposure conditions and 3.2×10^{-1} mrem/year for the RME conditions (Table 6-145). The total annual dose for the future office worker in AOC2 is 2.5×10^{-2} mrem/year for the average (CT) conditions and 9.9×10^{-2} for the RME conditions (Table 6-146). These values are below the DOE limits for radiological workers ($5,000$ mrem/year) and members of the public (100 rem/year).

6 7 4 5 **Future Open Space User**

Radionuclide exposure pathways for the adult recreational user were the same as for the ecological worker. The total annual dose for the adult receptor in AOC1 is 1.7×10^{-2} mrem/year for the CT exposure conditions and 6.0×10^{-2} mrem/year for the RME conditions (Table 6-145). Annual doses for the adult user in AOC2 is 3.3×10^{-3} mrem/year for CT exposure conditions and 1.3×10^{-2} mrem/yr for RME condition (Table 6-146). The radionuclide exposure pathways for AOC3 were the same as the AOC3 exposure pathways for the future ecological researcher. The total annual dose for the adult recreational user in AOC3 is 4.8×10^{-3} mrem/year for CT conditions and 2.5×10^{-2} mrem/yr for RME exposure conditions (Table 6-147). These values are below the DOE limits for radiological workers ($5,000$ mrem/year) and members of the public (100 rem/year).

Radionuclide exposure pathways for the child open space user in AOC1 and AOC2 were

Ingestion of surface soil

Ingestion of seep sediments

The total annual dose for the child receptor in AOC1 is 6.2×10^{-3} mrem/yr for CT conditions and 6.2×10^{-2} mrem/year for RME exposure conditions (Table 6-145). The total annual dose for the child open space user in AOC2 is 1.7×10^{-3} mrem/year for CT exposure conditions and 5.8×10^{-2} mrem/year for RME conditions. The radionuclide exposure pathways for the child receptor in AOC3 were the same as those for the adult open space user. The total annual dose for the child open space user in AOC3 is 9.6×10^{-3} mrem/year for CT conditions and 4.8×10^{-2} mrem/year for RME exposure conditions (Table 6-147).

6 7 5 **Summary of Results**

Annual radiation dose calculations were performed for six onsite receptors in AOC1 and AOC2. Annual radiation dose calculations were performed for 3 onsite receptors (ecological researcher, adult and child open space users) in AOC3. Dose conversion factors for radionuclide ingestion, inhalation and external irradiation are listed in Table 6-144. Results are provided in Tables 6-145 through 6-147.

Exposure pathways evaluated were soil/sediment ingestion, inhalation of particles from soil, ingestion of surface water (AOC3 only) and external irradiation from surface soil. Additional pathways evaluated for the future ecological researcher and future open space user (adult and child) in AOC3 were ingestion of pond sediments and ingestion of stream sediments.

Total annual radiation doses for all receptors in all AOCs were less than 1, which falls below the DOE limit of 100 mrem/yr for members of the public and indicates that exposure to radionuclides in OU 5 is negligible.

6 8 **RISK ASSESSMENT SUMMARY**

The results of the risk and health effect calculations for all applicable receptors and pathways are summarized in Tables 6-142 and 6-143. The greatest total estimated risk was for the current worker in AOC1 and is 3×10^{-5} . The driving pathway is exposure to external radiation and the dominant COC is uranium-238. The greatest total estimated noncarcinogenic health effect was for the current worker in AOC1 and is calculated to be 7×10^{-2} . The driving pathway is dermal absorption of surface soil and the dominant COC is Aroclor 1254 in surface soil.

Although the highest calculated risk is still within the National Oil and Hazardous Substances Pollution Contingency Plan (NAP) target risk range of 1×10^{-6} to 1×10^{-4} , some additional receptors and locations are mentioned here for comparison. The total RME estimated risk for a future office worker in AOC1 was calculated to be 3×10^{-5} and the current worker in AOC2 was estimated to be 4×10^{-6} . The estimated RME risk for a future open space user in AOC1 is 4×10^{-6} , a future office worker in AOC2 is 4×10^{-6} and an ecological researcher in AOC1 is 1×10^{-6} . All other receptors and respective pathways had total RME risks estimated to be less than 1×10^{-6} . Respective total CT estimated risks for the current worker at AOC1 and

the future office worker at AOC1 were both calculated to be $2E-06$. No other CT risk estimates exceeded $1E-06$.

Because RME total risk and RME HI estimates did not exceed $1E-04$ and unity respectively, a quantitative uncertainty analysis was not completed. Qualitative discussions of uncertainty are contained in Section 6.6.3 and a summary of the uncertainties and limitations is contained in Table 6.14.1. Uncertainties in this risk assessment are due to uncertainties in the risk assessment process in general, specific uncertainties in characterizing the site, and the uncertainties and limitations specific to this assessment. In general, health protective assumptions were used such that the magnitude of human health risks are expected to be less than those calculated, even with errors due to uncertainty in the approach. This process bounds the plausible upper limits of risk and facilitates an informed risk management decision. Information regarding the uncertainty in quantifying intakes, toxicological and carcinogenic response, credibility of future exposure scenarios, and the magnitude of background risks will be used by the risk manager for regulatory decision making.

Table 6 1
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Surface Soil

PCOC	Maximum Concentration (mg/kg)	RfD (mg/kg day) (1)	Type of RfD (2)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Acenaphthene	4 40E+01	6 00E-02	0	7 33E+02	3 09E-03	0 31%	No
Anthracene	4 70E+01	3 00E-01	0	1 57E+02	6 60E-04	0 07%	No
Aroclor 1254	3 90E+00	2 00E-05	0	1 95E+05	8 21E-01	82 12%	Yes
Benz(a,g,h,i)perylene	6 90E+00	n/a					No
Benzoic acid	7 70E-01	4 00E+00	0	1 93E-01	8 11E-07	0 00%	No
Bis(2 ethylhexyl)phthalate	2 00E-01	2 00E-02	0	1 00E+01	4 21E-05	0 00%	No
Cobalt	1 37E+01	6 00E-02	0	2 28E+02	9 62E-04	0 10%	No
Copper	1 84E+02	4 00E-02		4 60E+03	1 94E-02	1 94%	Yes
Di n butylphthalate	4 25E-01	1 00E-01	0	4 25E+00	1 79E-05	0 00%	No
Dibenzofuran	2 00E+01	n/a					No
Fluoranthene	1 40E+02	4 00E-02	0	3 50E+03	1 47E-02	1 47%	Yes
Fluorene	3 90E+01	4 00E-02	0	9 75E+02	4 11E-03	0 41%	No
Lindane	1 29E+02	n/a					No
Muriatic acid	6 60E-01	8 57E-05	1	7 70E+03	3 24E-02	3 24%	Yes
2 Methyl naphthalene	1 20E+01	n/a					No
Nitrobenzene	4 10E+01	4 00E-02		1 03E+03	4 32E-03	0 43%	No
Phenanthrene	1 70E+02	n/a					No
Pyrene	1 20E+02	3 00E-02		4 00E+03	1 68E-02	1 68%	Yes
Silver	9 43E+01	5 00E-03	0	1 89E+04	7 94E-02	7 94%	Yes
Zinc	1 99E+02	3 00E-01	0	6 63E+02	2 79E-03	0 28%	No
Total Risk Factor (Rj) =					2 37E+05	Total % =	100%

Notes

- (a) The most restrictive of the oral or inhalation reference dose is used.
- (b) 0 = oral 1 = inhalation
- (n/a) Applicable toxicological criteria is not available

Table 6-2
Rocky Flats OU 5 Concentration/Toxicity Screen of Carcinogens in Surface Soil

PCOC	Maximum Concentration (mg/kg)	Slope Factor (mg/kg-day) ^(a)	Type of Slope Factor ^(b)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Carcinogens							
Aroclor 1254	3 90E+00	7 70E+00	0	3 00E+01	6 33E 02	6 33%	Y ^s
Benz(a)anthracene	4 50E+01	7 30E 01		3 20E+01	6 92E 02	6 12%	Y
Benz(a)pyrene	4 10E+01	7 30E+00	0	2 99E+02	6 31E-01	63 07%	Y ^s
Benz(b)fluoranthene	4 90E+01	7 30E-01	0	3 58E+01	7 54E 02	7 54%	Yes
Benz(k)fluoranthene	2 50E+01	7 30E-02	0	1 83E+00	3 85E-03	0 38%	No
Bis(2-ethylhexyl)phthalate	2 00E-01	1 40E-02	0	2 80E-03	5 90E 06	0 00%	N
Chrysene	4 60E+01	7 30E-03	0	3 36E 01	7 08E 04	0 07%	N ^s
Dibenz(a,h)anthracene	7 00E+00	7 30E+00	0	5 11E+01	1 08E 01	10 77%	Yes
Indeno(1 2 3-cd)pyrene	3 20E+01	7 30E-01	0	2 34E+01	4 92E 02	4 92%	Y ^s
Total Risk Factor (Rj)				4 75E+02	Total %	100%	

Notes

(a) The most restrictive of the oral or inhalation slope factor is used

(b) = oral

Table 6-3
Rocky Flats OU5 Concentration/Toxicity Screen of Radionuclides in Surface Soil

PCOC	Maximum Concentration (pCi/g)	Slope Factor (risk/pCi) ^(a)	Type of Slope Factor ^(b)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Radionuclides							
Americium 241	8 00E-01	3 20E-08	1	2 56E-06	2 55E-05	0 00%	No
Plutonium 239/240	5 01E+00	3 80E-08	1	1 90E-07	1 90E-04	0 02%	No
Uranium 233/234	2 80E+03	2 70E-08	1	7 56E-05	7 53E-02	7 53%	Yes
Uranium 235	6 70E+02	2 50E-08	1	1 68E-05	1 67E-02	1 67%	Yes
Uranium 238	3 80E+04	2 40E-08	1	9 12E-04	9 08E-01	90 79%	Yes
Total Risk Factor (Rj)				1 00E-03	Total % =		100%

Notes

- (a) The most conservative of the oral or inhalation slope factor is used
(b) 1 = inhalation

Table 6 4
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Subsurface Soil

PCOC	Maximum Concentration (mg/kg)	RfD (mg/kg day) (1)	Type of RfD (2)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Acenaphthene	3 10E+01	6 00E-02	0	5 17E+02	4 67E-04	0 05%	No
Acetone	2 80E-01	1 00E-01	0	2 80E+00	2 53E-06	0 00%	No
Anthracene	4 60E+01	3 00E-01	0	1 53E+02	1 39E-04	0 01%	No
Antimony	1 49E+02	4 00E-04	0	3 73E+05	3 37E-01	33 69%	Yes
Aroclor 1254	9 60E-01	2 00E-05	0	4 80E+04	4 34E-02	4 34%	Yes
Barium	6 83E-01	1 40E-04	1	4 88E+03	4 41E-03	0 44%	No
Benz(a,h,i)perylene	1 90E+01	n/a					N
2 Butanone	6 90E-02	2 90E-01	1	2 38E-01	2 15E-07	0 00%	No
Benzoic acid	9 74E-01	4 00E+00	0	2 44E-01	2 20E-07	0 00%	No
Beryllium	1 31E+02	5 00E-03	0	2 62E+04	2 37E-02	2 37%	Yes
Bis(2 ethyl hexyl)phthalate	2 90E-01	2 00E-02	0	1 45E+01	1 31E-05	0 00%	No
Cadmium	5 69E+01	5 00E-04	0	1 14E+05	1 03E-01	10 29%	Y
Chromium	8 31E+03	1 00E+00	0	8 31E+03	7 52E-03	0 75%	No
Cobalt	6 76E+01	6 00E-02	0	1 13E+03	1 02E-03	0 10%	No
Copper	6 92E+03	4 00E-02		1 73E+05	1 56E-01	15 65%	Yes
Dibenzofuran	2 00E+01	n/a					N
Fluoranthene	1 60E+02	4 00E-02	0	4 00E+03	3 62E-03	0 36%	No
Fluorine	3 50E+01	4 00E-02	0	8 75E+02	7 91E-04	0 08%	No
Lead	9 35E+02	n/a					No
Methylene chloride	6 60E-02	6 00E-02	0	1 10E+00	9 95E-07	0 00%	No
2-Methylnaphthalene	1 50E+01	n/a					No
Molybdenum	1 90E+02	5 00E-03	0	3 80E+04	3 44E-02	3 44%	Yes
Naphthalene	6 10E+01	4 00E-02	0	1 53E+03	1 38E-03	0 14%	No
Nickel	4 75E+03	2 00E-02	0	2 38E+05	2 15E-01	21 48%	Yes
Phenanthrene	2 20E+02	n/a					No
Pyrene	1 50E+02	3 00E-02	0	5 00E+03	4 52E-03	0 45%	No
Silver	3 11E+02	5 00E-03	0	6 22E+04	5 63E-02	5 63%	Yes
Tetrachloroethene	9 20E-01	1 00E-02	0	9 20E+01	8 32E-05	0 01%	No
Toluene	3 10E-01	1 14E-01	1	2 72E+00	2 46E-06	0 00%	No
Zinc	2 39E+03	3 00E-01	0	7 97E+03	7 21E-03	0 72%	No
Total Risk Factor (Rj)				=	1 11E+06	Total % =	100%

N tes

(1) The maximum toxicological reference dose is used
 (2) = oral = inhalation
 (3) = available toxicological reference dose is not available

Table 6-5
Rocky Flats OU 5 Concentration/Toxicity Screen of Carcinogens in Subsurface Soil

PCOC	Maximum Concentration (mg/kg)	Slope Factor (mg/kg-day) ^(a)	Type of Slope Factor ^(b)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Carcinogens							
Aroclor 1254	9 60E-01	7 70E+00	0	7 39E+00	3 95E-03	0 39%	N
Benz(a)anthracene	4 80E+01	7 30E-01	0	3 50E+01	1 87E-02	1 87%	Y
Benz(a)pyrene	4 30E+01	7 30E+00	0	3 14E+02	1 68E-01	16 76%	Yes
Benz(b)fluoranthene	4 80E+01	7 30E-01	0	3 50E+01	1 87E-02	1 87%	Yes
Benz(k)fluoranthene	1 90E+01	7 30E-02	0	1 39E+00	7 40E-04	0 07%	N
Beryllium	1 31E+02	8 40E+00	1	1 10E+03	5 87E-01	58 74%	Y
Bis(2 ethylhexyl)phthalate	2 90E-01	1 40E-02	0	4 06E-03	2 17E-06	0 00%	N
Cadmium	5 69E+01	6 30E+00	1	3 58E+02	1 91E-01	19 14%	Y
Chrysene	5 30E+01	7 30E-03	0	3 87E-01	2 07E-04	0 02%	N
Dibenz(a,h)anthracene	7 00E-01	7 30E+00	0	5 11E+00	2 73E-03	0 27%	N
Indeno(1,2,3 cd)pyrene	2 20E+01	7 30E-01	0	1 61E+01	8 57E-03	0 86%	N
Methyl ne chloride	6 60E-02	7 50E-03	0	4 95E-04	2 64E-07	0 00%	N
Tetra chloroethene	9 20E-01	5 20E-02	0	4 78E-02	2 55E-05	0 00%	N
Tri chloroethene	4 40E-01	1 10E-02	0	4 84E-03	2 58E-06	0 00%	N
Total Risk Factor (Rj)				1 87E+03	Total % =	100%	

N 1

- () The most restrictive of the oral or inhalation slope factor is used
(b) 0 = oral 1 = inhalation

Table 6-6
Rocky Flats OU 5 Concentration/Toxicity Screen of Radionuclides in Subsurface Soil

PCOC	Maximum Concentration (pCi/g)	Slope Factor (risk/pCi) ^(a)	Type of Slope Factor ^(b)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Radionuclides							
Americium 241	6 10E-01	3 20E-08	1	1 95E-08	6 04E-04	0 06%	No
Plutonium 239/240	3 20E+00	3 80E-08	1	1 22E-07	3 76E-03	0 38%	No
Uranium 233/234	1 26E+02	2 70E-08	1	3 40E-06	1 05E-01	10 52%	Yes
Uranium 235	3 77E+01	2 50E-08	1	9 43E-07	2 92E-02	2 92%	Yes
Uranium 238	1 16E+03	2 40E-08	1	2 78E-05	8 61E-01	86 12%	Yes
Total Risk Factor (Rj) =				3 23E-05	Total % =	100%	

Notes

- (a) The most restrictive of the oral or inhalation slope factor is used
(b) 1 = inhalation

Table 6 7
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Groundwater

PCOC	Maximum Concentration (mg/L) ^(a)	RfD (mg/kg-day) ^(a)	Type of RfD	Chemical Specific Risk Factor (Rf)	Ratio of Rf/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Acenaphthene	5.00E-03	6.00E-02	0	8.33E-02	2.69E-05	0.00%	N
Aluminum	3.57E+02	2.90E+00	0	1.23E+02	3.97E-02	3.97%	Yes
Barium	3.04E+00	7.00E-02	0	4.34E+01	1.40E-02	1.40%	Yes
Beryllium	2.94E-02	5.00E-03	0	5.88E+00	1.89E-03	0.19%	N
Bis(2 ethylhexyl)phthalate	3.00E-03	2.00E-02	0	1.50E-01	4.83E-05	0.00%	No
Cadmium	8.20E-03	5.00E-04	0	1.64E+01	5.29E-03	0.53%	No
Chromium	4.42E-01	1.00E+00	0	4.42E-01	1.42E-04	0.01%	No
Cobalt	1.61E-01	6.00E-02	0	2.68E+00	8.65E-04	0.09%	N
Copper	4.20E-01	4.00E-02	0	1.05E+01	3.38E-03	0.34%	N
Di n butylphthalate	2.00E-03	1.00E-01	0	2.00E-02	6.45E-06	0.00%	N
Dihethylphthalate	6.00E-03	8.00E-01	0	7.50E-03	2.42E-06	0.00%	No
Fluoranthene	4.00E-03	4.00E-02	0	1.00E-01	3.22E-05	0.00%	N
Fluorene	4.00E-03	4.00E-02	0	1.00E-01	3.22E-05	0.00%	N
Lead	2.40E-01	n/a					N
Lithium	3.06E-01	2.00E-02	0	1.53E+01	4.93E-03	0.49%	No
Manganese	1.37E+01	5.00E-03	0	2.74E+03	8.83E-01	88.30%	N
Molybdenum	3.00E-03	3.00E-04	0	1.00E+01	3.22E-03	0.32%	Y
Naphthalene	1.80E-02	5.00E-03	0	3.60E+00	1.16E-03	0.12%	N
Nickel	3.13E-01	4.00E-02	0	3.25E-01	1.05E-04	0.01%	No
Phenanthrene	6.00E-03	2.00E-02	0	1.57E+01	5.04E-03	0.50%	No
Pyrene	6.50E-03	n/a					No
Silicon	3.54E+02	n/a					No
Silver	5.32E-02	5.00E-03	0	1.06E+01	3.43E-03	0.34%	No
Strontium	2.58E+00	6.00E-01	0	4.29E+00	1.38E-03	0.14%	No
Tin	3.00E-01	6.00E-01	0	5.00E-01	1.61E-04	0.02%	No
Vanadium	6.74E-01	7.00E-03	0	9.63E+01	3.10E-02	3.10%	Yes
Zinc	9.82E-01	3.00E-01	0	3.27E+00	1.05E-03	0.11%	No
Total Risk Factor (Rf) =				3.10E+03	Tal % = 100%		

Notes

(a) The more conservative total analyte maximum concentrations is used
(b) Only oral reference doses are used for inorganic compounds

(c) r l

(/) Appl abt t x i l l i t r i a t n t availabl

Table 6-8
Rocky Flats OU 5 Concentration/Toxicity Screen of Carcinogens in Groundwater

PCOC	Maximum Concentration (mg/L) ^(a)	Slope Factor (mg/kg-day) ^(b)	Type of Slope Factor ^(c)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Carcinogens							
Beryllium	2 94E-02	4 30E+00	0	1 26E-01	1 00E+00	99 97%	Yes
Bis(2 ethylhexyl)phthalate	3 00E-03	1 40E-02	0	4 20E-05	3 32E-04	0 03%	No
Total Risk Factor (Rj)		=		1 26E-01	T tal %	100%	

Notes

- (a) The more conservative total analyte maximum concentrations is used
- (b) Only oral slope factors are used.
- (c) 0 = oral 1 = inhalation

Table 6-9
Rocky Flats OU 5 Concentration/Toxicity Screen of Radionuclides in Groundwater

PCOC	Maximum Concentration (pCi/L) ^(a)	Slope Factor (risk/pCi) ^(b)	Type of Slope Factor	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Radionuclides							
Americium 241	2 00E-01	2 40E-10	0	4 80E-11	1 89E-02	1 89%	Y ^a
Plutonium 238	1 00E-02	2 20E-10	0	2 20E-12	8 64E-04	0 09%	N
Plutonium 239/240	1 04E+00	2 30E-10		2 31E-10	9 40E-02	3 40%	Y
Radium 226	4 40E+00	1 20E-10		5 28E-10	2 07E-01	20 74%	Y ^a
Uranium 233/234	4 90E+01	1 60E-11	0	7 84E-10	3 08E-01	30 80%	Y ^a
Uranium 235	4 00E+00	1 60E-11	0	6 40E-11	2 51E-02	2 51%	Y ^a
Uranium 238	4 40E+01	2 00E-11		8 80E-10	3 46E-01	34 57%	Y ^a
Total Risk Factor (Rj) =				2 55E-09	Total % =	100%	

Not's

(a) The maximum concentration used

(b) Only the slope factors are used

() - total

Table 6-10
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Surface Water

PCOC	Maximum Concentration (mg/L) ^(a)	RfD (mg/kg day) ^(a)	Type of RfD ^(c)	Chemical Specific Risk Factor (Rf)	Ratio of Rf/R _i	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Barium	1.87E-01	7.00E-02	o	2.67E+00	6.25E-01	62.54%	Yes
Lithium	1.38E-02	2.00E-02	o	6.90E-01	1.62E-01	16.15%	Yes
Strontium	5.46E-01	6.00E-01	o	9.10E-01	2.13E-01	21.30%	Yes
Total Risk Factor (R _i) =				4.27E+00	Total % =	100%	

Notes

- (a) The more conservative total analyte maximum concentrations is used
- (b) The most restrictive of the oral or inhalation reference dose is used
- (c) o = oral

Table 6-11
Rocky Flats OU 5 Concentration/Toxicity Screen of Radionuclides in Surface Water

PCOC	Maximum Concentration (pci/L) ^(a)	Slope Factor (risk/pci) ^(a)	Type of slope factor ^(a)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Radionuclides							
Americium 241	3 80E-01	2 40E 10	0	9 12E-11	2 98E 01	29 81%	Y s
Uranium 233/234	4 67E+00	1 60E-11	0	7 47E 11	2 44E-01	24 42%	Y s
Uranium 238	7 00E+00	2 00E 11	0	1 40E 10	4 58E-01	45 76%	Y s
Total Risk Factor (Rj) =				3 06E 10	Total % =		100%

Notes

- (a) The more conservative total analyte maximum concentrations is used
- (b) The most restrictive of the oral or inhalation slope factor is used
- (c) 0 = oral

Table 6-12
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Seep Water

PCOC	Maximum Concentration (mg/L) ^(a)	RfD (mg/kg day) ^(a)	Type of RfD ^(a)	Chemical Specific Risk Factor (Rf)	Ratio of Rf/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Acetone	6 50E-02	1 00E 01	o	6 50E-01	1 50E 01	14 98%	Y s
1,1 Di hl ruethene	4 00E-03	9 00E 03	o	4 44E 01	1 02E 01	10 24%	Y
1,2 Dichloromethene	4 00E-03	9 00E-03	o	4 44E-01	1 02E 01	10 24%	Yes
Tetrachloroethene	2 80E-02	1 00E-02	o	2 80E+00	6 45E-01	64 53%	Yes
1 1 1 Trichloroethane	2 00E-03	n/a					No
Total Risk Factor (Rf)				=	4 34E+00		
Total Risk Factor (Rj)						T t l x =	100%

Notes

Possible laboratory contaminant

() The most restrictive of the oral or inhalation referenced

(b) o = oral

(n/a) Applicable toxicological criteria not available

Table 6-13
Rocky Flats OU 5 Concentration/Toxicity Screen of Carcinogens in Seep Water

PCOC	Maximum Concentration (mg/L)	Slope Factor (mg/kg-day)^m	Type of Slope Factor^m	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Carcinogens							
1,1 Dichloroethene	4.00E-03	1.20E+00	1	4.80E-03	7.58E-01	75.79%	Yes
Tetra chloroethene	2.80E-02	5.20E-02	0	1.46E-03	2.30E-01	22.99%	Yes
Trichloroethene	7.00E-03	1.10E-02	0	7.70E-05	1.22E-02	1.22%	Yes
Total Risk Factor (Rj) =				6.33E-03	Total % =		100%

Notes

- (a) The most restrictive of the oral or inhalation slope factor is used
 (b) 0 = oral 1 = inhalation

Table 6-14
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Pond Sediment

PCOC	Maximum Concentration (mg/kg)	RfD (mg/kg-day) ^(a)	Type of RfD ^(b)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Benzonic acid	4 10E-01	4 00E+00	0	1 03E 01	5 30E 06	0 00%	No
Di n butylphthalate	1 10E-01	1 00E-01	0	1 10E+00	5 68E 05	0 01%	No
Fluoranthene	1 40E-01	4 00E 02	0	3 50E+00	1 81E 04	0 02%	No
Mercury	1 60E+00	8 57E 05	1	1 87E+04	9 65E-01	96 49%	Yes
Phenol	1 50E-01	6 00E-01	0	2 50E 01	1 29E-05	0 00%	No
Toluene	5 63E-01	1 10E-01	1	5 11E+00	2 64E-04	0 03%	No
Zinc	2 01E+02	3 00E 01	0	6 70E+02	3 46E 02	3 46%	Yes
Total Risk Factor (Rj)				=	1 93E+04	Total % =	100%

Notes

() The most restrictive of the oral or inhalation reference dose is used

(b) 0 = oral 1 = inhalation

(c) Applicable to all oral critical materials not available

**Table 6-15
Rocky Flats OU 5 Concentration/Toxicity Screen of Radionuclides in Pond Sediment**

PCOC	Maximum Concentration (pci/g)	Slope Factor (risk/pci) ^m	Type of slope factor ^m	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Radionuclides							
Americium 241	4.20E-01	3.20E-08	1	1.34E-08	4.89E-02	4.89%	Y _N
Plutonium 239/240	2.40E+00	3.80E-08	1	9.12E-08	3.32E-01	33.21%	Y _{CS}
Uranium 233/234	3.50E+00	2.70E-08	1	9.45E-08	3.44E-01	34.41%	Y _{CS}
Uranium 235	1.40E-01	2.50E-08	1	3.50E-09	1.27E-02	1.27%	Y _{CS}
Uranium-238	3.00E+00	2.40E-08	1	7.20E-08	2.62E-01	26.22%	Y _{CS}
		Total Risk Factor (Rj) =		2.75E-07	Total % =		100%

Notes

(a) The most restrictive (the oral or inhalation slope factor is used)

(b) 1 = inhalation

Table 6 16
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Seep Sediment

PCOC	Maximum Concentration (mg/kg)	RfD (mg/kg day) (1)	Type of RfD (2)	Chemical Specific Risk Factor (Rf)	Ratio of Rf/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Acetone	1 70E-02	1 00E-01	0	1 70E-01	1 27E-06	0 00%	No
Antimony	5 13E+01	4 00E-04	0	1 28E+05	9 62E-01	96 18%	Y
Beryllium	1 70E+00	5 00E-03	0	3 40E+02	2 55E-03	0 25%	N
Bis(2 ethylhexyl)phthalate	8 00E-02	2 00E-02	0	4 00E+00	3 00E-05	0 00%	No
Fluoranthene	9 70E-02	4 00E-02	0	2 43E+00	1 82E-05	0 00%	N
Methylene chlorid	5 00E-03	6 00E-02	0	8 33E-02	6 25E-07	0 00%	N
Nickel	2 50E+01	2 00E-02	0	1 25E+03	9 37E-03	0 94%	N
Phenanthrene	8 20E-02	n/a					N
Pyrene	9 70E-02	3 00E-02	0	3 23E+00	2 42E-05	0 00%	N
Tetrachloroethene	1 00E-03	1 00E-02	0	1 00E-01	7 50E-07	0 00%	N
Zinc	1 05E+03	3 00E-01	0	3 50E+03	2 62E-02	2 62%	Y s
Total Risk Factor (R _i) =				1 33E+05	Total % =		
					100%		

Not
() Ph m t i str u f th oral r inh al at i n r f r n d s i u s d
() t i l
() /) App h b l t x l b l i n t n a i n t a v i l a b l

Table 6-17
Rocky Flats OU 5 Concentration/Toxicity Screen of Carcinogens in Seep Sediment

PCOC	Maximum Concentration (mg/kg)	Slope Factor (mg/kg-day) ^{1 (a)}	Type of Slope Factor ^(b)	Chemical Specific Risk Factor (R _i)	Ratio of R _i /R _j	Percentage of Total Risk Factor	Consider a COC?
Carcinogens							
Benz(a)anthracene	3.80E-02	7.30E-01	0	2.77E-02	1.94E-03	0.19%	No
Beryllium	1.70E+00	8.40E+00	1	1.43E+01	9.98E-01	99.80%	Y
Bis(2-ethyl-6-terphenyl)phthalate	8.00E-02	1.40E-02	0	1.12E-03	7.83E-05	0.01%	No
Chrysene	4.10E-02	7.30E-03	0	2.99E-04	2.09E-05	0.00%	No
Methylene chloride	5.00E-03	7.50E-03	0	3.75E-05	2.62E-06	0.00%	No
Tetrachloroethene	1.00E-03	5.20E-02	0	5.20E-05	3.63E-06	0.00%	No
Total Risk Factor (R _j) =				1.43E+01	Total % =		100%

Notes

(a) The most restrictive of the oral or inhalation slope factor is used

(b) 0 = oral 1 = inhalation

Table 6-18
Rocky Flats OU 5 Concentration/Toxicity Screen of Radionuclides in Seep Sediment

PCOC	Maximum Concentration (pCi/g)	Slope Factor (risk/pCi) ^(a)	Type of Slope Factor ^(b)	Chemical Specific Risk Factor (Ri)	Ratio of Ri/Rj	Percentage of Total Risk Factor	Consider a COC?
Radionuclides							
Uranium 233/234	2.00E+00	2.70E-08	1	5.40E-08	3.70E-01	36.97%	Yes
Uranium 235	1.30E-01	2.50E-08	1	3.25E-09	2.23E-02	2.23%	Yes
Uranium 238	3.70E+00	2.40E-08	1	8.88E-08	6.08E-01	60.80%	Yes
Total Risk Factor (Rj)				1.46E-07	Total % =	100%	

Notes

- (a) The most restrictive of the oral or inhalation slope factor is used
(b) 1 = inhalation

Table 6-19
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Stream Sediment

PCOC	Maximum Concentration (mg/kg)	RfD (mg/kg day) ^(a)	Type of RfD ^(b)	Chemical Specific Risk Factor (Rf)	Ratio of Rf/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Copper	1.36E+02	4.00E-02	0	3.39E+03	8.22E-02	8.22%	Yes
Mercury	3.05E+00	8.60E-05	1	3.55E+04	8.60E-01	86.05%	Yes
Zinc	7.09E+02	3.00E-01	0	2.36E+03	5.73E-02	5.73%	Yes
Total Risk Factor (Rf) =				4.12E+04	Total % =		100%

Notes

(a) The most restrictive of the oral or inhalation reference dose is used

(b) 0 = oral 1 = inhalation

Table 6-16
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Seep Sediment

PCOC	Maximum Concentration (mg/kg)	RfD (mg/kg-day)	Type of RfD	Chemical Specific Risk Factor (Rf)	Ratio of Rf/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Acetone	1 70E-02	1 00E-01	0	1 70E-01	1 27E-06	0 00%	No
Antimony	5 13E-01	4 00E-04	0	1 28E+05	9 62E-01	96 18%	Yes
Beryllium	1 70E+00	5 00E-03	0	3 40E+02	2 55E-03	0 25%	No
Bis(2 ethylhexyl)phthalate	8 00E-02	2 00E-02	0	4 00E+00	3 00E-05	0 00%	No
Fluoranthene	9 70E-02	4 00E-02	0	2 43E+00	1 82E-05	0 00%	No
Methylene chloride	5 00E-03	6 00E-02	0	8 33E-02	6 25E-07	0 00%	No
Nickel	2 50E-01	2 00E-02	0	1 25E+03	9 37E-03	0 94%	No
Phenanthrene	8 20E-02	n/a					No
Pyrene	9 70E-02	3 00E-02	0	3 23E+00	2 42E-05	0 00%	No
Tetrachloroethene	1 00E-03	1 00E-02	0	1 00E-01	7 50E-07	0 00%	No
Zinc	1 05E+03	3 00E-01	0	3 50E+03	2 62E-02	2 62%	Yes
Total Risk Factor (Rf) =				1 33E+05	Total % =		100%

Notes:
 () Phthalate substituted for formaldehyde
 () - 1
 () Applicable to 161 nitrate is available

**Table 6-18
Rocky Flats OU 5 Concentration/Toxicity Screen of Radionuclides in Sheep Sediment**

PCOC	Maximum Concentration (pci/g)	Slope Factor (risk/pci)^m	Type of Slope Factor^m	Chemical Specific Risk Factor (R_i)	Ratio of R_i/R_j	Percentage of Total Risk Factor	Consider a COC?
Radionuclides							
Uranium 233/234	2.00E+00	2.70E-08	1	5.40E-08	3.70E-01	36.97%	Yes
Uranium 235	1.30E-01	2.50E-08	1	3.25E-09	2.23E-02	2.23%	Yes
Uranium 238	3.70E+00	2.40E-08	1	8.88E-08	6.08E-01	60.80%	Yes
Total Risk Factor (R_j) =				1.46E-07	Total % =		100%

Notes

- (a) The most restrictive of the oral or inhalation slope factor is used
 (b) 1 = inhalation

Table 6-19
Rocky Flats OU 5 Concentration/Toxicity Screen of Noncarcinogens in Stream Sediment

PCOC	Maximum Concentration (mg/kg)	RfD (mg/kg day) (1)	Type of RfD (a)	Chemical Specific Risk Factor (Rf)	Ratio of Rf/Rj	Percentage of Total Risk Factor	Consider a COC?
Noncarcinogens							
Copper	1.36E+02	4.00E-02		3.39E+03	8.22E-02	8.22%	Yes
Mercury	3.05E+00	8.60E-05	1	3.55E+04	8.60E-01	86.05%	Yes
Zinc	7.09E+02	3.00E-01	0	2.36E+03	5.73E-02	5.73%	Yes
Total Risk Factor (Rt)				4.12E+04	Total % =	100%	

N tes

(a) The most restrictive of the oral or inhalation reference dose is used

(b) 0 = oral 1 = inhalation

Table 6-21
Rocky Flats OU 5 Comparison of Concentrations to RBCs for Infrequently Detected Analytes in Surface Soil

Analyte	Range of Detected Concentrations (mg/kg)		Detection Frequency (%)	Range of Reporting Limits (mg/kg)		Range of Non-detect Values (mg/kg)		Residential Soil RBC (mg/kg) ¹	Max. Detected Concentration > RBC?	Max. Detected Concentration 1000 x RBC?	Max Non detect?	Percent of Non detect?
	Minimum	Maximum		Minimum	Maximum	Minimum	Maximum					
Organics												
Acenaphthylene	6.00E-01	6.00E-01	13	3.30E-1	1.5E+00	3.60E-01	2.30E-00	N ²	N	N	Y	6.9
Aldrin	1.70E-02	1.70E-02	14	8.00E-03		8.00E-03	8.60E-02	3.77E-02	N	N	Y	6.9
Butylbenzylphthalate	2.20E-01	2.20E-01	13	3.30E-01		3.60E-01	1.10E-00	5.49E-04	N	N	N	0.0
4,4-DDT	2.10E-02	2.10E-02	14	8.00E-03	1.60E-02	1.60E-02	1.70E-01	1.88E-00	N	N	N	0.0
Dieldrin	3.40E-02	3.40E-02	14	8.00E-03	1.60E-02	1.60E-02	1.70E-01	4.00E-02	N	N	Y	20.8
Di-n-octyl phthalate	8.30E-02	8.30E-02	13	3.30E-01		3.60E-01	1.10E-00	4.67E+01	N	N	N	0.0
Endosulfan sulfate	2.40E-02	2.40E-02	14	8.00E-03	1.60E-02	1.60E-02	1.70E-01	1.65E-03	N	N	N	0.0
Endrin ketone	3.60E-02	3.60E-02	14	8.00E-03	1.60E-02	1.60E-02	1.70E-01	N ³	N	N	Y	1.4
Heptachlor epoxide	1.00E-02	1.00E-02	14	8.00E-03		8.00E-03	8.60E-02	7.04E-02	N	N	Y	1.4
Isophorone	9.60E-02	9.60E-02	13	3.30E-01		3.60E-01	1.10E-00	6.74E+02	N	N	N	0.0
Menthylol	4.60E-01	4.60E-01	14	8.00E-03	8.00E-02	8.00E-02	8.60E-01	1.37E-03	N	N	N	0.0
Inorganics												
Antimony	3.98E-01	4.98E+01	24	1.20E-01		1.20E-01	1.76E-01	1.10E-02	N	N	N	0.0

N I
Applicable RBCs used RBC
Rocky Flats RBC

Table 6-21
Rocky Flats OU 5 Comparison of Concentrations to RBCs for Infrequently Detected Analytes in Surface Soil

Analyt	Range of Detected Concentrations (mg/kg)		Det tion Frequency (%)	Range of Reporting Limit (mg/kg)	Range of Non-detect Values (mg/kg)		Re id ntial Soil RBC (mg/kg) ^{1a}	Max. D tected Concentration > RBC?	Max D t t d Conc ntration 1000 x RBC?	Max Non d t t>	P rcnt of Non d t t>
	Minimum	Maximum			Minimum	Maximum					
Organic											
A enaphthyl n	6 00E-01	6 00E-01	13	3 30E 1 1 5E 00	3 50E-01	2 30E 00	n/				
Aldrin	1 70E-02	1 70E-02	14	8 00E-03	8 00E-03	8 50E-02	3 77E-02	N	N	Y	6 9
Butylbenzylphthal te	2 20E-01	2 20E-01	13	3 30E-01	3 50E-01	1 10E 00	5 49E 04	N	N	N	0 0
4,4-DDT	2 10E-02	2 10E-02	14	8 00E-03 1 60E-02	1 60E-02	1 70E-01	1 88E 00	N	N	N	0 0
Dh ldrin	3 40E-02	3 40E-02	14	8 00E-03 1 60E-02	1 60E-02	1 70E-01	4 00E-02	N	N	Y	208
Di -octyl phthal te	8 30E-02	8 30E-02	13	3 30E-01	3 50E-01	1 10E 00	4 57E 01	N	N	N	0 0
Endo ulf n sulfate	2 40E-02	2 40E-02	14	8 00E-03 1 60E-02	1 60E-02	1 70E-01	1 65E 03	N	N	N	0 0
E drin k tone	3 60E-02	3 60E-02	14	8 00E-03 1 60E-02	1 60E-02	1 70E-01	n/				
H ptachl r po de	1 00E-02	1 00E-02	14	8 00E-03	8 00E-03	8 50E-02	7 04E-02	N	N	Y	14
Isophorone	9 60E-02	9 60E-02	13	3 30E-01	3 50E-01	1 10E 00	6 74E 02	N	N	N	0 0
M tho y hlor	4 50E-01	4 50E-01	14	8 00E-03 8 00E-02	8 00E-02	8 50E-01	1 37E 03	N	N	N	0 0
Inorganics											
Antimony	3 98E 01	4 98E+01	24	1 20E 01	1 20E 01	1 76E 01	1 10E 02	N	N	N	0 0

N

(✓) Analytical RBC (✓) used RBC
(✓) Rocky Flats FPRC used RBC

**Table 6-23
Rocky Flats OU 5 Comparison of Concentrations to RBCs for Infrequently Detected Analytes in Groundwater**

Analyte	Range of Detected Concentrations (mg/L)		Detection Frequency (%)	Range of Reporting Limits (mg/L)		Range of Non-detect Value (mg/L)		Residential Groundwater RBC	Max. Detected Can entrainment > RBC?	Max. Detected Concentration > 1000 x RBC?	Max Non detect?	Percent of Non detect?
	Minimum	Maximum		Minimum	Maximum	Minimum	Maximum					
Methylene chloride	6.00E-03	6.00E-03	48	1.00E-04	1.00E-02	1.00E-04	1.00E-02	6.22E-03	N	N	Y	44

Note

() Rocky Flats PPRG air used as RBC

Table 6-23
Rocky Flats OU 5 Comparison of Concentrations to RBCs for Infrequently Detected Analytes in Groundwater

Analyte	hl rid	Range of Detected Concentrations (mg/L)		Detection Frequency (%)	Range of Reporting Limit (mg/L)	Range of Non-detect Value (mg/L)		Residual Groundwater RBC	Max. Detected Concentration > RBC?	Max. Detected Concentration 1000 x RBC?	Max. Non-detect >	Percent of Non-detect >
		Minimum	Maximum			Minimum	Maximum					
Methyl	hl rid	6.00E-03	6.00E-03	4.8	1.00E-04	1.00E-04	1.00E-02	6.22E-03	N	N	Y	4.4

Note

() Rocky Flats PPRG are used as RBC

Table 6 25
Rocky Flats OU 5 Summary of Chemicals of Concern by Medium

Chemical of Concern	Surface Soil	Subsurface Soil	Groundwater	Surface Water	Seep Water	Pond Sediment	Seep Sediment	Stream Sediment
Acetone			X					
Aluminum			X					
Antimony		X					X	
Aroclor 1254	X	X						
Barium			X	X				
Benzo(a)anthracene	X	X						
Benzo(a)pyrene	X	X						
Benzo(b)fluoranthene	X	X					X	
Beryllium		X	X					
Cadmium		X						
Copper	X	X						X
Dibenz(a,h)anthracene	X							
1,1-Dichloroethene					X			
1,2-Dichloroethene					X			
Fluoranthene	X							
Indeno(1,2,3-cd)pyrene	X							
Lithium				X				
Manganese			X					
Mercury	X					X		X
Molybdenum		X						
Nickel		X						
Pyrene	X							
Silver	X	X						
Strontium				X				
Tetrachloroethene					X			
Trichloroethene					X			
Vanadium			X					
Zinc						X	X	X

Table 6-25 (continued)

Chemical of Concern	Surface Soil	Subsurface Soil	Ground-water	Surface Water	Seep Water	Pond Sediment	Seep Sediment	Stream Sediment
Radionuclides								
Americium 241			X	X		X		X
Plutonium 239/240			X			X		X
Radium 226			X					
Uranium 233/234	X	X	X	X		X	X	
Uranium 235	X	X	X			X	X	
Uranium 238	X	X	X	X		X	X	

Table 6 26
Summary of Current and Future Land Uses^{a,b}

Land Use Category	Current			Future	
	Offsite	Onsite (OU 5)	Offsite	Onsite (OU 5)	
Residential	Yes	No	Credible	Credible	Improbable
Office Complex	Yes	No	Credible	Credible	Credible
Commercial/Industrial	Yes	No	Credible	Credible	Improbable
Open Space	Yes	No	Credible	Credible	Credible ^d
Ecological Reserve	No	No	Improbable	Credible ^d	Credible ^d
Agricultural	Yes	No	Credible	Credible	Improbable
Gravel Mining	Yes	No	Credible	Credible	Improbable ^e

^a Credible is used to indicate scenarios that may reasonably occur
^b Improbable is used to indicate scenarios that are unlikely to occur
^c Expected in the currently developed area of the plant site but not in the OU 5 area
^d Expected in the Site buffer zone including the OU 5 area

Table 6-27
Rocky Flats OU 5 Receptors and Pathways

Potentially Exposed Receptor		Potentially Complete Exposure Pathways by AOC	
		IHSS 115/196 Source Area (AOC 1)	IHSS 133 Source Area (AOC 2)
			SID C 2 Woman Creek C 1 Source Area (AOC 3)
Current			
Onsite worker (security guard)	Dermal contact with surface soil	Dermal contact with surface soil	Dermal contact with surface soil
	Inhalation of airborne particulates	Inhalation of airborne particulates	Inhalation of airborne particulates
	Ingestion of surface soil	Ingestion of surface soil	Ingestion of surface soil
	External irradiation	External irradiation	External irradiation
Future			
Onsite construction worker	Dermal contact with surface and subsurface soil	Dermal contact with surface and subsurface soil	Dermal contact with surface and subsurface soil
	Dermal contact with seep sediments	Dermal contact with seep sediments	Dermal contact with seep sediments
	Inhalation of airborne particulates	Inhalation of airborne particulates	Inhalation of airborne particulates
	Ingestion of surface and subsurface soil	Ingestion of surface and subsurface soil	Ingestion of surface and subsurface soil
	External irradiation	External irradiation	External irradiation
Onsite office worker	Dermal contact with surface soil	Dermal contact with surface soil	Dermal contact with surface soil
	Dermal contact with seep sediments	Dermal contact with seep sediments	Dermal contact with seep sediments
	VOCs in indoor air	VOCs in indoor air	Inhalation of VOCs in indoor air
	Inhalation of airborne particulates	Inhalation of airborne particulates	Inhalation of airborne particulates
	Ingestion of surface soil	Ingestion of surface soil	Ingestion of surface soil
	External irradiation	External irradiation	External irradiation

TABLE 6-27 (Continued)

Potentially Exposed Receptor		Potentially Complete Exposure Pathways by AOC		
		IHSS 115/196 Source Area (AOC 1)	IHSS 133 Source Area (AOC 2)	SID C-2 Woman Creek, C 1 Source Area (AOC 3)
Onsite ecological researcher	Dermal contact with surface soil	Dermal contact with surface soil	Dermal contact with surface soil	Dermal contact with surface water
	Dermal contact with seep sediments	Dermal contact with seep sediments	Dermal contact with seep sediments	Dermal contact with sediments
	Inhalation of airborne particulates	Inhalation of airborne particulates	Inhalation of airborne particulates	Ingestion of surface water
	Ingestion of surface soil	Ingestion of surface soil	Ingestion of surface water	Ingestion of sediments
	Ingestion of seep sediments	Ingestion of seep sediments		
Onsite open-space receptor	External irradiation	External irradiation	External irradiation	
	Dermal contact with surface soil	Dermal contact with surface soil	Dermal contact with surface water	
	Dermal contact with seep sediments	Dermal contact with seep sediments	Dermal contact with sediments	
	Inhalation of airborne particulates	Inhalation of airborne particulates	Ingestion of surface water	
	Ingestion of surface soil	Ingestion of seep sediments		
	Ingestion of seep sediments			
	External irradiation	External irradiation		

Table 6 28
Chemical Specific Concentrations for AOC1

(Chemical Concentration)	Surface Soil (mg/kg)	Sub surf Soil (mg/kg)	Groundwater (mg/L)	Surface Water (mg/L)	Soil Water (mg/L)	P nd Sediment (mg/kg)	Sediment (mg/kg)	St m nt (mg/kg)	(p rti ul te)
Aluminum									
Antimony			1 2E+02						
Aroclor 1254	6 1E+01	7 2E+00					5 1E+01		
Barium			1 5E+00						3 8E+09
Benzo(a)anthracene	1 1E+00	1 2E+00							1 7E+08
Benzo(a)pyrene	8 2E-01	1 1E+00							1 6E+08
Benzo(b)fluoranthene	1 1E+00	1 2E+00							1 9E+08
Beryllium		7 8E+01	9 6E+03				1 7E+00		
Cadmium		5 9E+01							
Copper	2 7E+01	4 4E+01							1 7E+10
Dibenzo(a,h)anthracene	5 0E+01								3 5E+09
1,1 Dichloroethene					4 0E+03				
1,2-Dichloroethene					4 0E-03				
Fluoranthene	1 9E+00								4 8E+08
1,2,3,4-dibenzopyrene	1 4E+00								1 2E+08
Fluorene									
Manganese			7 8E+00						
Molybdenum	1 2E+01								7 2E+12
Nickel		2 5E+01							
Pyrene		2 1E+01							
Silver	1 7E+00								4 3E+08
Strontium	1 6E+00	2 2E+00							5 8E+14
Tetrachloroethene									
Trichloroethene					2 8E-02				
Vanadium					7 0E-03				
Zinc			2 8E-01						
Americium 241							7 0E+01		
Plutonium-239/240			9 0E-02						1 6E+08
Radium-226			4 5E-01						5 3E+08
Uranium-233/234			4 4E+00						
Uranium-235	9 6E+00	1 7E+00	4 9E+01				1 4E+00		6 6E+06
Uranium-238	2 7E+00	1 3E-01	4 0E+00				1 1E-01		1 6E+05
	8 1E+01	1 6E+00	4 4E+01				1 2E+00		8 8E+04

Note: R denotes concentrations in units of pCi/g for soil, pCi/L for water, and pCi/m for air

**Table 6-29
Chemical-specific Concentrations for AOC2**

Chemical	Surface Soil (mg/kg)	Subsurface Soil (mg/kg)	Groundwater (mg/l)	Surface Water (mg/l)	Deep Water (mg/l)	1 st Sediment (mg/kg)	Deep Sediment (mg/kg)	Shoreline (μ g/g)	Air (μ g/m ³)
Acetone									
Aluminum			3.6E+02				4.4E+01		
Antimony		9.5E+00							
Aroclor 1254									
Barium			2.7E+00						
Benzofluoranthene	3.7E-01								4.4E-10
Benzofluoranthene	7.4E-03								4.0E-11
Beryllium		1.3E+00	2.9E-02				1.5E+00		
Cadmium		1.3E+00							
Copper	1.8E+01	4.1E+01							
Dibenz(a,h)anthracene	1.3E-02								9.6E-11
1,1-Dichloroethene						2.5E-03			6.5E-11
1,2-Dichloroethene					2.5E-01				
fluoranthene	8.9E-02								4.7E-10
Indeno(1,2,3-d)pyrene	1.8E-02								9.5E-11
Iron									
Manganese	8.0E-02		3.5E-00						
Molybdenum		2.2E-01							4.2E-15
Nickel		2.3E-01							
Silver	1.1E-01								5.6E-10
Strontium	1.6E+00	4.3E+00							0.0E+00
Tetrachloroethene					2.5E-03				
Trichloroethene					2.5E-03				
Vanadium			6.7E-01						
Zinc									
Americium 241			6.0E-02				1.1E+03		
Plutonium 239/240			3.3E-01						1.5E-07
Radium-226			3.9E+00						4.9E-07
Uranium-233/234	5.2E+00	3.4E+00	7.6E+00				2.0E-00		6.1E-05
Uranium 235	3.5E-01	5.9E-01	4.7E-01				1.3E-01		8.3E-06
Uranium 238	1.4E+01	9.1E-00	1.1E-01				3.7E-00		3.6E-04

Note: Radium-226, Uranium-233/234, Uranium-235, and Uranium-238 are in units of pCi/g of soil.

Table 6 30
Chemical specific Concentrations for AOC3

(Chemical of Concern)	Soil (mg/kg)	Subsurf (mg/kg)	Groundwater (mg/l)	Surface Water (mg/L)	Seep Water (mg/l)	Ind Sediment (mg/kg)	Sediment (mg/kg)	Air (parts ul u) (mg/m)
Asbestos								
Aluminum			5.2E+00					
Antimony		6.0E+00						
Aroclor 1254		2.1E 01						1.6E 10
Barium			9.4E-02	1.0E 01				
Benzo(a)anthracene		4.4E 01						1.7E 10
Benzo(a)pyrene		4.4E 01						1.4E-10
Benzo(b)fluoranthene		4.4E-01						1.9E-10
Beryllium		1.6E+00	4.0E-03					
Cadmium		6.2E+00						
Copper		3.4E+01					2.2E+02	9.5E 12
Dibenz(a,h)anthracene								6.5E 11
1,1-Dichloroethene								
1,2-Dichloroethene								
Fluoranthene								2.4E 10
Indeno(1,2,3-d)pyrene								8.0E 11
Lead				2.2E 02				
Manganese			1.6E+01			1.6E+00	2.2E+00	4.0E 14
Molybdenum		2.0E+01						
Nickel		1.8E+01						
Polychlorinated biphenyls								
Silver		1.0E+00						2.8E 10
Strontium				3.1E 01				2.4E 13
Trichloroethylene								
Vanadium			4.3E-02					
Zinc						2.4E+02	6.0E+02	
Americium-241			5.0E-01	8.0E-02		4.5E 01	2.9E-01	7.1E-09
Plutonium-238/240			1.0E-02			2.5E+00	1.6E+00	2.3E 08
Radium-226			4.6E+02					
Uranium-233/234		1.1E+00	3.1E+03	1.9E+00		3.3E+00		3.7E 06
Uranium-235		9.0E-02	1.4E+00			2.1E-01		4.8E 07
Uranium-238		1.6E+00	8.3E-01	2.1E+00		2.9E+00		2.5E-05

NOTE: Radioisotope concentrations are in units of pCi/g for soil and pCi/L for water and pCi/m³ for air

Table 6-31
OUS COC Chemical-Specific Parameters

Analyte	Oral RID (mg/kg day)	Oral CSF (mg/kg day)	Inhalation RID (mg/kg day)	Inhalation CSF (mg/kg day)	External CSF (ns/kg-yr per pc/vg)	EPA Cancer Weight of Evidence	Dermal Absorption Factor	Dermal Permeability (cm/hr)	GI Matrix Effect
Acetone	1 00E 01	NA	NA	NA	NA	NA	NA	6 00E 4	1 00E+00
Aluminum	2 90E+00	NA	NA	NA	NA	NA	NA	NA	1 00E+00
Antimony	4 00E 04	NA	NA	NA	NA	NA	NA	NA	5 00E 01
Aroclor 1254	2 00E 05	7 70E+00	NA	NA	NA	B2	6 00E-02	7 10E 01	5 00E 01
Barium	7 00E 02	NA	1 43E 04	NA	NA	NA	NA	NA	1 00E+00
Benzo(a)anthracene	NA	7 30E 01	NA	NA	NA	B2	5 00E 02	8 10E 01	1 00E+00
Benzo(a)pyrene	NA	7 30E+00	NA	NA	NA	B2	5 00E 02	1 20E+00	1 00E+00
Benzo(b)fluoranthene	NA	7 30E 01	NA	NA	NA	B2	5 00E 02	1 20E+00	1 00E+00
Beryllium	5 00E 03	4 30E+00	NA	8 40E+00	NA	B2	NA	NA	5 00E 01
Cadmium	1 00E 03	NA	NA	6 30E+00	NA	NA	1 00E 02	NA	1 00E+00
Copper	4 00E 02	NA	NA	NA	NA	D	NA	NA	1 00E+00
Dibenzo(a,h)anthracene	NA	7 30E+00	NA	NA	NA	B2	5 00E 02	2 70E+00	1 00E+00
1 1 Dichloroethene	9 00E 03	6 00E 01	NA	1 20E+00	NA	C	NA	1 60E 02	1 00E+00
1 2 Dichloroethene	9 00E 03	NA	NA	NA	NA	NA	NA	1 00E 02	1 00E+00
Fluoranthene	4 00E 02	NA	NA	NA	NA	NA	5 00E 02	3 60E 01	5 00E 01
Indeno(1 2 3-cd)pyrene	NA	7 30E 01	NA	NA	NA	B2	5 00E 02	1 90E+00	1 00E+00
Lithium	2 00E 02	NA	NA	NA	NA	NA	NA	NA	1 00E+00
Manganese	5 00E 03	NA	1 43E 05	NA	NA	D	NA	NA	1 00E+00

Table 6 31 (Continued)

Analyte	Oral RID (mg/kg day)	Oral CSF (mg/kg day)	Inhalation RID (mg/kg day)	Inhalation CSF (mg/kg day)	External CSF (risk/yr per pCi/g)	EPA Cancer Weight of Evidence	Dermal Absorption Factor	Dermal Permeability (cm/hr)	GI Matrix Effect
Mercury	3 00E 04	NA	8 60E 05	NA	NA	D	NA	NA	1 00E+00
Molybdenum	5 00E-03	NA	NA	NA	NA	NA	NA	NA	1 00E+00
Nickel	2 00E 02	NA	NA	NA	NA	NA	NA	NA	1 00E+00
Pyrene	3 00E-02	NA	NA	NA	NA	D	5 00E 02	NA	5 00E 01
Silver	5 00E 03	NA	NA	NA	NA	D	NA	NA	1 00E+00
Strontium	6 00E 01	NA	NA	NA	NA	NA	NA	NA	1 00E+00
Tetrachloroethene	1 00E 02	5 20E 02	NA	2 00E 03	NA	B2	NA	3 70E 01	1 00E+00
Trichloroethene	NA	1 10E 02	NA	6 00E 03	NA	B2	NA	2 30E 01	1 00E+00
Vanadium	7 00E 03	NA	NA	NA	NA	NA	NA	NA	1 00E+00
Zinc	3 00E 01	NA	NA	NA	NA	D	NA	NA	1 00E+00
Americium 241	NA	2 40E 10	NA	3 20E 08	4 90E 09	A	NA	NA	1 00E+00
Plutonium 239/240	NA	2 30E 10	NA	3 80E 08	2 70E 11	A	NA	NA	1 00E+00
Radium 226	NA	1 20E 10	NA	3 00E 09	6 00E 06	A	NA	NA	1 00E+00
Uranium 233/234	NA	1 60E 11	NA	2 70E 08	4 20E 11	A	NA	NA	1 00E+00
Uranium 235	NA	1 60E 11	NA	2 50E 08	2 40E 07	A	NA	NA	1 00E+00
Uranium 238	NA	2 00E 11	NA	2 40E-08	5 10E 08	A	NA	NA	1 00E+00

NA= Value is not available

Table 6-32

Note Radi nucl d intak re in units f pCi
 --- - not ppl bl pathw y
 NA 1 COC for th medium to ity f to 1 variable

Table 6-33

Note Radi nuclide intake are in units of pCi

-- not an applicable pathway

NA	not a COC for the medium	r no toxicity factor is available

Table 6-34

[illegible]

Note Radii include 1-tk re in units of ρ_{C1}

--- - not a ppl1 bl pathway

NA -- not a COC for this medium r no to city factor 1 a all bl

Table 6-35
Office Worker RME Carcinogenic Chemical Intakes for AOC1

[illegible]

Note Radionuclide intake re in units of pCi

--- -- not an applicable pathway y

NA = not a COC for this medium r no toxicity factor is available.

Table 6-36
Open Space User RME Carcinogenic Chemical Intakes for AOC1

Chemical of Concern	Ingestion of Soil (mg/kg day)	Ingestion of Subsurface Soil (mg/kg day)	Ingestion of Food Sediment (mg/kg-day)	Ingestion of Sheep Sediment (mg/kg-day)	Ingestion of Soil in Air (mg/kg-day)	Ingestion of Soil in Water (mg/kg-day)	Ingestion of Sheep Wastewater (mg/kg-day)	Inhalation of Airborne Particulate (mg/kg-day)	Dermal Absorption of Surface Soil (mg/kg-day)	Dermal Absorption of Soil (mg/kg-day)	Dermal Absorption of Sediment (mg/kg-day)	Dermal Absorption of Soil in Air (mg/kg-day)	Dermal Absorption of Soil in Water (mg/kg-day)	Dermal Absorption of Sheep Wastewater (mg/kg-day)	Estimated Exposure Factor
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Antimony	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Arsenic	5.1E-09	NA	NA	NA	NA	NA	NA	9.4E-12	8.2E-08	NA	NA	NA	NA	NA	NA
Barium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene	1.8E-08	NA	NA	NA	NA	NA	NA	4.3E-11	NA	NA	NA	NA	NA	NA	NA
Benzene	1.4E-08	NA	NA	NA	NA	NA	NA	4.0E-11	NA	NA	NA	NA	NA	NA	NA
Benzene	1.8E-08	NA	NA	NA	NA	NA	NA	4.7E-11	NA	NA	NA	NA	NA	NA	NA
Benzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Copper	4.6E-07	NA	NA	NA	NA	NA	NA	4.2E-13	NA	NA	NA	NA	NA	NA	NA
Dibenz(a,h)anthracene	8.4E-09	NA	NA	NA	NA	NA	NA	8.8E-12	NA	NA	NA	NA	NA	NA	NA
Dibenz(b,h)anthracene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Fluoranthene	1.6E-08	NA	NA	NA	NA	NA	NA	1.2E-10	NA	NA	NA	NA	NA	NA	NA
Indeno(1,2,3-cd)pyrene	2.3E-08	NA	NA	NA	NA	NA	NA	2.9E-11	NA	NA	NA	NA	NA	NA	NA
Lead	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Mercury	2.0E-09	NA	NA	NA	NA	NA	NA	1.8E-14	NA	NA	NA	NA	NA	NA	NA
Molybdenum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Nickel	1.4E-08	NA	NA	NA	NA	NA	NA	1.1E-10	NA	NA	NA	NA	NA	NA	NA
Phenanthrene	2.7E-08	NA	NA	NA	NA	NA	NA	1.4E-16	NA	NA	NA	NA	NA	NA	NA
Pyrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Thiophene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Americium 241	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Plutonium 239/240	NA	NA	NA	NA	NA	NA	NA	7.0E-06	NA	NA	NA	NA	NA	NA	NA
Radon-226	NA	NA	NA	NA	NA	NA	NA	2.4E-04	NA	NA	NA	NA	NA	NA	NA
Uranium 235/234	2.9E-02	NA	NA	NA	NA	NA	NA	2.9E-01	NA	NA	NA	NA	NA	NA	NA
Uranium 238	8.2E-01	NA	NA	NA	NA	NA	NA	6.9E-02	NA	NA	NA	NA	NA	NA	NA
Uranium 235	2.4E-03	NA	NA	NA	NA	NA	NA	3.9E-00	NA	NA	NA	NA	NA	NA	NA

Note: Radon nuclear decay rate in units of pCi
 --- not a plausible pathway
 NA not COC for this medium or too toxic factor; a and b)

Table 6-37
Construction Worker CT Carcinogenic Chemical Intakes for AOC1

[illegible]

Note Radi nuclide intakes are in units of pCi

-- = not applicable pathway

NA -- not a COC for this medium r n toxicity factor is available

Table 6-36
Current Worker CT Carcinogenic Chemical Intakes for AOCI

Chemicals of Concern	Ingestion of Surface Soil (mg/kg-day)	Ingestion of Surface Soil (mg/kg-day)	Ingestion of Pond Sediments (mg/kg-day)	Ingestion of Deep Sediments (mg/kg-day)	Ingestion of Stream Sediments (mg/kg-day)	Ingestion of Surface Water (mg/kg-day)	Ingestion of Deep Water (mg/kg-day)	Inhalation of Airborne Particulate (mg/kg-day)	Dermal Absorption of Surface Soil (mg/kg-day)	Dermal Absorption of Surface Soil (mg/kg-day)	Dermal Absorption of Pond Sediments (mg/kg-day)	Dermal Absorption of Deep Sediments (mg/kg-day)	Dermal Absorption of Stream Sediments (mg/kg-day)	Dermal Absorption of Surface Water (mg/kg-day)	Dermal Absorption of Deep Water (mg/kg-day)	Excretion Rate (mg/kg-day)
Acetone	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Antimony	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Arsenic-1264	1.4E-09	NA	NA	NA	NA	NA	NA	9.4E-12	1.1E-06	NA	NA	NA	NA	NA	NA	NA
Barium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzofluoranthene	4.8E-09	NA	NA	NA	NA	NA	NA	4.3E-11	NA	NA	NA	NA	NA	NA	NA	NA
Benzofluoranthene	3.6E-09	NA	NA	NA	NA	NA	NA	4.0E-11	NA	NA	NA	NA	NA	NA	NA	NA
Benzofluoranthene	4.8E-09	NA	NA	NA	NA	NA	NA	4.1E-11	NA	NA	NA	NA	NA	NA	NA	NA
Beryllium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Copper	1.2E-07	NA	NA	NA	NA	NA	NA	4.2E-13	NA	NA	NA	NA	NA	NA	NA	NA
Dibenzofluoranthene	2.2E-09	NA	NA	NA	NA	NA	NA	8.7E-12	NA	NA	NA	NA	NA	NA	NA	NA
1,1-Dichlorobenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
1,2-Dichlorobenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Fluoranthene	4.2E-09	NA	NA	NA	NA	NA	NA	1.2E-10	NA	NA	NA	NA	NA	NA	NA	NA
Indeno(1,2,3-cd)pyrene	6.0E-09	NA	NA	NA	NA	NA	NA	2.9E-11	NA	NA	NA	NA	NA	NA	NA	NA
Phenanthrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Pyrene	5.3E-10	NA	NA	NA	NA	NA	NA	1.0E-14	NA	NA	NA	NA	NA	NA	NA	NA
Methylmercury	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Nickel	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Pyrene	3.7E-07	NA	NA	NA	NA	NA	NA	1.1E-10	NA	NA	NA	NA	NA	NA	NA	NA
Pyrene	7.8E-09	NA	NA	NA	NA	NA	NA	1.4E-16	NA	NA	NA	NA	NA	NA	NA	NA
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Trichloroethylene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Trichloroethylene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Americium-241	NA	NA	NA	NA	NA	NA	NA	6.9E-05	NA	NA	NA	NA	NA	NA	NA	NA
Plutonium-239/240	NA	NA	NA	NA	NA	NA	NA	2.4E-04	NA	NA	NA	NA	NA	NA	NA	NA
Radium-226	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Uranium-235/234	7.5E-01	NA	NA	NA	NA	NA	NA	2.9E-01	NA	NA	NA	NA	NA	NA	NA	NA
Uranium-235	2.1E-01	NA	NA	NA	NA	NA	NA	6.9E-02	NA	NA	NA	NA	NA	NA	NA	NA
Uranium-238	6.4E-02	NA	NA	NA	NA	NA	NA	3.9E-00	NA	NA	NA	NA	NA	NA	NA	NA

NA = Not available
 --- = Not applicable
 NA = Not available
 COC = Carcinogenic
 this medium = this medium
 r = relative
 n = number
 toxicity factor = toxicity factor
 val = value

Table 6-40
Office Worker CT Carcinogenic Chemical Intakes for AOC1

Chemical	Inhalation of Air (mg/kg day)	Inhalation of Soil (mg/kg day)	Ingestion of Pond Sediments (mg/kg day)	Ingestion of Deep Sediments (mg/kg day)	Ingestion of Stream Sediments (mg/kg day)	Ingestion of Surface Water (mg/kg day)	Ingestion of Deep Water (mg/kg day)	Inhalation of Automobile Exhaust (mg/kg day)	Dermal Absorption from Skin (mg/kg day)	Dermal Absorption from Subsoil (mg/kg day)	Dermal Absorption from Pond Sediments (mg/kg day)	Dermal Absorption from Deep Sediments (mg/kg day)	Dermal Absorption from Surface Water (mg/kg day)	Dermal Absorption from Deep Water (mg/kg day)	Residual Risk (mg/kg day)
Acetone	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Antimony	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Arsenic	6.8E-10	NA	NA	NA	NA	NA	NA	7.1E-12	6.8E-09	NA	NA	NA	NA	NA	NA
Barium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene	3.4E-09	NA	NA	NA	NA	NA	NA	3.3E-11	NA	NA	NA	NA	NA	NA	NA
Benzene	1.8E-09	NA	NA	NA	NA	NA	NA	3.0E-11	NA	NA	NA	NA	NA	NA	NA
Benzene	2.4E-09	NA	NA	NA	NA	NA	NA	3.0E-11	NA	NA	NA	NA	NA	NA	NA
Benzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	6.0E-08	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Copper	1.1E-09	NA	NA	NA	NA	NA	NA	3.2E-13	NA	NA	NA	NA	NA	NA	NA
Dibenz(a,h)anthracene	NA	NA	NA	NA	NA	NA	NA	6.8E-12	NA	NA	NA	NA	NA	NA	NA
1,1-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Phenanthrene	2.1E-09	NA	NA	NA	NA	NA	NA	9.1E-11	NA	NA	NA	NA	NA	NA	NA
Indene(1,2,3-cd)pyrene	8.0E-09	NA	NA	NA	NA	NA	NA	3.2E-11	NA	NA	NA	NA	NA	NA	NA
Naphthalene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Manganese	2.0E-10	NA	NA	NA	NA	NA	NA	1.4E-14	NA	NA	NA	NA	NA	NA	NA
Molybdenum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Nickel	1.9E-09	NA	NA	NA	NA	NA	NA	6.1E-11	NA	NA	NA	NA	NA	NA	NA
Pyrene	3.5E-09	NA	NA	NA	NA	NA	NA	1.1E-16	NA	NA	NA	NA	NA	NA	NA
Silica	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Starch	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Tar	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Asbestos	NA	NA	NA	NA	NA	NA	NA	6.8E-05	NA	NA	NA	NA	NA	NA	NA
Plutonium	NA	NA	NA	NA	NA	NA	NA	1.8E-04	NA	NA	NA	NA	NA	NA	NA
Radium	3.8E-01	NA	NA	NA	NA	NA	NA	2.2E-01	NA	NA	NA	NA	NA	NA	NA
Uranium	1.1E-01	NA	NA	NA	NA	NA	NA	5.3E-02	NA	NA	NA	NA	NA	NA	NA
Uranium	3.2E-02	NA	NA	NA	NA	NA	NA	3.0E-03	NA	NA	NA	NA	NA	NA	NA

Note: Radionuclide intake are in units of pCi.
 - = not an applicable pathway
 NA = not a COC for this medium or a toxicity factor is available

Table 6-41

Note	1950-1952	1953-1954	1955-1956	1957-1958	1959-1960	1961-1962	1963-1964	1965-1966	1967-1968	1969-1970	1971-1972	1973-1974	1975-1976	1977-1978	1979-1980	1981-1982	1983-1984	1985-1986	1987-1988	1989-1990	1991-1992	1993-1994	1995-1996	1997-1998	1999-2000	2001-2002	2003-2004	2005-2006	2007-2008	2009-2010	2011-2012	2013-2014	2015-2016	2017-2018	2019-2020	2021-2022	2023-2024	2025-2026	2027-2028	2029-2030	2031-2032	2033-2034	2035-2036	2037-2038	2039-2040	2041-2042	2043-2044	2045-2046	2047-2048	2049-2050	2051-2052	2053-2054	2055-2056	2057-2058	2059-2060	2061-2062	2063-2064	2065-2066	2067-2068	2069-2070	2071-2072	2073-2074	2075-2076	2077-2078	2079-2080	2081-2082	2083-2084	2085-2086	2087-2088	2089-2090	2091-2092	2093-2094	2095-2096	2097-2098	2099-2100	2101-2102	2103-2104	2105-2106	2107-2108	2109-2110	2111-2112	2113-2114	2115-2116	2117-2118	2119-2120	2121-2122	2123-2124	2125-2126	2127-2128	2129-2130	2131-2132	2133-2134	2135-2136	2137-2138	2139-2140	2141-2142	2143-2144	2145-2146	2147-2148	2149-2150	2151-2152	2153-2154	2155-2156	2157-2158	2159-2160	2161-2162	2163-2164	2165-2166	2167-2168	2169-2170	2171-2172	2173-2174	2175-2176	2177-2178	2179-2180	2181-2182	2183-2184	2185-2186	2187-2188	2189-2190	2191-2192	2193-2194	2195-2196	2197-2198	2199-2200	2201-2202	2203-2204	2205-2206	2207-2208	2209-2210	2211-2212	2213-2214	2215-2216	2217-2218	2219-2220	2221-2222	2223-2224	2225-2226	2227-2228	2229-2230	2231-2232	2233-2234	2235-2236	2237-2238	2239-2240	2241-2242	2243-2244	2245-2246	2247-2248	2249-2250	2251-2252	2253-2254	2255-2256	2257-2258	2259-2260	2261-2262	2263-2264	2265-2266	2267-2268	2269-2270	2271-2272	2273-2274	2275-2276	2277-2278	2279-2280	2281-2282	2283-2284	2285-2286	2287-2288	2289-2290	2291-2292	2293-2294	2295-2296	2297-2298	2299-2300	2301-2302	2303-2304	2305-2306	2307-2308	2309-2310	2311-2312	2313-2314	2315-2316	2317-2318	2319-2320	2321-2322	2323-2324	2325-2326	2327-2328	2329-2330	2331-2332	2333-2334	2335-2336	2337-2338	2339-2340	2341-2342	2343-2344	2345-2346	2347-2348	2349-2350	2351-2352	2353-2354	2355-2356	2357-2358	2359-2360	2361-2362	2363-2364	2365-2366	2367-2368	2369-2370	2371-2372	2373-2374	2375-2376	2377-2378	2379-2380	2381-2382	2383-2384	2385-2386	2387-2388	2389-2390	2391-2392	2393-2394	2395-2396	2397-2398	2399-2400	2401-2402	2403-2404	2405-2406	2407-2408	2409-2410	2411-2412	2413-2414	2415-2416	2417-2418	2419-2420	2421-2422	2423-2424	2425-2426	2427-2428	2429-2430	2431-2432	2433-2434	2435-2436	2437-2438	2439-2440	2441-2442	2443-2444	2445-2446	2447-2448	2449-2450	2451-2452	2453-2454	2455-2456	2457-2458	2459-2460	2461-2462	2463-2464	2465-2466	2467-2468	2469-2470	2471-2472	2473-2474	2475-2476	2477-2478	2479-2480	2481-2482	2483-2484	2485-2486	2487-2488	2489-2490	2491-2492	2493-2494
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4

Note Radionuclide intake are in units of pCi
 -- = not an applicable pathway
 NA - not a COC for this medium r no toxicity factor is available

Table 6-44
Ecological Worker Dose Carcinogenic Chemical Intakes for AOC2

Chemicals of Concern	Ingestion of Large Use f Surface Soil (mg/kg-day)	Ingestion of Subsurface Soil (mg/kg-day)	Ingestion of Pond Sediments (mg/kg-day)	Ingestion of Deep Sediments (mg/kg-day)	Ingestion of Stream Sediments (mg/kg-day)	Ingestion of Surface Waste (mg/kg-day)	Ingestion of Deep Water (mg/kg-day)	Inhalation of Airborne Particulates (mg/kg-day)	Dermal Absorption f Surface Soil (mg/kg-day)	Dermal Absorption f Subsurface Soil (mg/kg-day)	Dermal Absorption of Pond Sediments (mg/kg-day)	Dermal Absorption of Deep Sediments (mg/kg-day)	Dermal Absorption of Stream Sediments (mg/kg-day)	Dermal Absorption f Surface Waste (mg/kg-day)	Dermal Absorption f Deep Water (mg/kg-day)	Estimated Risk to Exposed
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Antimony	NA	NA	NA	2.1E-07	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Archer 1264	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Barium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzofuran	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzofuran	3.6E-09	NA	NA	NA	NA	NA	NA	4.3E-13	NA	NA	NA	NA	NA	NA	NA	NA
Benzofuran	7.1E-11	NA	NA	NA	NA	NA	NA	3.8E-14	NA	NA	NA	NA	NA	NA	NA	NA
Beryllium	NA	NA	NA	7.3E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Copper	1.7E-07	NA	NA	NA	NA	NA	NA	6.3E-14	NA	NA	NA	NA	NA	NA	NA	NA
Dibenzofuran	1.2E-10	NA	NA	NA	NA	NA	NA	5.6E-14	NA	NA	NA	NA	NA	NA	NA	NA
1,1 Dichlorobenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
1,2 Dichlorobenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Fluoranthene	4.3E-10	NA	NA	NA	NA	NA	NA	4.1E-13	NA	NA	NA	NA	NA	NA	NA	NA
Indeno[1,2,3-cd]pyrene	1.6E-10	NA	NA	NA	NA	NA	NA	6.3E-14	NA	NA	NA	NA	NA	NA	NA	NA
Lithium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Manganese	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Mercaptyl	7.7E-10	NA	NA	NA	NA	NA	NA	3.6E-16	NA	NA	NA	NA	NA	NA	NA	NA
Methylbenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Nicot	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Pyrene	5.2E-10	NA	NA	NA	NA	NA	NA	4.6E-13	NA	NA	NA	NA	NA	NA	NA	NA
Silene	1.5E-06	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Suntan	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Tetrachlorobenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Tetrachlorobenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Vinylbenzene	NA	NA	NA	1.6E-05	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Asbestos m 241	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Plastic m 289246	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Radon m 228	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Uranium m 238/234	8.6E-01	NA	NA	3.4E-01	NA	NA	NA	9.4E-02	NA	NA	NA	NA	NA	NA	NA	7.6E-01
Uranium 235	6.6E-00	NA	NA	3.3E-00	NA	NA	NA	1.5E-02	NA	NA	NA	NA	NA	NA	NA	5.3E-02
Uranium 238	3.4E-02	NA	NA	6.4E-01	NA	NA	NA	5.6E-01	NA	NA	NA	NA	NA	NA	NA	2.1E-00

Note: Radionuclide intake are in units of pCi

NA - not applicable pathway

NA - not a COC for this medium or no toxicity factor is available

Table 6-45

[illegible]

Note Radionuclide intake are in units of pCi

--- = Not applicable pathway

NA not a COC for this medium or no toxicity factor is available

NOTICE:

"BEST AVAILABLE COPY"

**PORTIONS OF THE FOLLOWING
DOCUMENT ARE ILLEGIBLE**

The Administrative Record Staff

Table 6-46

NA	not applicable	not an applicable pathway	not applicable to this model	no tax	by factor	variable
Note	Keduo	vehicle	take	are	mls	of pc

Table 8-49
Ecological Worker CT Carcinogenic Chemical Intakes for AOC2

[illegible]

N is Radionuclide i takes are in units of pC

not applicable pathway

NA	not	COC for this medium	no	toxic	factor is	available.

NA not COC for this medium

10

10

10

•

Table 6-50

NA	not	COC	to	this	med	in	no	tax	y	factu	va	l	blat
Note	Radionuclide	take	re	rate	of	PC							
	not	an	applicab	p	th	y							

Table 8-51
Open Space User CT Carcinogenic Chemical Intakes for AOC2

[illegible]

Note Radonucleide intakes are in units of pCi

not an palpable pathway

NA	not	COC for this medium or no contact y facto	o	available.
NA	not	COC for this medium or no contact y facto	o	available.

2A

NA	not	COC for this medium or no longer y factor	o	available.

Table 6-52
Ecological Worker RME Carcinogenic Chemical Intakes for AOC3

Ecological Worker Risk Carcinogenic Chemical Intakes for AOCs														
Chemical	Ingestion (mg/kg day)	Inhalation (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)
Chemical	Ingestion (mg/kg day)	Inhalation (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)	Dermal (mg/kg day)
Acetone	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Antimony	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Aroclor-1248	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Barium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene in the air	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene in the water	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene in the soil	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Beryllium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Chlorine	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Dibenz(a,h)anthracene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
1,1-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
1,2-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Fluoranthene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Indene(1,2,3-cd)pyrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Lithium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Manganese	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Mercury	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Molybdenum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Nickel	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Pyrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Thallium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Aroclor-1248	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene in the air	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene in the water	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene in the soil	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Beryllium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Chlorine	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Dibenz(a,h)anthracene	NA													

Note Radio welds take no miles of PC of applicable pathway NA not COC in this medium no toxicology lab

Table 6-53

Note Radionuclide labels are in units of pCi

NA	not an applicable pathway	not COC for this medium	no toxicity factor is available.

Table B-54

Note	Radionuclide	take	re	rule of PC
		not a	applicable	pathway
NA	not	COC	to this med	in no toxic ly facto
				lable

Table 6-55
Open Space User CT Carcinogenic Chemical Intakes for AOC3

()	In g S f Sh i (ug/kg day)	f ge f S bu f Sa l (g/kg day)	In ge f P ad Sa l m ta (mg/kg day)	I g j Se p Sa l m ta (mg/kg day)	I ge f S ro u Sa l m ta (ug/kg day)	I ge f W te (ng/L day)	I g f Sa p W (g/kg day)	I bal f A bu n f e (ug/kg day)	D al Al so pt q f c Sa l (g/kg day)	D ml Ab o p f S b f Sa l (g/h day)	D tal Ab o p f Ind Sa l (ug/kg day)	D al De o p f Se p Sa l (ug/kg day)	D I Ab o p f Sa l (g/kg day)	D I W te (g/L day)	D t Al so f Sa l m ta (ug/kg day)
Aetone	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Animo y	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Arclo 1254	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Ban m	-	-	NA	-	NA	6 SE-08	-	-	-	-	NA	-	NA	NA	-
Be au(la th ace	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Be au(pyruva	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Benzo(fluor he	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Beryl m	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Cadin m	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Cupre	-	-	NA	-	2 IE-07	NA	-	-	-	-	NA	-	NA	NA	-
Dibenz(hia th acene	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
1,1 Dichloroethane	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
1,2 Dichloroethen	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Fluore the	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Indanol(2,3-cd)pyrene	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Lithu m	-	-	NA	-	NA	14E-08	-	-	-	-	NA	-	NA	NA	-
M g nose	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
M reury	-	-	1 SE-09	-	2 IE-09	NA	-	-	-	-	NA	-	NA	NA	-
M lyble	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
N k i	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Pyre	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Sa	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
T	-	-	NA	-	NA	19E-07	-	-	-	-	NA	-	NA	NA	-
V	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
V adu	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Z	-	-	2 SE-07	-	6 SE-07	NA	-	-	-	-	NA	-	NA	NA	-
Amo i , 241	-	-	7 SE-01	-	5 IE-01	9 OE-02	-	-	-	-	NA	-	NA	NA	-
Pfuent m 239240	-	-	4 SE-00	-	2 SE-00	NA	-	-	-	-	NA	-	NA	NA	-
Rach m 226	-	-	NA	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Urethan 88/234	-	-	5 IE-00	-	NA	2 IE-00	-	-	-	-	NA	-	NA	NA	-
Urethan 235	-	-	3 IE-01	-	NA	NA	-	-	-	-	NA	-	NA	NA	-
Urethan 238	-	-	5 IE-00	-	NA	24E-00	-	-	-	-	NA	-	NA	NA	-

Note Redonucleide intakes re n units of pCi
not an applicable pathway

NA not COC for this medium or no toxicity factor is available.

Tablo 6-56

Note Radionuclide intake are in units of pCi
 -- not in ppb by pathway
 NA -- is a COC for the medium to city factor
 at the

Table 6-57
Current Worker FIME Noncarcinogenic Chemical Intakes for AOC1

[illegible]

Note Radionuclide intakes are in units of pCi

--- = not an applicable pathway

NA not a COC for this medium or no toxicity factor is available

Table 6-58

Note	Read	let	take	are	rate of PC
NA	not	COC	to	in	no toxic ty facto
	not	an	plausible	pathway	lable

Table 6-59
Office Worker RME Noncarcinogenic Chemical Intakes for AOC1

Chemicals of Concern	Ingestion Surface Soil (mg/kg day)	Ingestion Subsurface Soil (mg/kg day)	Ingestion of Pond Sediments (mg/kg day)	Ingestion of Sediment (mg/kg day)	Ingestion of Surface Water (mg/kg day)	Ingestion of Seep Water (mg/kg day)	Inhalation of Airborne (mg/kg day)
Acetone	NA	-	-	-	-	-	NA
Aluminum	NA	-	-	-	-	-	NA
Antimony	NA	-	-	-	-	-	NA
Aroclor 1254	1.5E-07	-	-	-	-	-	2.1E-10
Barium	NA	-	-	-	-	-	NA
Benzo(a)anthracene	5.3E-07	-	-	-	-	-	9.6E-10
Benzo(a)pyrene	4.0E-07	-	-	-	-	-	8.8E-10
Benzo(b)fluoranthene	5.4E-07	-	-	-	-	-	1.0E-09
Beryllium	NA	-	-	-	-	-	NA
Cadmium	NA	-	-	-	-	-	NA
Copper	1.3E-06	-	-	-	-	-	9.4E-12
Dibenz(a,h)anthracene	2.4E-07	-	-	-	-	-	1.9E-10
1,1-Dichloroethene	NA	-	-	-	-	-	NA
1,2-Dichloroethene	NA	-	-	-	-	-	NA
Fluoranthene	4.6E-07	-	-	-	-	-	2.7E-09
Indeno(1,2,3-cd)pyrene	6.7E-07	-	-	-	-	-	6.4E-10
Lead	NA	-	-	-	-	-	NA
Manganese	NA	-	-	-	-	-	NA
Mercury	5.9E-08	-	-	-	-	-	4.0E-13
Molybdenum	NA	-	-	-	-	-	NA
Nickel	NA	-	-	-	-	-	NA
Pyrene	4.1E-07	-	-	-	-	-	2.4E-09
Silver	7.8E-07	-	-	-	-	-	3.2E-15
Strontium	NA	-	-	-	-	-	NA
Tetrachloroethene	NA	-	-	-	-	-	NA
Trichloroethene	NA	-	-	-	-	-	NA
Vanadium	NA	-	-	-	-	-	NA
Zinc	NA	-	-	-	-	-	NA
Americium 241	NA	-	-	-	-	-	NA
Plutonium-238/240	NA	-	-	-	-	-	NA
Radium-226	NA	-	-	-	-	-	NA
Uranium-233/234	NA	-	-	-	-	-	NA
Uranium-235	NA	-	-	-	-	-	NA
Uranium-238	NA	-	-	-	-	-	NA

Not listed in units (p) not applicable
NA not available for this medium or no toxicity factor is available

Table 6-60
Adult Open Space User RME Carcinogenic Chemical Intakes for AOC1

Chemical (CAS #)	Ingestion of Surface Soil (mg/kg-day)	Ingestion of Subsurface Soil (mg/kg-day)	Ingestion of Pond Sediment (mg/kg-day)	Ingestion of Seap Sediment (mg/kg-day)	Ingestion of Stream Sediment (mg/kg-day)	Ingestion of Surface Water (mg/kg-day)	Ingestion of Deep Water (mg/kg-day)	Inhalation of Airborne Particulate Matter (mg/kg-day)	Dermal Absorption of Seap Soil (mg/kg-day)	Dermal Absorption of Subsurface Soil (mg/kg-day)	Dermal Absorption of Pond Sediment (mg/kg-day)	Dermal Absorption of Seap Sediment (mg/kg-day)	Dermal Absorption of Surface Water (mg/kg-day)	Dermal Absorption of Subsurface Water (mg/kg-day)	Dermal Absorption of Pond Water (mg/kg-day)	Dermal Absorption of Seap Water (mg/kg-day)	Excretion (mg/kg-day)
Acetone	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Asbestos	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Asphalt	1.5E-08	NA	NA	NA	NA	NA	NA	2.2E-11	1.9E-07	NA	NA	NA	NA	NA	NA	NA	NA
Benzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene Anthracene	5.3E-08	NA	NA	NA	NA	NA	NA	1.0E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene Pyrene	4.0E-08	NA	NA	NA	NA	NA	NA	9.3E-11	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzophenone Anthracene	5.4E-08	NA	NA	NA	NA	NA	NA	1.1E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA
Beryllium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Copper	1.3E-06	NA	NA	NA	NA	NA	NA	9.8E-13	NA	NA	NA	NA	NA	NA	NA	NA	NA
Dibenz(a,h)anthracene	2.4E-08	NA	NA	NA	NA	NA	NA	2.0E-11	NA	NA	NA	NA	NA	NA	NA	NA	NA
1,2-Dichloroethane	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
1,2-Dichlorobenzene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Fluorene Anthracene	4.6E-08	NA	NA	NA	NA	NA	NA	2.8E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA
Indeno(1,2,3-cd)pyrene	6.7E-08	NA	NA	NA	NA	NA	NA	6.7E-11	NA	NA	NA	NA	NA	NA	NA	NA	NA
Lead	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Mercury	5.4E-09	NA	NA	NA	NA	NA	NA	4.2E-14	NA	NA	NA	NA	NA	NA	NA	NA	NA
Molybdenum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Nickel	NA	NA	NA	NA	NA	NA	NA	2.5E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA
Phenanthrene	7.4E-08	NA	NA	NA	NA	NA	NA	3.3E-16	NA	NA	NA	NA	NA	NA	NA	NA	NA
Pyrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Trichloroethylene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Asbestos	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Polycyclic aromatic hydrocarbons (PAHs)	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Radon	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Uranium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Uranium-235	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Uranium-238	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA

Not Ready to be included in the units of the
 - not applicable pathway
 NA 1 COC for the medium term to city factor 1 a table

Table 6-61
Child Open Space User RME Noncarcinogenic Chemical Intakes for AOC1

[illegible]

Not Radionuclide intakes are in units of pCi

-- -- not an appliablw pathw y

NA - not COC for this medium no tox city factor 1 a all bl

Table 6-62

[illegible]

Not Radi nuclide intake are in units of pCi

--- not an applicable pathway

NA = not COCf this in drum r n toxic factor : a alab

Table 6-64

Not Radi uclide intake re in units f pCi
--- not n pplicable p thw y
NA - n t COC f th medium tr n toxicity facto al bl

Table 6-65
Office Worker CT Noncarcinogenic Chemical Intakes for AOC1

Not. Radi nuclide intakes are in units of pCi

--- not a pllicable pathway

NA not COC for the medium r n toxicity factor is avail bl

Table 6-66

[illegible]

Not Radi uel deniak rei unit fpc
-- not n plicabl pathw y
NA - n t GOC f r th medium r n toxicity factor i a alab

Table 6-68

Not Radi	nucleide intake	are n units	f PC ₁
--	not n applicabl	pathway	
NA	n t COC f r th	medium	no to cty factor i

Table 6-69

Not Radionuclide intake are in units of pCi

~ not applicable pathway

NA not a COC for this medium r no toxicity factor is available

Table 6-70

Not Redoncul de intak re n unites f pCi
 -- = not ppl c bl p thw y
 NA n t COC f thus medium n toxicity facto i alabl

Table 6-71
Office Worker RIME Noncarcinogenic Chemical Intakes for AOC2

[illegible]

Note Radi nuclide intake are in units of pCi

--- = not an applicable pathw y

NA - not a COC for this medium or no toxicity factor 1

Table 6-72

[illegible]

Note	Radical	used in	units	factors
--	not	used in <td>units <td>factors</td> </td>	units <td>factors</td>	factors
NA	not	used in <td>units <td>factors</td> </td>	units <td>factors</td>	factors

Table 6-73
Child Open Space User RME Noncarcinogenic Chemical Intakes for AOC2

[illegible]

Not Radionuclide intakes are in units of pCi

-- -- not an applicable pathway

NA	not a COC for this medium	no toxicity factor is available

Table 6-74

[illegible]

NA	not COG fo	hi med m	rw box	y facto	1 bl
Note	Radonuclei	take re	ml of pc		
	not an pplic	blep thw	y		

Table 6-75

NA to Radonoclide takes are in nts of μCi
not an plicable pathway
NA not COC for this modit m no toxicity factor is available

Table 6-76

Note	Radonucleotide	take	are	note	of	PC
N/A	not	COC	to	hi	mod	in
						no
						tox
						ty
						facto
						table

Table 8-77
Office Worker CT Noncarcinogenic Chemical Intakes for AOC2

[illegible]

Note: Radionuclide intakes are in units of μCi .

not applicable p thway

NA	not	COC for the	media	is	no	toxicity	factor	is	available.
----	-----	-------------	-------	----	----	----------	--------	----	------------

Table 6-78

[illegible]

Note	Ratio	include	take	re	rate of	pC
not	ppu	the	p	th	y	
NA	no	COC	for	this	med	in
					no	toxic
					by	facto
						table

Table 6-79
Child Open Space User CT Noncarcinogenic Chemical Intakes for AOC2

[illegible]

Note Radionuclide taken in units of μCi
not an applicable pathway
NA not COC for this medium or no toxicity factor is available.

Table 8-80
Ecological Worker RME Noncarcinogenic Chemical Intakes for AOC3

[illegible]

Notes Radio uclide take re nu of pC
an applicable pathway
NA not COC fu hi mod m no tox by facto

Table 8-81

Note: Radionuclide intakes are in units of μCi not an applicable pathway y NA not COC for this medium no toxicity factor is available.

Table B-82

NA no COC for this mod in no toxic by factor

Table 6-84

NA	not	COC	for this medium	no	hazard	factor	available
Note	Each	include	take	are	rate of	PC	
	at	applicable	pathway				

Table 6-86
Carcinogen Groups

Weight of Evidence	Description
A	Human Carcinogen (sufficient evidence of carcinogenicity in humans)
B	Probable Human Carcinogen (B1 limited evidence of carcinogenicity in humans B2 sufficient evidence of carcinogenicity in animals with inadequate or lack of evidence in humans)
C	Possible Human Carcinogen (limited evidence of carcinogenicity in animals and inadequate or lack of human data)
D	Not Classifiable as to Human Carcinogenicity (inadequate or no evidence)
E	Evidence of Noncarcinogenicity for Humans (no evidence of carcinogenicity in adequate studies)

Table 6-87
Construction Worker RME Carcinogenic Risk Factors for AOC1

Ch	I C n o e n	I g S r f c e S o l	I g S b e r f c e S o l	I g f f u n d b e d m n i s	I g t a S e p S e d m	I g S r e m S e d m	I g S f c e W t e	I g S e p W t e	f h a l f A i r b u r P r t l e	D e r m a l A b s o p f S f e S o l	D e r m a l A b s o p S b e f a c S o l	D e r m a l A b s o p f A l s o p t i o P a d S e d	D e r m a l A b s o p f S t r e i S e d m t	D e r m a l A b s o p f S f e W t e	D e r m a l A b s o p f R a i E a y e
Acetone	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
A m m	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
A m y	19E-08	63E-09	NA	--	--	--	--	--	NA	NA	77E-09	NA	NA	NA	NA
Bari m	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Be so l a th e n	63E-09	63E-09	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Benzol pyren	48E-08	64E-08	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Be so l m q r n i s	64E-09	71E-09	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Beryll m	NA	14E-08	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Cadm m	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Copper	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
D benzol h i a th reo ne	29E-08	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
11D chloroth na	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
12D chlorothene	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Fl o a th	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
I ch a d 123-cy pyro m	80E-09	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
I l i t h m	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Mang nose	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
M re ry	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
M lyld m	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
N k l	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Pyre	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
S i	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
f f h i h	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
f f h	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
V adu	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Z	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
A .41	NA	NA	NA	--	--	--	--	--	14E-13	NA	NA	NA	NA	NA	NA
P i m 23P240	NA	NA	NA	--	--	--	--	--	58E-13	NA	NA	NA	NA	NA	NA
Radi m 226	NA	NA	NA	--	--	--	--	--	NA	NA	NA	NA	NA	NA	NA
Uran m 233/234	22E-09	39E-10	NA	--	--	--	--	--	51E-10	NA	NA	NA	NA	NA	NA
Uran m 235	63E-10	30E-11	NA	--	--	--	--	--	11E-10	NA	NA	NA	NA	NA	NA
Uran m 239	23E-08	45E-10	NA	--	--	--	--	--	60E-09	NA	NA	NA	NA	NA	NA
	14E-07	99E-08	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	6.6E-09	2.3E-08	77E-09	0.0E+00	0.0E+00	0.0E+00	1.4E-07

- not an applicable pathway

NA not a COC for this medium or no toxicity factor is available

Table 6-68

1

NA

NA not a COC r this medium r n to rctly factio : all bl

Table 6-90
Office Worker PNE Carcinogenic Risk Factors for AOC1

[illegible]

not an applicable pathway
not COC if this medium is a toxicity factor and all

Table 6-82
Construction Worker CT Carcinogenic Risk Factors for AOC1

Chemical of Concern	Ingestion of Surface Soil	Ingestion of Subsurface Soil	Ingestion of Pond Sediments	Ingestion of Deep Sediments	Ingestion of Stream Sediments	Ingestion of Surface Water	Ingestion of Soap Waste	Inhalation of Airborne Particulate	Dermal Absorption of Surface Soil	Dermal Absorption of Subsurface Soil	Dermal Absorption of Pond Sediments	Dermal Absorption of Deep Sediments	Dermal Absorption of Stream Sediments	Dermal Absorption of Surface Water	Dermal Absorption of Soap Waste	External Radiation Exposure	TIR Risk by Chemical
Acetone	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Antimony	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Arsenic-154	3.4E-09	1.2E-09	NA	NA	NA	NA	NA	NA	4.0E-09	1.4E-09	NA	NA	NA	NA	NA	NA	1.0E-09
Barium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Benz(a)anthracene	1.1E-09	1.2E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.3E-09
Benz(b)fluoranthene	6.6E-09	1.1E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.0E-09
Benz(k)fluoranthene	1.1E-09	1.2E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.4E-09
Beryllium	NA	2.4E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.4E-09
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Copper	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Dibenz(a,h)anthracene	5.2E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	5.2E-09
1,1-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
1,2-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Fluoranthene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Indene(1,2,3-cd)pyrene	1.4E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1.4E-09
Lithium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Manganese	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Mercury	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Molybdenum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Nickel	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Pyrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Silica	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Selenium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Tetrachloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Trichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Arsenic-154	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Phenanthrene-230/240	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Radon-226	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.06+00
Uranium-238/234	3.6E-10	6.9E-11	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	9.6E-12
Uranium-235	1.1E-10	5.3E-12	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	8.8E-10
Uranium-238	4.2E-09	8.0E-11	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1.6E-08
Rate by pathway																	1.6E-07
2.6E-08	1.8E-08	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	5.3E-09	4.0E-09	1.4E-09	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.2E-07	
1.7E-07																	

not possible pathway
NA COC for this medium toxicity factor available

Table 6-93

not an applicable pathway

NA	not	COC for the	medium	r	no toxicity factor is available
NA	not	COC for the	medium	r	no toxicity factor is available

NA

Table 6-94
Ecological Worker CT Noncarcinogenic Hqs for AOC1

Chemical of Concern	Ingestion of Surface Soil	Ingestion of Subsurface Soil	Ingestion of Food of Pond	Ingestion of Deep Sediments	Ingestion of Stream Sediments	Ingestion of Surface Water	Ingestion of Deep Water	Inhalation of Airborne Particulates	Dermal Absorption of Surface Soil	Dermal Absorption of Subsurface Soil	Dermal Absorption of Pond Sediments	Dermal Absorption of Stream Sediments	Dermal Absorption of Surface Water	Dermal Absorption of Deep Water	External Radiation Exposure	Tal Risk by (h m l)
Acetone	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Aluminum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Ammonia	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Arsenic-124	6.1E-09	NA	NA	NA	NA	NA	NA	NA	2.2E-08	NA	NA	NA	NA	NA	NA	0.0E+00
Barium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Benz(a)anthracene	2.1E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Benz(b)pyrene	1.6E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.1E-09
Benz(a)fluoranthene	2.2E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	1.6E-09
Beryllium	NA	NA	NA	6.0E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.2E-09
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	9.9E-09
Copper	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Diethylhexylsebacate	9.9E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
1,1-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	9.9E-09
1,2-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Phenanthrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Indeno(1,2,3-cd)pyrene	2.7E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Ulin m	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.7E-09
Manganese	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Mercury	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Methylalum	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Nickel	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Pyrene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Quin m	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Trichloroethylene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Trichloroethylene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Vanad m	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Americ m 411	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Polonium-210	NA	NA	NA	NA	NA	NA	NA	4.1E-13	NA	NA	NA	NA	NA	NA	NA	4.1E-13
Radon-222	NA	NA	NA	NA	NA	NA	NA	1.7E-12	NA	NA	NA	NA	NA	NA	NA	1.7E-12
Uranium-235/234	7.1E-10	NA	NA	1.1E-10	NA	NA	NA	1.5E-09	NA	NA	NA	NA	NA	NA	NA	4.8E-11
Uranium-235	2.1E-10	NA	NA	8.5E-13	NA	NA	NA	3.2E-10	NA	NA	NA	NA	NA	NA	NA	7.8E-08
Uranium-238	7.0E-09	NA	NA	1.2E-10	NA	NA	NA	1.7E-08	NA	NA	NA	NA	NA	NA	NA	5.0E-07
Risks by pathway																
4.8E-06	0.0E+00	0.0E+00	1.0E-08	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.9E-06	2.2E-08	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	5.8E-07	
Tal risk	6.8E-07															

not applicable pathway y
NA of a COC for the medium r do toxicity factor is available

Table 6-95

-- = not an applicable pathway

NA not a COC for this medium or no toxicity factor is available

Table 6-98
Open Space User CT Carcinogenic Risk Factors for AOC1

Chemical or Compound	Ingestion of Surface Soil	Ingestion of Subsurface Soil	Ingestion of Pond Sediments	Ingestion of Sheep Sediments	Ingestion of Stream Sediments	Ingestion of Surface Water	Ingestion of Sheep Water	Inhalation of Airborne Particulate	Dermal Absorption of Surface Soil	Dermal Absorption of Subsurface Soil	Dermal Absorption of Pond Sediments	Dermal Absorption of Sheep Sediments	Dermal Absorption of Stream Sediments	Dermal Absorption of Surface Water	Dermal Absorption of Sheep Water	External Radiation Exposure	Total Risk (Annual)
Acetone	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Amblygonite	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Ammonium Arsenate 1254	2.3E-09	NA	NA	NA	NA	NA	NA	NA	2.9E-09	NA	NA	NA	NA	NA	NA	NA	5.2E-09
Barytes	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	0.0E+00
Benzofluoranthrene	7.7E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	7.7E-10
Benzofluoranthrene	6.8E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	6.8E-09
Benzofluoranthrene	7.3E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	7.3E-10
Beryllium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Cadmium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Copper	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Dibenzofluoranthrene	3.6E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	3.6E-09
1,1-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
1,2-Dichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Fluoranthene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Indeno(1,2,3-cd)pyrene	9.8E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	9.8E-10
LiAlSi4O10	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Magnetite	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Muscovite	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Nickel sulfide	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Pyrite	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Silver	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Sulfur	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Tetrachloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Trichloroethene	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Vanadium	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Zinc	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Ammonium 241	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Fluoranthene-250/254	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Benzene-252	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA
Uranium-238/234	2.7E-10	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.7E-10
Uranium-235	7.6E-11	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	7.6E-11
Uranium-238	2.8E-09	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	2.8E-09
Risk by pathway																	
	1.7E-08	0.0E+00	0.0E+00	3.7E-09	0.0E+00	0.0E+00	0.0E+00	2.3E-09	2.9E-09	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.5E-07
Total Risk	3.7E-07																

-- = not applicable pathway
NA = not a COC for this medium r no toxicity factor is available

Table 6-95
Current Worker PNE Carcinogenic Risk Factors for AOC2

[illegible]

NA - not applicable
COC - not in COC medium

Table 6-99
Ecological Worker RME Carcinogenic Risk Factors for AOC2

[illegible]

NA not an applicable pathway
-- not a COC for this medium r no toxicity factor 1 available

o plicable p thw y
NA not COC fo hi med m no tox y facto labl

[illegible]

Table 6-101

NA	not COC for this medium	not an applicable pathway	toxicity factor : a label
--			

-- not an applicabl pathway y

Table 6 103
Current Worker CT Carcinogenic Risk Factors for AOC2

[illegible]

not an applicable pathway

NA	not	COC for this medium	r no toxicity factor available.
NA	not	COC for this medium	r no toxicity factor available.

Table 8-104

at an applicable pathway y
not COC for this med in no toxicly facto all bl
NA

Table 6-105

not	applicable pathway	no toxicity factor available.
not	not	not

[illegible]

1	applicable pathway	yes	no	toxicity factor	1
NA	not	COC	in	med	in

Table 6 107
Ecological Worker RME Carcinogenic Risk Factors for AOC3

[illegible]

NA	not applicable pathway	not COC for this medi	no toxicity facto is va

Table 6-106

no applicable pathway
not COC for this med in no toxic y facto all b

no applicable pathway
not COC for this med in no toxic y facto all b

Table 6-109
Ecological Worker CT Carcinogenic Risk Factors for AOC3

[illegible]

of applicable pathway y no toxicity factor is available.

[illegible]

1561

Table 6-112
Current Worker RME Noncarcinogenic HIs for AOCT

[illegible]

Table 6-114
Office Worker PME Noncarcinogenic Hhs for AOC1

[illegible]

NA not COC of the medium or toxicity factor and by

Table 6-115
Adult Open Space User RME Noncarcinogenic H I s for AOC1

[illegible]

-	not applicable pathway
NA	not CUC for this medium or no toxicity factor available

Table 6-116
Child Open Space User Rate Noncarcinogenic HIs for AOC1

[illegible]

not ppl bl p thw y
i COCf th medium to tyfacto i ail bl
NA

Table 6-117

--- = not applicable pathway
NA not a COC for this medium or no toxicity factor 1 available

--- = not applicable pathway

NA not a COC for this medium or no toxicity factor 1 available

Table 6.18

-- not pph b) pathw y
NA not COCf th medium r n to icaly facto 1 avail bl

-- not pph b) pathw y
NA not COCf th medium r n to icaly facto 1 avail bl

Table 6-119

not a applicable pathway
not a COC for this medium r no toxicity factor is avail bl

not a applicable pathway

not a separate pathway

Table 6-120

[illegible]

— t ppl bl p thw y
NA not (X) t thi m dium n to cilyfacto i an l l

Table 6-121
Adult Open Space User CT Noncarcinogenic Hls for AOC1

[illegible]

-- not an applicabl pathway y

NA not a COC for this medium or no toxicity factor is a suitable

Table 6-122
Child Open Space User CT Noncarcinogenic HIs for AOCT

[illegible]

not applicable	not a COC of the medium	toxicity factor	all but
NA	not applicable	toxicity factor	all but

Table 6-123
Construction Worker RME Noncarcinogenic HIs for AOC2

[illegible]

NA	not COC for this medium	not an applicable pathway	no toxicity factor is available

Table 6-124

publica p ihw y
NA not COC fu hu medi m no tunc y facto I ble

NA not COC fu hi medi m no tunc y facto

1 ble

Table 6-125
Ecological Worker RME Noncarcinogenic Hls for AOC2

[illegible]

	-	not an applicable pathway	not COC for this medium or no toxicity factor available.
NA			

Table 6-126

[illegible]

not	iplic bl path	y	no tax	ty facto	! ble
not	COC fo	hi uned			
NA					

Table 6-127

not an applicable pathway	not applicable for this medium	no toxicity factor is available
NA	NA	NA

not an applicable pathway Y

Table 6-129
Construction Worker CT Noncarcinogenic HIs for AOC2

[illegible]

NA	not an applicable pathway	not COC for this media	no toxicity factor is available
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Table 8-130

NA	not	COC fo	hi med m	no tax	y facto	variable
at	pplicable p	thw y				

NA	not	COC fo	hi med m	no tax	y facto	variable
at	pplicable p	thw y				

Table 6-132
Office Worker CT Noncarcinogenic HIs for AOC2

[illegible]

at ppleabl p thw y
not CUC fo hi med m no tax y factu tabl

Table 6-134

Hi by pathw y

no	aplicable pathw y	no toxic y facto	lable
not	COC fo thi used in		
NA			

Table 6-135
Ecological Worker RME Noncarcinogenic HI's for AOC3

[illegible]

NA	not an applicable pathway	COC for this medium	no toxicity factor is available.
NA	not applicable	COC for this medium	no toxicity factor is available.

Table 6-136
Adult Open Space User RME Noncarcinogenic HIs for AOC3

[illegible]

	not applicable	yes	no
pathway y			
COC for this medium			
NA not			
for city factor			
table			

Table 8-137

NA	not an	uptake pathway	no toxicity factor available
NA	not	COC for this medium	

[illegible]

John

Table 8-140

at applicable p the y no toxic y facto is table

Table 6 141
HHRA Uncertainty Factors at OU 5

Uncertainty Factor	Effect of Uncertainty	Comments
Data Collection and Evaluation		
Use of unvalidated data	May slightly over or underestimate risk.	When available and appropriate unvalidated data was replaced with validated data. Unvalidated data used are consistent with previous measurements and should only slightly affect risk estimates. Subsequent evaluation of the validation results for unvalidated data used in the HHRA indicates that no impacts to the conclusions of the HHRA result (see Section 4.1)
Identification and selection of OU 5 PCOCs and COCs	May slightly over or underestimate risk.	Professional judgement was used to analyze and aggregate OU data. However the approved selection process was used and agency meetings were held to minimize uncertainty. Additional discussions regarding lead are contained in the text.
Selection of source areas and AOCs	May slightly underestimate risk.	Professional judgement was used to analyze and aggregate OU data. However the agreed-upon process for selection of source areas and AOCs was used and agency meetings were held to minimize uncertainty. Six source areas were identified resulting in three AOCs.
Arsenic was not considered a PCOC in groundwater, pond sediments, and stream sediments.	May slightly underestimate risk.	Background comparison and professional judgement was applied to eliminate arsenic from these media. An agency meeting was held specifically for this issue and all three agencies agreed to this approach.
Pond sediment data collection.	May slightly underestimate risk.	Calculations of inhalation intake of pond sediment used data from the inlet and midpoint sampling locations but not from the deep sampling location. This approach was agreed to by the agencies and is not expected to significantly affect inhalation risk.

Table 6 141 (Continued)

Uncertainty Factor	Effect of Uncertainty	Comments
Exposure Assessment		
Exposure scenario assumptions	May over or underestimate risk.	Exposure scenarios are qualitatively evaluated and documented in the OU 5 Exposure Assessment TM
Exposure parameter assumptions	May slightly over or underestimate risk.	Site specific RFETS exposure factors were used. The values have been reviewed and agreed to by all three agencies and uncertainty is assumed to be low.
Chemical specific matrix effects	May overestimate risk.	Chemical-specific matrix effects were derived for applicable OU 5 COCs. The values are conservative.
Nickel evaluated as a noncarcinogen only	May underestimate risk.	Based on process knowledge at RFETS nickel subsulfide (carcinogenic form) is not expected to be a contaminant in soils.
Dermal exposure	May over or underestimate risk.	Soil adherence factors, skin absorption factors, and dermal permeability can introduce potential uncertainty. Dermal absorption of metals is expected to be insignificant compared to the ingestion pathway.
Toxicity Assessment		
Critical toxicity values derived primarily from animal studies.	May over or underestimate risk.	Extrapolation from animal to humans may induce error due to differences in absorption, pharmacokinetics, target organs, enzymes, and population variability.
Critical toxicity values derived primarily from high doses and OU 5 exposures are at low doses.	May over or underestimate risk.	Assumes a linear extrapolation to low doses. OU 5 exposure assumptions are also conservative.
Critical toxicity values and classification of carcinogens.	May over or underestimate risk.	Not all toxicity values represent the same degree of certainty. All are subject to change as new evidence becomes available.

Table 6-141 (Continued)

Uncertainty Factor	Effect of Uncertainty	Comments
Lack of dermal absorption or direct action toxicity values.	May slightly underestimate risk.	The unavailability of consensus absorption values does not facilitate comparison of absorbed dose to toxicity constants based on administered dose. Dermal absorption of metals is expected to be insignificant when compared to ingestion. Consistent with RAGS dermal absorption of PAHs is not quantitatively evaluated.
Risk Characterization		
Use of cancer slope factors	May overestimate risk.	Potencies are upper 95th percentile confidence limits. Considered unlikely to underestimate true risk.
Lack of toxicological data for some PCOCs	May underestimate risk.	No EPA-established toxicity criteria are provided for benzo(g,h,i)perylene, dibenzofuran, lead, 2-methylnaphthylene, phenanthrene, silicon, and 1,1,1-trichloroethane.
Addition of risks across weight-of-evidence classifications.	May overestimate risk.	Addition of risks across weight-of-evidence classifications is extremely health conservative and potentially even inappropriate.

Table 6-142
Summary of RME Point Estimates of Carcinogenic Risk

Receptor/Location	Total Risk	Dominant COC	Dominant Pathway
Future Construction Worker AOC1	4E 07	uranium 238	Ingestion of surface soil and external radiation
Future Construction Worker AOC2	8E 08	uranium 238	Ingestion of surface soil
Current Security Worker AOC1	3E 05	uranium 238	External radiation
Current Security Worker AOC2	4E 06	uranium 238	External radiation
Future Ecological Researcher AOC1	1E 06	uranium 238	External radiation
Future Ecological Researcher AOC2	2E 07	uranium 238	External radiation
Future Ecological Researcher AOC3	2E 08	plutonium 239/240	Ingestion of pond sediments
Future Office Worker AOC1	3E 05	uranium 238	External radiation
Future Office Worker AOC2	4E 06	uranium 238	External radiation
Future Open Space User AOC1	4E 06	uranium 238	External radiation
Future Open Space User AOC2	6E 07	uranium 238	External radiation
Future Open Space User AOC3	4E 08	plutonium 239/240	Ingestion of pond sediment

Table 6-143
Summary of RME Point Estimates of Noncarcinogenic Hazard Indices

Receptor/Location	Total HI	Dominant COC	Dominant Pathway
Future Construction Worker AOC1	4E 02	Aroclor 1254	Ingestion of subsurface soil
Future Construction Worker AOC2	1E 02	antimony	Ingestion of subsurface soil
Current Security Worker AOC1	7E 02	Aroclor 1254	Dermal absorption of surface soil
Current Security Worker AOC2	5E 04	copper	Ingestion of subsurface soil
Future Ecological Researcher AOC1	4E 02	Aroclor 1254	Dermal absorption of surface soil
Future Ecological Researcher AOC2	2E 02	antimony	Ingestion of seep sediments
Future Ecological Researcher AOC3	4E 03	mercury	Ingestion of stream sediments
Future Office Worker AOC1	5E 02	Aroclor 1254	Dermal absorption of surface soil
Future Office Worker AOC2	5E 04	copper	Ingestion of surface soil
Future Adult Open Space User AOC1	1E 02	Aroclor 1254	Dermal absorption of surface soil
Future Adult Open Space User AOC2	3E 03	antimony	Ingestion of seep sediments
Future Adult Open Space User AOC3	8E 04	mercury	Ingestion of stream sediments
Future Child Open Space User AOC1	4E 02	antimony	Ingestion of seep sediments
Future Child Open Space User AOC2	3E 02	antimony	Ingestion of seep sediments
Future Child Open Space User AOC3	7E 03	mercury	Ingestion of stream sediments

Table 6-144
Effective Dose Conversion Factors for Radionuclides

Radionuclide	$f_1^{(1)}$	Ingestion DCF (Sv/Bq) ⁽²⁾	Lung Clearance Class ⁽¹⁾	Inhalation DCF (Sv/Bq) ⁽²⁾	External DCF (mrem/yr per pCi/ m)
Americium 241	1 00E 03	9 84E 07	W	1 20E 04	2 99E 02
Plutonium 239 ⁽³⁾	1 00E 03	9 56E 07	W	1 16E 04	3 78E 04
Uranium 234 ⁽³⁾	5 00E 02	7 66E 08	W	2 13E 06	8 07E 04
Uranium 235	5 00E-02	7 19E 08	W	1 97E 06	1 90E 01
Uranium 238	5 00E-02	6 88E 08	W	1 90E 06	2 59E 02

⁽¹⁾ Fractional uptake from the small intestine to the blood

⁽²⁾ To convert to conventional units of mrem/pCi multiply the table entry by 3 7E+03

⁽³⁾ Lung clearance class W = weeks

⁽⁴⁾ Used to evaluate Pu 239/240

⁽⁵⁾ Used to evaluate U 233/234

Table 6-144
Effective Dose Conversion Factors for Radionuclides

Radionuclide	$f_1^{(1)}$	Ingestion DCF (Sv/Bq) ⁽²⁾	Lung Clearance Class ⁽¹⁾	Inhalation DCF (Sv/Bq) ⁽³⁾	External DCF (mrem/yr per pCi/ m)
Americium 241	1 00E 03	9 84E 07	W	1 20E 04	2 99E 02
Plutonium 239 ⁽⁴⁾	1 00E 03	9 56E 07	W	1 16E 04	3 78E 04
Uranium 234 ⁽⁵⁾	5 00E 02	7 66E 08	W	2 13E 06	8 07E 04
Uranium 235	5 00E-02	7 19E 08	W	1 97E 06	1 90E 01
Uranium 238	5 00E-02	6 88E 08	W	1 90E 06	2 59E 02

⁽¹⁾ Fractional uptake from the small intestine to the blood

⁽²⁾ To convert to conventional units of mrem/pCi multiply the table entry by 3 7E+03

⁽³⁾ Lung clearance class W = weeks

⁽⁴⁾ Used to evaluate Pu 239/240

⁽⁵⁾ Used to evaluate U 233/234

Table 6 146
Summary of Annual Radiation Dose for AOC2

Pathway	Annual Radiation Dose	
	Central Tendency (mrem/yr)	Reasonable Maximum (mrem/yr)
Construction Worker		
Ingestion of surface soil	1 4E-02	7 4E-02
Ingestion of subsurface soil	9 3E-03	4 9E-02
Inhalation of airborne particulates	1 0E-03	1 1E-03
External irradiation from subsurface soil	7 1E-03	8 8E-03
Total	3 1E-02	1 3E-01
Current Worker		
Ingestion of surface soil	1 1E-02	6 4E-02
Inhalation of airborne particulates	4 9E-03	5 6E-03
External irradiation from surface soil	1 6E-02	3 0E-02
Total	3 2E-02	9 9E-02
Ecological Worker		
Ingestion of surface soil	4 8E-02	3 5E-02
Ingestion of seep sediments	3 3E-03	1 1E-02
Inhalation of airborne particulates	2 4E-03	2 4E-03
External irradiation from surface soil	8 5E-03	1 1E-02
Total	6 2E-02	5 9E-02
Office Worker		
Ingestion of surface soil	5 6E-03	6 4E-02
Inhalation of airborne particulates	3 7E-03	5 6E-03
External irradiation from surface soil	1 6E-02	3 0E-02
Total	2 5E-02	9 9E-02
Open Space Recreational User (adult)		
Ingestion of surface soil	1 3E-03	6 4E-03
Ingestion of seep sediments	3 9E-04	1 9E-03
Inhalation of airborne particulates	2 2E-04	9 4E-04
External irradiation from surface soil	1 4E-03	3 5E-03
Total	3 3E-03	1 3E-02
Open Space Recreational User (child)		
Ingestion of surface soil	1 3E-03	5 5E-02
Ingestion of seep sediments	3 9E-04	2 3E-03
Total	1 7E-03	5 8E-02

Table 6 145
Summary of Annual Radiation Dose for AOC1

Pathway	Annual Radiation Dose	
	Central Tendency (mrem/yr)	Reasonable Maximum (mrem/yr)
Construction Worker		
Ingestion of surface soil	6 5E 02	3 5E-01
Ingestion of subsurface soil	2 5E 03	1 3E-02
Inhalation of airborne particulates	2 1E 03	2 3E-03
External irradiation from subsurface soil	1 6E 03	2 0E-03
Total	7 1E 02	3 6E 01
Current Worker		
Ingestion of surface soil	5 3E 02	3 0E-01
Inhalation of airborne particulates	1 0E 02	1 1E-02
External irradiation from surface soil	1 2E-01	2 3E-01
Total	1 8E-01	5 4E-01
Ecological Worker		
Ingestion of surface soil	1 2E-01	1 7E-01
Ingestion of seep sediments	1 6E-03	5 0E-03
Inhalation of airborne particulates	5 0E-03	5 0E-03
External irradiation from surface soil	6 5E-02	8 1E-02
Total	1 9E-01	2 6E 01
Office Worker		
Ingestion of surface soil	2 6E-02	3 0E 01
Inhalation of airborne particulates	7 6E-03	1 1E-02
External irradiation from surface soil	1 2E-01	1 1E 02
Total	1 6E-01	3 2E-01
Open Space Recreational User (adult)		
Ingestion of surface soil	6 0E-03	3 0E-02
Ingestion of seep sediments	1 8E-04	9 1E-04
Inhalation of airborne particulates	4 6E-04	1 9E-03
External irradiation from surface soil	1 1E-02	2 7E-02
Total	1 7E-02	6 0E-02
Open Space Recreational User (child)		
Ingestion of surface soil	6 0E-03	6 0E-02
Ingestion of seep sediments	1 8E-04	1 8E-03
Total	6 2E 03	6 2E-02

Table 6 147
Summary of Annual Radiation Dose for AOC3

Pathway	Annual Radiation Dose	
	Central Tendency (mrem/yr)	Reasonable Maximum (mrem/yr)
Ecological Worker		
Ingestion of pond sediments	2 6E-02	8 4E-02
Ingestion of stream sediments	1 4E 02	4 6E-02
Ingestion of surface water	9 6E-05	8 2E-04
Total	4 1E-02	1 3E-01
Open Space Recreational User (adult)		
Ingestion of pond sediments	3 1E-03	1 5E-02
Ingestion of stream sediments	1 7E-03	8 4E-03
Ingestion of surface water	1 0E-04	1 0E-03
Total	4 8E-03	2 5E-02
Open Space Recreational User (child)		
Ingestion of pond sediments	6 1E-03	3 1E-02
Ingestion of stream sediments	3 4E-03	1 7E-02
Ingestion of surface water	1 7E-04	3 4E-04
Total	9 6E-03	4 8E-02

Table 6 146
Summary of Annual Radiation Dose for AOC2

Pathway	Annual Radiation Dose	
	Central Tendency (mrem/yr)	Reasonable Maximum (mrem/yr)
Construction Worker		
Ingestion of surface soil	1 4E-02	7 4E-02
Ingestion of subsurface soil	9 3E-03	4 9E-02
Inhalation of airborne particulates	1 0E-03	1 1E-03
External irradiation from subsurface soil	7 1E-03	8 8E-03
Total	3 1E-02	1 3E-01
Current Worker		
Ingestion of surface soil	1 1E-02	6 4E-02
Inhalation of airborne particulates	4 9E-03	5 6E-03
External irradiation from surface soil	1 6E-02	3 0E-02
Total	3 2E-02	9 9E-02
Ecological Worker		
Ingestion of surface soil	4 8E-02	3 5E-02
Ingestion of seep sediments	3 3E-03	1 1E-02
Inhalation of airborne particulates	2 4E-03	2 4E-03
External irradiation from surface soil	8 5E-03	1 1E-02
Total	6 2E-02	5 9E-02
Office Worker		
Ingestion of surface soil	5 6E-03	6 4E-02
Inhalation of airborne particulates	3 7E-03	5 6E-03
External irradiation from surface soil	1 6E-02	3 0E-02
Total	2 5E-02	9 9E-02
Open Space Recreational User (adult)		
Ingestion of surface soil	1 3E-03	6 4E-03
Ingestion of seep sediments	3 9E-04	1 9E-03
Inhalation of airborne particulates	2 2E-04	9 4E-04
External irradiation from surface soil	1 4E-03	3 5E-03
Total	3 3E-03	1 3E-02
Open Space Recreational User (child)		
Ingestion of surface soil	1 3E-03	5 5E-02
Ingestion of seep sediments	3 9E-04	2 3E-03
Total	1 7E-03	5 8E-02

7 0 ECOLOGICAL RISK ASSESSMENT FOR THE WOMAN CREEK PRIORITY DRAINAGE

The ecological risk assessment (ERA) for the Woman Creek Priority Drainage is summarized in this section. ERAs for the Walnut Creek and Woman Creek watersheds were combined and results presented in a single report (Appendix N). The ERAs represent the ecological portions of the baseline risk assessments associated with the RFI/RI for OUs 1, 2, 4 (in part), 5, 6, 7, 10 (in part), and 11. ERAs were formerly planned for each OU, and preliminary ecological field investigations were conducted on that basis. The resulting analyses fulfill the requirements of Attachment 2, Section VIII, Interagency Agreement.

The combined ERA was conducted based on recent agreements among the EPA, CDPHE, and DOE. The agencies agreed that it is ecologically more appropriate to conduct the ERAs for each watershed. This scale is more relevant to ecological receptors because they are not constrained by the administrative boundaries associated with the OUs. ERAs are now required for four areas: (1) the industrial area/protected area (IA/PA), (2) the Walnut Creek watershed, (3) the Woman Creek watershed, and (4) offsite areas including Great Western Reservoir, Standley Lake, and Mower Reservoir. The ERA accompanying this report addresses ecological risks from contaminant sources in the Walnut Creek and Woman Creek watersheds with the Site boundaries but outside of the IA/PA.

An ERA is required to support the Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) Record of Decision or the Resource Conservation and Recovery Act (RCRA) Corrective Action Decision for any of the OUs within the areas mentioned above. Sections within CERCLA include statements that both human health and the environment must be considered when assessing risks associated with releases from hazardous waste sites. Also, the National Contingency Plan (NCP) specifically states that an environmental evaluation must be performed to assess threats to the environment (40 CFR Part 300.430 [e][2][i][G]) during the overall process of assessing the need to remediate a hazardous waste site. The Interagency Agreement (IAG) negotiated among DOE, EPA, and CDPHE states that one objective of the

RFI/RI is to provide data to establish the baseline risk assessment for human health and the environment for the OU. The methodology used here evaluates the likelihood that adverse ecological effects are occurring or may occur as a result of exposure to one or more chemical stressors (EPA 1992d).

7.1 SUMMARY OF ECOLOGICAL RISK ASSESSMENT METHODOLOGY

An ecological risk assessment methodology (ERAM) for the Site was developed to support risk management decisions for individual OUs. The approach used is consistent with a screening level risk assessment appropriate for sites where ecological effects have not been observed but contaminant levels have been measured and can be compared with concentrations considered protective of ecological receptors. The Site ERAM draws from DOE and EPA guidance and ERA tools developed at Oak Ridge National Laboratory (ORNL) and the Savannah River Site (DOE 1993k, 1993b, EPA 1992d, 1994f, Norton *et al.* 1992, Opresko *et al.* 1994).

The ERAM is documented in three technical memoranda (TMs):

ERA TM1: Assessment Endpoints (in preparation)

ERA TM2: Sitewide Conceptual Model

ERA TM3: Ecological Chemicals of Concern (ECOCs) Screening Methodology

The ERA TM1 is currently in preparation and will provide sitewide guidance on developing assessment endpoints, the ecological resources to be protected, and the objectives of the assessments. Specific assessment endpoints and objectives for the Walnut Creek and Woman Creek ERA are identified in Appendix N, Section N4.

The ERA TM2 (DOE 1995f) describes ecological components of the site that are potentially affected by contamination and presents baseline assumptions and parameter values used in exposure estimates and risk characterization. The following information was included in the ERA TM2:

Descriptions of the key ecological features of the Site including vegetation, wildlife, aquatic organisms, and protected species.

Summaries of existing sitewide monitoring programs

Exposure pathway models which describe the contaminant transport and exposure mechanisms important in evaluating exposure of ecological receptors to the chemical stressors at the Site

Selection criteria for the identification of key ecological receptors

General exposure parameters for key receptor species

The ERA TM3 (DOE 1995g) describes a phased approach to identify ECOCs the environmental contaminants that are the focus of risk characterization. Tier 1 screening consisted of identifying contaminants within each source area that were detected at levels above background concentrations. This was done using a statistical methodology developed specifically for the Site. The result of Tier 1 was a list of PCOCs that was further screened in Tier 2 and Tier 3 using ecotoxicity criteria. Tier 2 and Tier 3 screens each required estimates of exposure for the key ecological receptors at the Site. Methods used in Tiers 1, 2, and 3 screening are explained in detail in Appendix N (Section N3). The watershed ERA focused on identification and characterization of ECOCs because chemical stressors are usually of greatest concern for ERAs conducted as part of CERCLA investigations (EPA 1994f).

7.2 PRELIMINARY EXPOSURE AND RISK SCREEN

An initial step in conducting the watershed ERAs was to evaluate contaminant distribution and identify ECOCs. This evaluation required screening level exposure and risk estimations using data collected during RFI/RI activities and sitewide environmental monitoring programs. The screen corresponds to the preliminary exposure and risk calculation step of the EPA procedure for conducting ERAs at Superfund sites (EPA 1994g).

The purpose of the sitewide ERA is to provide information that is useful for both evaluating ecological risk on a watershed basis and making decisions regarding remedial actions associated with the individual OUs and IHSSs within them. Therefore, ecological risks were estimated for distinct subareas of each watershed called ERA source areas which were identified by grouping IHSSs based on OU location and contaminant sources (Figure 7.2.1). Source area boundaries were determined based on abiotic and biotic sampling locations. Risks were quantified for each source area separately and their contribution to overall risk in the watershed was determined.

The primary objective of the ecotoxicity screen is to evaluate exposures to determine if the chemical concentrations represent an ecotoxicological threat. The risk was evaluated by comparing site exposures

to toxicity reference values (TRVs) or benchmark exposures that if exceeded could result in adverse effects. TRVs were derived to represent the No Observed Adverse Effects Level (NOAEL) for sublethal systemic and reproductive effects. The approach to derivation of TRVs is described in TM3. Specific uses of TRVs for the watershed ERAs is presented in Appendix N. Section N3.2.6.

Assistance in developing TRVs was solicited from other sites in the DOE complex and associated academic institutions. Site specific ecotoxicological benchmarks were derived using methods developed at Oak Ridge National Laboratories (ORNL) (Opresko *et al.* 1994). Toxicologists from Clemson University and radioecologists from Oregon State University and Argonne National Laboratory conducted extensive literature searches for the remaining PCOCs and developed preliminary benchmarks. Life history information on representative species found at the Site was obtained from EPA (1993b) or scientific literature and documented by in the ERA TM2 (DOE 1995f).

Risk was estimated by comparing the site exposures to TRVs using the hazard quotient (HQ) approach (EPA 1994f). The HQ is the ratio of the site exposure versus the TRV (exposure – TRV). The hazard index (HI) is the sum of individual HQs for individual chemicals and was used to approximate cumulative risk in an area (DOE 1995g). TRVs and exposures were based on calculating effects on individual organisms. This approach was taken because the most reliable methods for estimating exposure and effects are individual based. Extrapolation to populations or communities was qualitative and based on area of affected habitat, quality of resources, and species specific behaviors.

ECOC screens were conducted for three wide ranging species (coyote, mule deer, and red tailed hawk) and four receptors with more restricted home ranges (limiting species). Risk for wide ranging species was negligible; no HQs or HIs were greater than 1. ECOCs were identified for limiting species and aquatic receptors that may spend all or most of their time in small areas and therefore are in more frequent contact with contaminants. ECOCs were identified by source area and receptor type and included metals, radionuclides, and organic compounds (Table 7.1). Cumulative risks were identified based on HIs (Figure 7.2.2).

7.3 PROBLEM FORMULATION AND RISK CHARACTERIZATION

The preliminary risk screen identified ECOCs based on chemical concentrations in abiotic and biotic media and conservative assumptions concerning exposure and toxicity. The remainder of the ERA focuses

on further characterization of ecological risk from exposure to the ECOCs. Specific objectives and the approach for risk characterization are described in problem formulation (EPA 1994f).

7.3.1 Problem Formulation

The risk characterization has two main goals: (1) refine risk estimates through use of less conservative and more realistic assumptions and characterize remaining uncertainty and (2) identify areas, chemicals, and media contributing to risk. Where feasible, guidance for developing cleanup criteria protective of assessment endpoints was also provided. Where appropriate, exposures and risk were summarized by watershed, OU, and IHSS to aid in risk management and remediation decisions.

Conservative assumptions were used in the Tier 3 screen to improve efficiency of the screen or to account for uncertainty in exposure or toxicity estimates. Conservative assumptions were selected to minimize the probability of underestimating risk so that uncertainty would be biased in only one direction (EPA 1994f). Refinement of risk estimates involved use of less conservative assumptions and/or site data on direct measurement of toxic effects to reduce uncertainty. In most cases, a combination of data types was used in a weight of evidence approach to risk characterization.

The risk characterization for each of the ECOCs included the following activities: (1) refine exposure estimates to more accurately reflect site conditions, including bioavailability, contaminant distribution, and frequency and duration of exposures; (2) refine toxicity estimates based on more specific evaluation of contaminant forms and potential toxicity; (3) review site data to determine if predicted effects were manifested; (4) if appropriate, extrapolate effects on individuals to estimate effects to the Site populations or communities; and (5) identify, characterize, and rank sources of uncertainty and identify data needed to further refine estimates.

The risk characterization focused on the potential toxic effects of ECOCs on five ecological receptor groups:

- 1 Aquatic life
- 2 Aquatic feeding birds
- 3 Terrestrial feeding raptors

- 4 Small mammals
- 5 Vegetation communities

These receptor groups were selected based on results of the ECOC screen presented in Appendix N Section N3 either because potential toxicity from ECOCs was identified or because available data were inadequate to conclude that risk was negligible

Assessment endpoints and specific objectives of the risk characterization were identified for each resource category and presented in Appendix N Table N4.1 Assessment endpoints are explicit expressions of the environmental values to be protected (Suter 1989 and EPA 1992d). The purpose of assessment endpoints in this phase of the watershed ERAs was to focus the risk characterization on potential exposures to ECOCs and the specific effects that may result. The potential for exposure and toxicity was established in the Tier 3 screen. In most cases the specific effect is defined by the toxicological endpoints on which the TRVs were based. Most of these endpoints were based on chronic sublethal or reproductive effects that were not measured at the Site. Results of toxicity testing or other measurements of effects were available for some groups and were used where appropriate.

For each receptor group assessment endpoints, exposure pathways, and specific goals and objectives are identified and described in Appendix N Section N4. Where appropriate, a working null hypothesis (H_0) was defined to help guide analysis and evaluation of uncertainty.

7.3.2 Risk Characterization

The risk characterization was completed using qualitative and quantitative approaches described in the problem formulation step. In some cases the evaluation focused on assessing the adequacy of data used in exposure calculations. In other cases more accurate or quantitative methods were used to estimate frequency or duration of exposures.

Specific measurements of metals, radionuclides, and PCBs in biota were available for evaluating exposures and food web transfers. These data were reliable indicators of exposure (Suter 1993) and were also used to evaluate potential impacts to upper level consumers from ECOCs accumulated in forage or prey. However, for other ECOCs the risk characterization was largely conducted without the benefit of

sampling and analysis specifically designed to evaluate effects of ECOCs. Results of risk characterization are detailed in Appendix N and summarized in the following subsections. Analyses of potential effects on aquatic life for the watersheds were combined. Evaluation of effects on terrestrial biota are discussed for the Woman Creek watershed. Risks are summarized by receptor group, ECOC, and ERA source areas in Table 7.2.

7.3.2.1 Summary of Risks to Aquatic Life

The preliminary risk screen was based on comparisons of chemical concentrations in sediments and surface water to TRVs derived from the literature or calculated using methods recommended by EPA (EPA 1992d). The screen identified several ECOCs in sediments but none for surface water. Sediment ECOCs included volatile and semivolatile organics, PCBs, and metals.

The magnitude of sediment HQ and HI values for some sites in Walnut Creek suggested a high level of toxicity to benthic organisms, especially in the A and B series ponds furthest upstream and closest to the IA of the Site. HQs exceeded 100 for some chemicals at these sites as shown in Appendix N, Figure N5.5. PAHs were the main contributors to risk estimates at most sites in Walnut Creek, accounting for 90 percent or more of the HI in ponds A-1 and B-1. Risk estimates were much lower in the Woman Creek watershed where HIs were below 3; no HQ exceeded 2.6.

The risk levels predicted by the HQ and HI calculations were verified using results of sediment toxicity tests and site data on benthic community structure. If estimates of potential toxicity (i.e., TRVs) and exposures were relatively accurate, then the extremely wide range of HI and HQ values should correspond to varying levels of toxicity to test organisms and impacts on benthic communities. Physical stresses such as fluctuating water levels and the presence of organisms in upper trophic levels (e.g., fish) represent confounding factors in this analysis. However, if toxicity is an important factor in controlling benthic community structure, then results should indicate some level of correlation between predicted toxicity (i.e., HIs or HQs) and level of impacts.

Correlations were evaluated using cluster analysis and regression methods. Cluster analyses (Ludwig and Reynolds, 1988) were conducted to determine if groups of sites with similar community composition (e.g., total organism density and species richness) also had similar HIs or HQs. Regression methods (Sokal and

Rholf 1968) were used to estimate if the proportion of variation in community structure could be explained by differences in HIs

Results indicate that predicted toxicity accounts for some of the variation in community composition but other factors are clearly important. Groups that were identified by cluster analysis based on density richness and pollution tolerance were not similar to those identified when the same analysis was conducted using HIs. However, differences in HIs accounted for about 50 percent of the variation in rank order of ponds with respect to richness. Results of sediment toxicity testing indicated significant toxicity in only Pond B 2 but this pond did not have the highest HIs.

These results suggest that although toxicity tests do not show robust toxicity effects of sediment contamination may be manifested in the benthic community structure of the detention ponds. However, other factors such as size, fluctuating water levels, and the presence or absence of upper trophic levels are also important. Potential toxicity of sediment contaminants, particularly PAHs, may be important factors in limiting aquatic communities if physical stress was reduced through a change in management of the ponds.

It should be noted that the ponds were constructed to minimize offsite transport of contaminants, especially radionuclides, in sediments and surface water. The presence of PAHs and metals in sediments are, in part, a result of runoff from industrial areas and input from the wastewater treatment plant. The fact that sediment contaminant concentrations decrease dramatically with distance downstream indicates that the ponds are effective in attenuating offsite transport of sediment-bound contaminants.

7.3.2.2 Summary of Risks to Aquatic Feeding Birds

Risks from PCBs Sediment contamination in ponds, streams, and wetlands may also affect wildlife that feed in contaminated areas. ECOCs identified for aquatic feeding wildlife in OU 5 included PCBs (Aroclor 1254), mercury, and antimony. Great blue herons and mallards were identified as representative receptors because birds are more sensitive to many contaminants than mammals. Analyses used in the risk characterization are described in Appendix N, Section N4.3. The following subsections provide more detail on methods and present results. Because the analysis approach differed by chemical, results are presented separately for each ECOC.

Aroclor 1254 was identified as an ECOC in the 903 Pad ERA source area, primarily due to concentrations detected in sediments in the SID. The initial risk calculations were based on estimates of PCB uptake by aquatic biota, because no tissue data were available for the site. Initial uptake estimates were based on potential bioconcentration of PCBs from interstitial water. When compared to actual data from the B ponds, this method greatly overestimated tissue concentrations.

Therefore, potential risk from PCB exposure was further evaluated using data from B ponds to establish site specific uptake rates for accumulation of PCBs from sediments. This information was then used to identify sediment PCB concentrations that would result in exposures equal to or less than the TRVs and thus be protective of aquatic birds. These criteria were based on partitioning of PCBs between lipid in biota and organic carbon in sediments. The criteria vary with the intensity of site use and complexity of food chains (see Appendix N Table N5.10). The most restrictive criteria are associated with the highest level of site use and longest food chains. Available data on PCB concentrations in sediments were then compared to the criteria.

Data on total organic carbon in sediment from the SID were not available. However, the maximum Aroclor 1254 concentration detected in bulk sediments (0.26 mg/kg) was below the average concentrations in sediments of Pond A-3, which represented negligible risk even if aquatic feeding birds obtained all of their food from there. Thus, sediments of the SID do not appear to represent a risk to aquatic feeding birds.

Risks from Mercury Mercury was identified as an ECOC in the C Ponds and the Original Landfill source areas. Mercury was identified as a PCOC in soil, groundwater, stream sediments, and pond sediments in OU 5 (see Appendix N Table N5.11A). In each source area, mercury was included as an ECOC because of measured or calculated concentrations in fish tissues.

Mercury was detected in 2 of 13 (15 percent) fish collected from Pond C-1 (see Appendix N Table N5.11A). The maximum detected concentration (0.47 mg/kg) was greater than the average dietary concentration (0.027 mg/kg) considered safe for great blue herons (Opresko *et al.* 1994) and corresponds to an HQ of 17. Mercury was identified as an ECOC for the Old Landfill source area based on the estimated bioconcentration in fish tissue calculated from the maximum detected concentration in surface water.

Mercury was detected in less than 50 percent of samples from all abiotic media in OU 5 except pond sediments (see Appendix N Table N5 11A). Therefore, pond sediments are probably the primary source for uptake of mercury by fish. However, only 15 percent of fish collected from Pond C 1 contain detectable quantities of mercury. It is possible that the two samples with detectable quantities may have had sediment in the gastrointestinal tract when analyzed.

Actual risks to great blue herons from mercury ingestion are probably less than indicated by the HQ of 17 because this value was calculated using the maximum detected mercury concentration in fish and assumed that the herons obtain all of their food from Pond C 1. Although Great blue herons return frequently to feeding areas, they could not use a pond the size of C 1 exclusively. Thus, the exposure calculation probably overestimates both the exposure point concentration and the frequency of exposure.

Risks from Antimony Antimony was identified as an ECOC based on incidental ingestion of sediments from Woman Creek. The HQ of 1.6 was based on 100 percent site use by herons in the section of Woman Creek in the Old Landfill source area. This segment of Woman Creek is seasonally intermittent and supports a minimal fish population. Herons have not been observed in this area, although they have been sighted at Pond C 1. It is unlikely that a heron would use this segment of Woman Creek to the extent necessary to exceed an HQ of 1.

7.3.2.3 Summary of Risks to Terrestrial Feeding Raptors

Chromium, lead, mercury, and vanadium were detected in terrestrial arthropods from OU 2 at concentrations that could be toxic to raptors feeding extensively in the areas. American kestrels were selected to represent ecological receptors because they have relatively small home ranges and are known to breed at the Site.

The preliminary risk estimate for chromium in terrestrial arthropods from OU 2 was based on the maximum detected concentration from the East Trenches source area. Chromium concentrations in terrestrial arthropods from the 903 Pad area were estimated based on data from the East Trenches. Thus, data were inadequate to accurately estimate exposures. However, review of the OU 2 data suggests that the maximum concentration was anomalously high and that its use overestimates risk. The mean chromium concentration in OU 2 soils was not elevated compared to background, and chromium was included in the PCOCs because of two samples that exceeded the background UTL_{99/99}. The OU 2 source

areas represent a small portion of the mesic and xeric mixed grassland habitat type at the Site. Thus exposure to chromium in OU 2 does not appear to represent a significant ecological risk to kestrels given the low magnitude of the exposures, probable overestimate of exposure, and relatively small area involved.

7.3.2.4 Summary of Risks to Small Mammals

Preliminary risk estimates indicated little risk to small mammals from inhalation of organic contaminants volatilizing from subsurface soils into burrow air. Risk was evaluated for populations of more common species and individuals of Preble's meadow jumping mouse, a species of special concern at the Site.

Toluene exceeded the EEC for exposure of small mammals to burrow air in areas of OU 2 that are known to contain buried waste or contaminated soil (see Appendix N Table N5.16 Figure N5.18). Inhalation TRVs were available for only six other organic PCOCs (see Appendix N Attachment 6 Table 9); soil concentrations for these compounds did not exceed TRVs. At the time this report was prepared, adequate information on respiratory toxicity was not available for most of the organic PCOCs found in soils, and inhalation TRVs could not be set. Review of existing information in IRIS (EPA 1994b) indicates that EPA is currently developing reference concentrations (RfCs) for some of the compounds. Respiratory exposures were estimated for all organic PCOCs, which are presented in Appendix N Attachment 6 Table 9.

Toluene irritates mucosal membranes of the eyes and respiratory tract at very low concentrations (EPA 1994b). Therefore, animals may avoid areas of contaminated soil when constructing burrows, fortuitously reducing their exposure. However, for purposes of this study, no avoidance behavior is assumed, and all areas exceeding the EEC are included in Appendix N Figure N5.18.

Areas in which toluene exceeded the EEC were identified using Thiessen polygons. These areas covered approximately 0.31 ha in the 903 Pad areas and 0.27 ha in the East Trenches area. All of the affected polygons lie within or adjacent to IHSSs (see Appendix N Figure N5.18). This suggests that risks to burrowing animals from toluene exposure in OU 2 may be restricted to the primary contaminant source areas. However, risk from organic PCOCs without TRVs remains unclear.

Areas impacted by toluene are found in the mesic and xeric mixed grassland habitat types on the ridge between South Walnut Creek and Woman Creek (see Appendix N Figure N5.18). None of the areas

overlap with probable Preble's meadow jumping mouse habitat (see Appendix N Figure N5 18). The Thiessen polygons represent about 0.011 percent of the mesic and 0.088 percent of the xeric grassland habitat types at the Site. These percentages may be used as a rough estimate of the proportion of burrowing habitat affected for more common species such as deer mice and prairie voles that use the drier, more upland areas of the site.

7.3.2.5 Summary of Risks to Vegetation Communities

Results of the Tier 3 screen indicated that several PCOCs exceed subsurface soil or sediment TRVs in several source areas (see Appendix N Table N3 23). This group of chemicals included mostly metals. Concentrations of organic PCOCs did not exceed TRVs (see Appendix N Attachment 6 Table 1). However, TRVs were not available for several organic compounds that were PCOCs for subsurface soil and sediments (see Appendix N Attachment 6 Tables 2 and 7). Subsurface soil data were not available for the OU 5 Surface Disturbance; no HQs exceeded 1 for PCOCs in the OU 1 881 Hillside or OU 2 East Trenches.

Chromium (7.9), nickel (3.7), and zinc (3.0) all had HQs of 3 or greater in the Ash Pits source area (see Appendix N Table N3 23). All other HQs for metals in subsurface soil were 2 or below. Many of the TRVs for metals were equal to the Site background soil concentrations because literature-based toxicity values were below the UCL₉₅ for background. Thus, HQs greater than 1 indicate concentrations that exceed background. Soil toxicity tests were not conducted using site soils. However, the risk associated with HQ values near 1 is unclear because background concentrations can vary by orders of magnitude. As noted previously, areas of obvious vegetation stress were not observed during preliminary field surveys. Thus, the importance of these risk estimates is not clear.

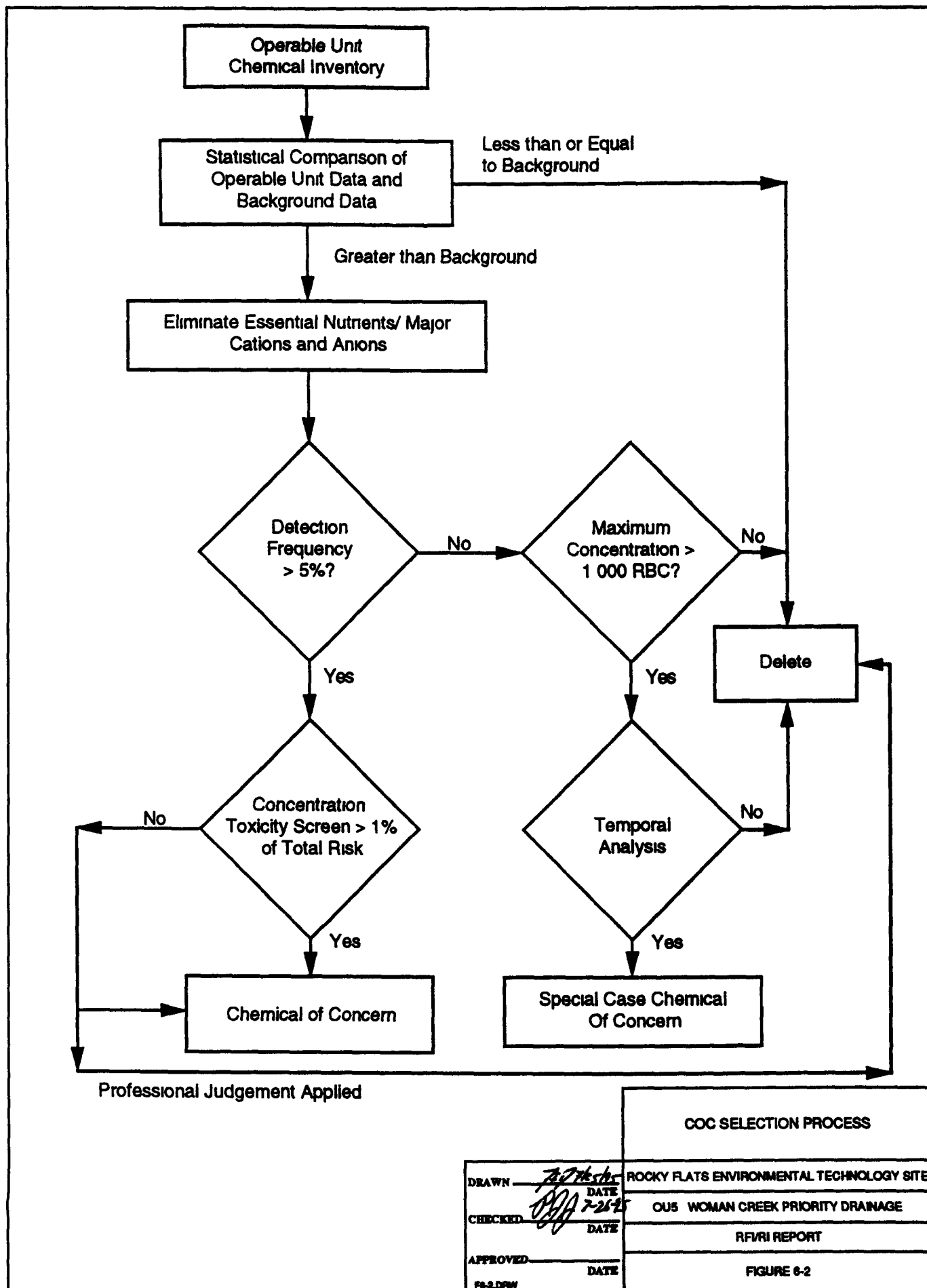
TRVs were not available for most organic soil or sediment PCOCs. HQs were well below 1 for organic PCOCs for which TRVs were available. However, as with metals, the potential phytotoxicity of most organic PCOCs was not quantified with plant toxicity tests.

7.3.2.6 Summary of Risks from Radionuclides

Transuranic radionuclides were identified as PCOCs for most OUs. The ECOC screen indicated relatively few areas with radionuclide concentrations (activities) in soils that exceeded TRVs. Plutonium 239/240

and americium 241 concentrations in soils exceeded TRVs in two locations in the 903 Pad source areas and uranium 233/234 and uranium 238 concentrations in soils exceeded TRVs at two locations in the Old Landfill source area. Radionuclides were also elevated in vegetation and small mammals collected from ERA source areas.

The potential risks from radionuclide uptake by biota were evaluated by calculating the internal radiological dose and comparing it to the TRV. The TRV was based on a benchmark value of 0.1 rad/day which was identified by IAEA (1992) as protective of biological receptors. Results indicated that maximum radionuclide concentrations measured in small mammals resulted in dose rates at least 1,000 times less than the TRV. The potential uptake by predators was also evaluated and indicated that risks to predators were also not significant. Although abiotic media and biota contain elevated concentrations of transuranic radionuclides, the risks of adverse effects appear to be negligible.



Professional Judgement Applied

COC SELECTION PROCESS

DRAWN 7/27/95 DATE 7-26-95
 CHECKED [Signature] DATE 7-26-95
 APPROVED _____ DATE _____
 PG-2.DRW

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
 OU5 WOMAN CREEK PRIORITY DRAINAGE
 RFVRI REPORT
 FIGURE 6-2

Table 7 1
Summary of Risk Estimates for ECOCs by Source Area

Source Area				
Woman Creek Watershed				
Woman Creek	Wetland Vegetation Communities	Sediments	Zinc	1 6
OU5 Ash Pits	Aquatic Species	Surface Water	Barium	17
	Vegetation Communities	Subsurface Soil	Chromium	7 9
			Nickel	3 7
			Zinc	3 0
			Silver	2 0
			Antimony	1 3
			Copper	1 1
			Lead	1 1
			Cadmium	1 0
OU5 C Ponds	Aquatic Species	Surface Water	Barium	24
	Great Blue Heron	Fish	Mercury	6 4
	Vegetation Communities	Subsurface Soil	Chromium	2 7
			Zinc	1 1
Pond C 1	Aquatic Species	Sediments	Benzoic acid	2 6
	Wetland Vegetation Communities	Sediments	Mercury	6 0
			Zinc	1 5
Pond C 2	Aquatic Species	Sediments	Benzoic acid	1 7
			Zinc	1 3
	Wetland Vegetation Communities	Sediments	Zinc	2 8
			Mercury	2 3
OU5 Original Landfill	Aquatic Species	Surface Water	Barium	37
	Great Blue Heron	Fish	Mercury	29
		Sediments	Antimony	1 6
	Small Mammals ¹	Surface Soils	Uranium-233/234	1 6
			Uranium-238	23 8
	Vegetation Communities	Subsurface Soil	Copper	2 6
			Zinc	2 0
OU2 903 Pad	American Kestrel	Terrestrial Arthropods	Chromium	5 6
	Aquatic Species	Surface Water	Barium	39
	Great Blue Heron	Fish	Aroclor 1254	5 8
	Small Mammals	Burrow Air (Calc from Soils ²)	Toluene	1,900
	Small Mammals ¹	Surface Soils	Plutonium-239/240	1 92
	Vegetation Communities	Subsurface Soil	Zinc	1 2
OU2 East Trenches	American Kestrel	Terrestrial Arthropods	Chromium	4 4
	Small Mammals	Burrow Air (Calc from Soils ²)	Toluene	20

Radionuclide benchmarks use small mammals as the limiting exposure scenario. Preble's meadow jumping mouse was used to represent this group.

² HQ is for maximum concentration of toluene in soils.

Table 7 2
Summary of Ecological Risks for Woman Creek Watershed

Receptor Group	ECOCs	ERA Source Area	Media/Exposure Point	Conclusions
Wide Ranging Wildlife Aquatic Life	None	Not Applicable	Not Applicable	No ECOCs were identified as result of Tier 3 screen
	Metals and organics in sediments	OU2 903 Pad OU5 C Ponds OU5 Original Landfill	Sediments	Risks are primarily due to PAHs in sediments However no toxicity was detected in sediment toxicity tests with <i>Hyalella azteca</i> The importance of sediment contamination is unclear but does not appear to be the primary factor controlling benthic community structure
Aquatic Feeding Birds	Aroclor 1254	OU5 C Ponds	Sediments of SID	Aroclor 1254 concentrations in sediment did not exceed risk based criteria developed for sediment at the Site
	Mercury	OU5 Original Landfill OU5 C Ponds	Fish Tissue	Mercury was detected in 2 of 24 fish from the C ponds Mercury was not detected in other fish Risks are significant only if birds obtain all food from Pond C 1
	Antimony	OU5 Original Landfill	Sediments	The screening estimate assumes 100% site use Actual use is much less because the stream supports a small fish population Risks were not significant when adjusted for realistic site use factor
Terrestrial Feeding Raptors	Chromium	OU2 903 Pad OU2 East Trenches	Terrestrial Arthropods	The mean chromium concentration in soils was not greater than the background mean No clear contaminant source exists Chromium was not a risk to the kestrel population at the Site
Small Mammals	Plutonium-239/240 Americium 241	OU2 903 Pad OU2 East Trenches	Soils	Radionuclides do not present significant risk to terrestrial receptors Maximum tissue concentrations do not result in dose rates that exceed TRVs (0.1 rad/day)
	Uranium 233/234 Uranium 238	OU5 Original Landfill	Soils	See text for plutonium and americium conclusions
	Toluene	OU2 903 Pad OU2 East Trenches	Burrow Air	Organic PCOCs in subsurface soil could volatilize into burrow air Soil toluene concentrations in some areas of OU2 could lead to air concentrations > TRV Little toxicity data are available for assessing other organics
Vegetation	Metals	Most Source Areas	Soils Sediments	Soils of the Ash Pits contained several metals with HQs >1 The highest HQ (7.9) was for chromium Ecological risk to vegetation communities is minimal because each of the Ash Pits involves relatively small areas
				Sediments of C ponds contain mercury at concentrations that exceed TRVs for wetland vegetation However growth of vegetation in littoral zone appears normal

8 0 PRELIMINARY EVALUATION OF REMEDIAL ALTERNATIVES

Section 5.7 of the OU 5 RFI/RI Work Plan (DOE 1992a) describes the process to be used for the development and screening of remedial alternatives for OU 5. The process to be employed to develop and evaluate alternatives for OU 5 is similar to that described in EPA's *Guidance for Conducting Remedial Investigations and Feasibility Studies under CERCLA* (EPA 1988c) and as mandated by the IAG. This process complies with both RCRA and CERCLA guidance. This process uses the site-characterization data generated by the RFI/RI along with data generated under other investigations such as treatability studies, to develop, refine and select remedial alternatives appropriate for each IHSS where contamination is present and remediation is warranted.

The development and screening of remedial alternatives for OU 5 will be conducted under the OU 5 CMS/FS program if a further action is warranted. Two technical memoranda will be prepared under the CMS/FS program and will be issued at a later date. CMS/FS TM1, Development of Corrective/Remedial Action Objectives, will provide a description of corrective/remedial action objectives based on chemical and radionuclide specific standards (when available), site specific risk related factors, and other criteria, as appropriate. CMS/FS TM2, Detailed Screening of Alternatives, will describe the evaluation of remedial alternatives applicable to OU 5 against the short and long term aspects of the following specific evaluation criteria.

- Overall protection of human health and the environment,
- Compliance with ARARs
- Long term effectiveness and permanence
- Reduction of toxicity, mobility, or volume
- Short term effectiveness
- Implementability
- Cost,
- State acceptance, and
- Community acceptance

These criteria are described in EPA (1988c). The initial two criteria are considered threshold criteria because these criteria must be satisfied before further consideration of the remaining criteria. The next five criteria are considered the primary criteria on which the analysis is based. The final two criteria, state and community acceptance, are addressed during the final decision making process after completion of the CMS/FS.

9 0 PRELIMINARY IDENTIFICATION OF DATA GAPS

Throughout the RFI/RI process it is necessary to evaluate the available data to determine if they are sufficient to define the risk associated with a site and to develop remedial alternatives. The observational approach employed for the OU 5 RFI/RI allowed the data collected during each stage of the investigation to be evaluated and subsequent stages to be designed to obtain the data needed for assessing risk (i.e. determining the need for remedial action) and for developing remedial alternatives. Additionally, the field program defined by TM15 (DOE 1994a) was in large part, designed to obtain data needed for the evaluation of remedial alternatives in the OU 5 CMS/FS. For example, the geotechnical drilling program at IHSS 115/196 was designed to obtain data that are required for an assessment of the stability of the slopes in this area in anticipation that a likely remedial alternative for this area will be to stabilize the slopes and cover the area with a soil cap. Also, during the drilling program at IHSS 133 to investigate the additional pits identified by the TDEM survey, samples of ash were collected from IHSS 133 2 for use in treatability studies.

At this time, the data collected under the Phase I RFI/RI at OU 5 are believed to be adequate for defining the risk associated with each of the IHSSs (Chapters 6 0 and 7 0). In addition, these data are adequate for the development and screening of remedial alternatives. As the OU 5 CMS/FS progresses, additional data gaps may be identified, and data gathering programs will be developed to fill these gaps.

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10 0 SUMMARY AND RECOMMENDATIONS

This chapter summarizes the results of the OU 5 Phase I RFI/RI and provides recommendations for additional investigations that may be required

10 1 SUMMARY

A Phase I RFI/RI of OU 5 was conducted as directed by the Interagency Agreement of 1991. The purpose was to assess the site physical characteristics, characterize contaminant sources and the nature and extent of potential contamination in surface soil, subsurface soil, groundwater, surface water, sediment, and air; assess fate and transport of environmental contaminants; and estimate potential risks to human health and the environment from the identified contaminants.

Field investigations indicate that the site physical characteristics are complex. Site meteorologic, geologic, hydrologic, and hydrogeologic conditions are interconnected and provide mechanisms and pathways for surface and subsurface constituents to migrate through the environment. For example, because most of the UHSU groundwater pathways discharge to surface water within OU 5, thus there is limited potential for migration of VOCs to offsite locations via groundwater.

The nature and extent of environmental contamination within OU 5 have been characterized through the collection, analysis, and assessment of hundreds of samples of various environmental media. Environmental samples were analyzed for a comprehensive suite of chemicals to help characterize potential contamination associated with waste handling and disposal practices conducted during the operating history of Rocky Flats in the area of OU 5. The OU 5 data assessment process, including rigorous data validation, was designed to be conservative to ensure a healthy, protective, and comprehensive understanding of potential contamination conditions in OU 5.

The results of the OU 5 data assessment indicated the presence of PCOCs in surface soil, subsurface soil, groundwater, pond seep, and stream water, and pond seep and stream sediments. PCOCs identified in one or more of these environmental media include VOCs, SVOCs, PCBs/pesticides, metals, and other inorganic constituents, including radionuclides. The Phase I RFI/RI indicated that both the lateral and vertical extent of the PCOCs are limited. The limited extent of PCOC migration is due to the low

hydraulic conductivities the hydrogeologic setting and the small amounts of highly mobile wastes disposed in OU 5. The list of PCOCs for each medium was then screened using risk based and other screening methods to identify COCs for both the HHRA and the ERA. COCs were identified as the chemicals in each medium that were likely to contribute at least 1 percent of overall risk (**incorporate ERA results when available**). For the HHRA, COCs were selected on an OU wide basis; for the ERA, the COCs were identified for the Woman Creek watershed. In groundwater and surface water, metals and radionuclides are the primary COCs; however, in seep water, the COCs are all VOCs. The COCs in surface soil and subsurface soil include uranium isotopes, several metals, PAHs, and PCBs. In all sediments, radionuclides and metals are the only COCs.

The presence of COCs in all media is a result of historical releases to the environment. Under the hydrogeochemical conditions of OU 5, metals and radionuclides are not expected to be very mobile via the groundwater pathway. However, several mechanisms of contaminant transport are present, such as storm water runoff which may transport contaminated soils to surface waters with subsequent transport to downstream receptors. The presence of COCs in stream seep and pond sediments as a result of surface water transport of contaminated surface soils to and along Woman Creek, supports this exposure mechanism. Fugitive dust emissions from OU 5 surface soils and dry sediments may also contribute contaminated particulates to future onsite receptors. Exposure to subsurface soils by future onsite construction workers may result from contaminant inhalation and ingestion during an excavation.

The results of the OU 5 HHRA indicate estimated health risks and annual radiation doses for current and future onsite receptors who could potentially be exposed directly or indirectly to COCs at, or released from, sources in OU 5. Exposure scenarios that were evaluated involved a current industrial worker (security guard), a future industrial/office worker, a future ecological researcher, a future open space recreational user, and a future construction worker. Future onsite residential receptors were not considered in the HHRA because future land use plans do not include residential use. It was determined during HHRA negotiations with the regulatory agencies that health risks to offsite receptors would not be addressed on an OU specific basis but would best be examined on a sitewide basis.

For the HHRA, exposure media that were evaluated included surface soil, subsurface soil, outdoor and indoor air, stream seep and pond water, and stream seep and pond sediments. Groundwater was not evaluated as an exposure pathway because there are no current or future receptors.

Risks were evaluated for three AOCs. The Original Landfill (IHSS 115/196 Source Area) is AOC No 1 and AOC No 2 includes the Ash Pits (IHSS 133 Source Area). AOC No 3 includes the SID and the Pond C 2 Source Area, Woman Creek and due Pond C 1 Source Area.

The risk characterization process combines average and reasonable maximum estimates of exposure with upperbound estimates of toxicity in order to yield conservative (protective) estimates of human health risk. Estimates of human health risk for average (CT) and RME conditions are provided so that risk management decisions can be based on a range of potential risks for different exposure scenarios.

The following are the major conclusions of the HHRA.

- AOC1 Cumulative HIs were below 1 and RME cancer risk estimates were $3E-05$ or below for all receptors. The maximum cancer risk estimate of $3E-05$ for both the current worker (security guard) and the future office worker. This risk is still within EPA's acceptable risk range of $1E-06$ to $1E-04$. External irradiation due to exposure of uranium 238 in surface soil is the primary contributor to this estimate of cancer risk.
- AOC2 Cumulative HIs were below 1 and RME cancer risk estimates were $4E-06$ or below for all receptors. The maximum cancer risk estimate of $4E-06$ for both the current worker (security guard) and the future office worker. This risk is at the low end of EPA's acceptable risk range of $1E-06$ to $1E-04$. External irradiation due to exposure of uranium 238 in surface soil is the primary contributor to this estimate of cancer risk.
- AOC3 Cumulative HIs were below 1 and the RME cancer risk estimates were below EPA's point of departure of $1E-06$ for both receptors. These results indicate that no adverse noncarcinogenic health hazards and negligible cancer risk are expected for all receptors evaluated.

The ERA for Woman Creek was conducted for aquatic and terrestrial biota exposed to contaminants in OUs 1, 2, and 5. Assessment of ecological risks was based on evaluating exposure of biological receptors to PCOCs in designated ERA source areas. Source areas include individual or groups of IHSSs within an OU and were based on abiotic and biotic sampling locations in and around IHSSs. A preliminary exposure and risk calculation was conducted for PCOCs in source areas. The analysis was conducted to estimate the contribution of each PCOC and each source area to overall risk in the watershed. Ecological chemicals of concern (ECOCs) were identified from preliminary risk calculations and evaluated further in risk characterization.

Ecotoxicological risk to terrestrial receptors in OU 5 was minimal. Concentrations (activities) of uranium 233/234 and uranium 238 in soils exceeded the risk based screening criteria developed for the Site.

However the criteria were exceeded in only two locations both of which are in the Old Landfill source area and which represent a negligible portion of habitat in the watershed. In addition maximum concentrations of radionuclides in small mammals were not associated with levels that exceed the benchmarks for safe radiological doses. Thus risk from exposure to radionuclides appears to be minimal.

The screening level assessment also indicated that concentrations of mercury, antimony, and Aroclor 1254 could represent risks to aquatic feeding birds if they acquired all of their food from the SID Pond C 1 and segments of Woman Creek. However, it is unlikely that birds would spend all of the time in the areas of concern because the size and quality of habitat in these areas is inadequate to support their needs.

10.2 RECOMMENDATIONS

The results of the HHRA support the conclusions that environmental contamination within OU 5 does not pose a threat to human health under the evaluated exposure scenarios. Therefore remediation of environmental media to address risk to human health and the environment is not warranted. In addition no further investigations are recommended.

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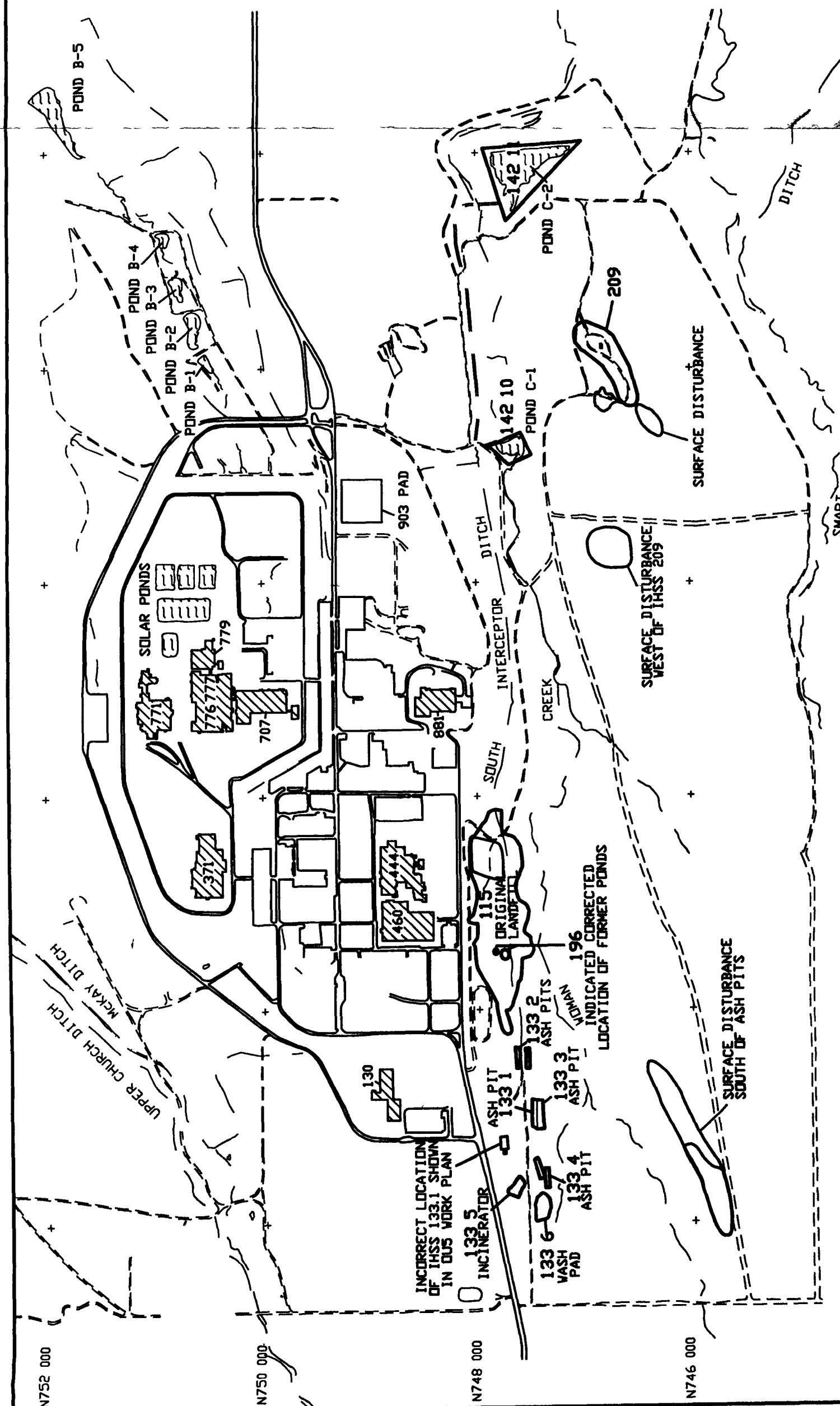
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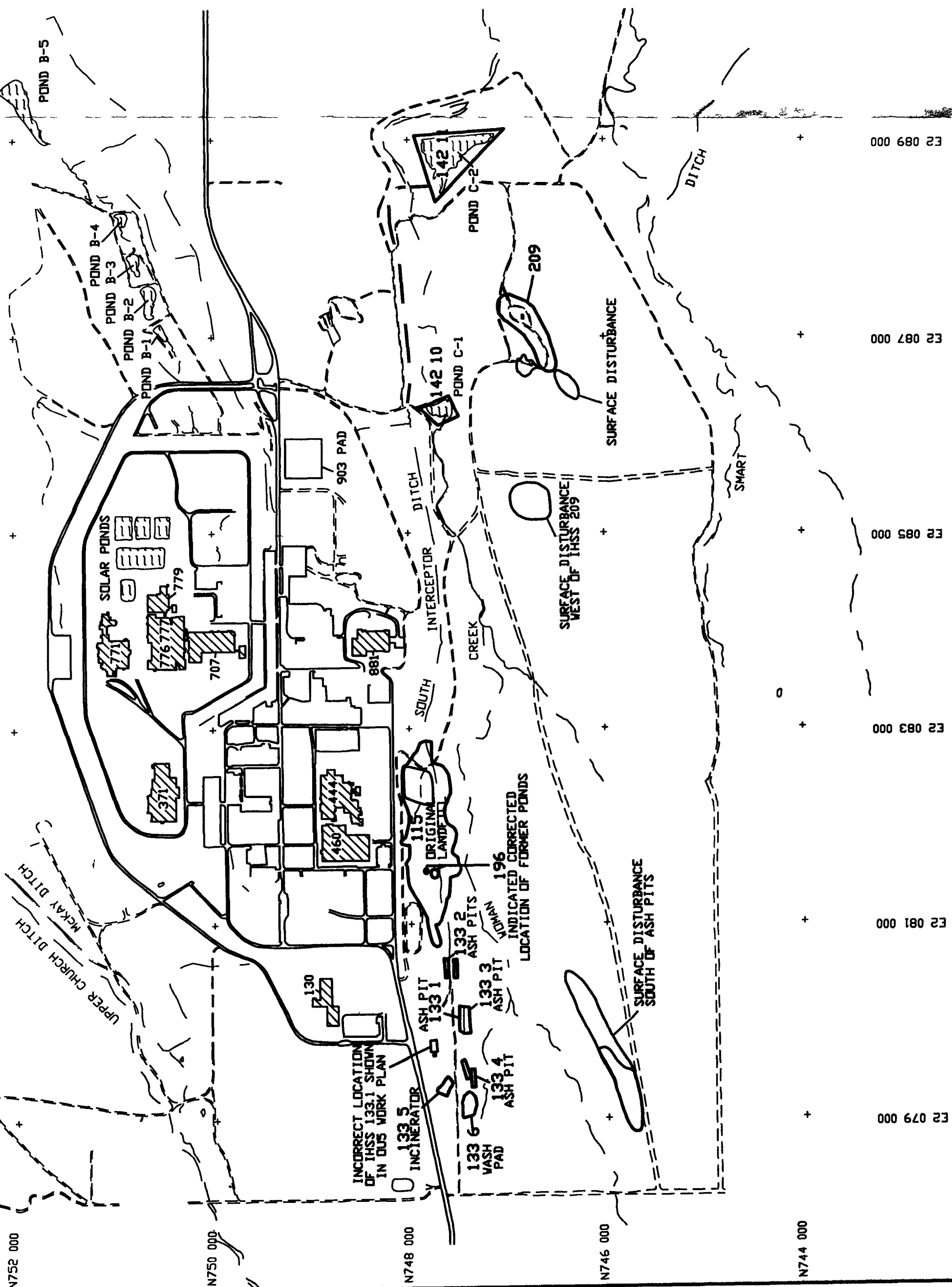
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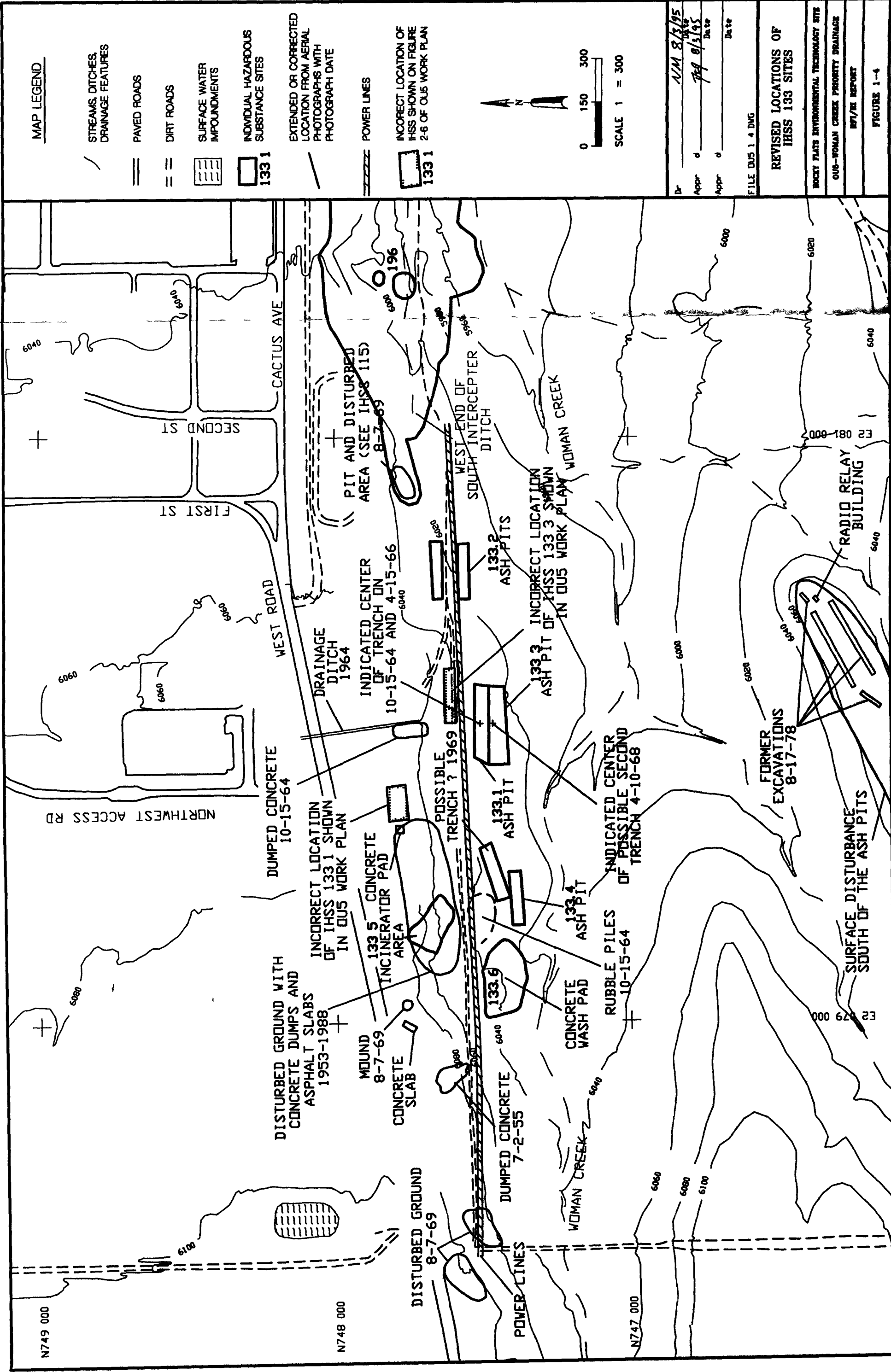
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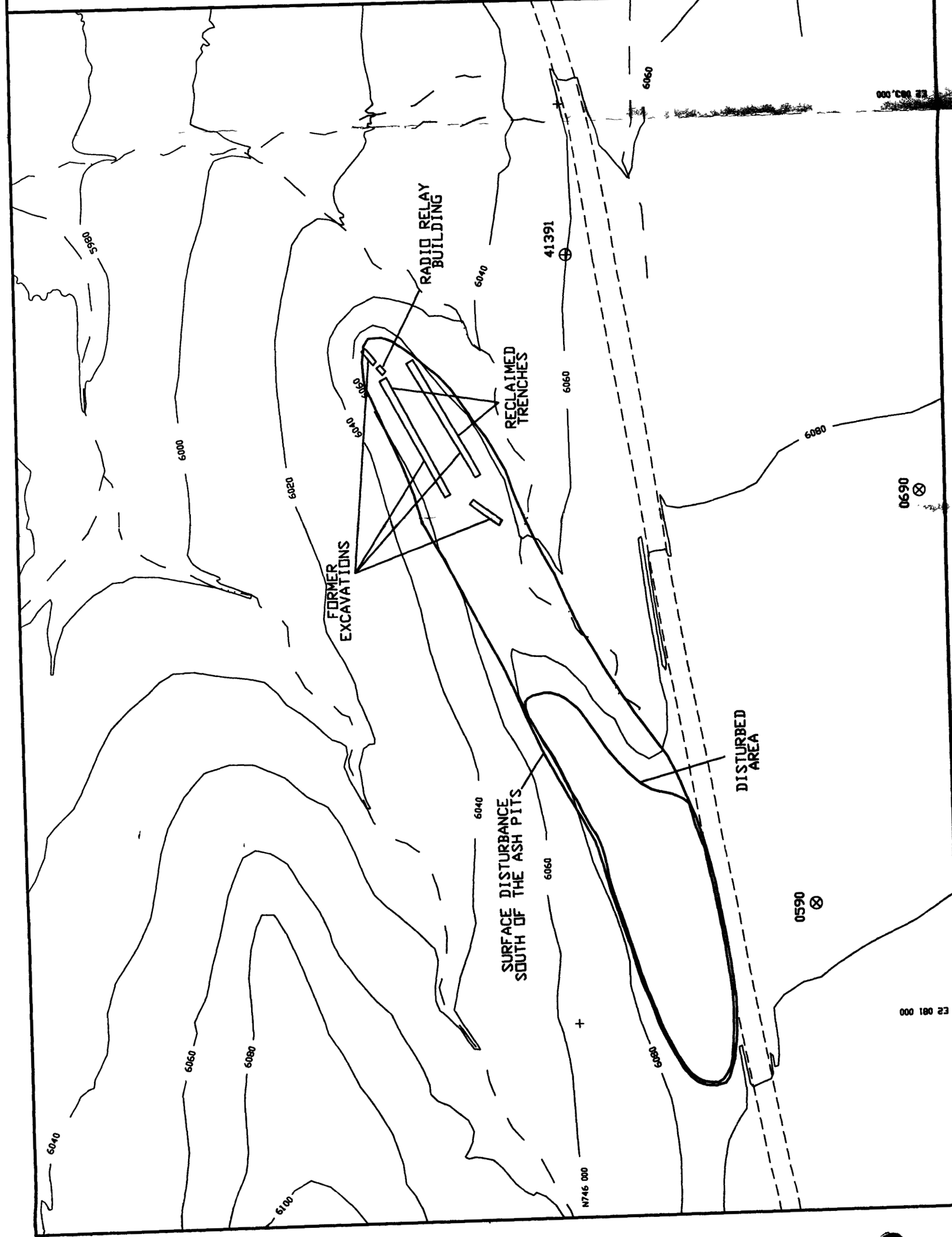
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FILE DUS 1 2 DWG	
WOMAN CREEK PRIORITY DRAINAGE AREA (OPERABLE UNIT No 5)	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
OUB-WOMAN CREEK PRIORITY DRAINAGE	
RPT/RE REPORT	
FIGURE 1-2	







MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

DIRT ROADS

SURFACE WATER
IMPOUNDMENTS

INDIVIDUAL HAZARDOUS
SUBSTANCE SITES (HSS)

EXISTING BOREHOLE

EXISTING MONITORING
WELLS

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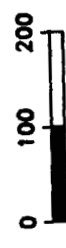
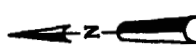


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













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SURFACE DISTURBANCE SOUTH OF THE ASH PITS LOCATION MAP	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
OUG-WOMAN CREEK PRIORITY DRAINAGE	
RTI/RE REPORT	
FIGURE 1-6	

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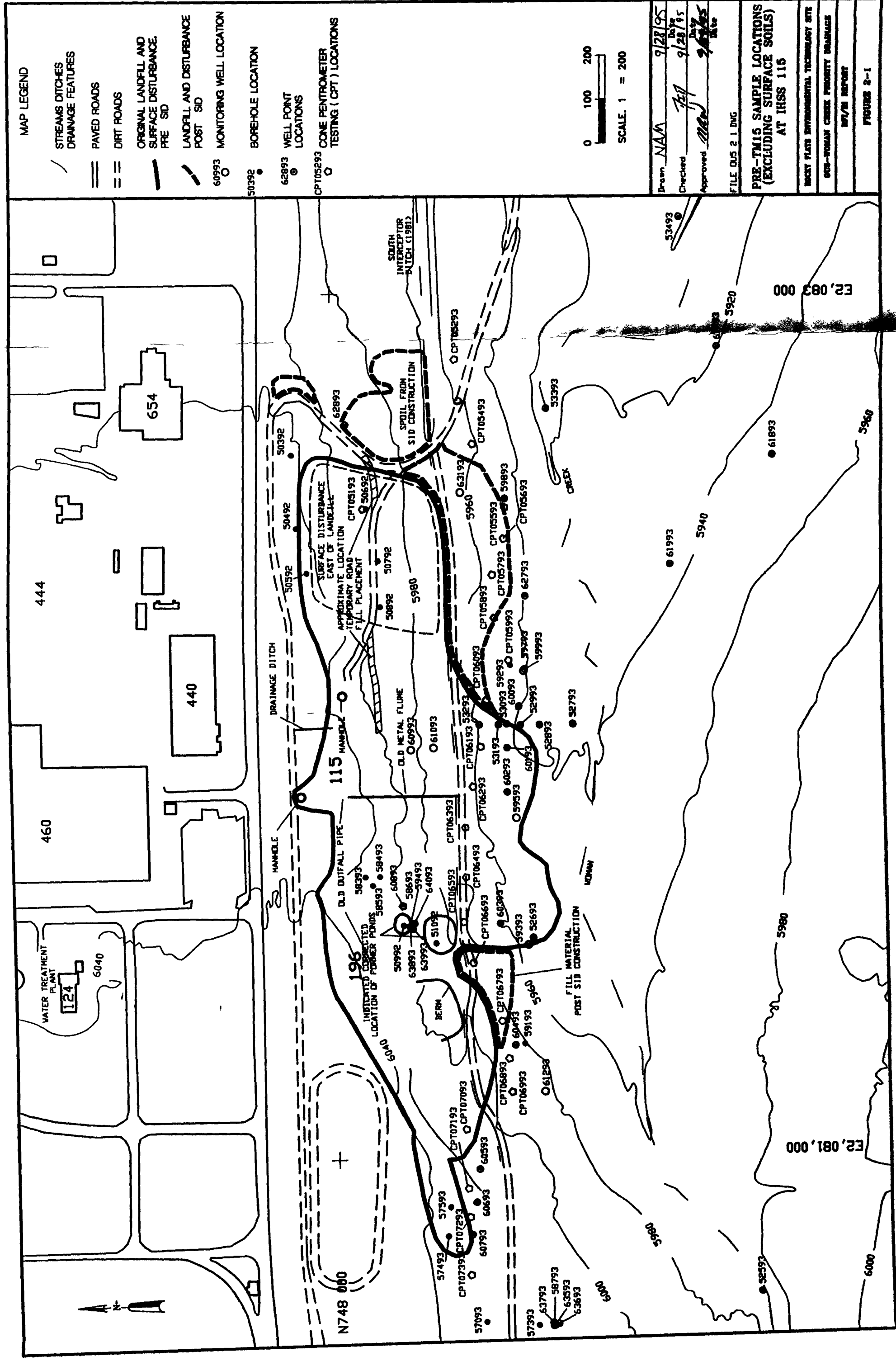
EXPLANATION	
	Operable Unit 5 IHSS s
	Surface Disturbance
	Individual Hazardous Substance Sites (IHSS)
	South Interceptor Ditch
	French Drainage System
Standard Map Features	
	Buildings or other structures
	Lakes and ponds
	Streams, ditches, or other drainage features
	Fences
	Contours (20 Intervals)
	Paved roads
	Dirt roads

**U.S. Department of Energy
Rocky Flats Environmental Technology Site**

1. The first step is to identify the problem or question that needs to be addressed. This involves understanding the context and the specific requirements of the task.

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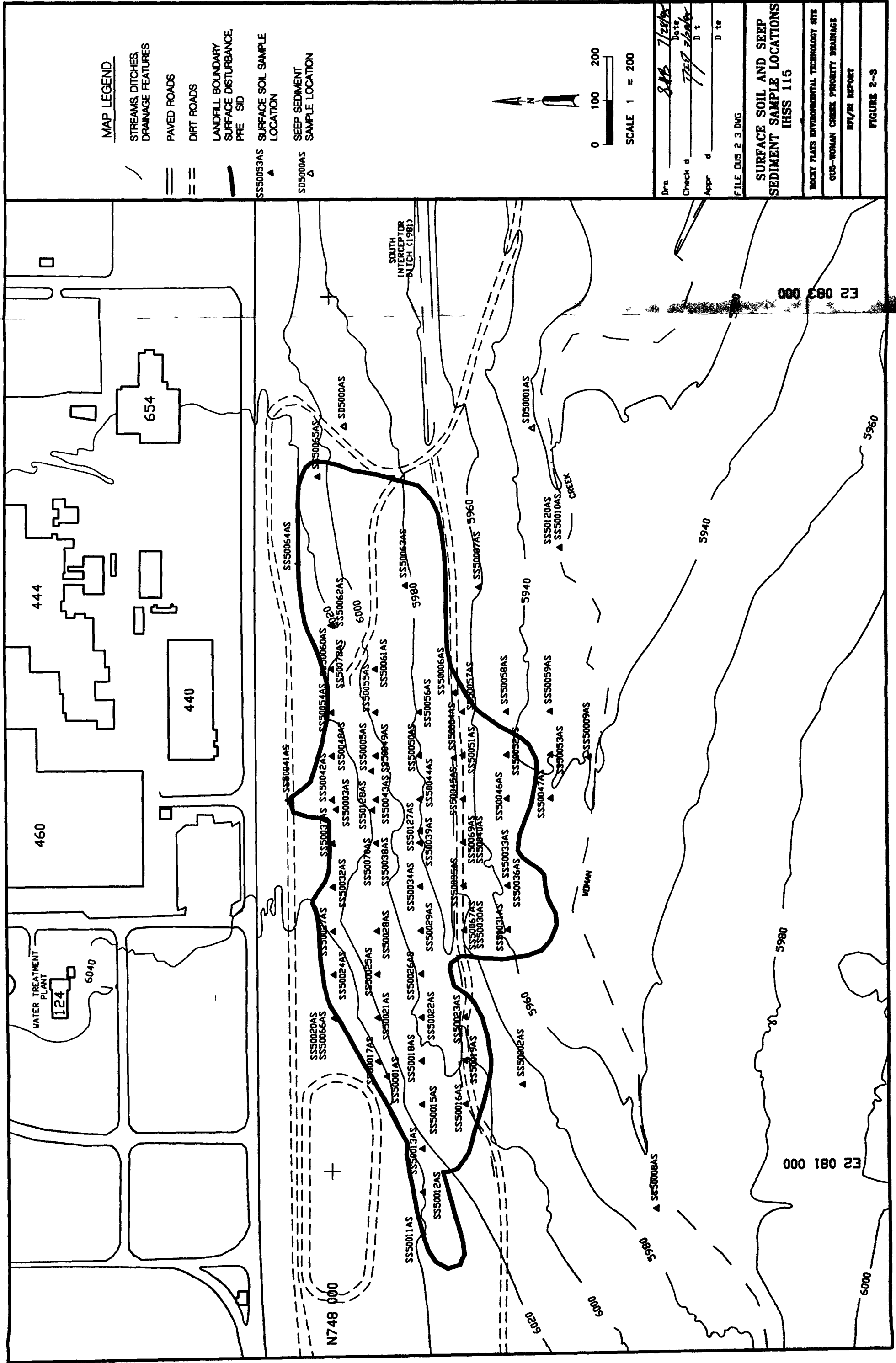
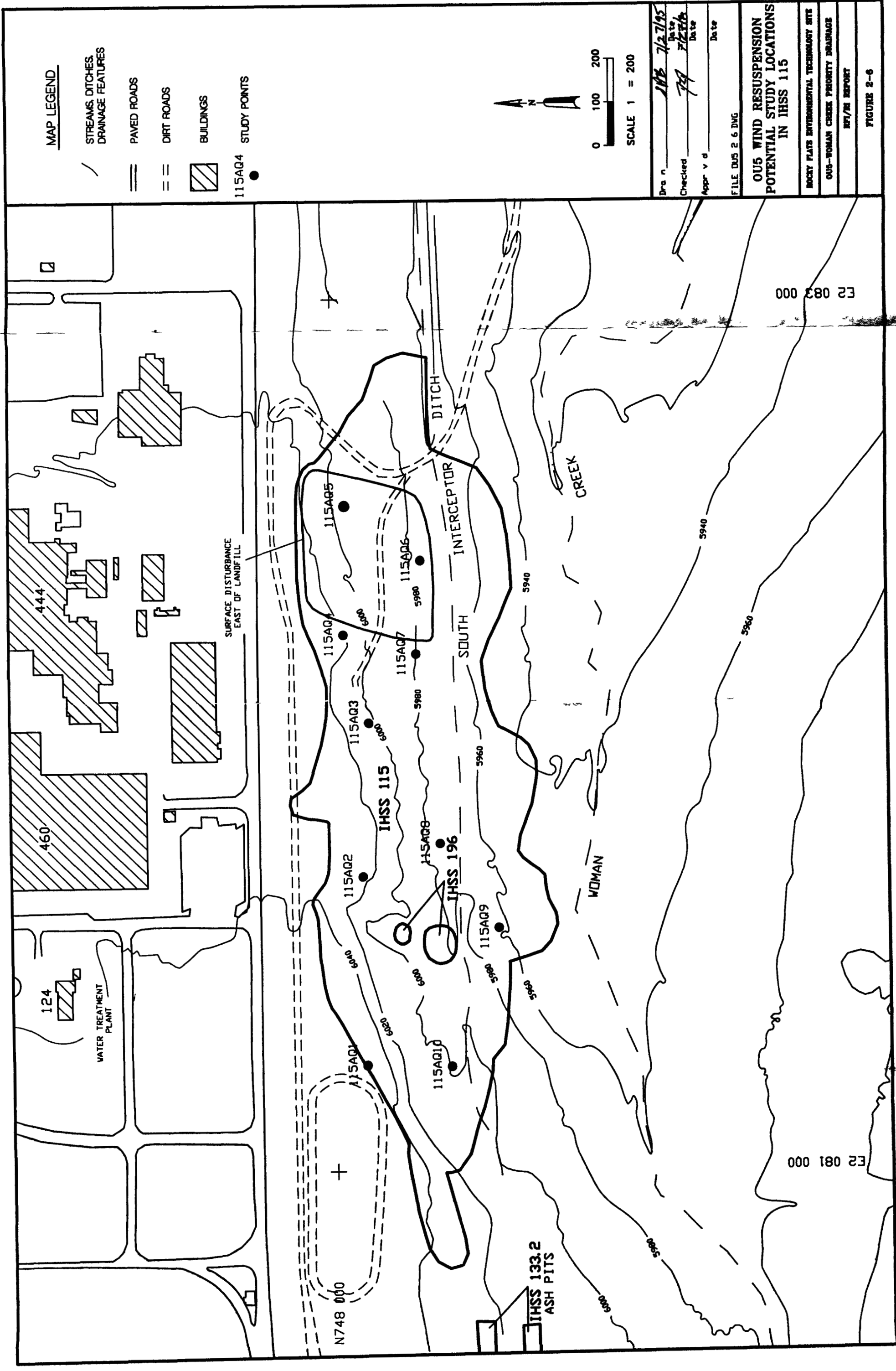


FIGURE 2-3

FIGURE 2-3



MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

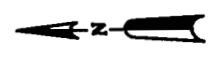
PAVED ROADS

DIRT ROADS

BUILDINGS

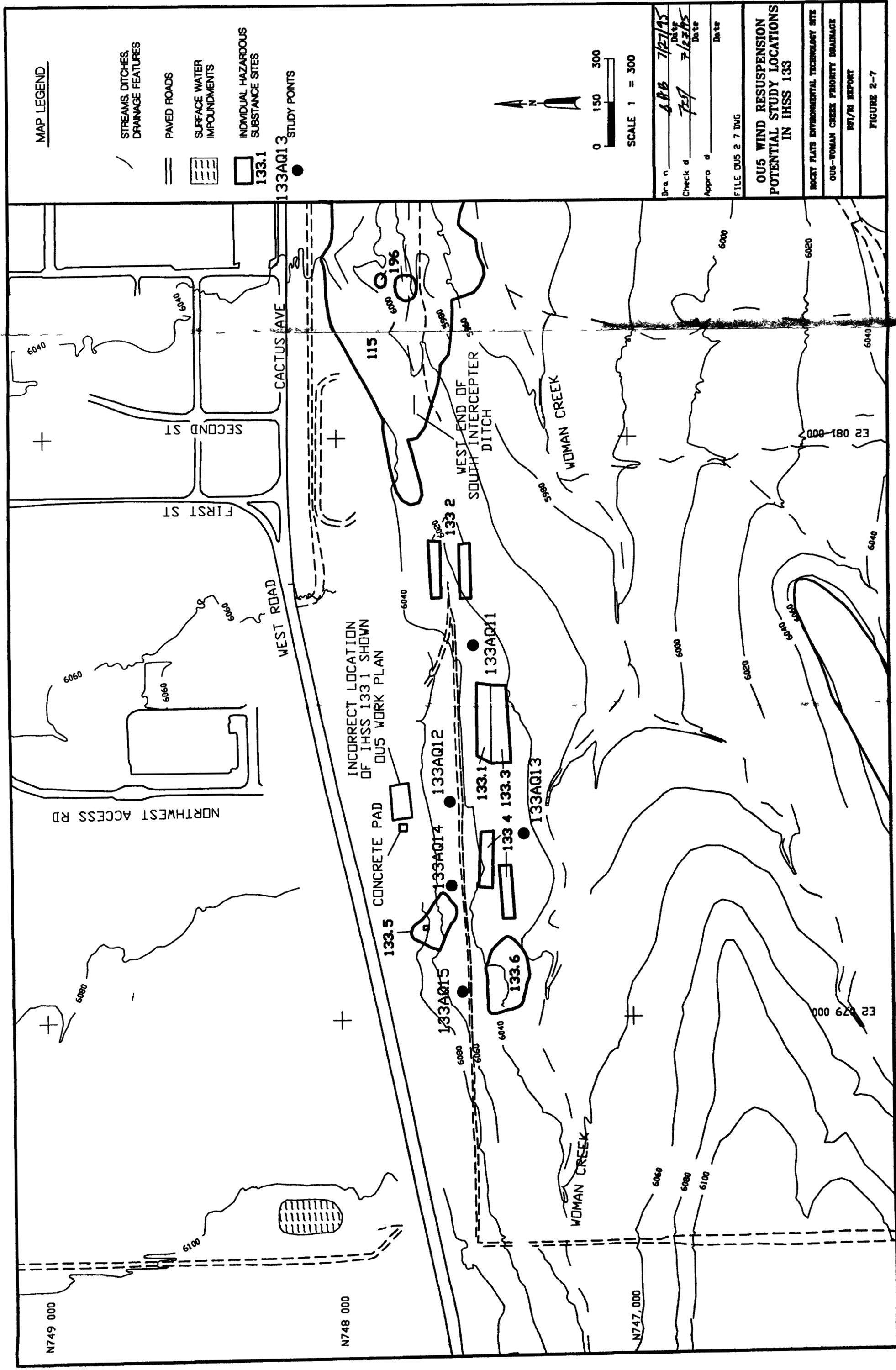
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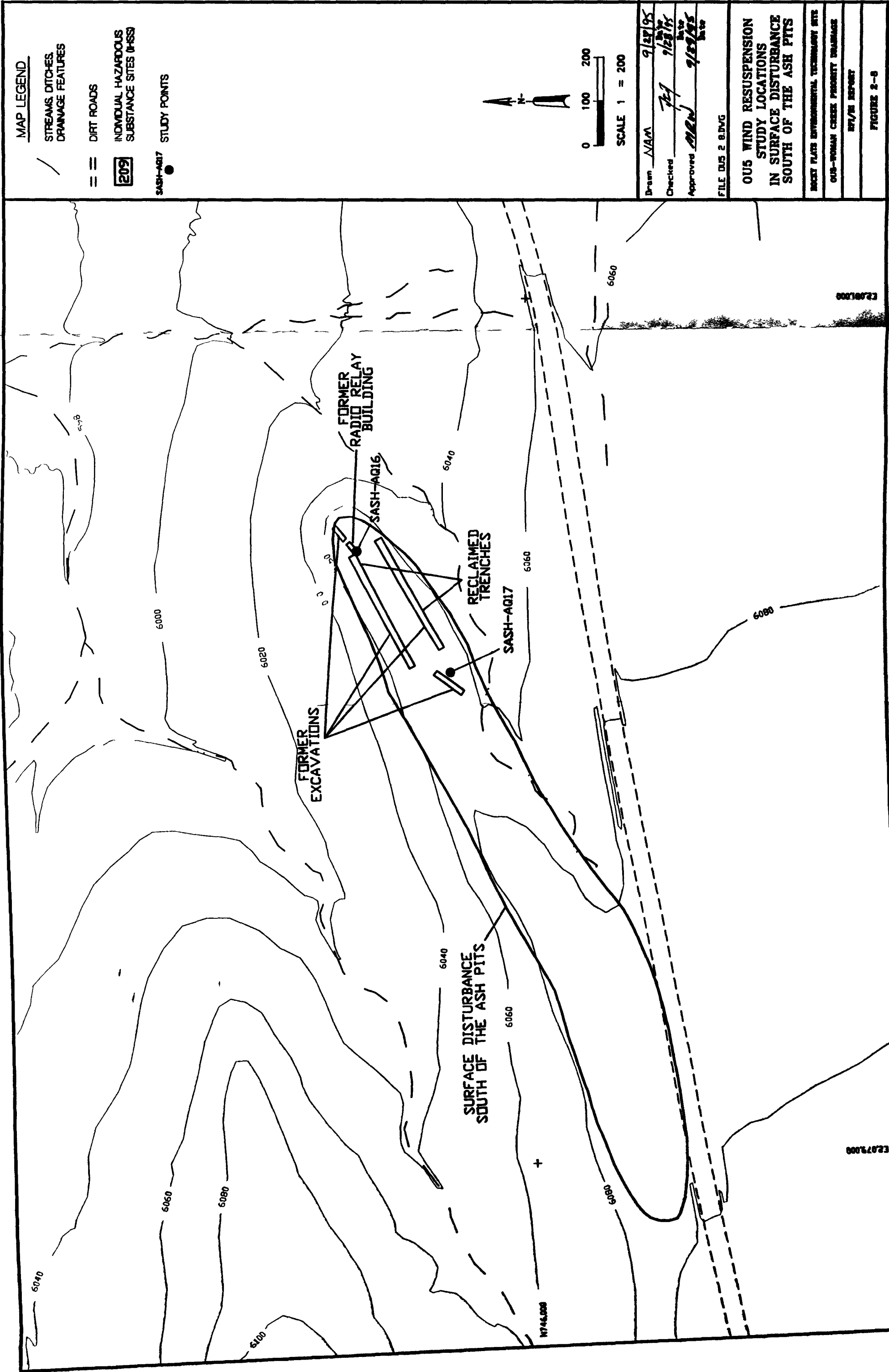
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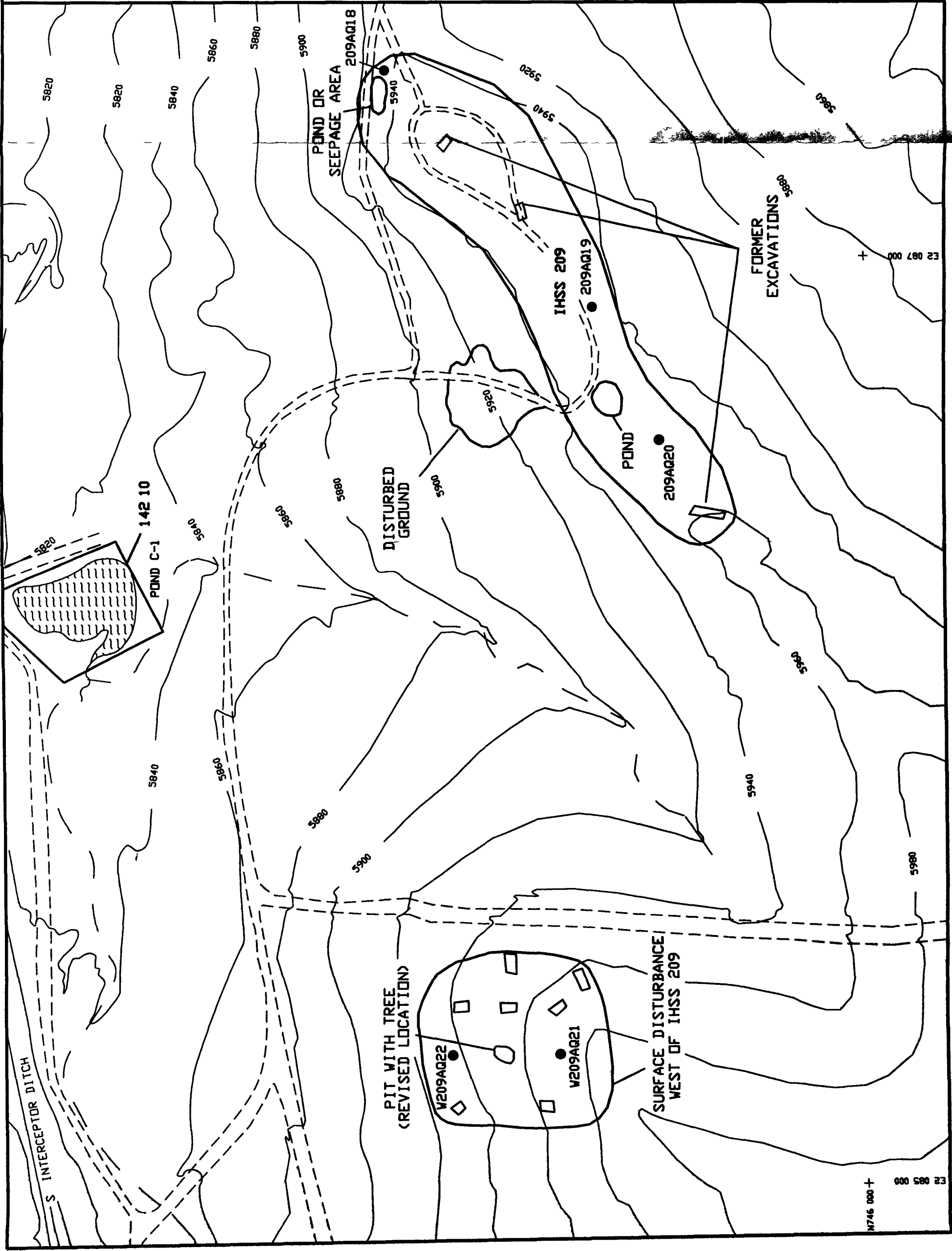


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FILE DUS 2 6 DWG			
OU5 WIND RESUSPENSION POTENTIAL STUDY LOCATIONS IN IHSS 115			
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE			
OU5-WOMAN CREEK PRIORITY DRAINAGE			
RPT/RI REPORT			
FIGURE 2-6			

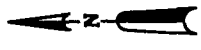






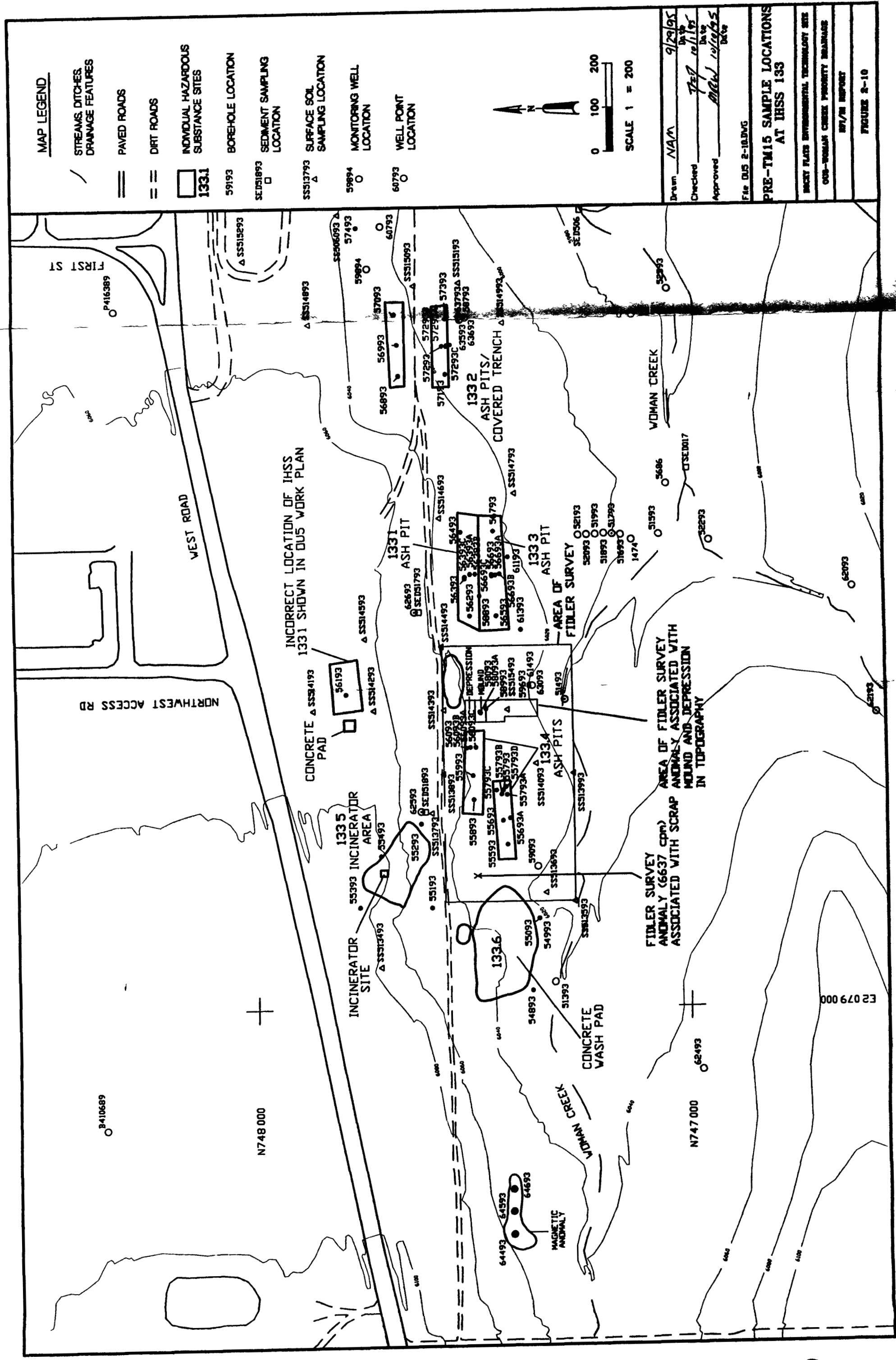
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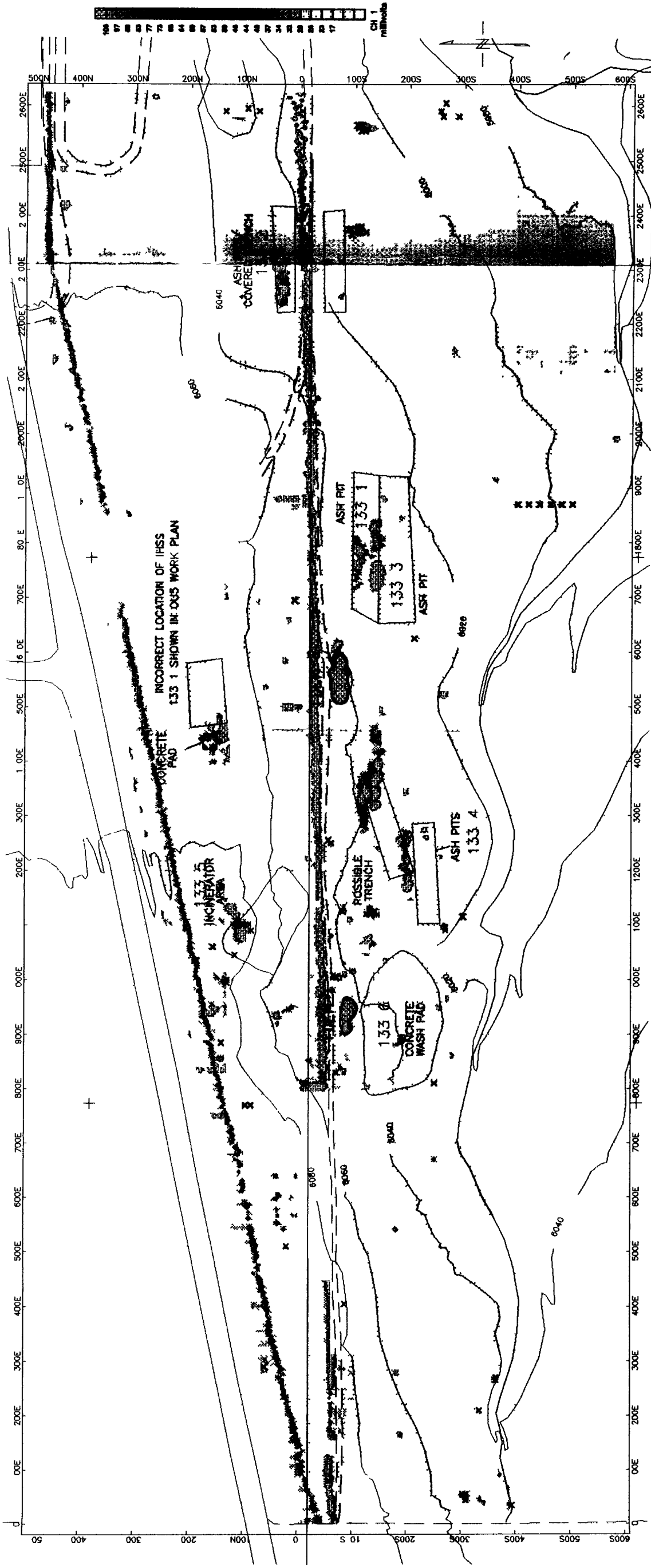
- STREAMS, DITCHES, DRAINAGE FEATURES
- DIRT ROADS
- SURFACE WATER IMPOUNDMENTS
- REVISED PIT LOCATIONS
- INDIVIDUAL HAZARDOUS SUBSTANCE SITES (IHSS)
- STUDY POINTS



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OVS WIND RESUSPENSION POTENTIAL STUDY LOCATIONS IN IHSS 209 AND SURFACE DISTURBANCE WEST OF IHSS 209	
ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE	
OVS-TOMAM CREEK PRIORITY DRAINAGE	
EPA/RI REPORT	
FIGURE 2-9	

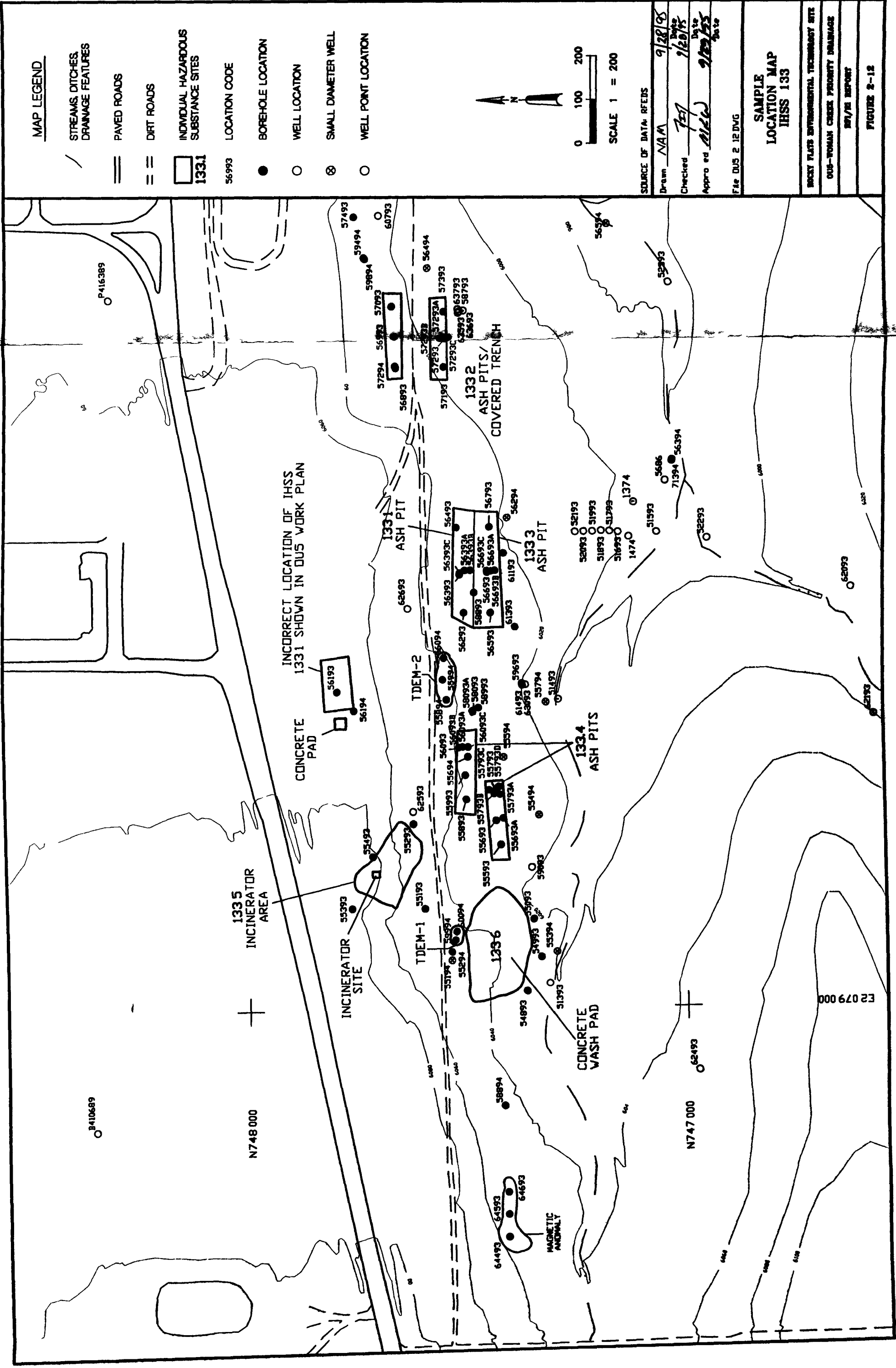


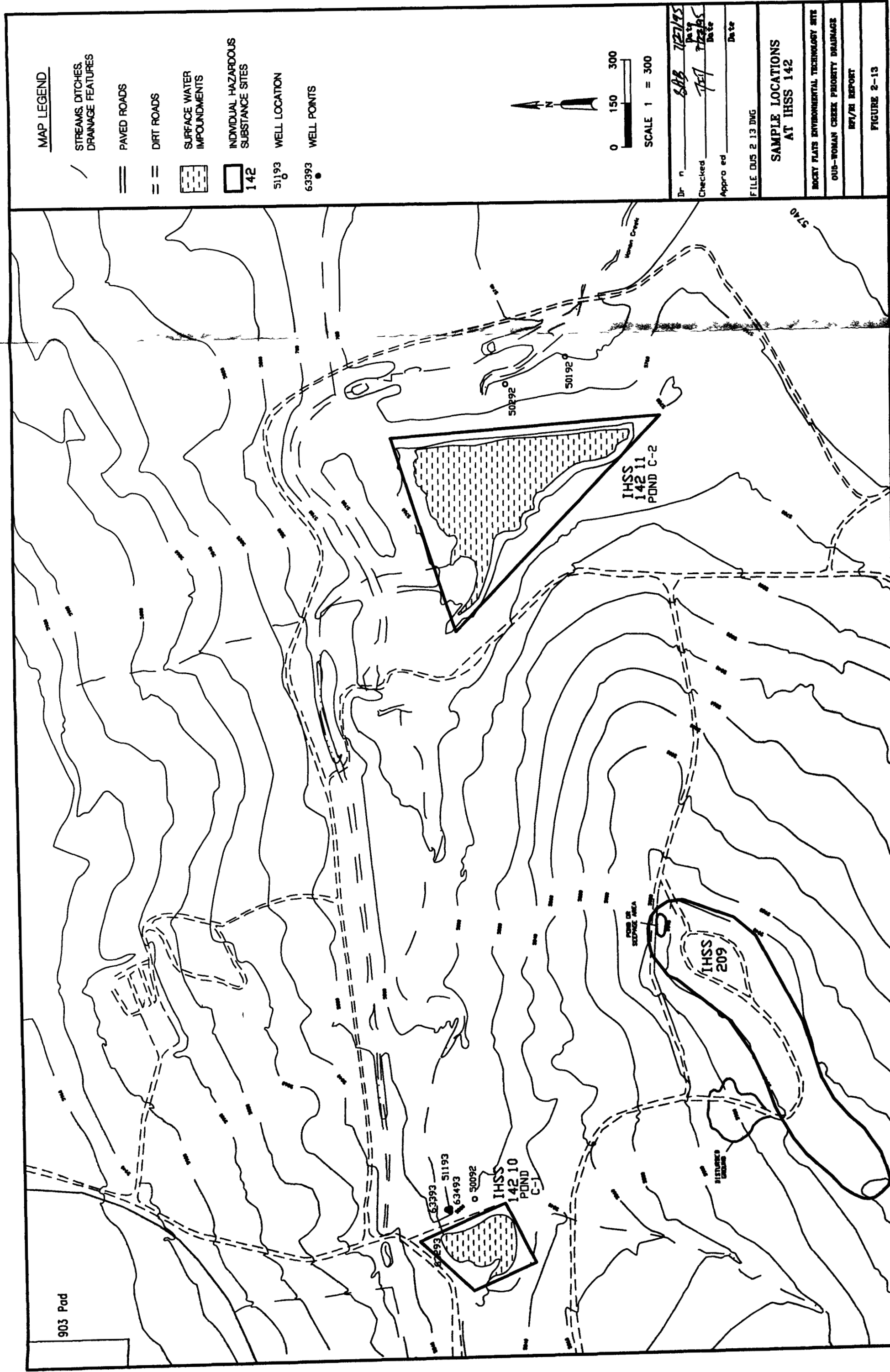


IHSS LOCATIONS SHOWN ON THIS FIGURE WERE SUBSEQUENTLY REVISED (SEE FIGURE 1 2)
 X SURFACE METALLIC DEBRIS IDENTIFIED DURING SURVEY

TIME-DOMAIN EM CONDUCTIVITY - IHSS 133	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
OU5 - WOMAN CREEK PRIORITY DRAINAGE	
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RPI/RI REPORT	
FIGURE 2-11	

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903 Pad

IHSS 142 10 POND C-1

IHSS 209

IHSS 142 11 POND C-2

51193
63393
50092

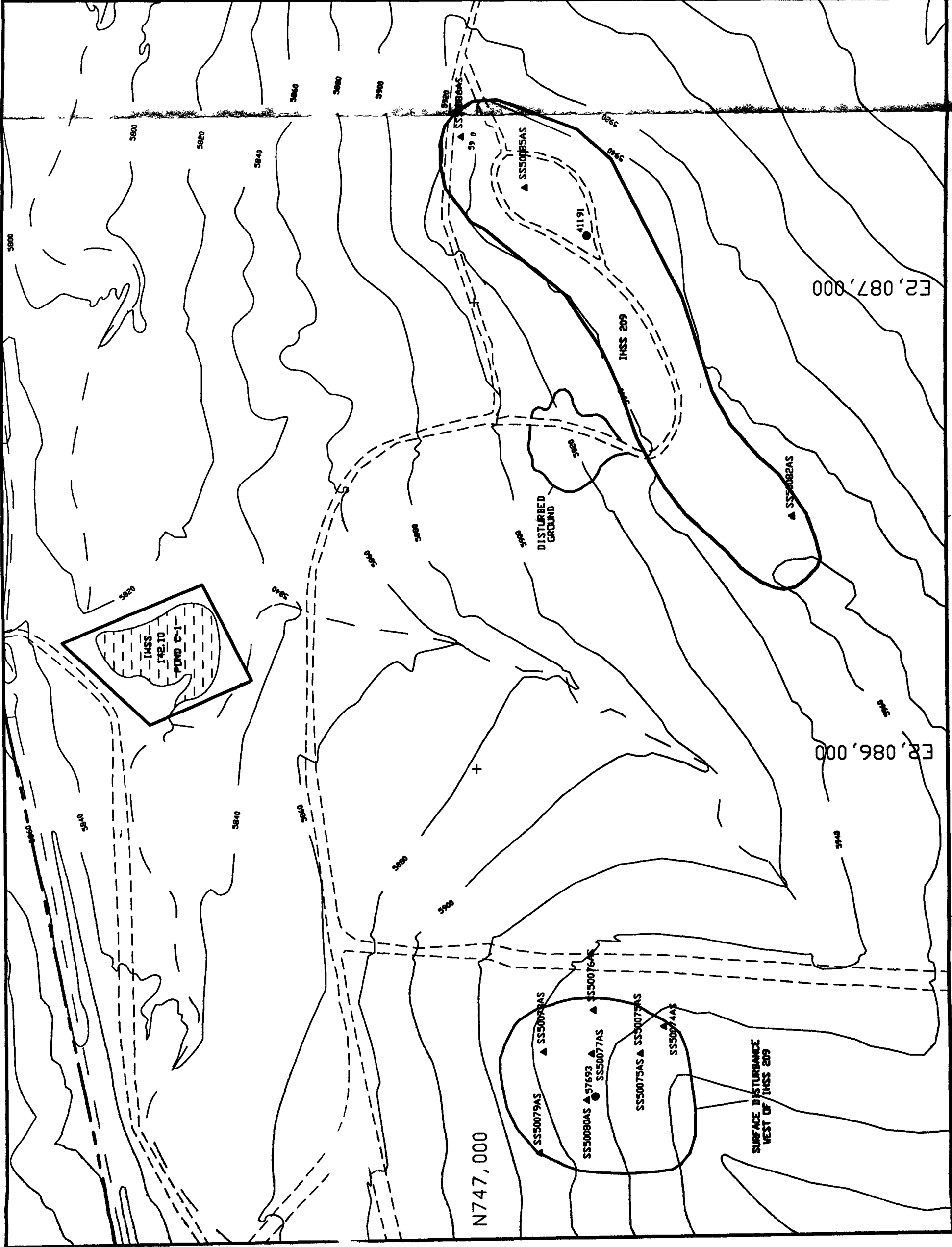
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POD OF SURFACE AREA

DISTURBED

5740



MAP LEGEND

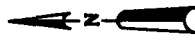
STREAMS, DITCHES,
DRAINAGE FEATURES

== DIRT ROADS

209 INDIVIDUAL HAZARDOUS
SUBSTANCE SITES (IHSS)

SS50086AS SURFACE SOIL SAMPLE
LOCATIONS

57693 BOREHOLE LOCATION



SCALE 1" = 200'

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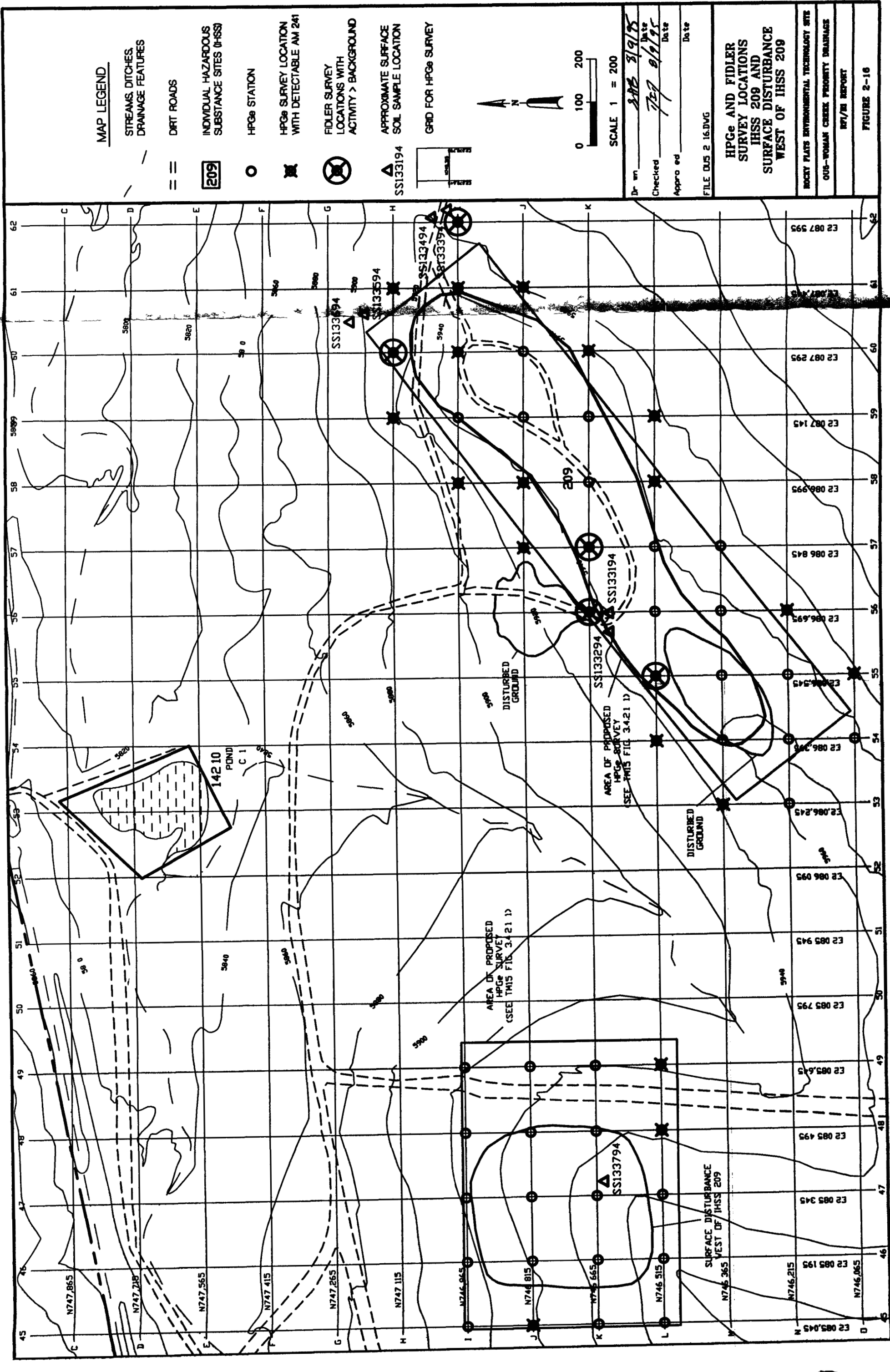
PRE-TM15 SAMPLE LOCATIONS
AT IHSS 209 AND
SURFACE DISTURBANCE
WEST OF IHSS 209

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

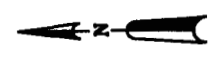
RTI/RI REPORT

FIGURE 2-14



MAP LEGEND

- STREAMS, DITCHES, DRAINAGE FEATURES
- DIRT ROADS
- INDIVIDUAL HAZARDOUS SUBSTANCE SITES (IHSS)
- HPGe STATION
- HPGe SURVEY LOCATION WITH DETECTABLE AM 241
- FIDLER SURVEY LOCATIONS WITH ACTIVITY > BACKGROUND
- APPROXIMATE SURFACE SOIL SAMPLE LOCATION
- GRID FOR HPGe SURVEY



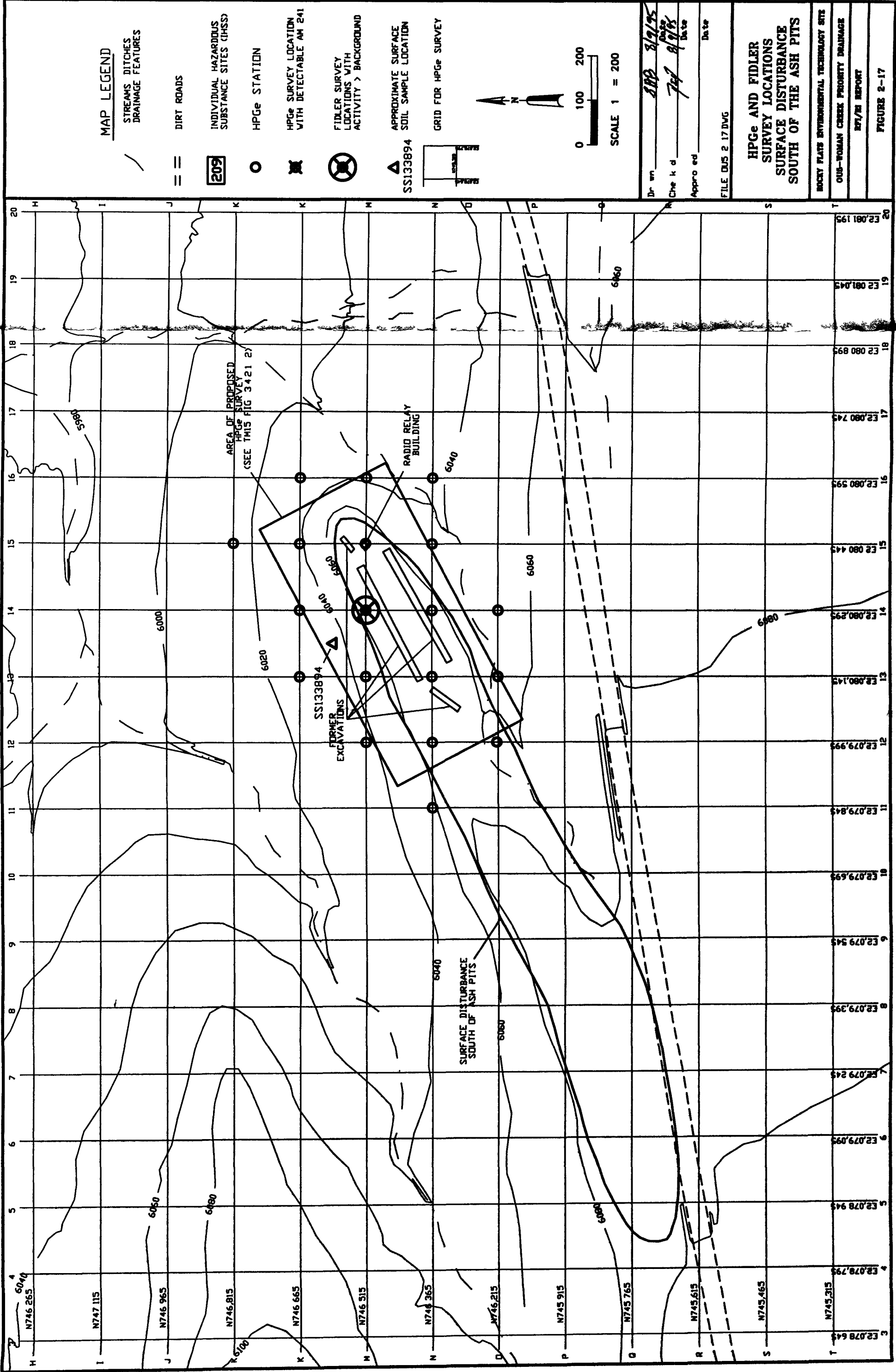
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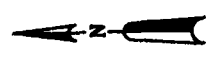
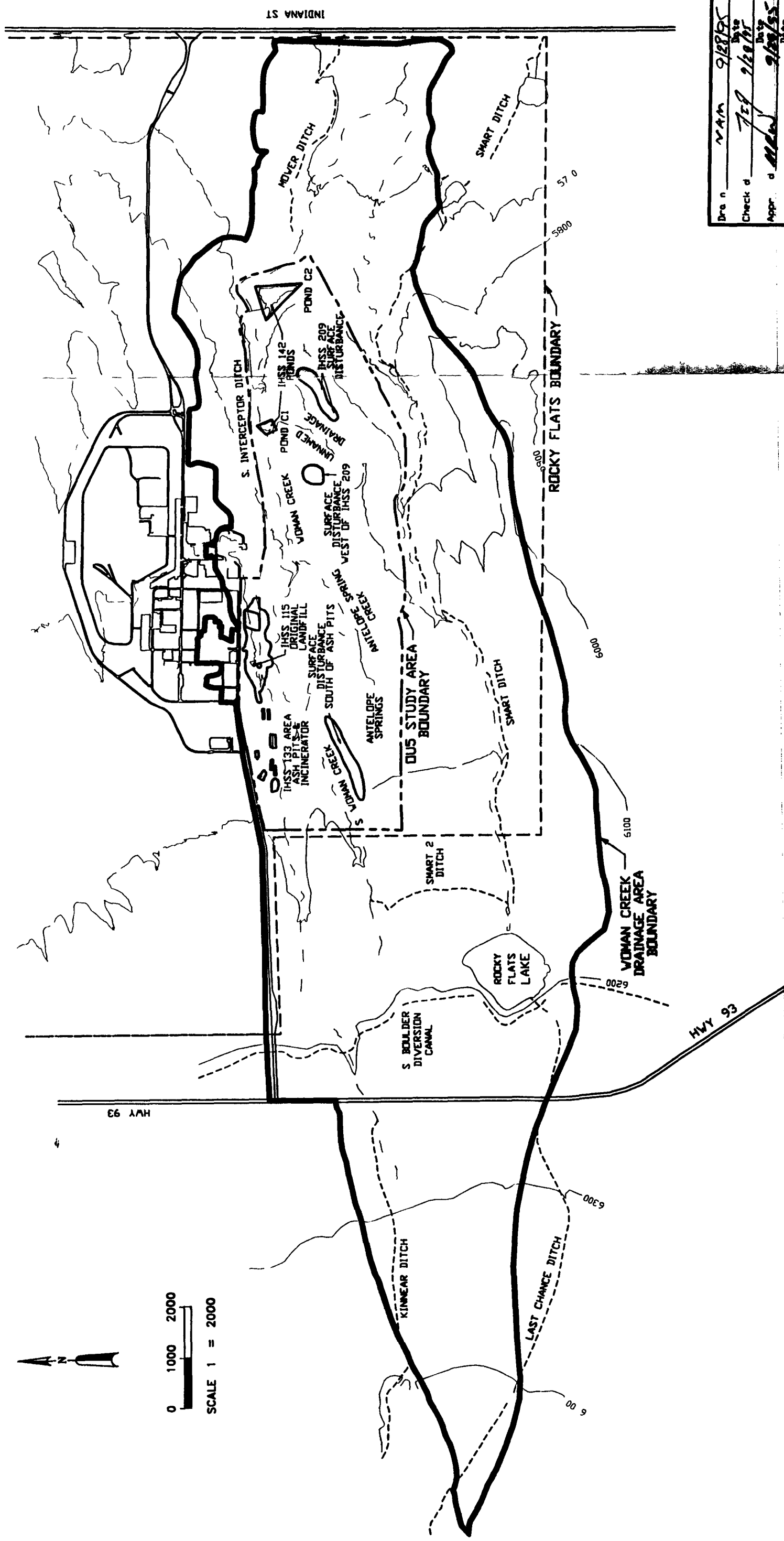
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HPGe AND FIDLER SURVEY LOCATIONS
IHSS 209 AND
SURFACE DISTURBANCE
WEST OF IHSS 209

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE
CUB-WOMAN CREEK PRIORITY DRAINAGE
RPT/BI REPORT

FIGURE 2-16

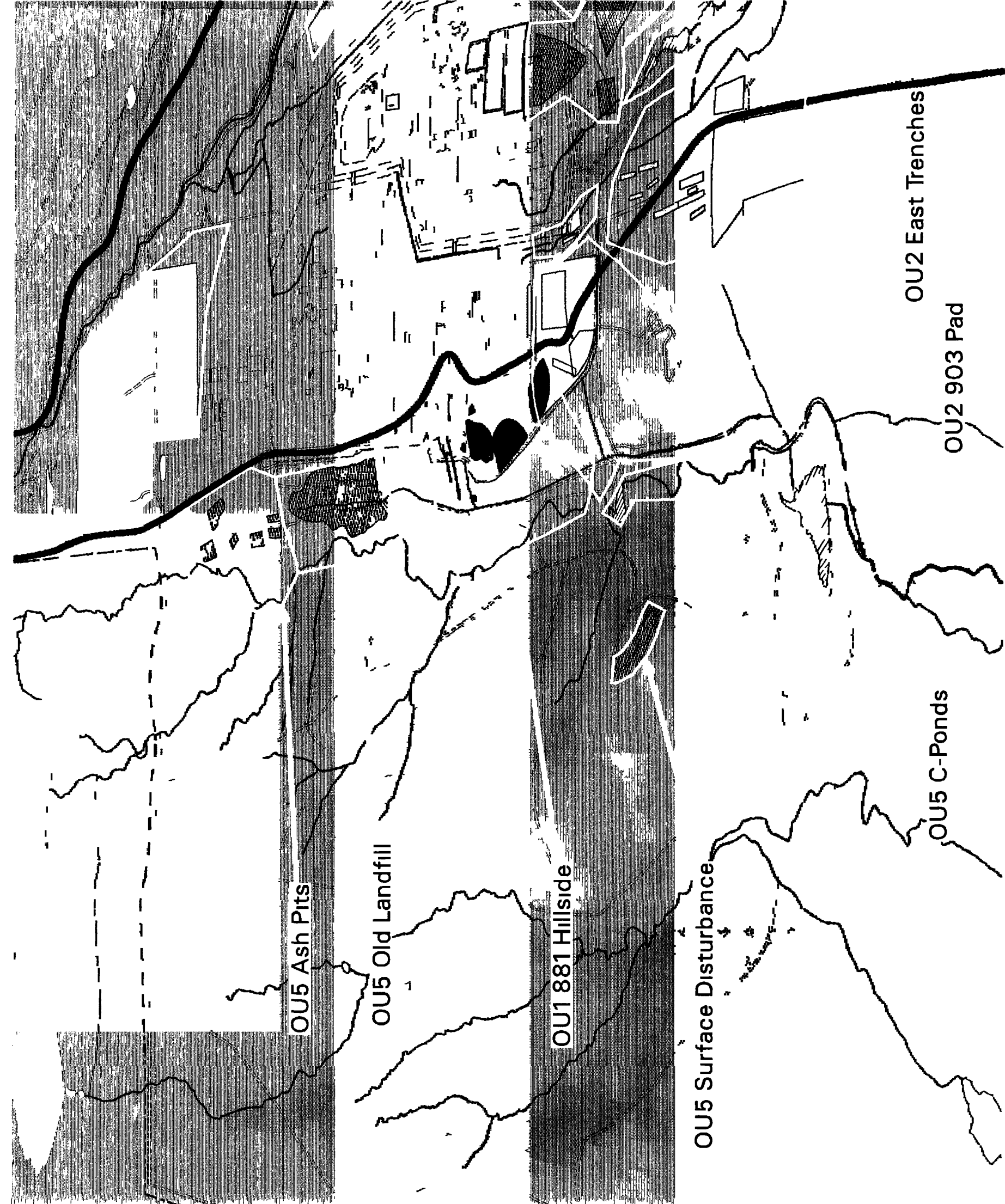




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WOMAN CREEK DRAINAGE	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
DUS-WOMAN CREEK PRIORITY DRAINAGE	
EPA/RI REPORT	
FIGURE 3-1	



EXPLANATION

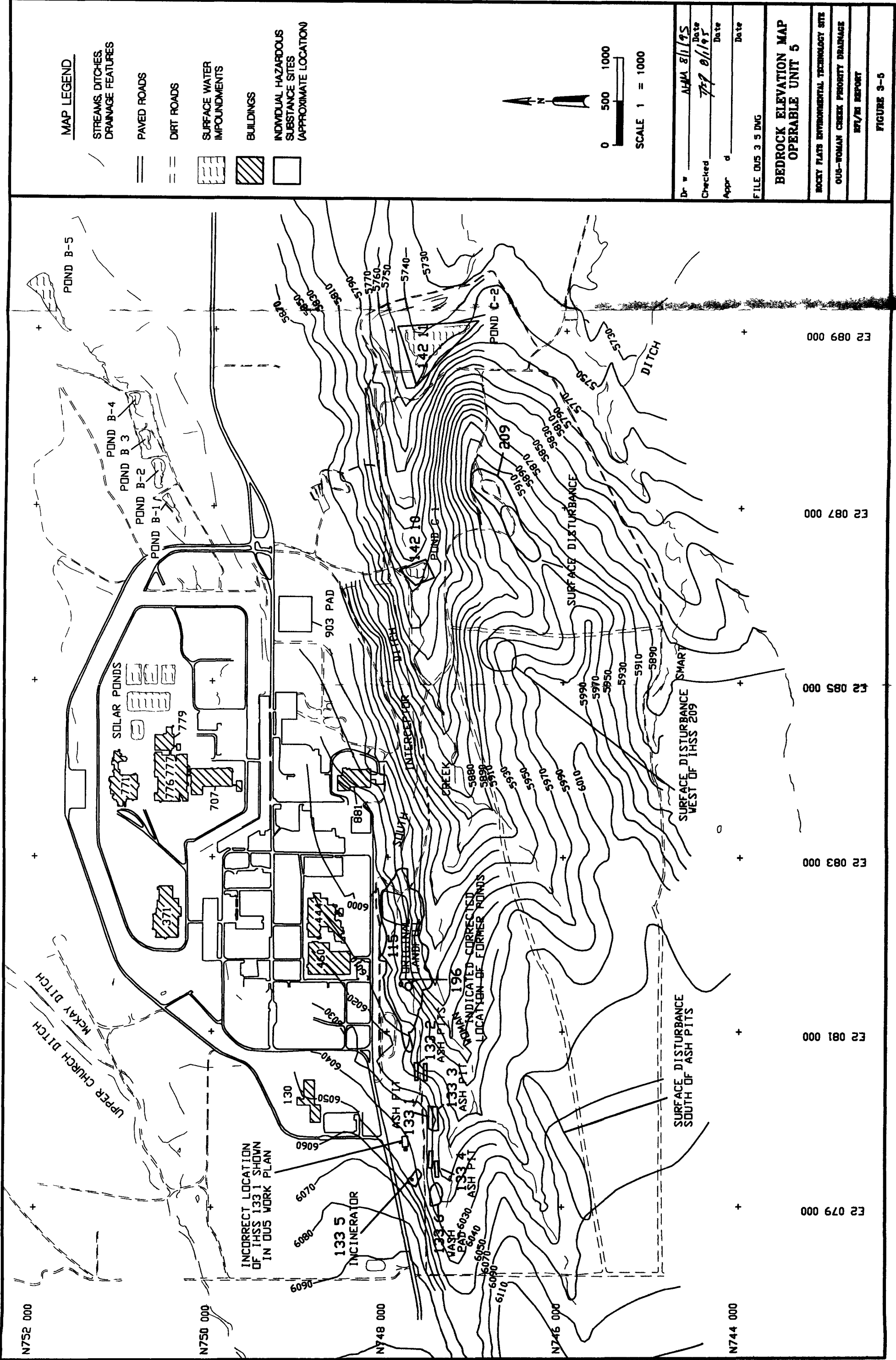
- Watershed Boundary
- Rock Creek Watershed
- Walnut Creek Watershed
- Woman Creek Watershed
- Central Avenue
- Dirt Roads
- Canals and Ditches
- Security Fences
- Rocky Flats Buffer Zone
- Lakes and Ponds
- Buildings
- Operable Unit 1
881 Hillside
- Operable Unit 2
903 Pad Mound and East Trenches
- Operable Unit 4
Solar Ponds
- Operable Unit 5
Woman Creek
- Operable Unit 6
Walnut Creek
- Operable Unit 10
Other Outside Closures
- Operable Unit 11
West Spray Field
- ERA Source Areas



U.S. Department of Energy
Rocky Flats Environmental Technology Site
Golden, Colorado

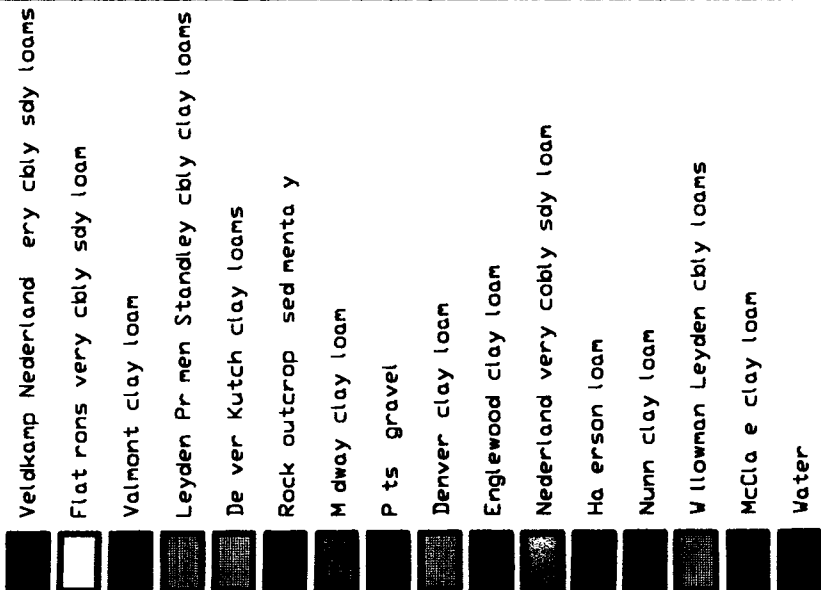
ERA for Walnut Creek and Woman Creek
Watersheds

ERA Source Areas
in
Woman Creek Watershed





DUS SURFACE SOILS MAP



Source USDA SCS
Soil Survey of
Golden Area CO
1980

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Che k d 7/27/85
Appr d 8/11/85

FILE DUS 3 6.DWG AND AML

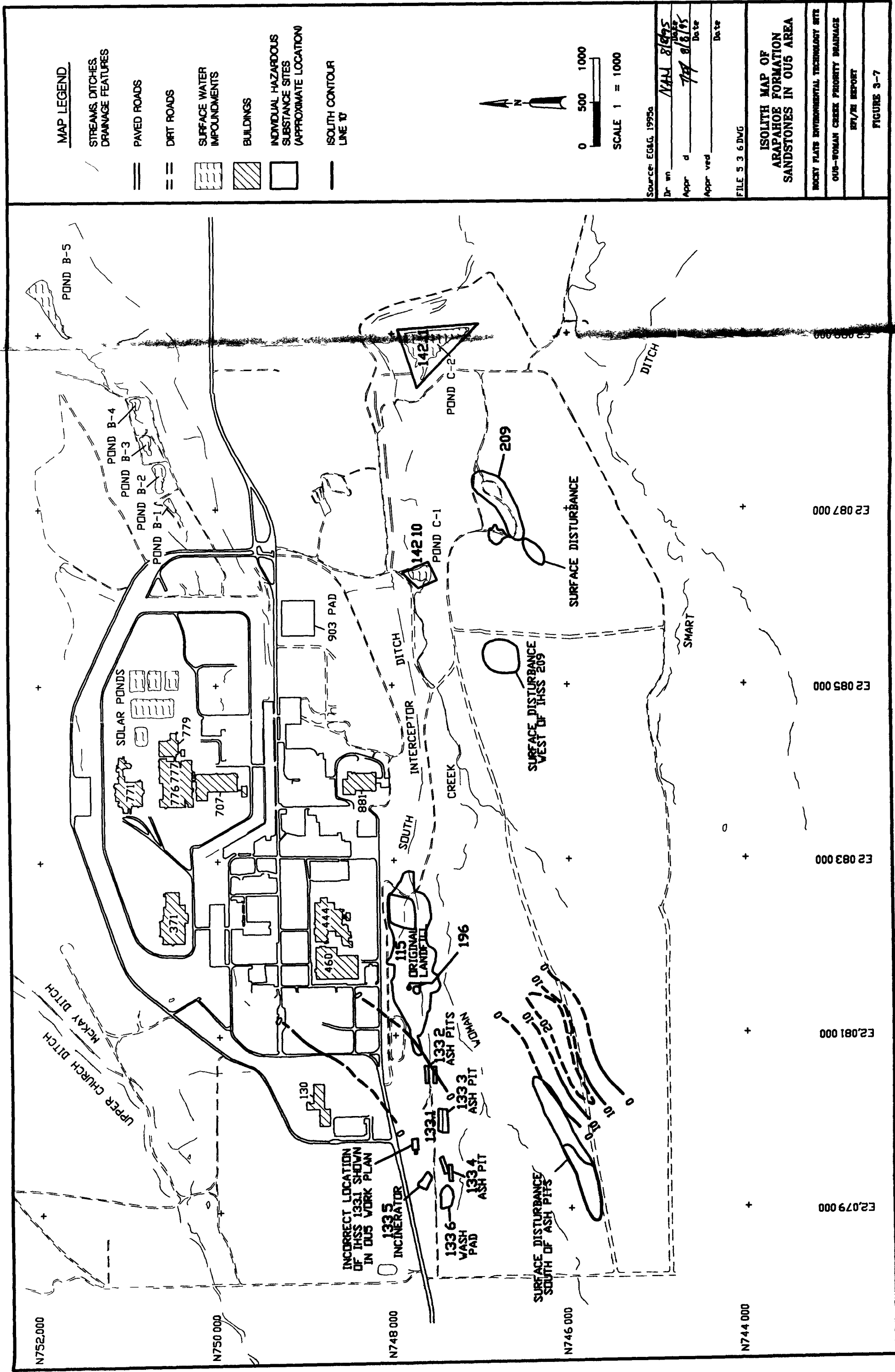
OPERABLE UNIT 5 SURFACE SOIL MAP

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

DUS WOLAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

FIGURE 3-6





LEGEND

SURFICIAL DEPOSITS

RECENT	PLEISTOCENE	RECENT AND PLEISTOCENE	QUATERNARY
Qp	Q1s	Q1a	Q1b
Q1c	Q1d	Q1e	Q1f
Q1g	Q1h	Q1i	Q1j

MAP SYMBOLS

ROAD CLASSIFICATION

Heavy Duty	Medium Duty	Light Duty	Unimproved Drt
Rocky Flats Boundary	IHSS Boundaries		

MAP SYMBOLS

BEDROCK

Upper Cretaceous	Lower Cretaceous	Upper Paleocene	Lower Paleocene
U1	U2	U3	U4
U5	U6	U7	U8

Source Geologic Characterization Report by EG&G March 1995

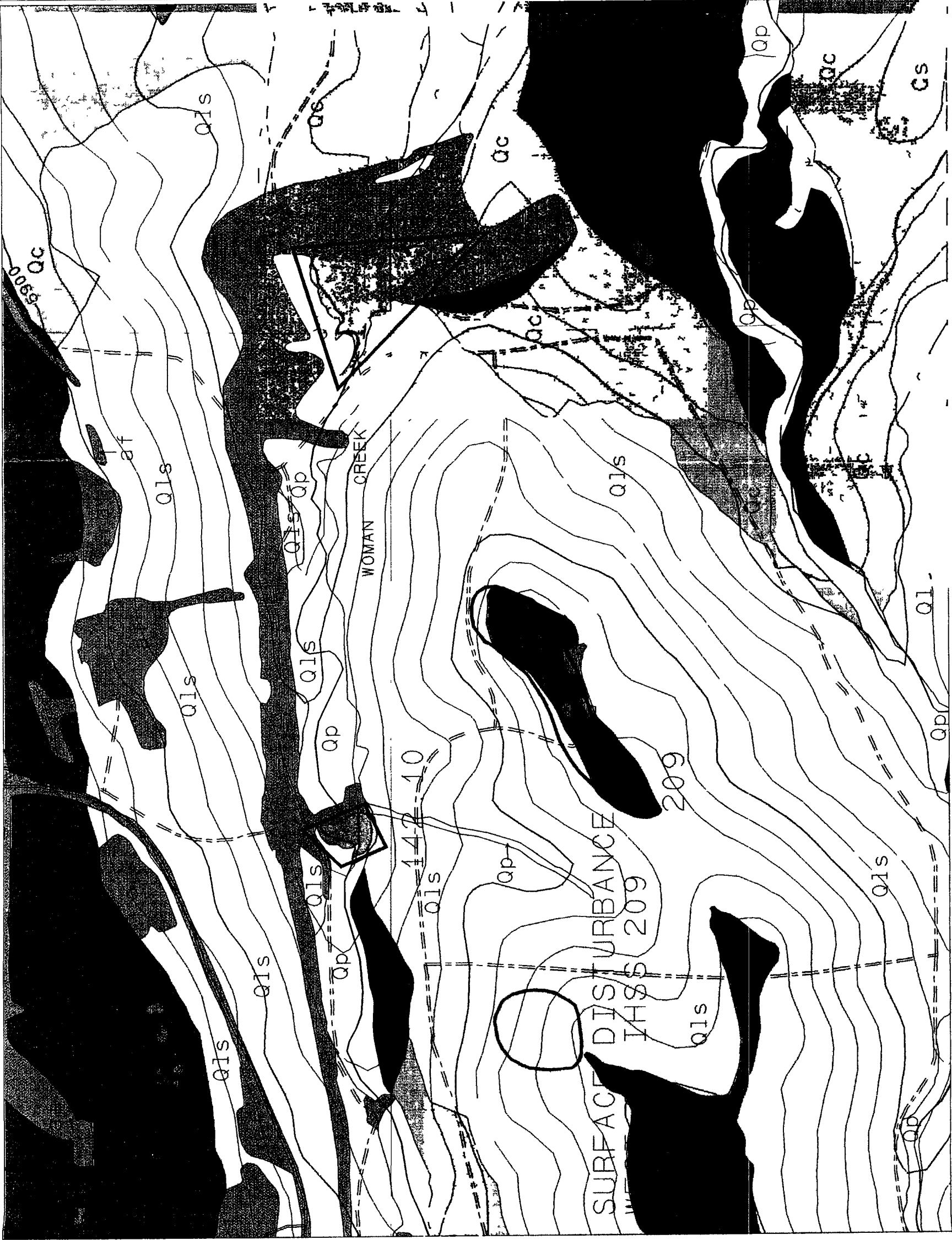
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OPERABLE UNIT 5
WESTERN PORTION
SURFICIAL GEOLOGIC MAP

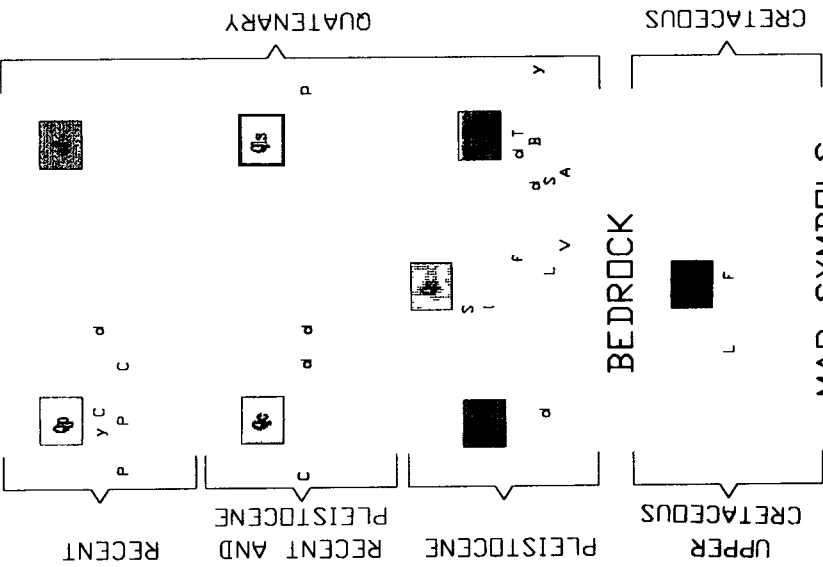
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS WOMAN CREEK PRIORITY DRAINAGE
RTI/RI REPORT

FIGURE 3 9

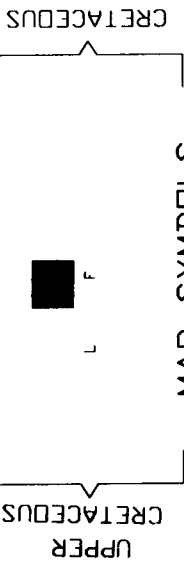


LEGEND

SURFICIAL DEPOSITS

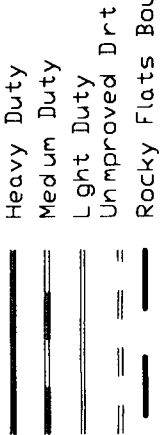


BEDROCK



MAP SYMBOLS

ROAD CLASSIFICATION



Rocky Flats Boundary



IHSS Boundaries

Source Geologic
Characterization
Report by EG&G
March 1995

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FILE DUS 3 10 DWG D L

OPERABLE UNIT 5

EASTERN PORTION

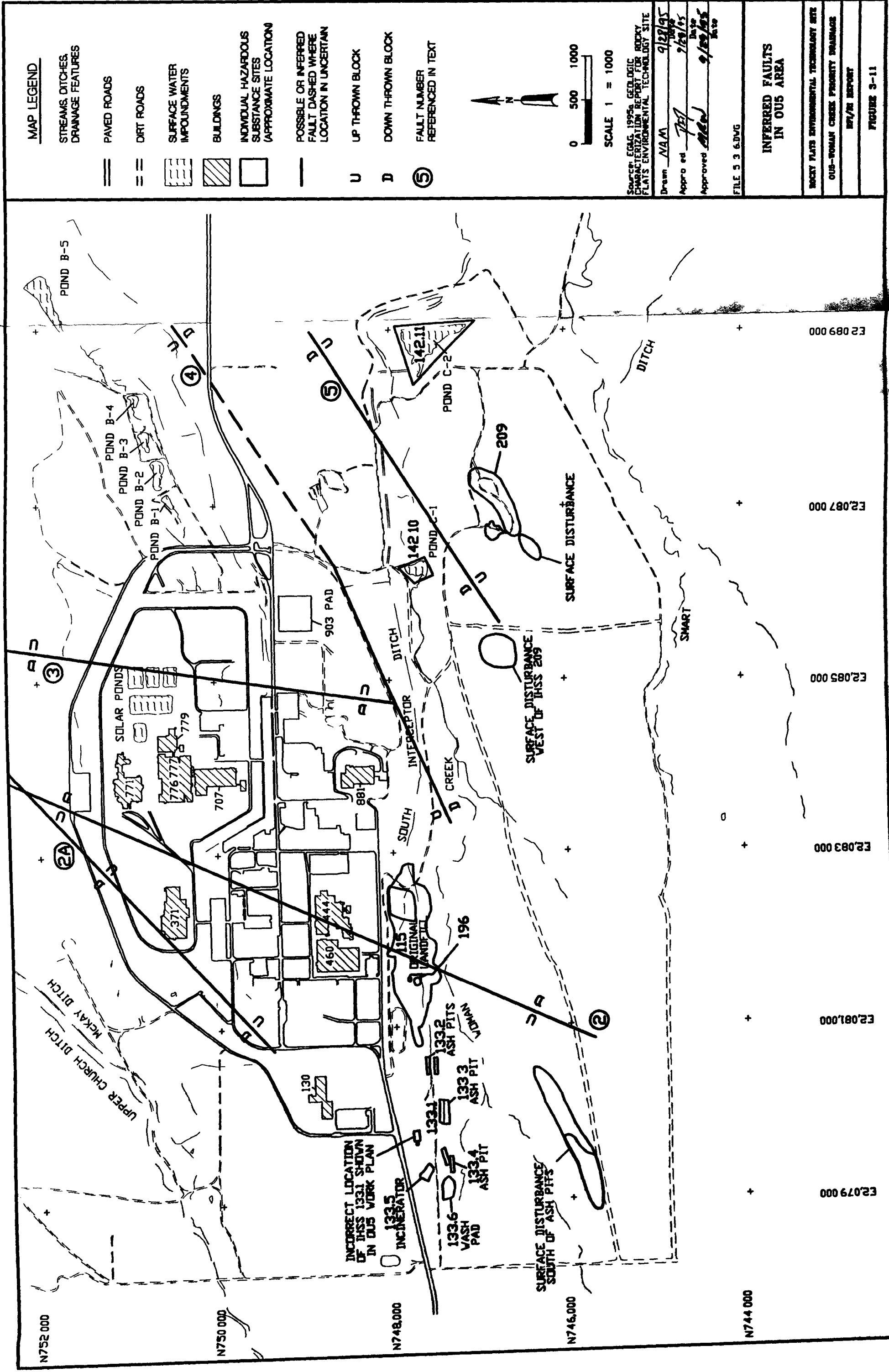
SURFICIAL GEOLOGIC MAP

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 WOMAN CREEK PRIORITY DRAINAGE

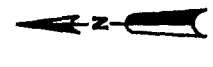
RFI/RI REPORT

FIGURE 3-10



MAP LEGEND

- STREAMS, DITCHES, DRAINAGE FEATURES
- PAVED ROADS
- DIRT ROADS
- SURFACE WATER IMPOUNDMENTS
- BUILDINGS
- INDIVIDUAL HAZARDOUS SUBSTANCE SITES (APPROXIMATE LOCATION)
- POSSIBLE OR INFERRED FAULT DASHED WHERE LOCATION IN UNCERTAIN
- UP THROWN BLOCK
- DOWN THROWN BLOCK
- FAULT NUMBER REFERENCED IN TEXT



0 500 1000
SCALE 1" = 1000'

SOURCE: EG&G, 1995a, GEOLOGIC CHARACTERIZATION REPORT FOR ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

Drawn: N/A
Approved: JEP
Approved: MDE
Date: 9/28/95
Date: 7/28/95
Date: 9/28/95

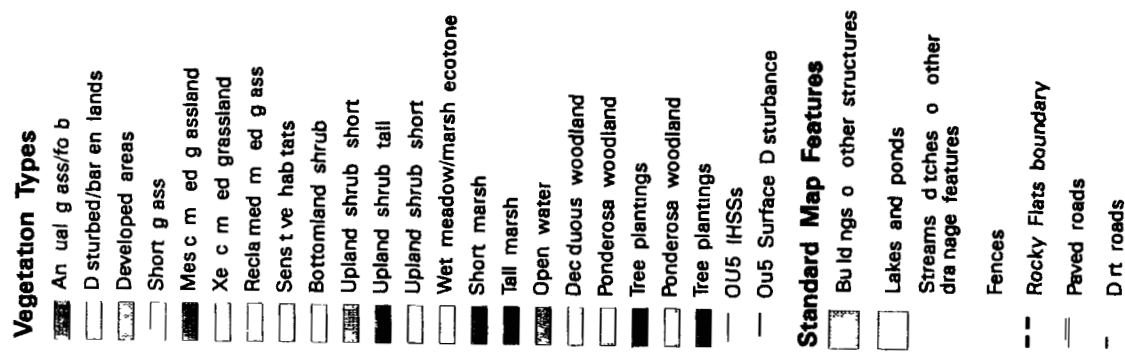
FILE 5 3 6.DWG

INFERRED FAULTS IN OUS AREA

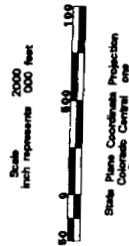
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS-WOMAN CREEK PRIORITY DRAINAGE
EPA/RI REPORT
FIGURE 3-11

Vegetation Types Identified in Woman Creek Watershed in Vicinity of OU5 IHSSs

Figure 3-12




DATA SOURCE
 Satellite reads are furnished by
 Facilities Egr. Plans, Inc.
 CA Rocky Flats, Inc.
 Hydrolog provided by
 USGS
 The vegetation data from Ebasco Associates, Inc. which was
 generated using aerial photos and digitizing hand drawn
 field maps. 993
 Ebasco



DATA SOURCE:
 Wetlands data surveyed, compiled, and assembled by the U.S. Army Corps of Engineers: 1984.
 Buildings, roads, and fences provided by Facilities Eng.
 EOLGO Realty Firm, Inc. 89
 Hydrology provided by USGS (data unknown)

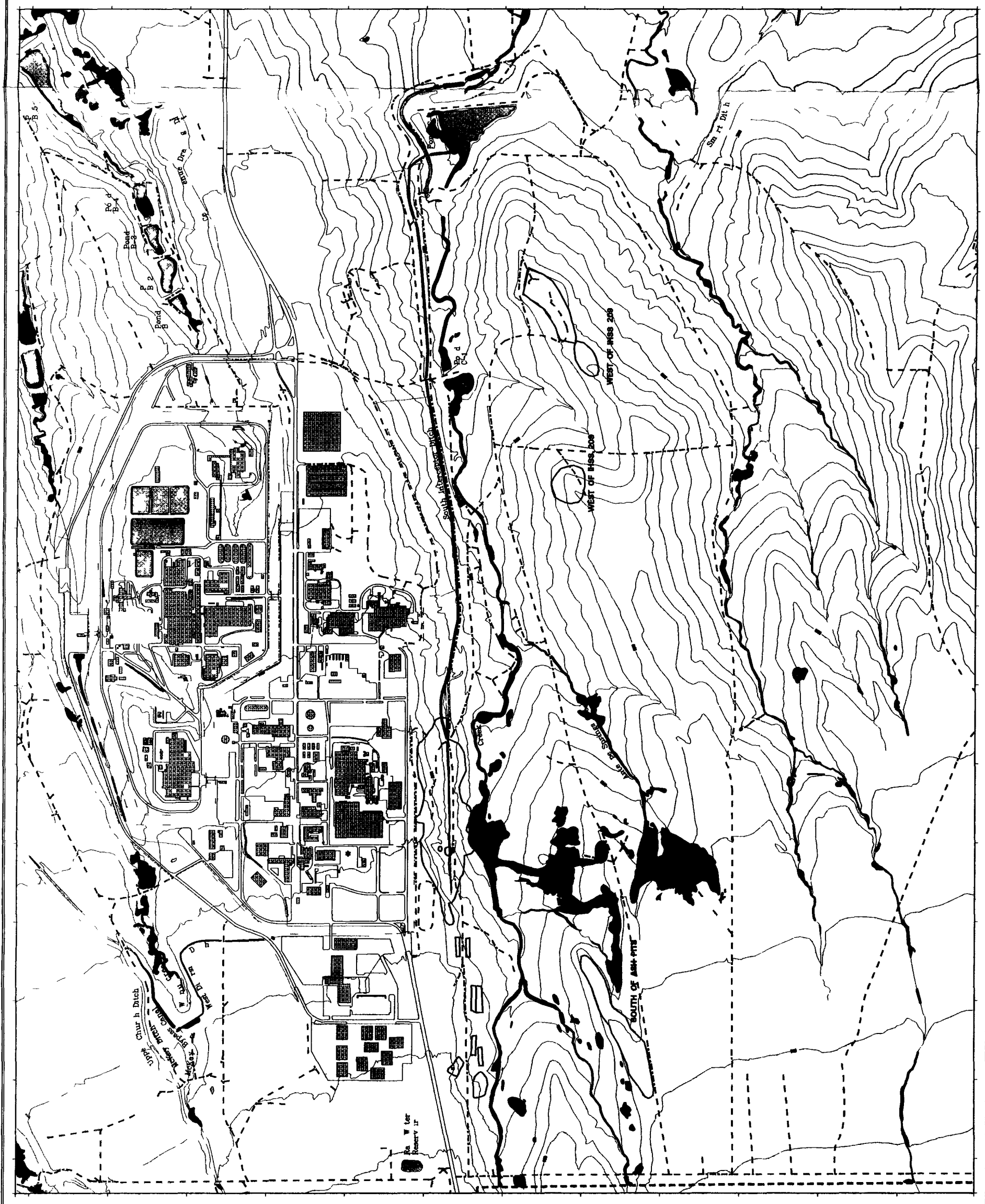
Scale
1 inch represents 1000 feet



East Flats Discharge Population
Controlled by
Damper (MADZ)

U.S. Department of Energy
Rocky Flats Environmental Technology Site

MAP ID: 98-4-18 August 07, 1996



Capture Locations and
Probable Range of
Preble's Meadow Jumping
Mouse
in OUS Vicinity

Figure 3-14

- Probable Range
- Records of (PMJM)
(Zapus hudsonius preblei)
- OUS IHSSs
- OUS Surface Disturbance

Standard Map Features

- Buildings or other structures
- Lakes and ponds
- Streams, ditches, or other
drainage features
- Fences
- Contours (20 intervals)
- Rocky Flats boundary
- Paved roads
- Dirt roads

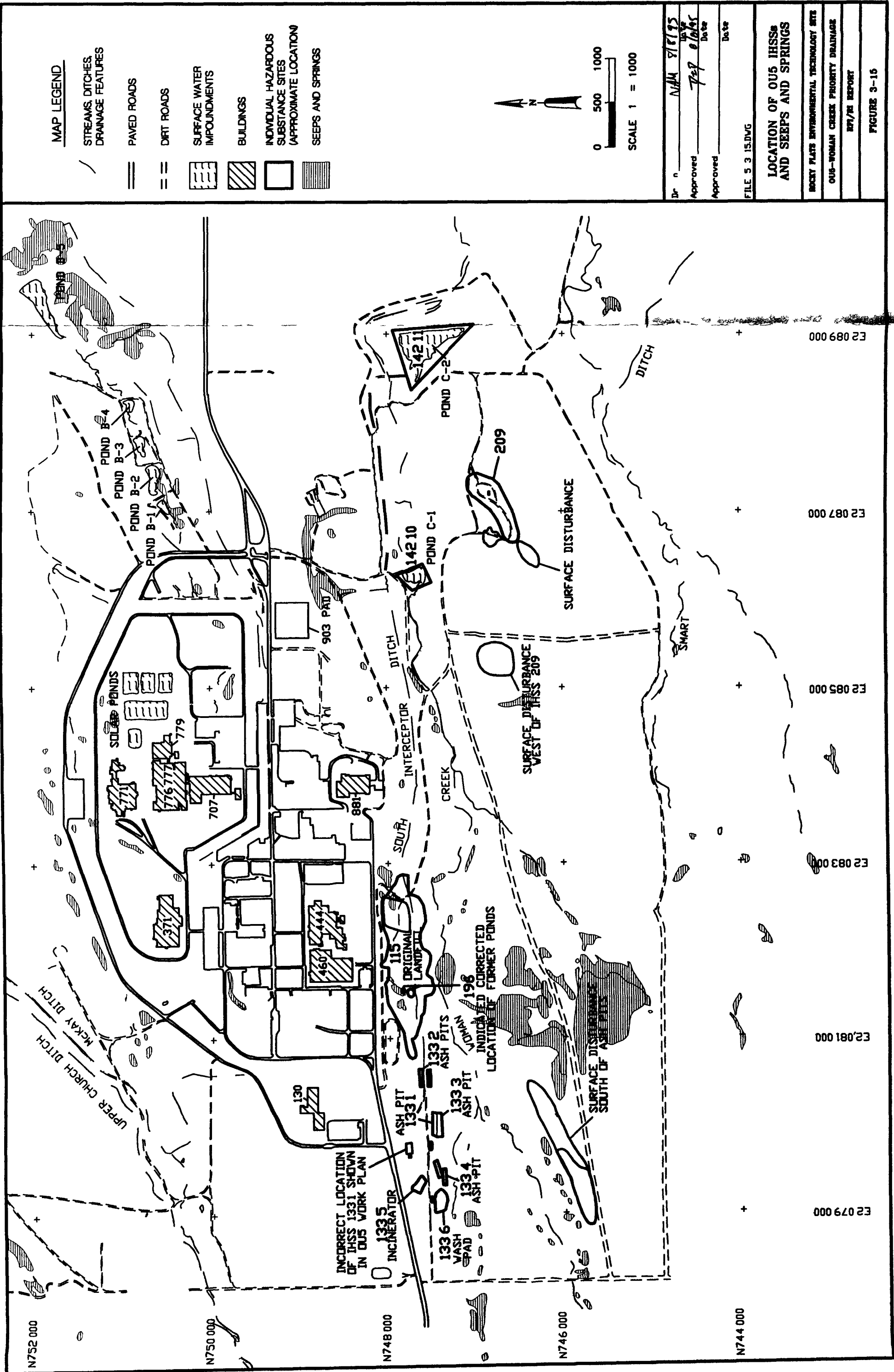
DATA SOURCE:
Topographic maps and fences provided by
Rocky Flats Environmental Technology Site,
Rocky Flats, CO.
Hydrology provided by
USGS (US Geological Survey)
Probable Range provided by Alaska Bureau of
ENTOMOLOGY

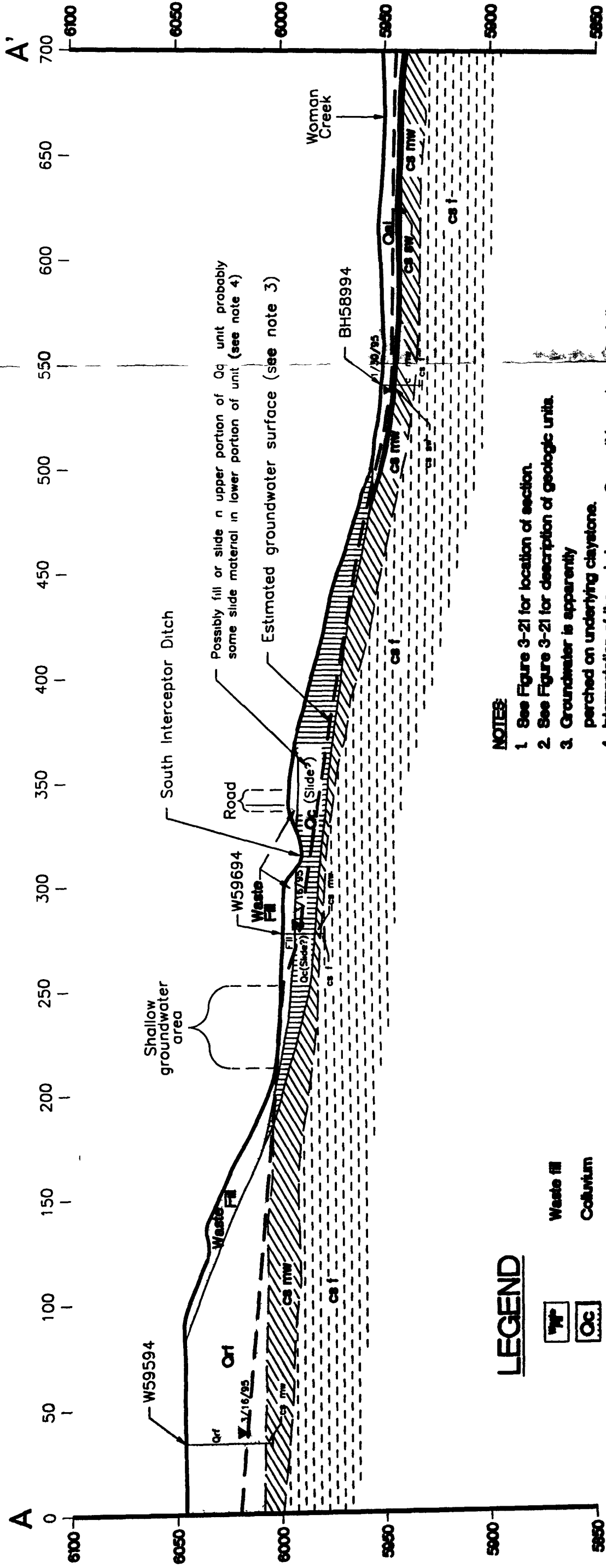


Scale
1 inch represents 1000 feet



Rocky Flats Environmental Technology Site
Capture Locations
Date: 10/27/87

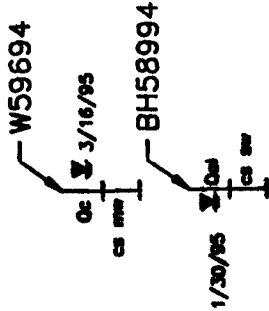




LEGEND



Waste Fill
Colluvium
Valley Fill Alluvium
Rocky Flats Alluvium
Laramie Formation Claystone
sw - severely weathered
mw - moderately weathered
f - fresh

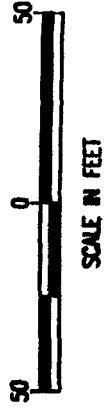


Geotechnical boring with monitoring well, showing geologic unit, groundwater elevation and date measured.

Geotechnical boring, backfilled, showing geologic unit, groundwater elevation and date encountered.

NOTES:

1. See Figure 3-21 for location of section.
2. See Figure 3-21 for description of geologic units.
3. Groundwater is apparently perched on underlying claystone.
4. Interpretation of the unit shown as Oc on this section is tentative and based on materials encountered in W59694. The location of pre-landfill ground surface along this section is needed to more confidently interpret origin of these materials.



Drawn	N/A/M	9/28/95
Checked	JEP	1/29/95
Approved	MEJ	9/29/95
		Date

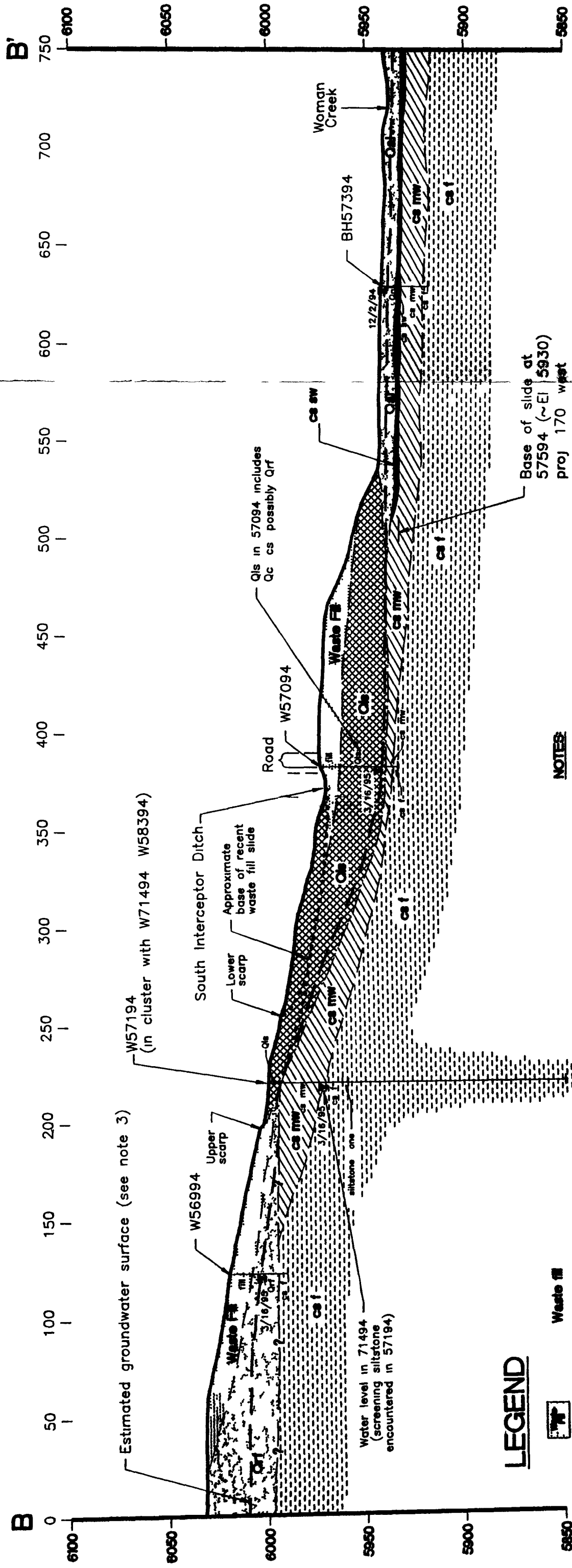
FILE QUS-3-17 DWG

GEOLOGIC CROSS SECTION A-A
IHSS 115/198

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
QUS-WOMAN CREEK PRIORITY DRAINAGE
WPA/NE REPORT

FIGURE 3-17

SOURCE: ECAC 1985a; PRELIMINARY ROCKY FLATS TECHNOLOGY SITE GEOTECHNICAL INVESTIGATION (DRAFT)



LEGEND

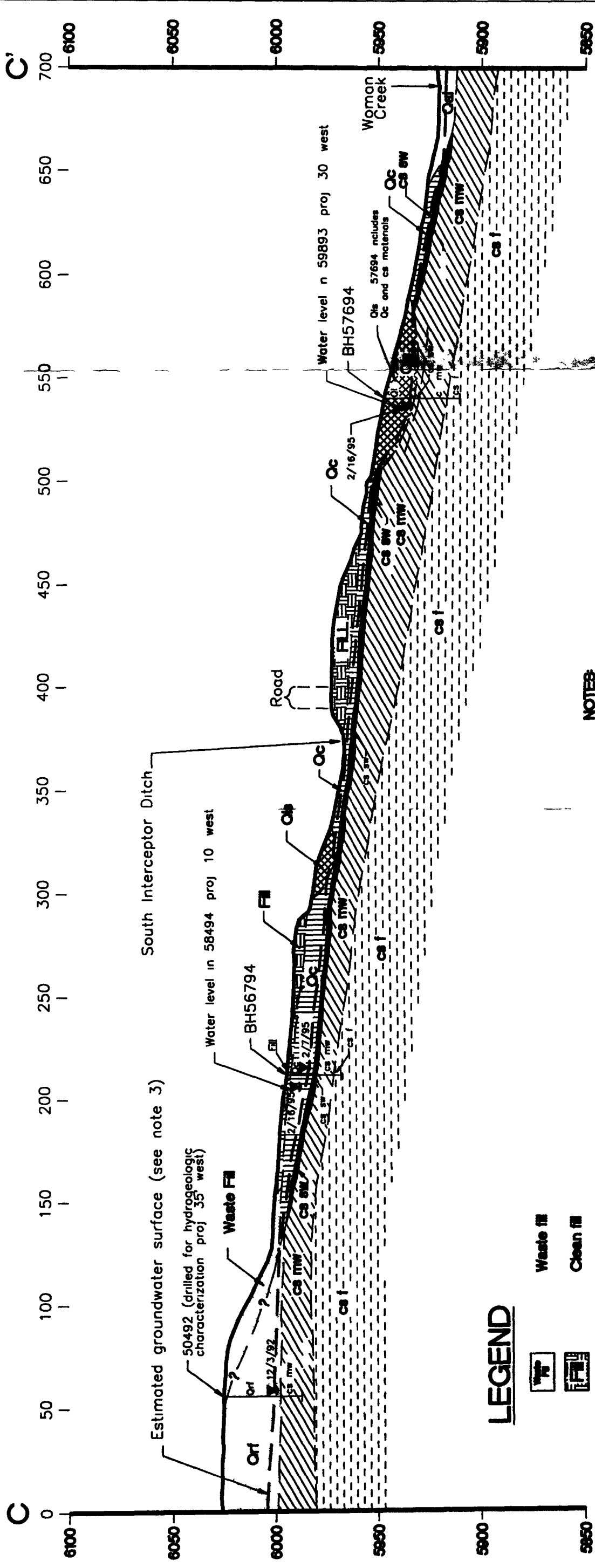
- Waste fill
- Landslide Deposits (unit may contain material from several discrete landslides)
- Valley Fill Alluvium
- Rocky Flats Alluvium
- Laramie Formation Claystone
 - sw - severely weathered
 - mw - moderately weathered
 - f - fresh
- Geotechnical boring, with monitoring well, showing geologic units, groundwater elevation and date measured
- Geotechnical boring, backfilled, showing geologic units, groundwater elevation and date encountered

NOTES:

1. See Figure 3-21 for location of section.
2. See Figure 3-21 for description of geologic units.
3. Groundwater is apparently perched on underlying claystone.



Drawn	NAM	9/28/95
Checked	FEJ	9/28/95
Approved	MEL	9/29/95
FILE 5-3-18.DWG		
GEOLOGIC CROSS SECTION B-B IHSS 115/196		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUI--WOMAN CREEK PROPERTY DRAINAGE		
INT/EXT REPORT		
FIGURE 3-18		



LEGEND

- Waste fill
- Clean fill
- Colluvium
- Landslide Deposits (unit may contain material from several discrete landslides)
- Valley Fill Alluvium
- Rocky Flats Alluvium
- Laramie Formation Claystone:
 - sw - severely weathered
 - mw - moderately weathered
 - f - fresh



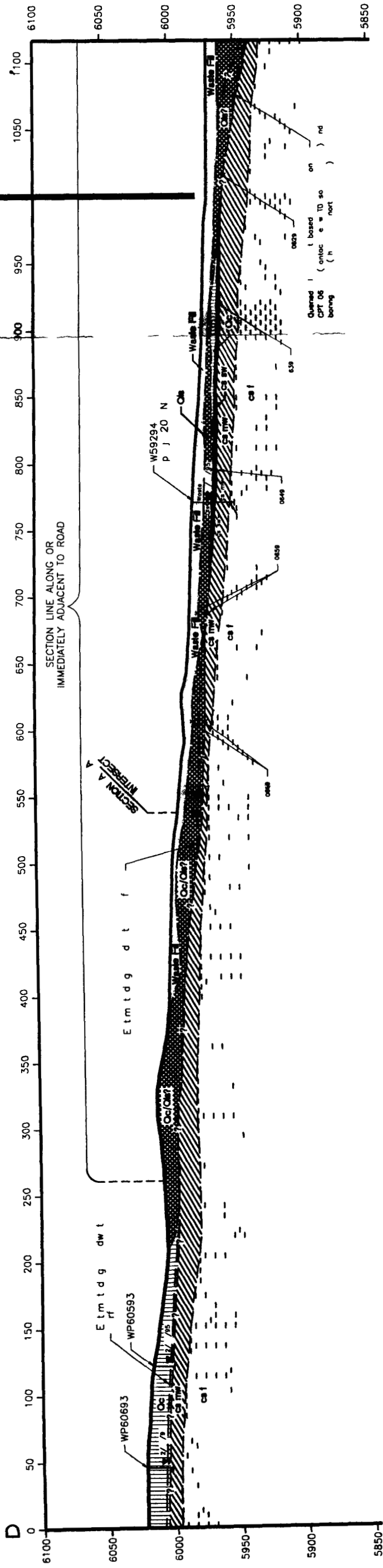
NOTES

1. See Figure 3-21 for location of section.
2. See Figure 3-21 for description of geologic units.
3. Groundwater is apparently perched on underlying claystone.

Drawn	NAM	9/22/95
Checked	JEP	2/28/95
Approved	MW	9/22/95
FILE OUS-3-19 DWG		
GEOLOGIC CROSS SECTION C-C IHSS 115/196		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUS-WOMAN CREEK PROPERTY DRAINAGE		
RFT/WM REPORT		
FIGURE 3-19		

MATCH
LINE

FIGURE 3-20B



LEGEND



Waste FI: road fill probably including some waste material
Clean road fill
Waste FI: clean fill, undifferentiated
Colluvium
Landslide Deposits: (unit may contain material from several discrete landslides)
Claystone: or severely weathered
moderately weathered
fresh

NOTES:

1. See Figure 3-21 for location of section.
2. See Figure 3-21 for description of geologic units.
3. Geologic contacts from projected exploration locations are adjusted to assumed elevation along line of section.

W57094

CS / 7/95
CS / 7/95

BH57494

CS / 7/95
CS / 7/95

W57094

CS / 7/95
CS / 7/95

W57094

CS / 7/95
CS / 7/95

Geotechnical boring with monitoring well, showing geologic units, groundwater elevation, and date measured.

Geotechnical boring, backfilled, showing geologic units, groundwater not encountered.

Interpreted geologic contact based on projected CPT (Cone Penetration Test) with sounding number

Well point installed for hydrogeologic characterization, showing groundwater elevation and date measured.



SCALE IN FEET

Drawn N/A 9/22/95

Checked 7/9 9/28/95

Approved Mew 9/28/95

FILE 5-3-20ADWING

GEOLOGIC CROSS
SECTION D-D
IHSS 115/196

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

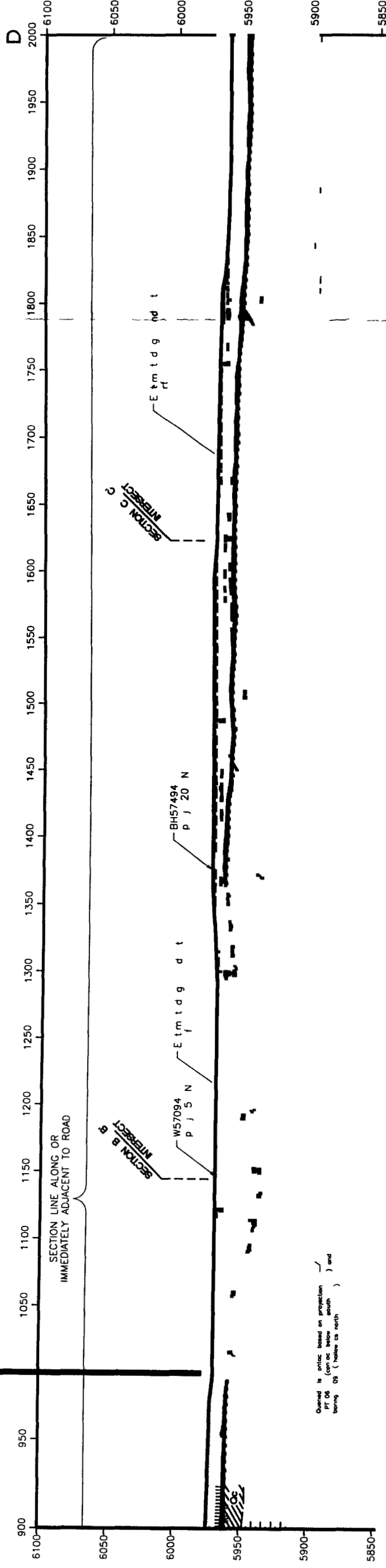
W/ME REPORT

FIGURE 3-20A

SOURCE: EG&G, 1995a: PRELIMINARY ROCKY FLATS TECHNOLOGY SITE GEOTECHNICAL INVESTIGATION (DRAFT)

MATCH
LINE

FIGURE 3-20A



LEGEND

	Waste fill: road fill probably including some waste material
	Clean road fill
	Waste fill, clean fill, undifferentiated
	Colluvium
	Landslide Deposits (unit may contain material from several discrete landslides)
	Claystone: sw severely weathered, mw moderately weathered, f fresh

NOTES:

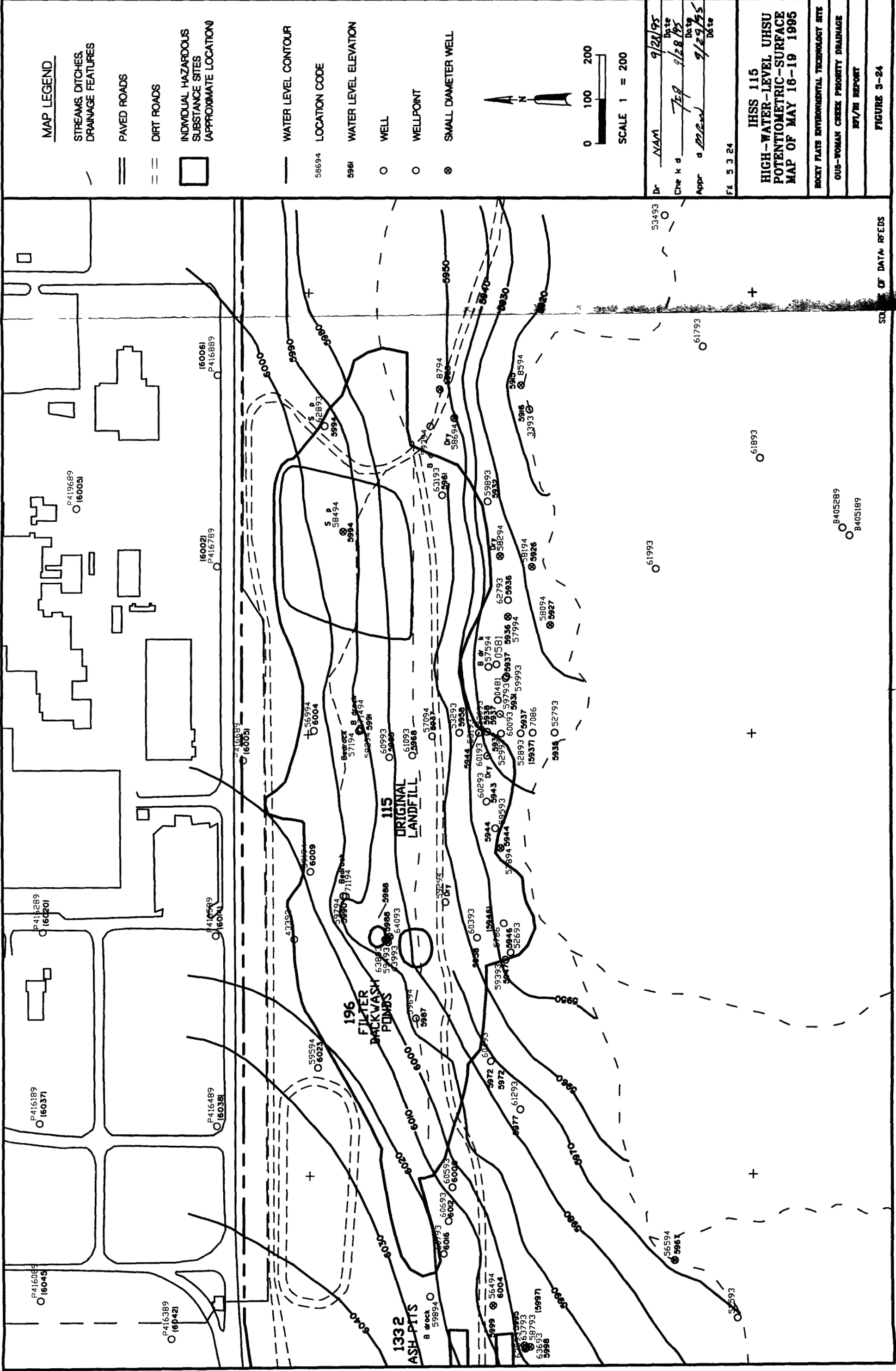
1. See Figure 3-21 for location of section.
2. See Figure 3-21 for description of geologic units.
3. Geologic contacts from projected exploration locations are adjusted to assumed elevation along line of section.

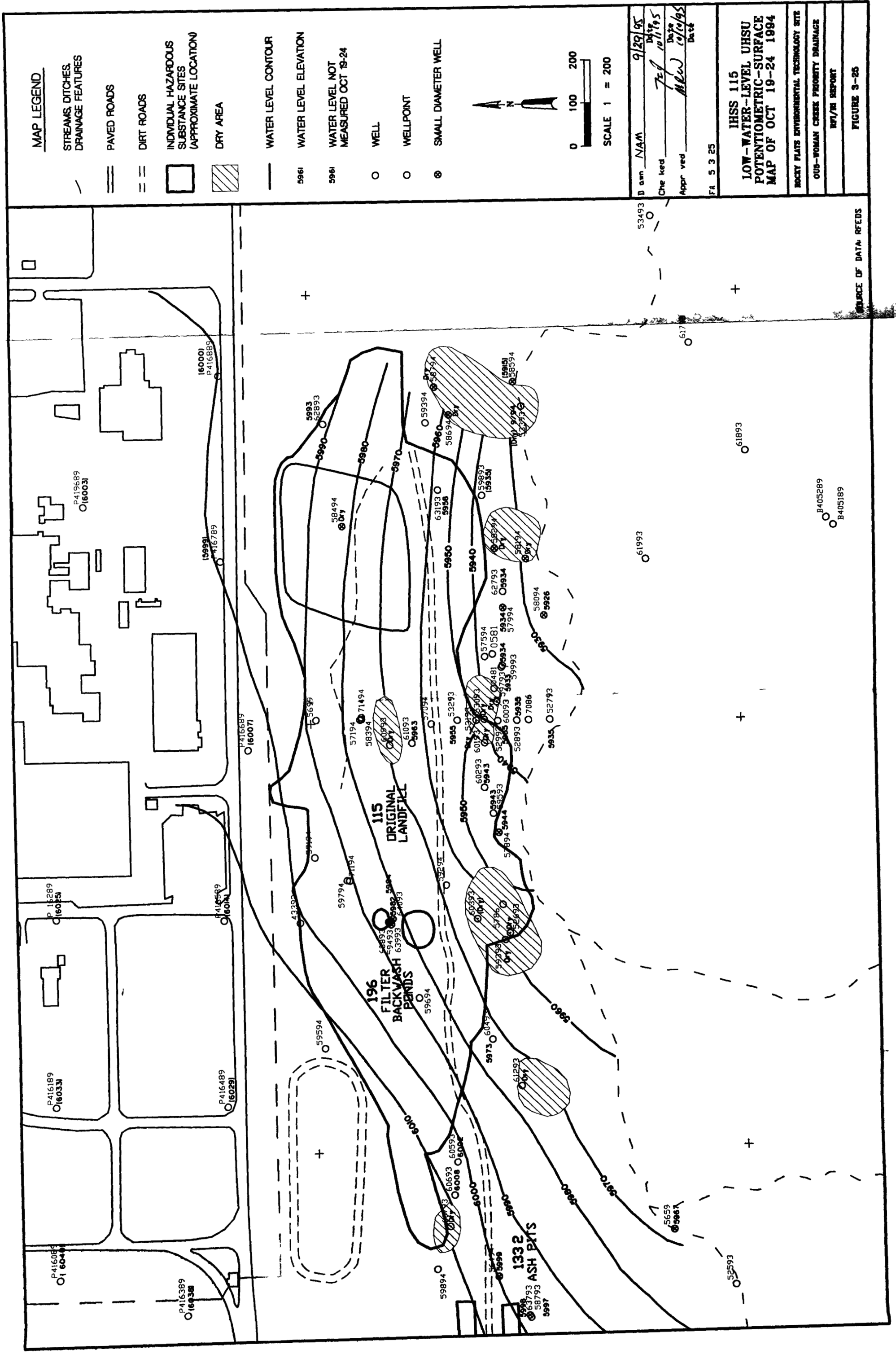
Geotechnical boring with monitoring well, showing geologic units, groundwater elevation, and date measured.

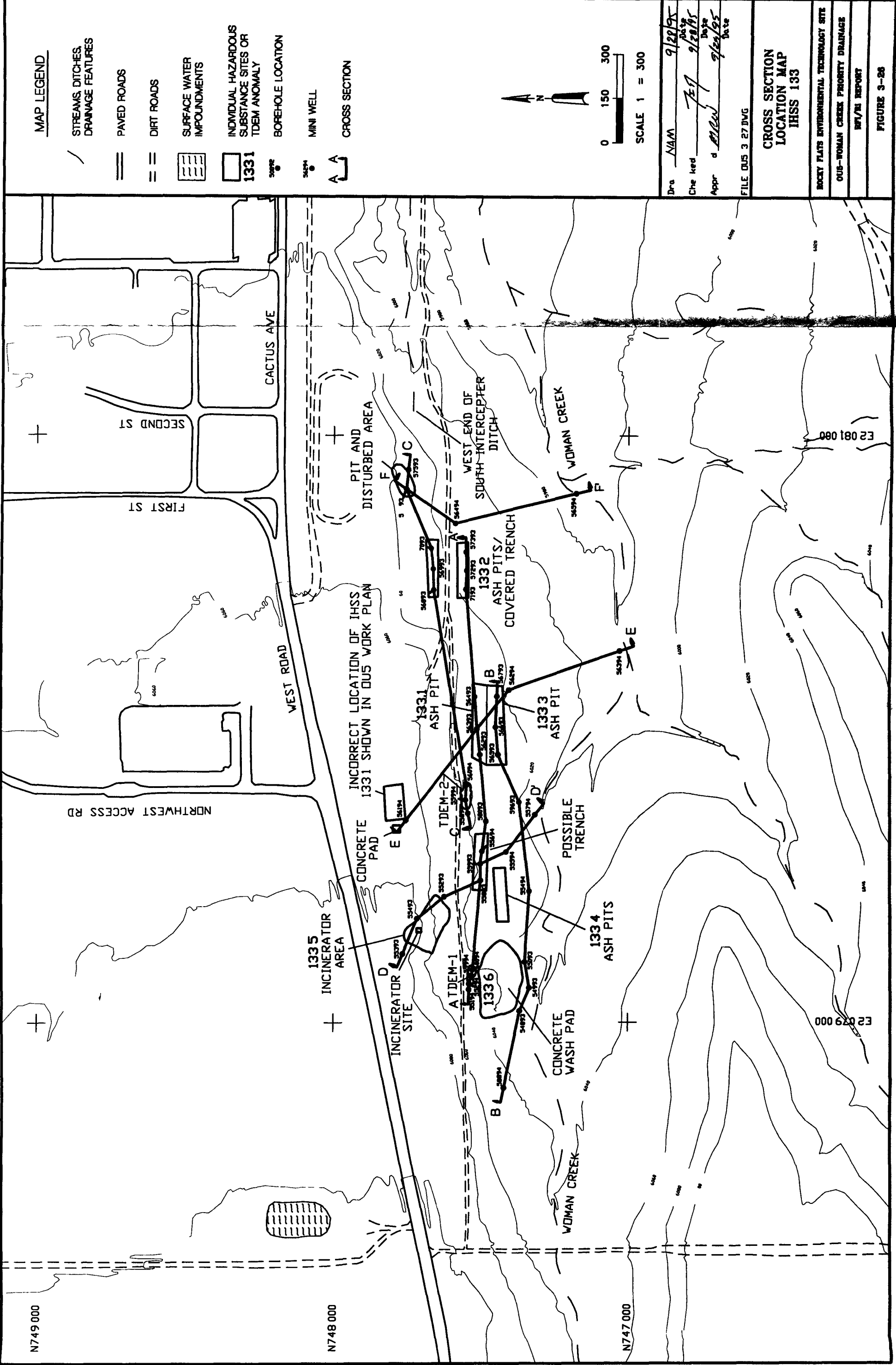
W57094
BH57494
WP60693

Drawn	NAH	9/28/95
Checked	FEJ	9/29/95
Approved	MEL	9/29/95
FILE 5-3-208.DWG		
GEOLOGIC CROSS SECTION D-D IHSS 115/196		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUIS-WOMAN CREEK PRIORITY DRAINAGE		
RPT/RE REPORT		
FIGURE 3-20B		







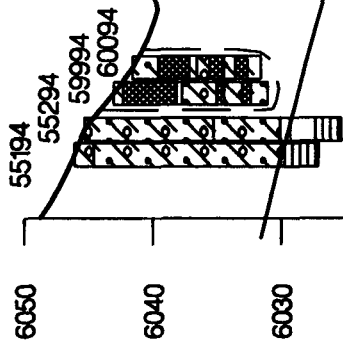


Dra	NAM	9/28/95
Chk	led	9/28/95
Appr	d	9/28/95
		9/28/95
FILE DUS 3 27 DWG		
CROSS SECTION LOCATION MAP IHSS 133		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
DUS-WOMAN CREEK PRIORITY DRAINAGE		
RFT/M REPORT		
FIGURE 3-26		

A

ELEVATION
FEET MSL

(TDEM 1)



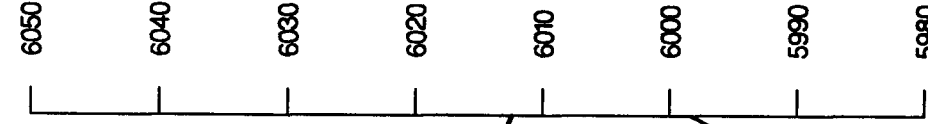
IHSS 1334

IHSS 1331

IHSS 1332
SOUTH TRENCH

A'

ELEVATION
FEET MSL



BEDROCK SURFACE WAS
INTERPRETED FROM BEDROCK
ELEVATION MAP FIGURE 3 5.

SEE FIGURE 3 26
FOR CROSS SECTION LOCATION

NOTES

DISTANCE BETWEEN BOREHOLES IN FEET

APPROXIMATE LATERAL
EXTENT OF ASH PIT BASED
ON TDEM ANOMALY MAP (FIG. 2 11)

ALLUVIAL
MATERIAL

CLAYSTONE &
SILTSTONE
BEDROCK

WASTE FILL

Dr. NAM 9/29/95
Checked by FEP 10/1/95
Approved by MDA 10/10/95
File 5 3 31

CROSS SECTION A-A
IHSS 133

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

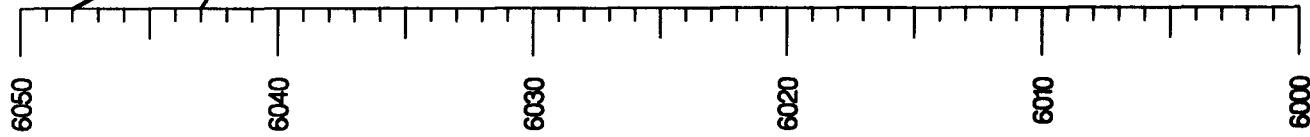
RPT/RI REPORT

FIGURE 3-27

SOURCE DATA LOGIT LOGS

B

ELEVATION
FEET MSL



ALLUVIAL
MATERIAL

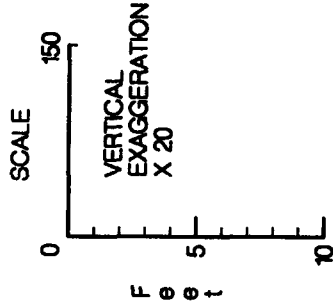
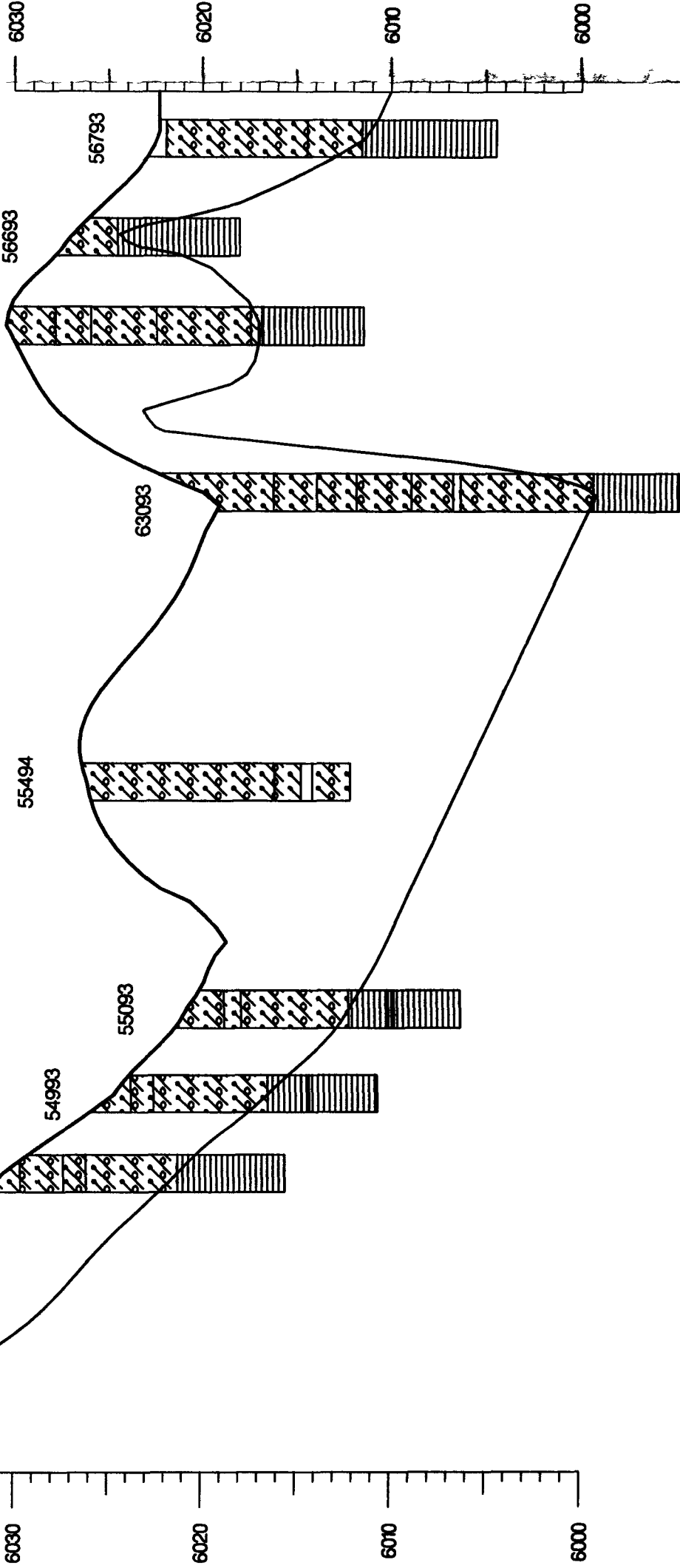
CLAYSTONE &
SILTSTONE
BEDROCK



IHSS 1333

B'

ELEVATION
FEET MSL



NOTES:
BEDROCK SURFACE WAS
INTERPRETED FROM BEDROCK
ELEVATION MAP FIGURE 3 5.
SEE FIGURE 3 26
FOR CROSS SECTION LOCATION

Drawn	VA M	9/29/95
Checked	7-1	9/11/95
App'd	MWW	10/18/95
File		5 3 33

CROSS SECTION B-B IHSS 133
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUR-WOMAN CREEK PRIORITY DRAINAGE
RPT/RI REPORT
FIGURE 3-28

DISTANCE BETWEEN BOREHOLES IN FEET



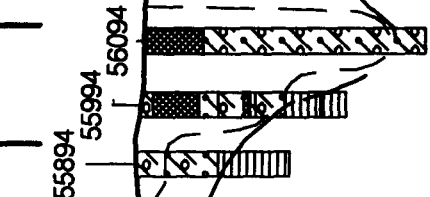
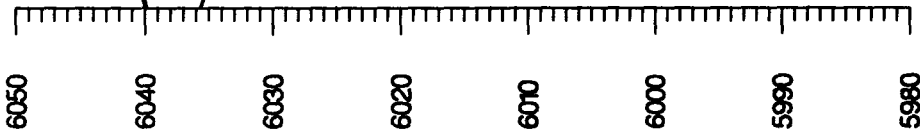
136797

SOURCE OF DATA LOGIT LOGS

C

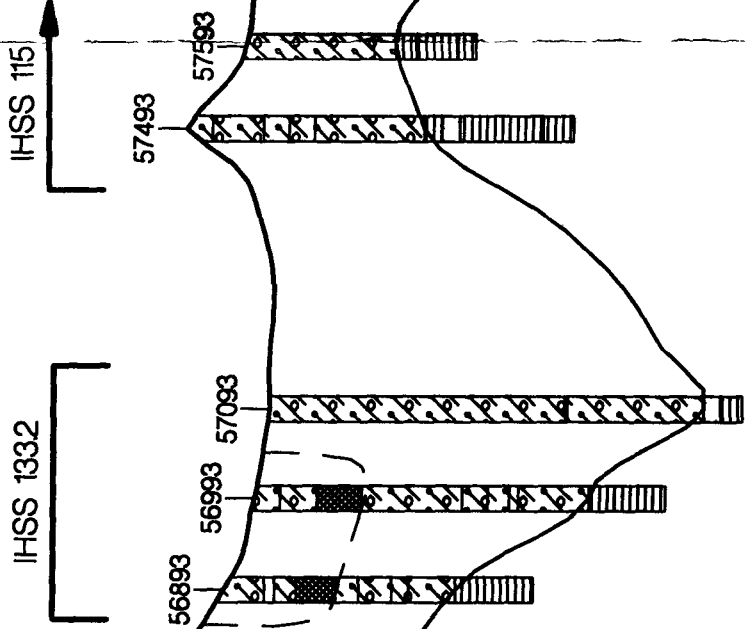
ELEVATION
FEET MSL

(ITEM 2)

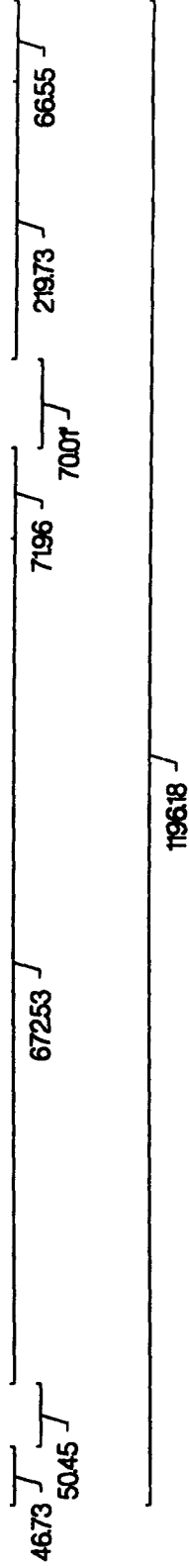


C'

ELEVATION
FEET MSL



DISTANCE BETWEEN BOREHOLES IN FEET



NOTES:
BEDROCK SURFACE WAS
INTERPRETED FROM BEDROCK
ELEVATION MAP FIGURE 3.5.
SEE FIGURE 3.26
FOR CROSS SECTION LOCATION

APPROXIMATE LATERAL
EXTENT OF ASH PIT BASED
ON THEM ANALYSIS MAP (FIG. 2.11)

ALLUVIAL
MATERIAL

CLAYSTONE &
SILTSTONE
BEDROCK

CLAYEY
SANDSTONE
BEDROCK

WASTE FILL

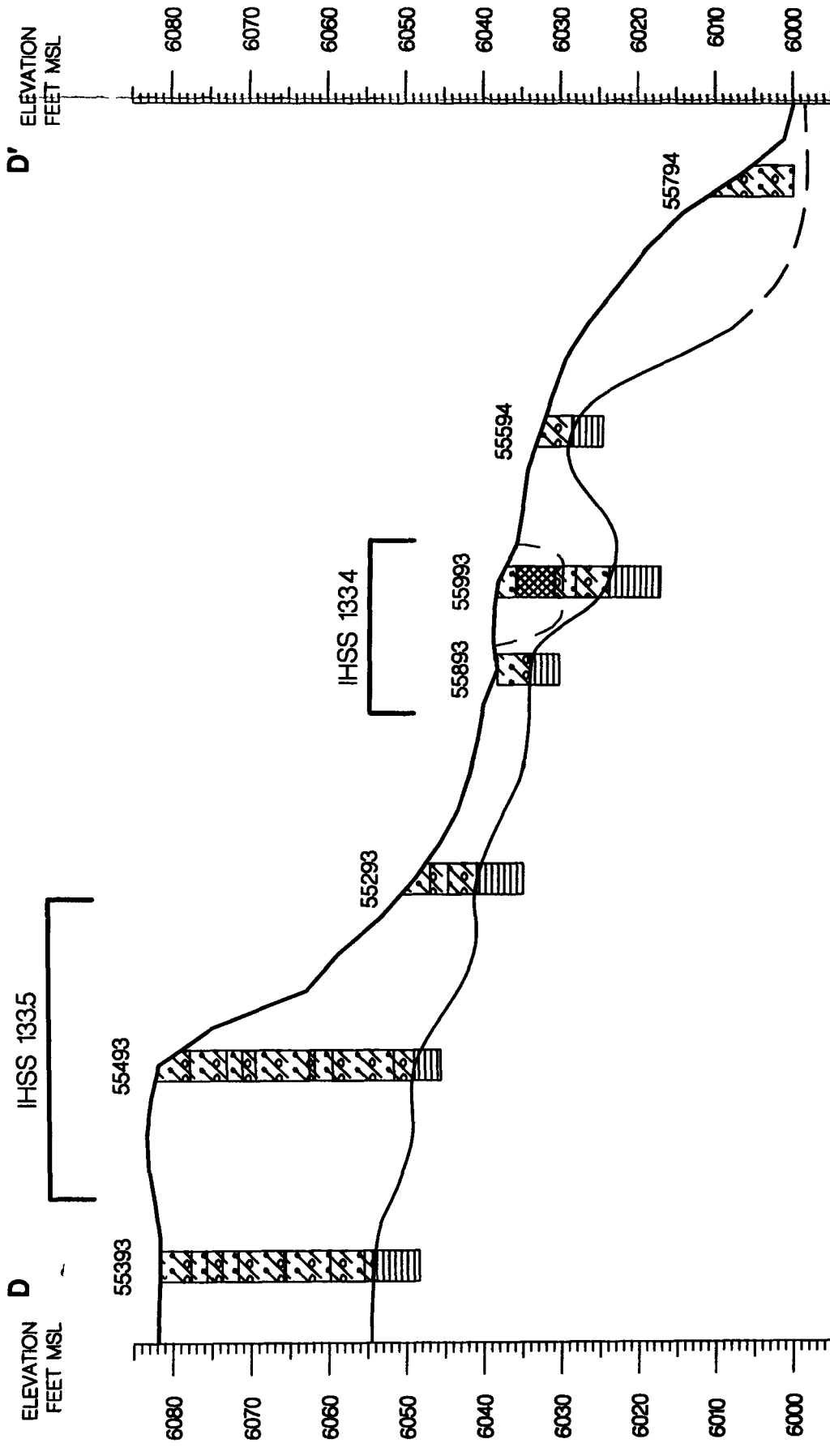
Drawn	NAM	Date	9/29/95
Checked	728	Date	6/95
Approved	new	Date	10/29/95
File	3.32		

CROSS SECTION C-C
IHSS 133

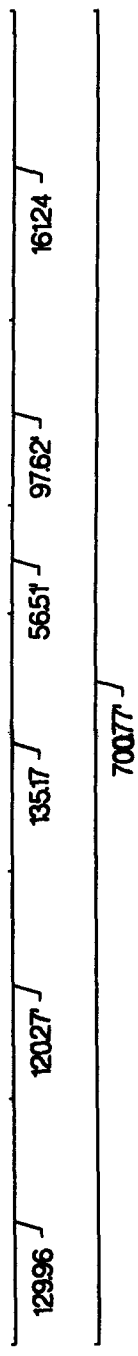
ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE
OUG-WOMAN CREEK PRIORITY DRAINAGE
RPT/RI REPORT

FIGURE 3-29

SOURCE: DATA LOGIT LOGS



DISTANCE BETWEEN BOREHOLES IN FEET



APPROXIMATE LATERAL
EXTENT OF ASH PIT BASED
ON TDEM ANOMALY MAP (FIG. 2.11)

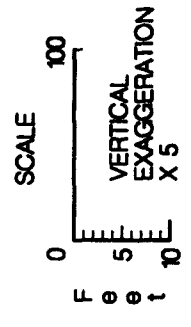


ALLUVIAL
MATERIAL

CLAYSTONE &
SILTSTONE
BEDROCK

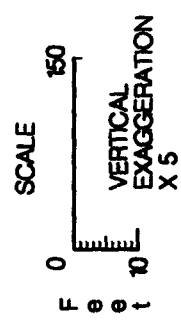
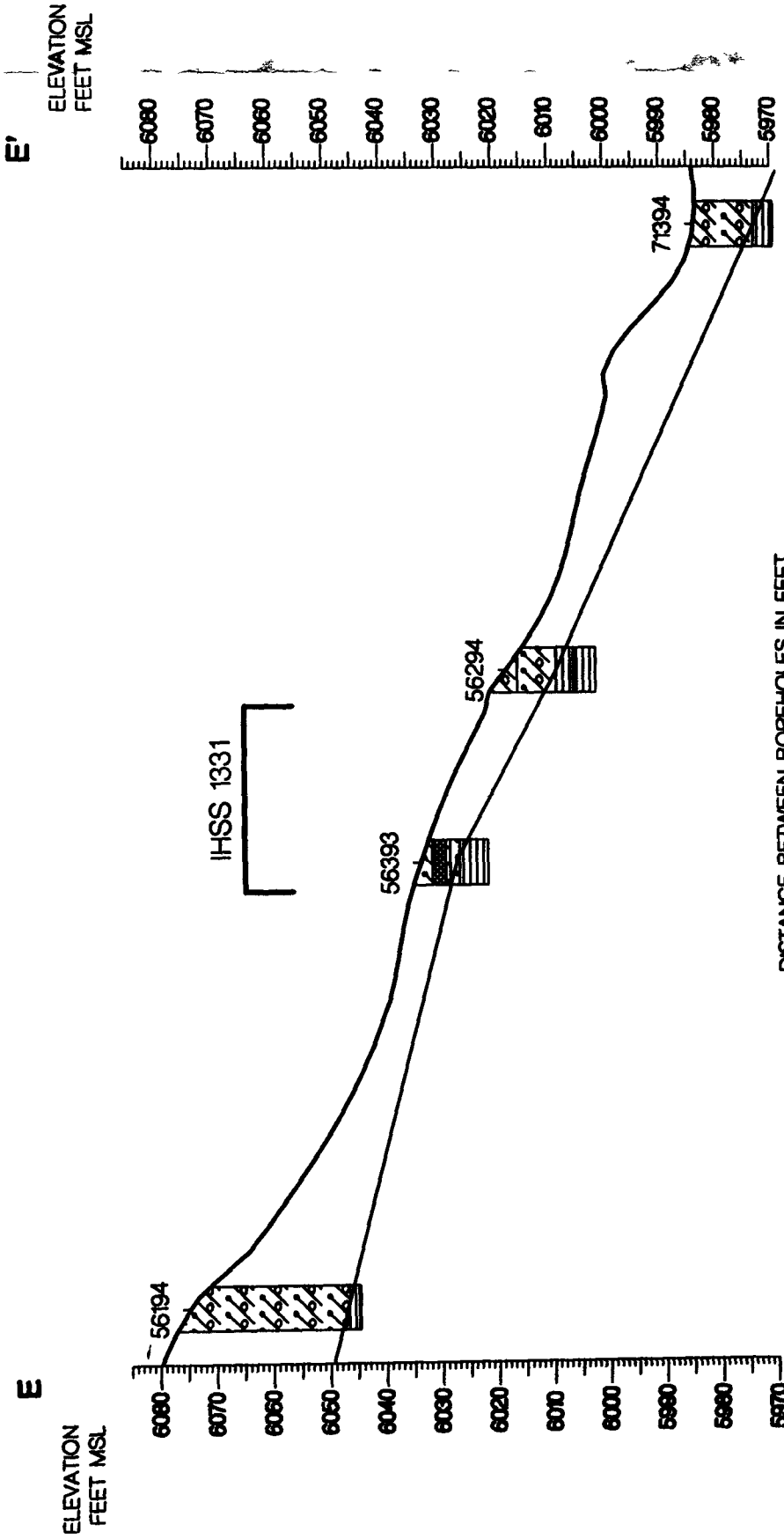
WASTE FILL

NOTES: BEDROCK SURFACE WAS
INTERPRETED FROM BEDROCK
ELEVATION MAP FIGURE 3.5.
SEE FIGURE 3.26
FOR CROSS SECTION LOCATION



Dr	NAM	9/29/95
Check d	727	10/1/95
Approved	MW	10/10/95
FA	5 3 27	
CROSS SECTION D-D IHSS 133		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
GUS-BOMAN CREEK PRIORITY DRAINAGE		
EFT/RI REPORT		
FIGURE 3-30		

SOURCE OF DATA: LOGIT LOGS



NOTES: BEDROCK SURFACE WAS
INTERPRETED FROM BEDROCK
ELEVATION MAP FIGURE 3.5.

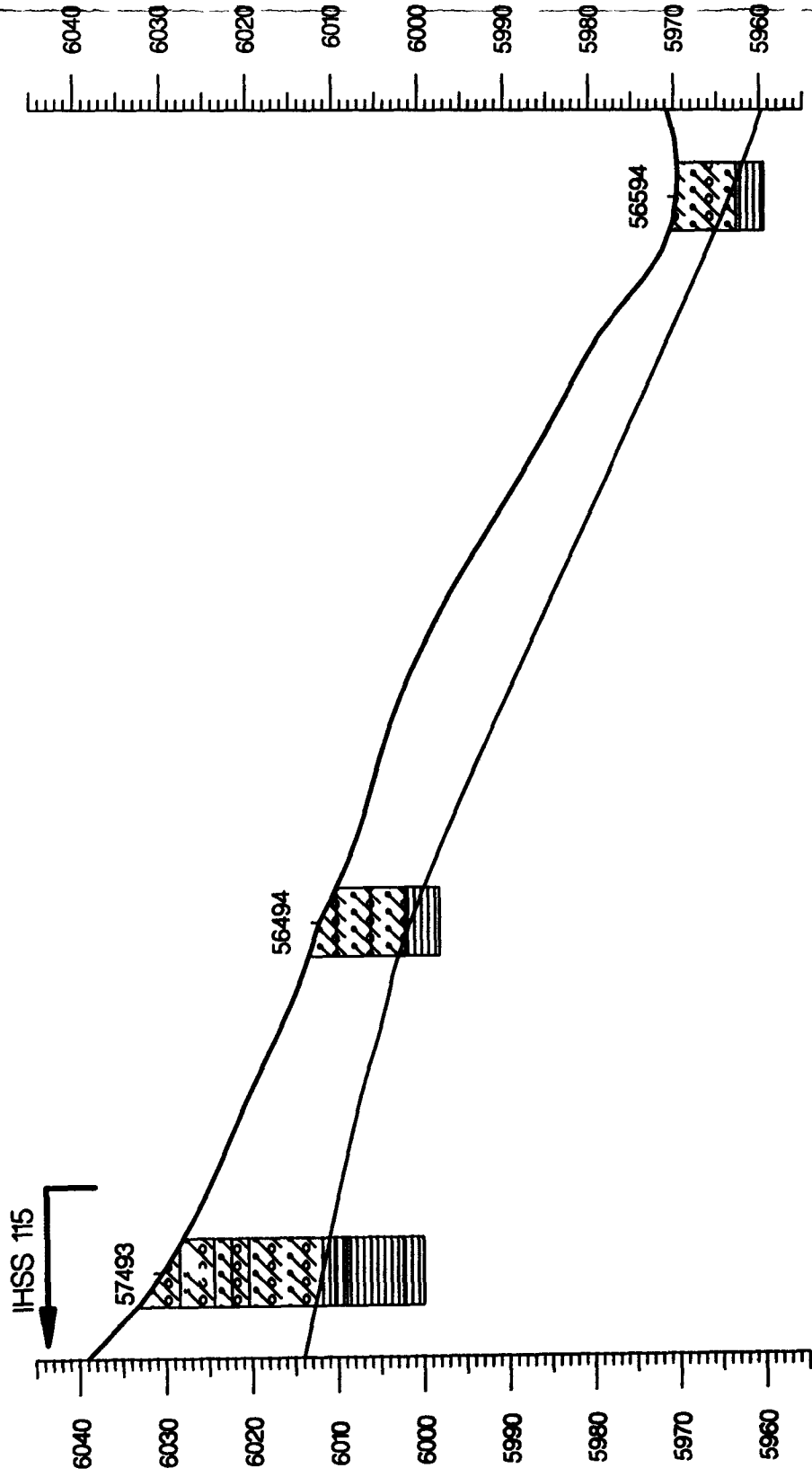
SEE FIGURE 3.26
FOR CROSS SECTION LOCATION

Drawing	NAM	9/29/95
Checked	727	10/1/95
Approved	MEN	10/3/95
File 5 3 28		
CROSS SECTION E-E IHSS 133		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUB-TOHAY CREEK PRIORITY REMEDIATION		
M/T/R REPORT		
FIGURE 3-31		

SOURCE: DATA LOGIT LOGS

F
ELEVATION
FEET MSL

F'
ELEVATION
FEET MSL



203.50'

42198'

62548'

DISTANCE BETWEEN BOREHOLES IN FEET

ALLUVIAL
MATERIAL

CLAYSTONE &
SILTSTONE
BEDROCK

SCALE
0 5 10
F e e t
VERTICAL
EXAGGERATION
X 5

NOTES:
BEDROCK SURFACE WAS
INTERPRETED FROM BEDROCK
ELEVATION MAP FIGURE 3.5.

SEE FIGURE 3.26
FOR CROSS SECTION LOCATION

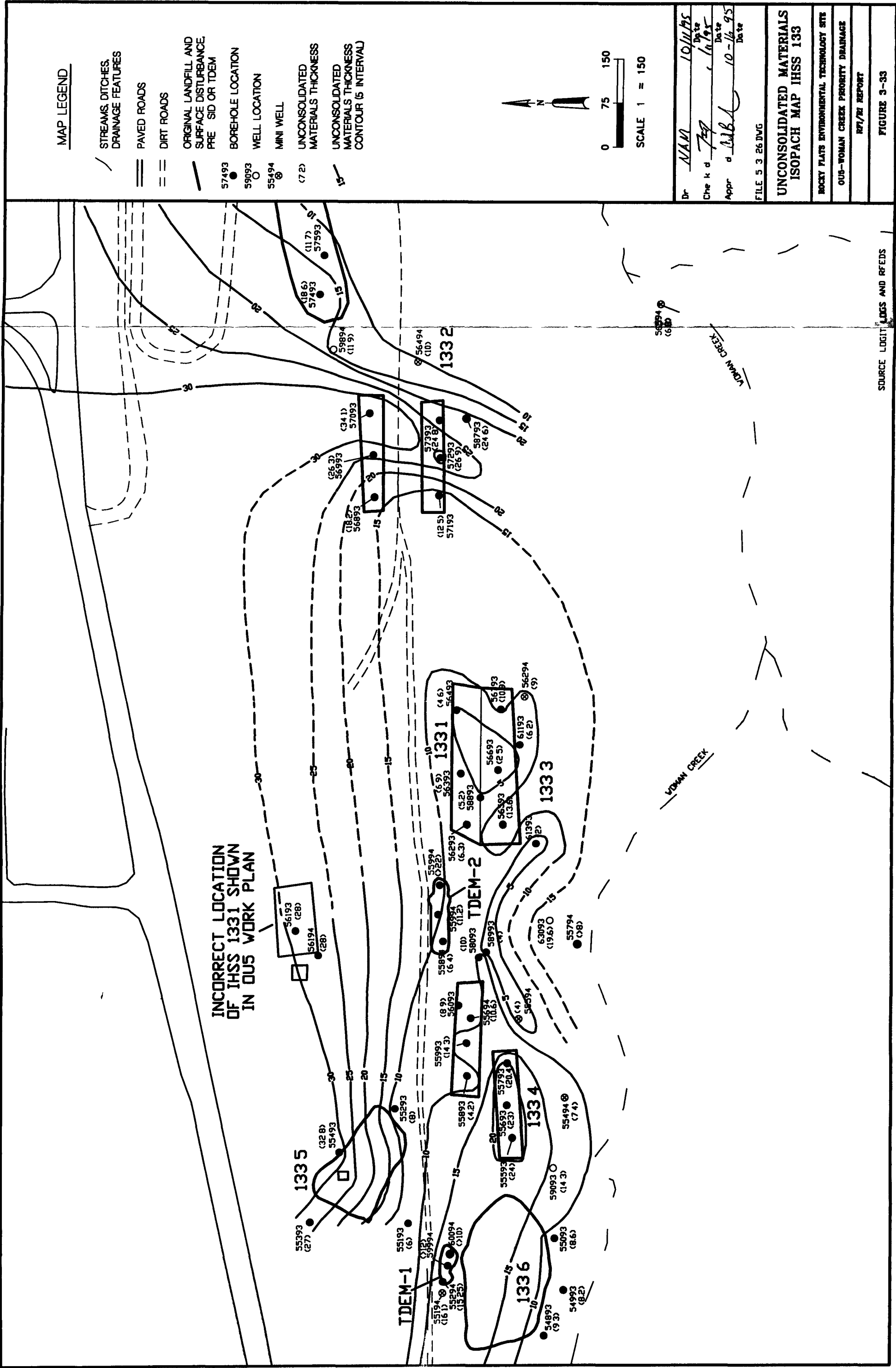
Drawn	NAM	9/29/95
Checked	729	10/1/95
Approved	MEL	10/1/95
File	S 3 29	

CROSS SECTION F-F'
IHSS 133

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE
OUG-WOMAN CREEK PROPERTY DRAINAGE
RPT/RS REPORT

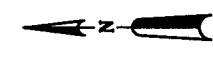
FIGURE 3-32

SOURCE: DATA LOGIT LOGS



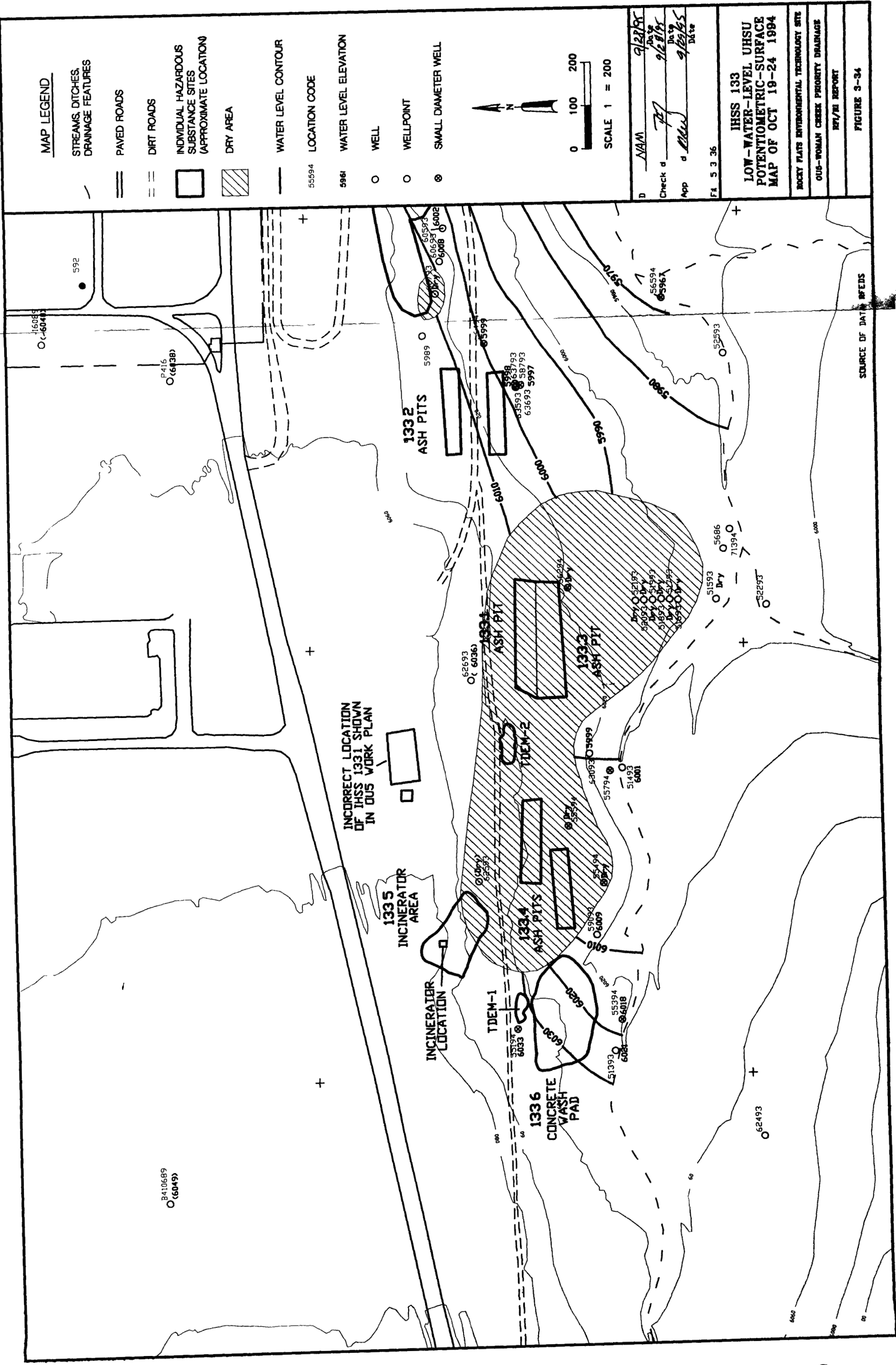
MAP LEGEND

- STREAMS, DITCHES, DRAINAGE FEATURES
- PAVED ROADS
- DIRT ROADS
- ORIGINAL LANDFILL AND SURFACE DISTURBANCE, PRE SD OR TDEM
- BOREHOLE LOCATION
- WELL LOCATION
- MINI WELL
- UNCONSOLIDATED MATERIALS THICKNESS
- UNCONSOLIDATED MATERIALS THICKNESS CONTOUR (5 INTERVAL)



0 75 150
SCALE 1" = 150'

Dr	NAM	10/11/95
Chk'd	7/9	10/11/95
Appr'd	11/11/95	10-11-95
FILE	5 3 26 DWG	
UNCONSOLIDATED MATERIALS ISOPACH MAP IHSS 133		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUG-WOMAN CREEK PROPERTY DRAINAGE		
R77/R2 REPORT		
FIGURE 3-33		



MAP LEGEND

- STREAMS, DITCHES, DRAINAGE FEATURES
- PAVED ROADS
- DIRT ROADS
- INDIVIDUAL HAZARDOUS SUBSTANCE SITES (APPROXIMATE LOCATION)
- DRY AREA

WATER LEVEL CONTOUR

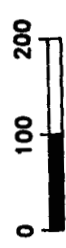
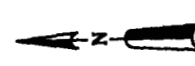
LOCATION CODE

WATER LEVEL ELEVATION

WELL

WELLPOINT

SMALL DIAMETER WELL



SCALE 1 = 200

D	NAM	9/22/95
Check d	7/7	9/28/95
App d	9/28/95	9/28/95
Date		

F4 5 3 36

IHSS 133
LOW-WATER-LEVEL UHSU
POTENTIOMETRIC-SURFACE
MAP OF OCT 19-24 1994

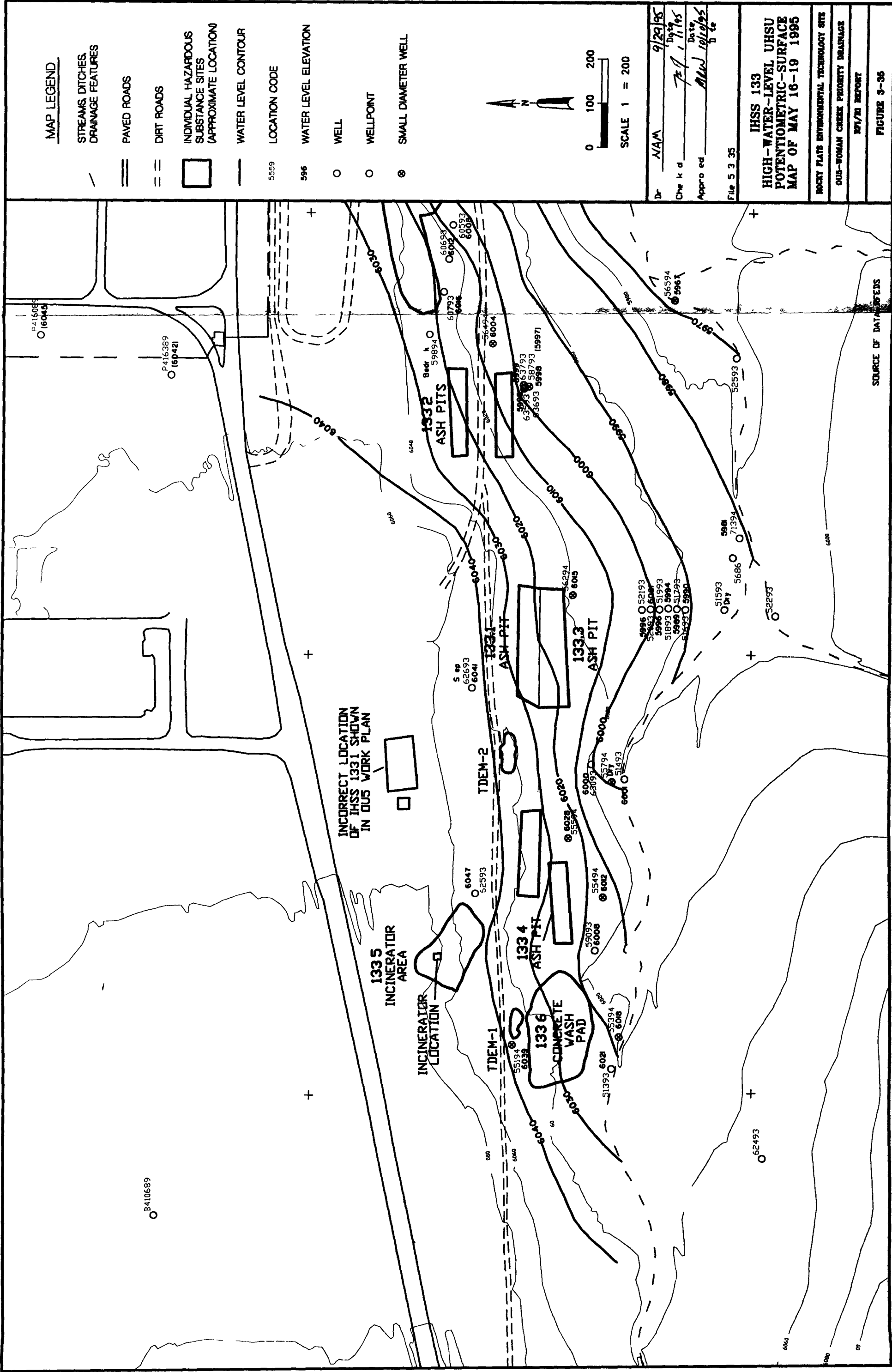
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

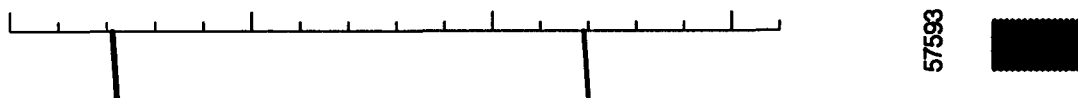
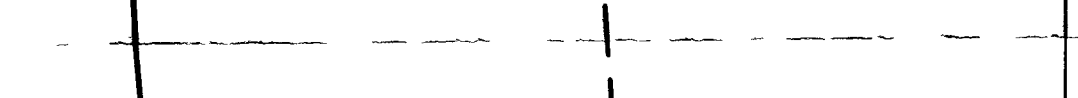
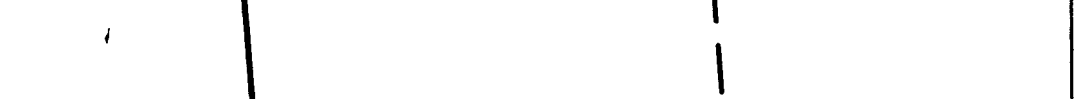
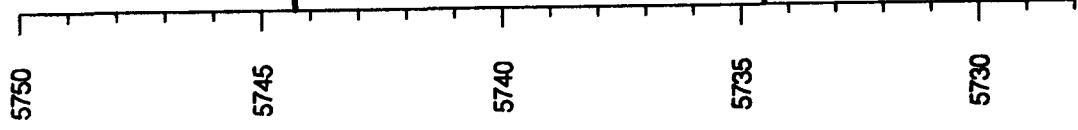
FIGURE 3-34

SOURCE OF DATA: RFEDS



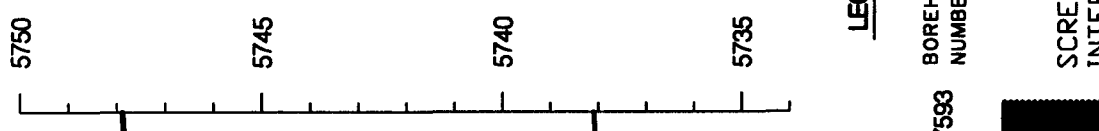
A

ELEVATION
FEET MSL



A'

ELEVATION
FEET MSL



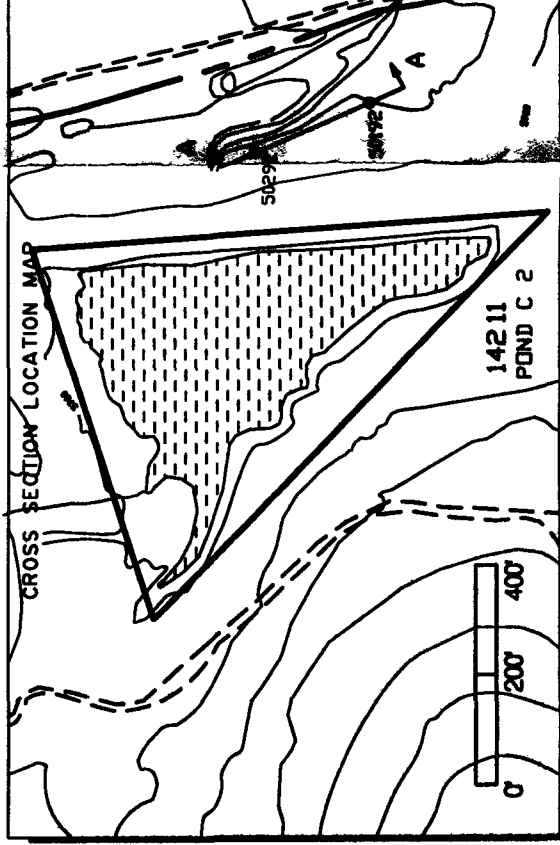
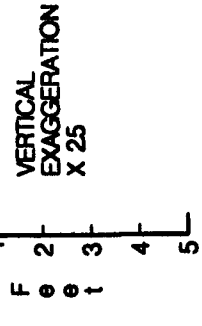
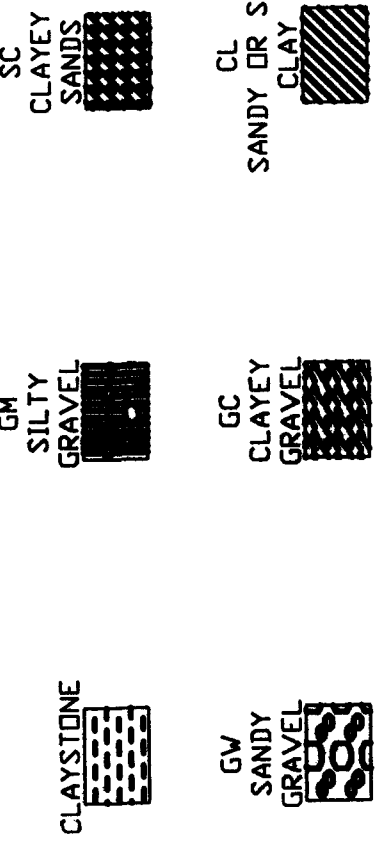
LEGEND

BOREHOLE IDENTIFICATION
NUMBER

57593

SCREENED
INTERVAL

SCALE



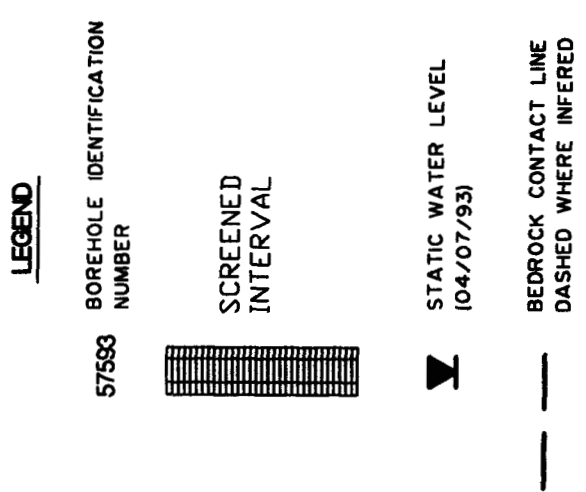
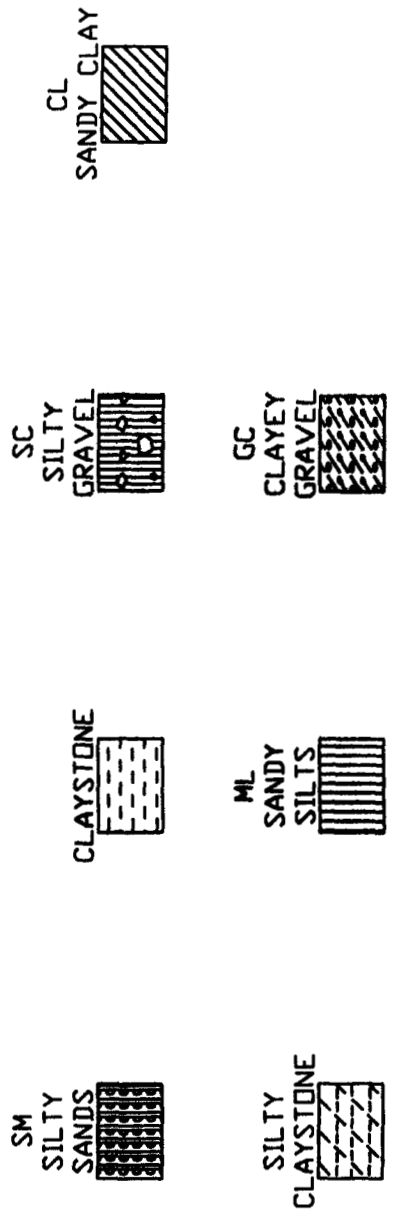
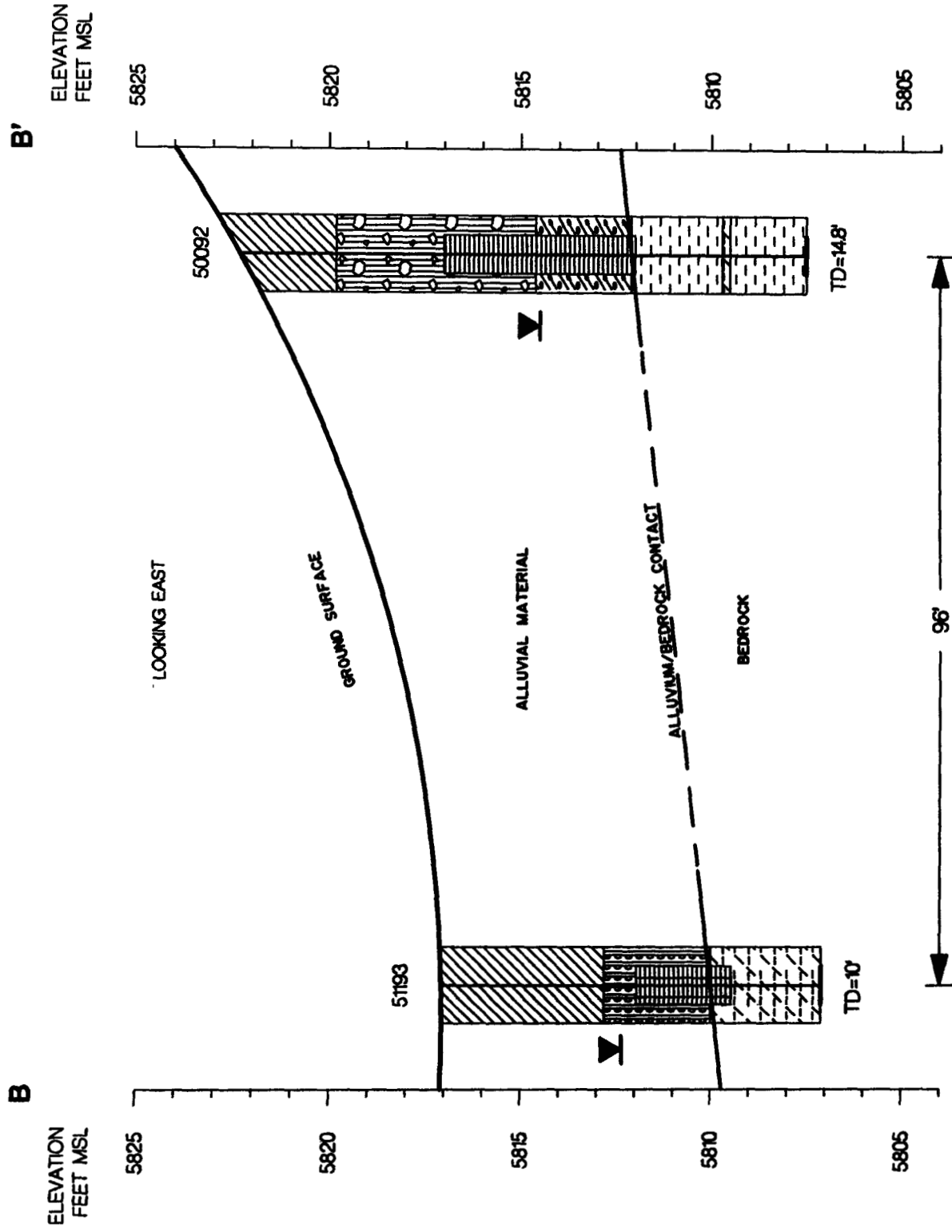
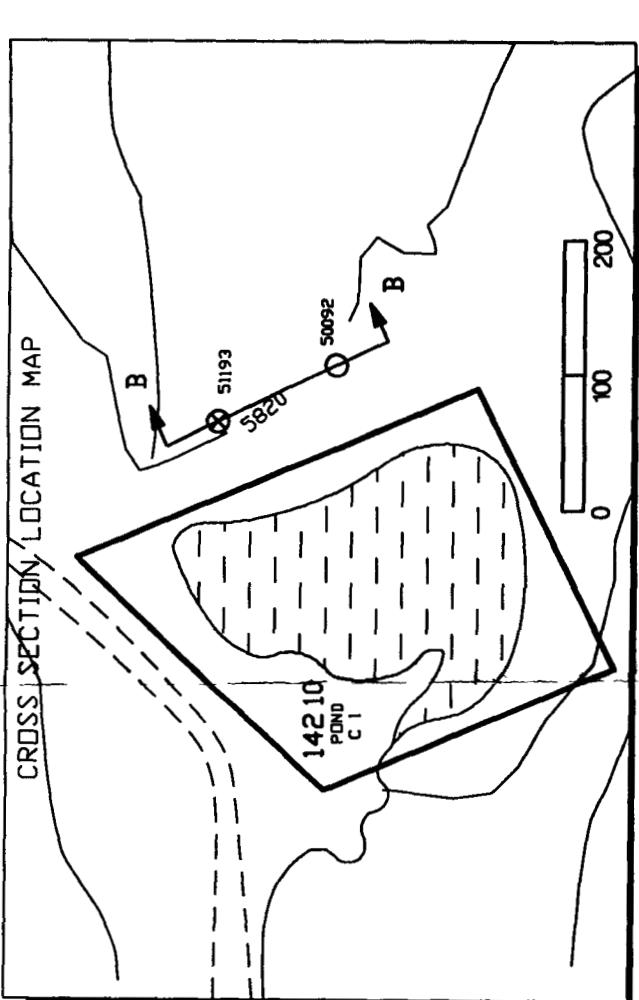
FILE OUS 3 37 DVG

GENERALIZED GEOLOGIC
CROSS SECTION A-A
IHSS 142

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS - WOMAN CREEK PRIORITY DRAINAGE
RT/RI REPORT
FIGURE 3-37

NOTE No water levels are on record for these wells

SOURCE OF DATA LOGIT LOGS AND RFEDS



Drawn by NAM 9/28/95
Checked by FEJ 9/29/95
Approved by MEW 9/29/95

FILE DUS 3 38.DWG

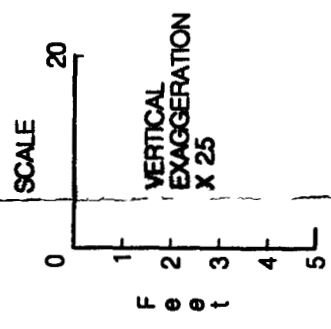
**GENERALIZED GEOLOGIC
CROSS SECTION B-B
IHSS 142**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

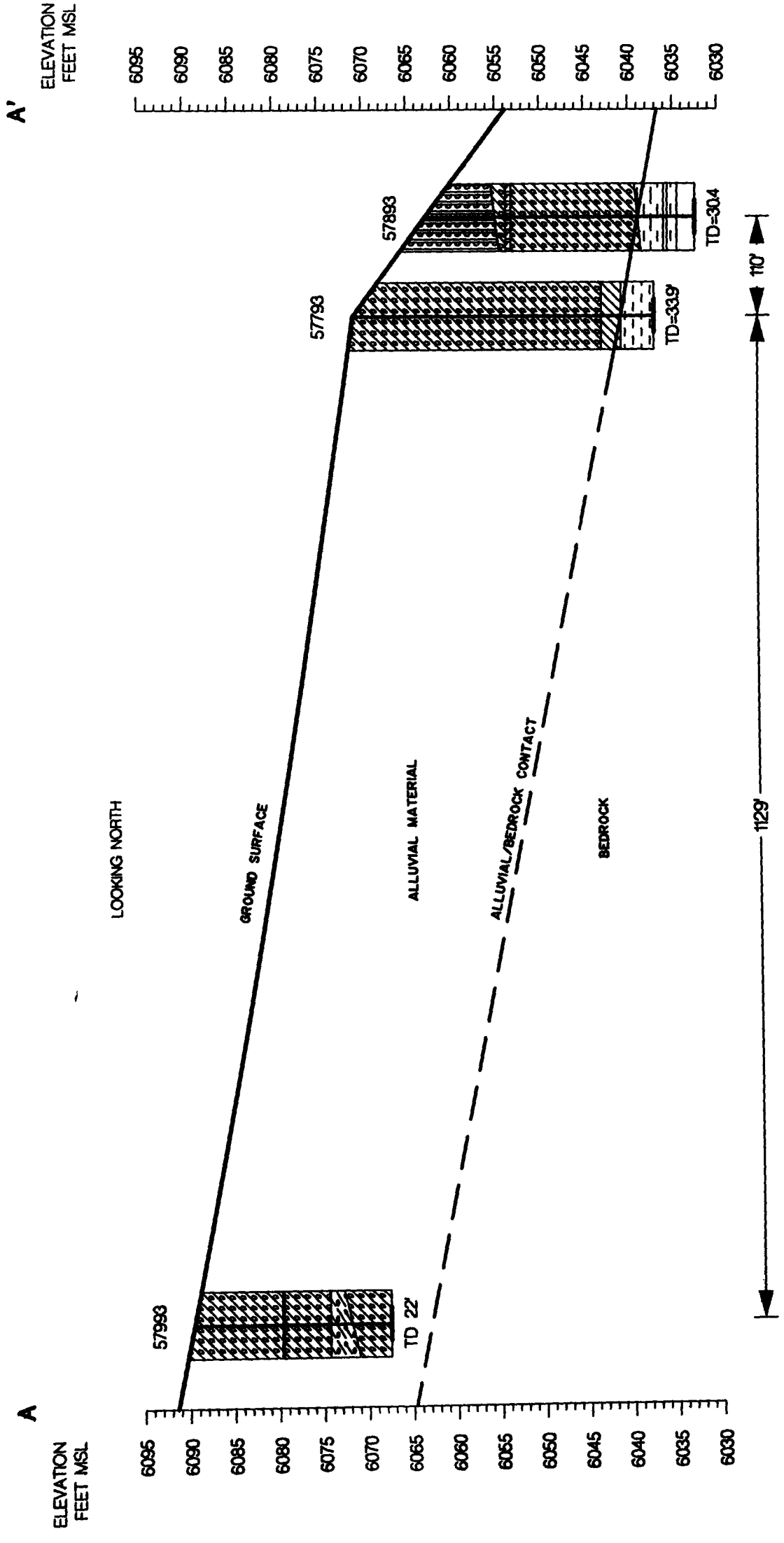
OUS WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 3-36

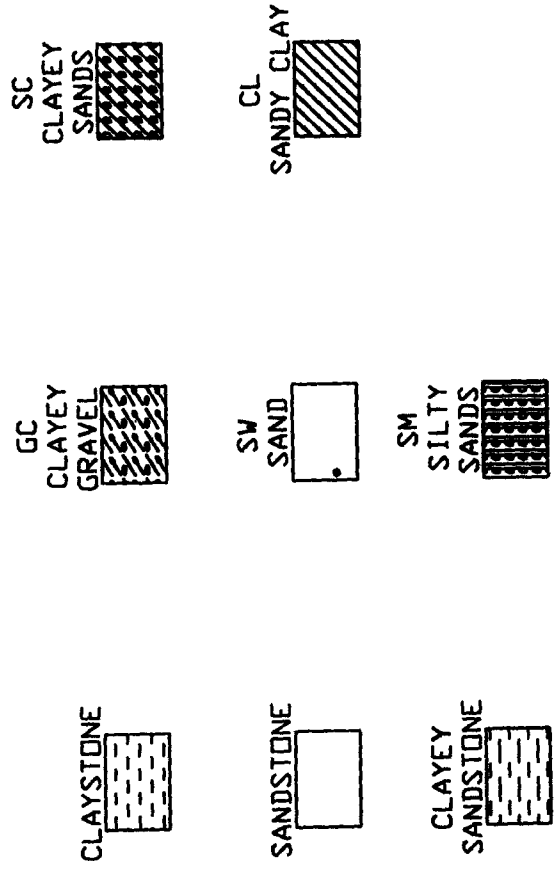
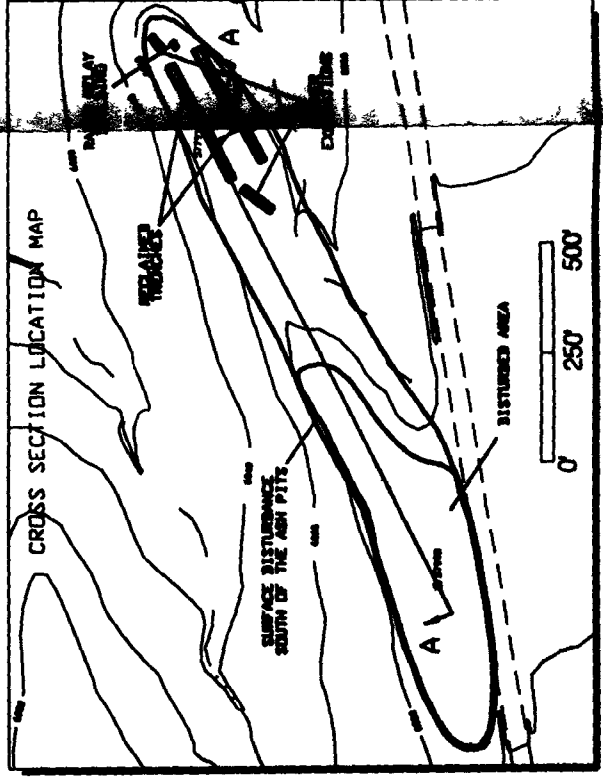
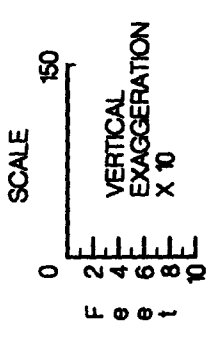


SOURCE OF DATA: LOGIT LOGS APPENDIX B AND RFDS



LEGEND

- BOREHOLE IDENTIFICATION NUMBER
- 57593
- BEDROCK CONTACT LINE
- DASHED WHERE INFERRED
- NOTE NO GROUNDWATER WAS ENCOUNTERED DURING DRILLING OF THESE BOREHOLES



Drawn NAM 9/28/95

Checked 7/17 9/28/95

Approved M26 9/29/95

Date Date Date

FILE DUS 3 39 DVG

GENERALIZED GEOLOGIC CROSS SECTION A-A

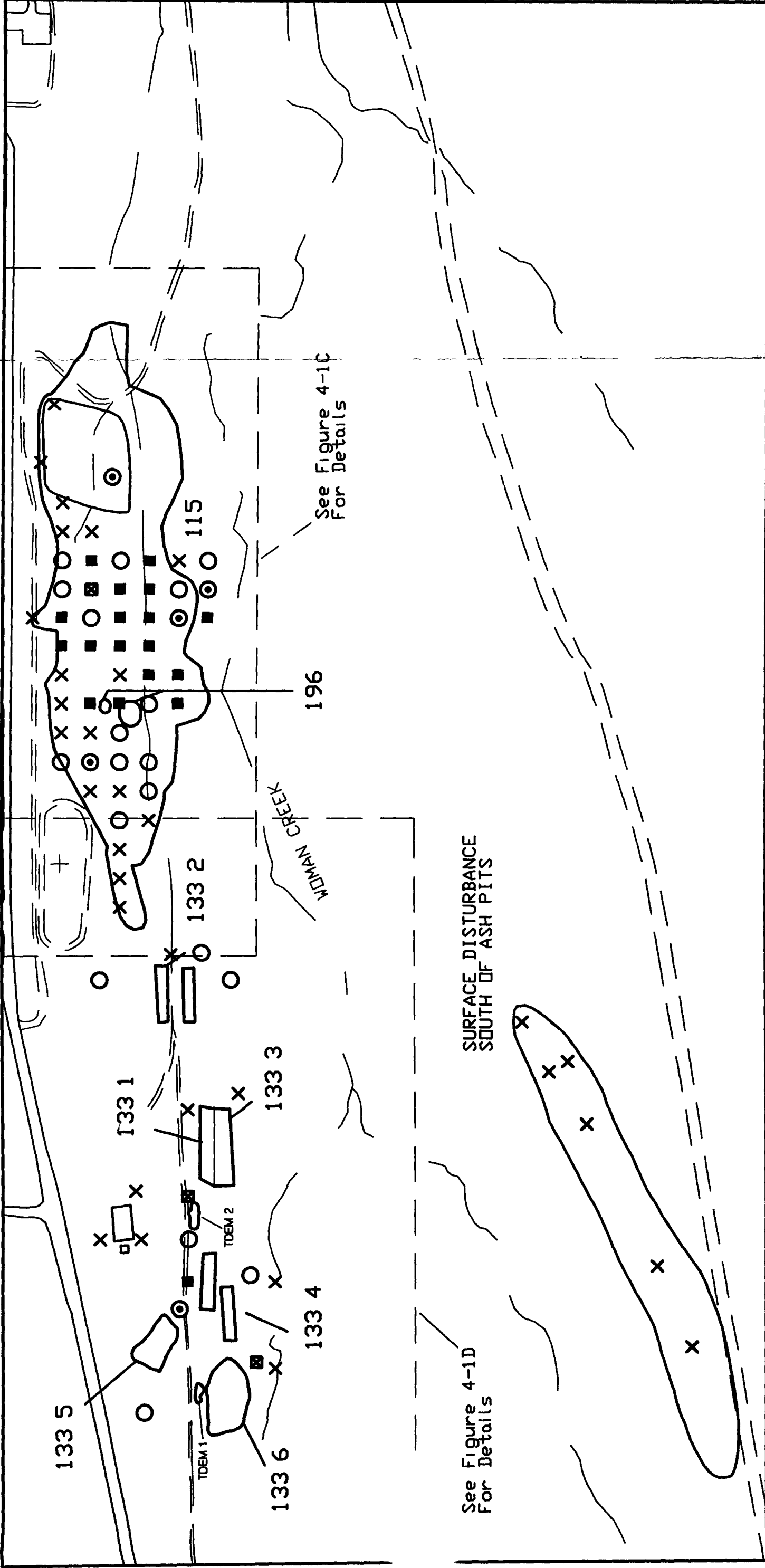
SURFACE DISTURBANCE SOUTH OF THE ASH PITS

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

DUS - WOMAN CREEK PRIORITY DRAINAGE

RPI/RI REPORT

FIGURE 3-39



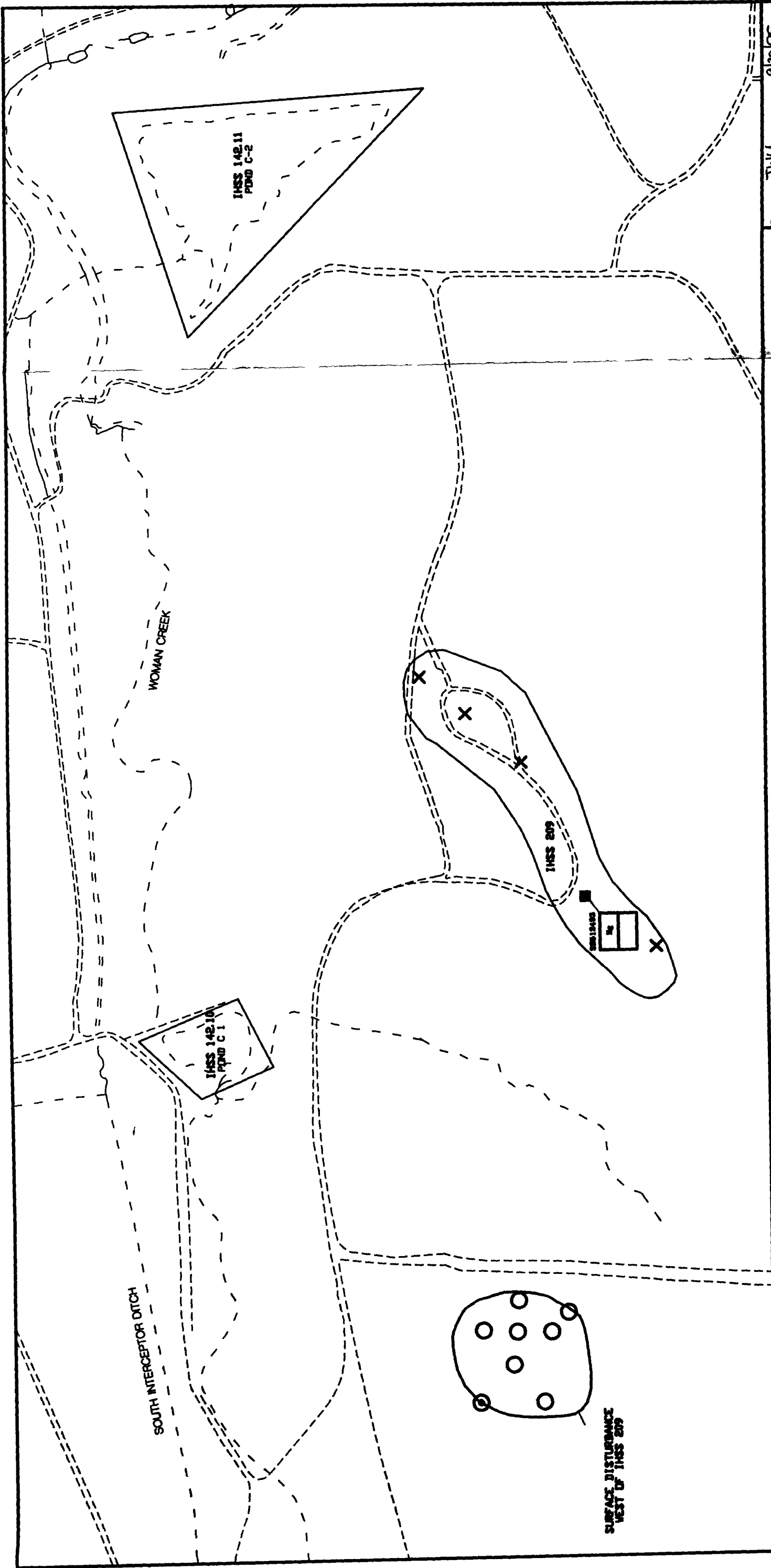
Dr	JWH	9/30/95
Check d	728	10/2/95
Appro d	new	10/10/95
FILE DUS 4 1A.DWG		
EXTENT OF METAL COCs IN SURFACE SOIL		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUS-WOMAN CREEK PROPERTY DRAINAGE		
RFT/RI REPORT		
FIGURE 4-1A		

MAP LEGEND

- STREAMS, DITCHES, DRAINAGE FEATURES
- PAVED ROADS
- DIRT ROADS
- HSS BOUNDARY
- X < Background Mean (BM)
- > BM and <= BM 1 STD DEV
- ⊗ > BM 1 STD DEV and <= BM 2 STD DEV
- ⊠ > BM 2 STD DEV and <= BM 3 STD DEV
- > BM 3 STD DEV

0 175 350

SCALE 1" = 350'



Dr. m. JKH 9/30/95
Checked: JKH 1/12/95
Approved: MHW 10/1/95

FILE DJS 4 1B.DWG

EXTENT OF METAL COCs
IN SURFACE SOIL
IHSS 142/209

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUB-WOMAN CREEK PRIORITY DRAINAGE

MT/MI REPORT

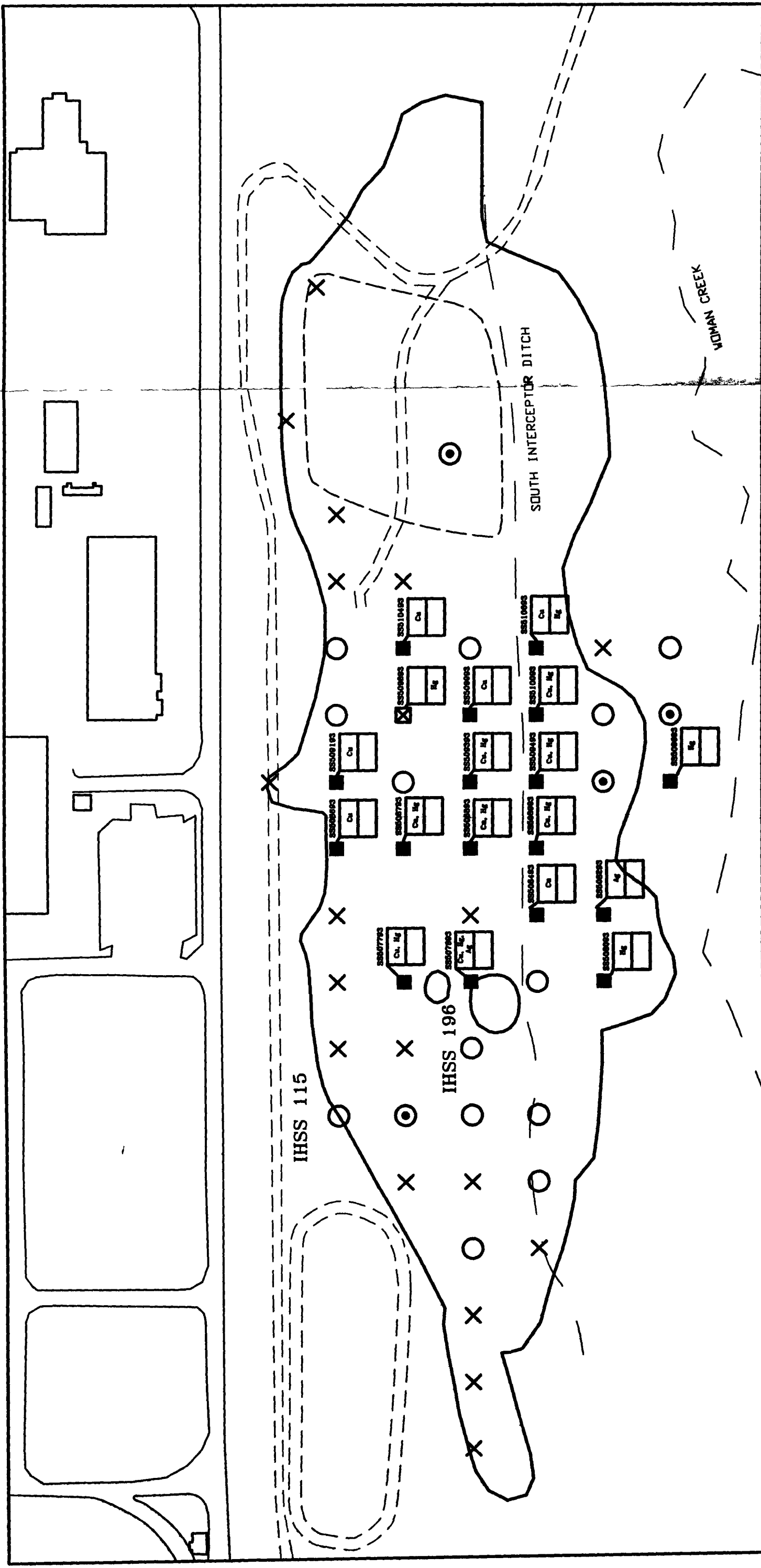
FIGURE 4-1B

MAP LEGEND

- STREAMS, DITCHES,
DRAINAGE FEATURES
- PAVED ROADS
- DIRT ROADS
- IHSS BOUNDARY
- X <- Background Mean (BM)
- O > BM and <= BM 1 STD DEV
- ⊙ > BM 1 STD DEV and <= BM 2 STD DEV
- > BM 2 STD DEV and <= BM 3 STD DEV
- > BM 3 STD DEV

BACKGROUND DATA			
SYMBOL	CONSTITUENT	MEAN(mg/kg)	STD. DEV
Cu	Copper	13.41	4.22
Hg	Mercury	0.08	0.03
Ag	Silver	2.80	2.04

LOCATION	
CONSTITUENTS	> BM+3 STD DEV
CONSTITUENTS	> BM+2 STD DEV
CONSTITUENTS	> BM+1 STD DEV
CONSTITUENTS	> BM+0 STD DEV



Dr. JWH 9/30/95

Checked Date 7/9 10/2/95

Approved Date MJD 1/10/95

FILE DJS 41C DNG

EXTENT OF METAL COCs
IN SURFACE SOIL
IHSS 115/196

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

FIGURE 4-1C

MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

X < Background Mean (BM)

O > BM and < BM 1 STD DEV

⊙ > BM 1 STD DEV and < BM 2 STD DEV

■ > BM 2 STD DEV and < BM + 3 STD DEV

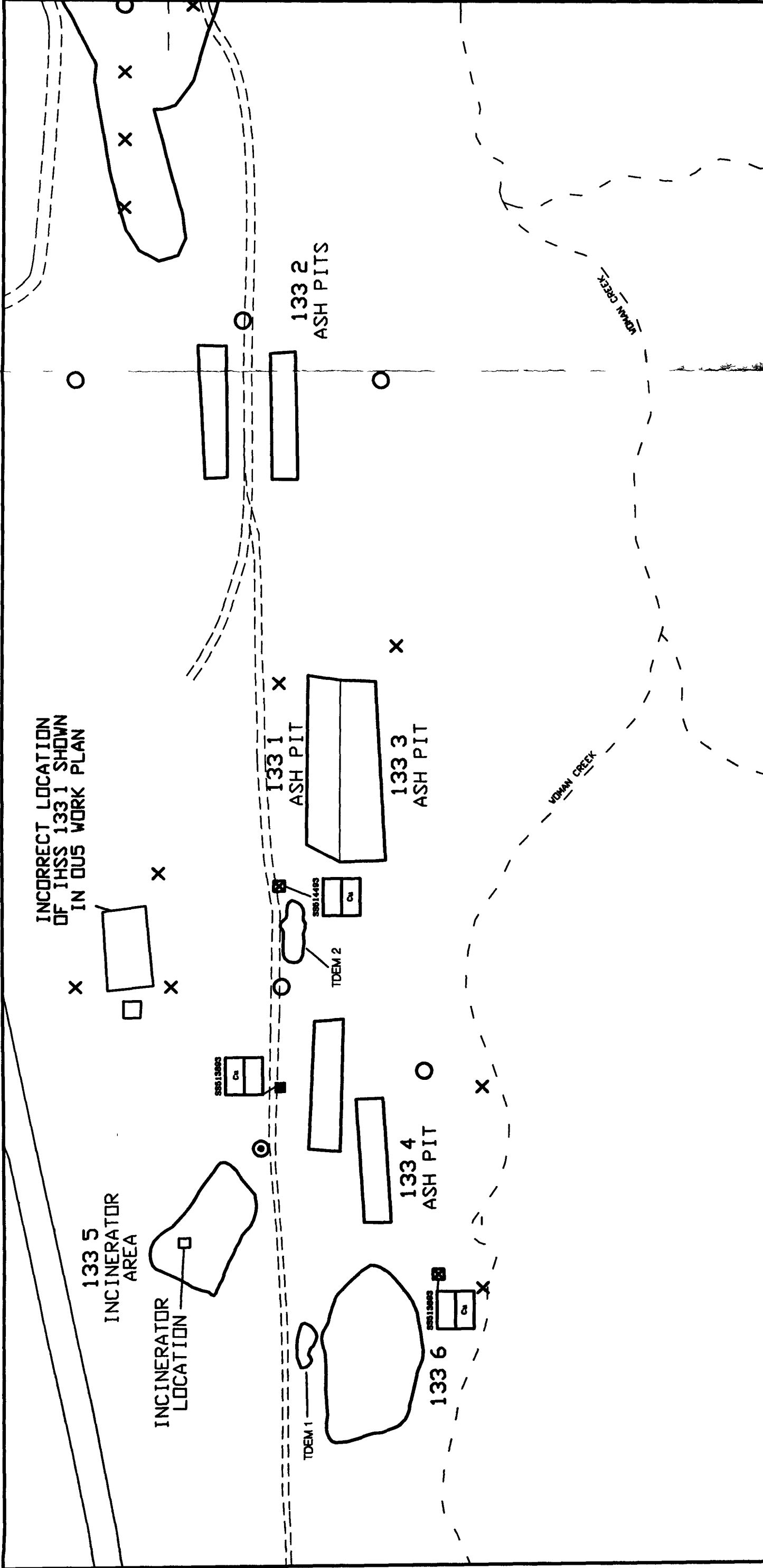
■ > BM 3 STD DEV

BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (mg/kg)	STD. DEV.
Cu	Copper	13.41	4.22
Hg	Mercury	0.08	0.03
Ag	Silver	2.80	2.04

LOCATION

CONSTITUENT	> BM + 3 STD DEV	> BM + 2 STD DEV	> BM + 1 STD DEV	AND	< BM - 1 STD DEV	< BM - 2 STD DEV	< BM - 3 STD DEV
Cu							
Hg							
Ag							



Drawn JWH 9/30/95

Che k d 727 10/16/95

Appr d Mew 10/16/95

FILE DUS 4 13.DWG

EXTENT OF METAL COCs
IN SURFACE SOIL
IHSS 133

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUR-WOMAN CREEK PRIORITY DRAINAGE

877/MI REPORT

FIGURE 4-1D

MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

INCINERATOR LOCATION

INCINERATOR AREA

INCORRECT LOCATION OF IHSS 133 1 SHOWN IN DUS WORK PLAN

133 5

133 6

133 4

133 3

133 2

133 1

ASH PIT

ASH PIT

ASH PIT

ASH PIT

ASH PIT

WOMAN CREEK

TDEM 1

TDEM 2

S8013963

S8014483

S8013962

INCINERATOR LOCATION

INCINERATOR AREA

INCORRECT LOCATION OF IHSS 133 1 SHOWN IN DUS WORK PLAN

BACKGROUND DATA

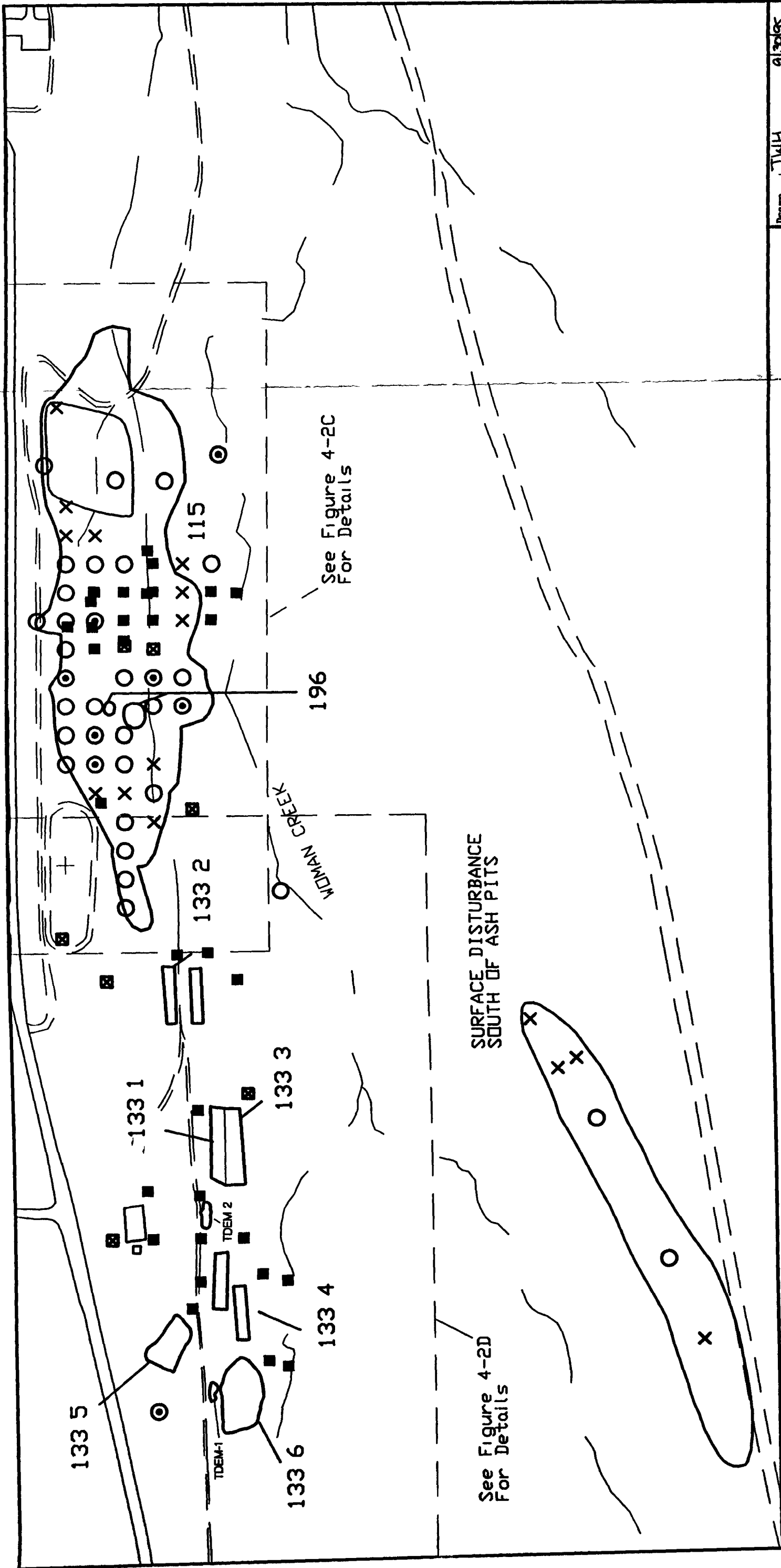
SYMBOL	CONSTITUENT	MEAN(MG/LG)	STD DEV
Cu	Copper	13.41	4.22
Hg	Mercury	0.08	0.03
Ag	Silver	2.80	2.04

LOCATION

CONSTITUENTS	MEAN(MG/LG)	STD DEV
> BM and < BM	1 STD DEV	
> BM	1 STD DEV and < BM	2 STD DEV
> BM	2 STD DEV and < BM	3 STD DEV
> BM	3 STD DEV	

SCALE 1" = 150'

0 75 150



Drawn JWH 9/30/95

Checked 727 10/2/95 Date

Approved MEW 10/10/95 Date

FILE OUS 4 2A.DWG

**EXTENT OF RADIONUCLIDE COCs
IN SURFACE SOIL**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

FIGURE 4-2A

MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

HSS BOUNDARY

X Background Mean (BM)

○ BM and
○ BM + 1 STD DEV

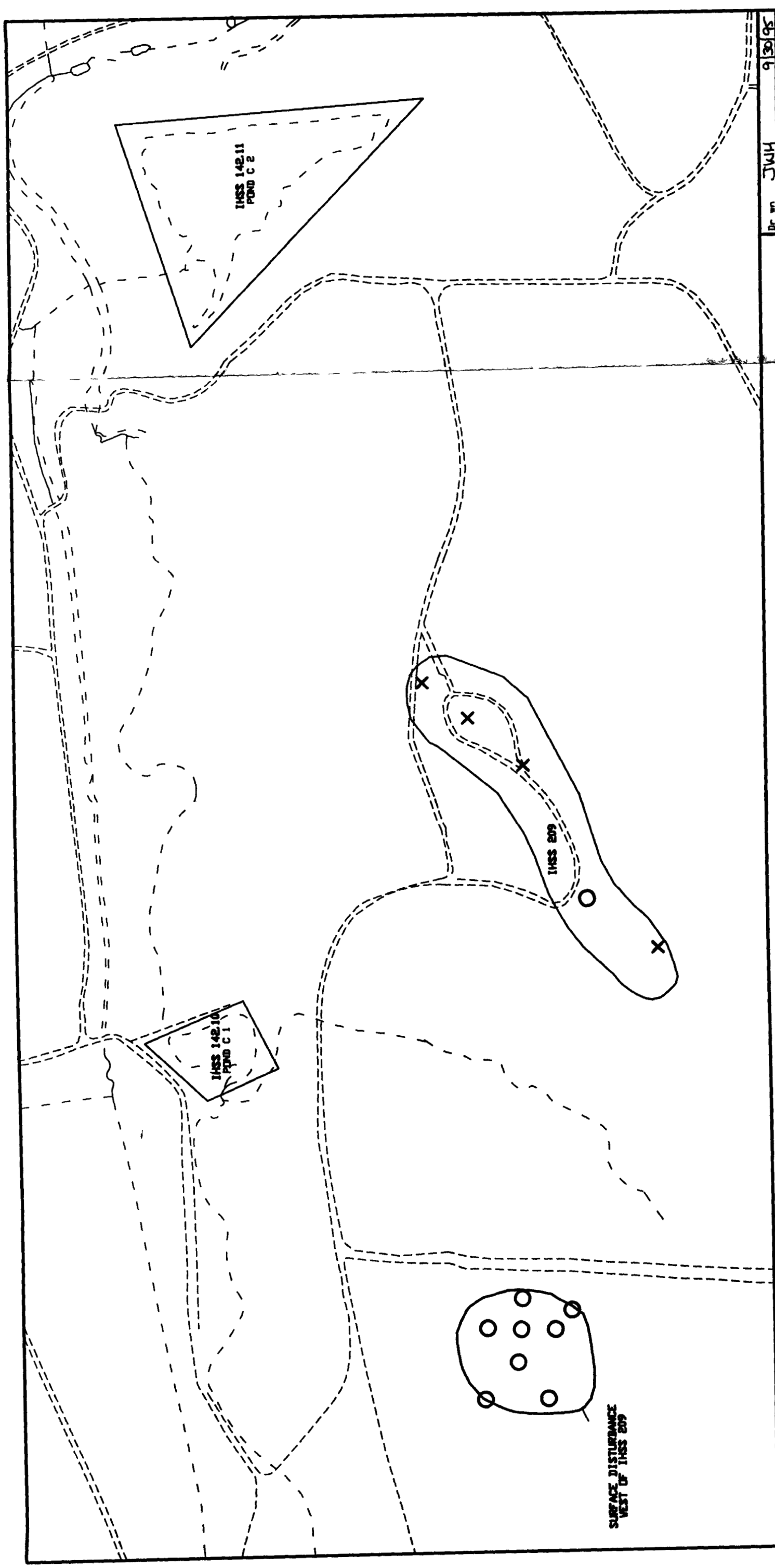
⊙ BM + 1 STD DEV and
⊙ BM + 2 STD DEV

■ BM + 2 STD DEV and
■ BM + 3 STD DEV

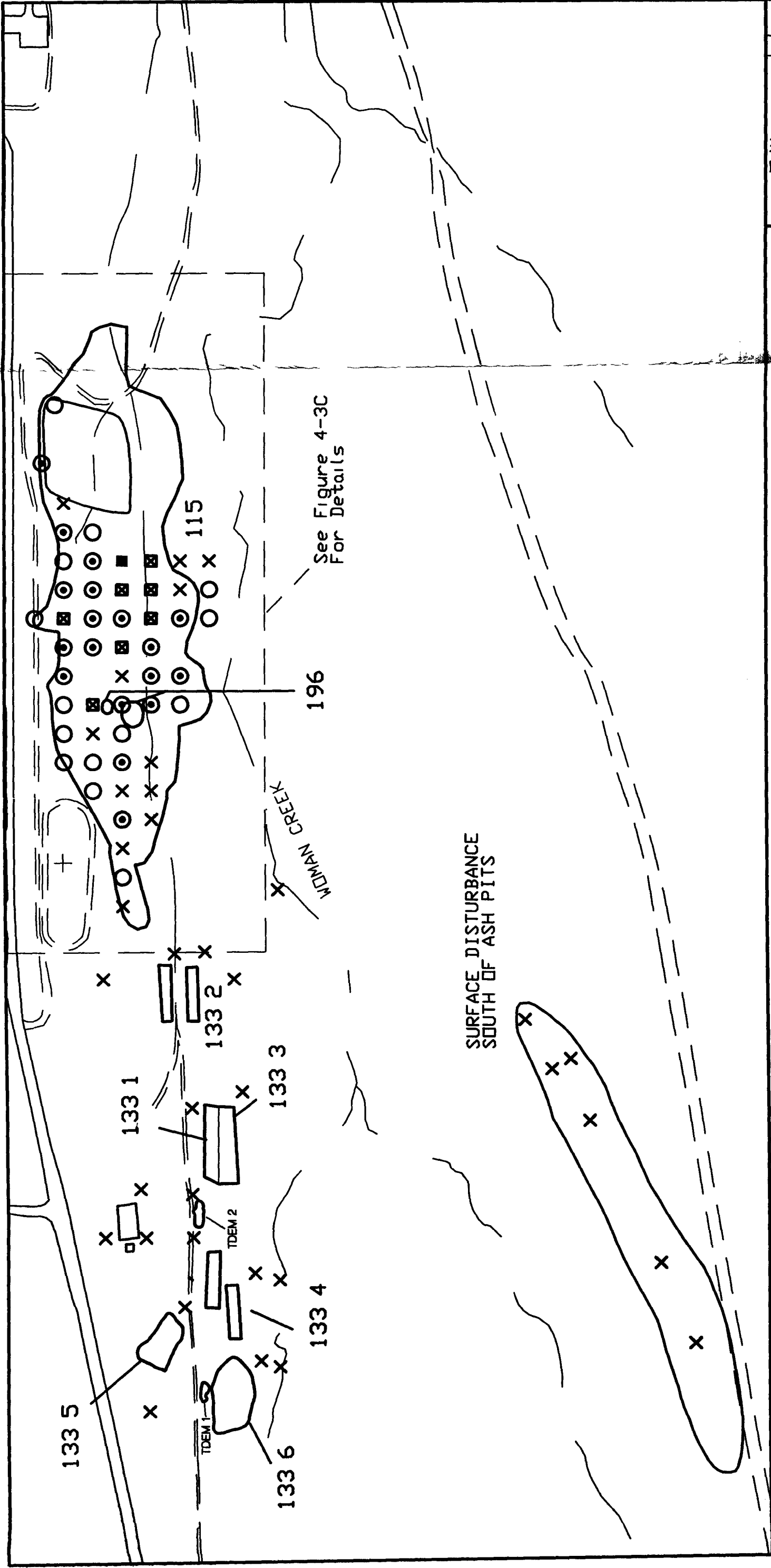
■ BM + 3 STD DEV

0 175 350

SCALE 1" = 350'



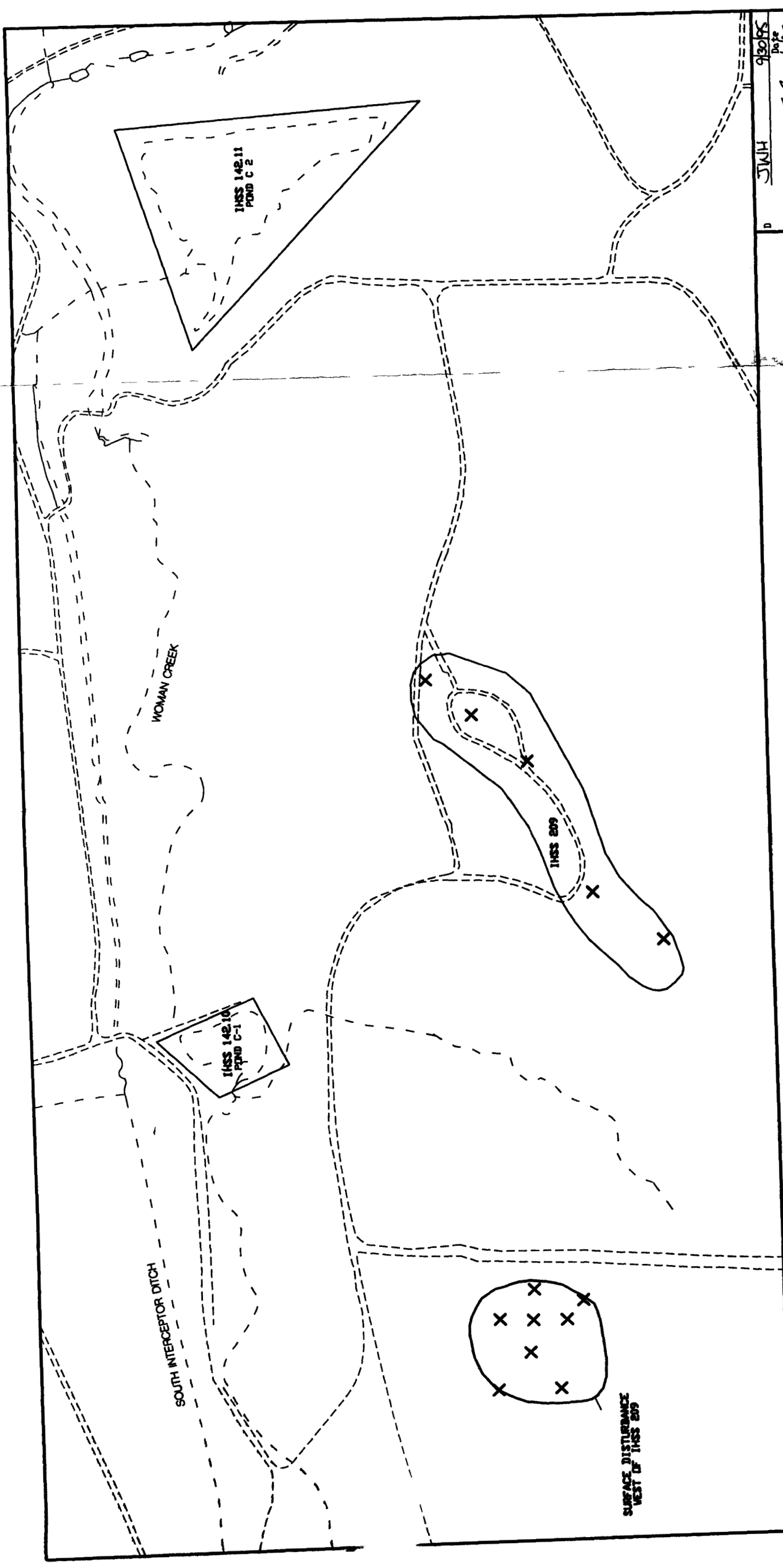
Dr wn	JWH	9/30/95
Checked	7/1	8/2/95
Appr d	M. W.	10/1/95
FILE QUS 4 2B.DWG		
EXTENT OF RADIONUCLIDE COCs IN SURFACE SOIL IHSS 142/209		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUG-POMAN CREEK PRIORITY DRAINAGE		
RPT/RP REPORT		
FIGURE 4-2B		



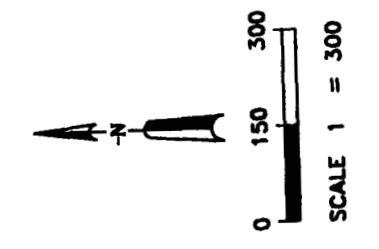
Dwg n	JWH	9/30/95	Date
Check d	7/9	10/2/95	Date
Appr d	MRS	11/1/95	Date
FILE DJS 4 3A DWG			
EXTENT OF ORGANIC COCs IN SURFACE SOIL			
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE			
OUS-WOMAN CREEK PRIORITY DRAINAGE			
RTI/RI REPORT			
FIGURE 4-3A			

MAP LEGEND

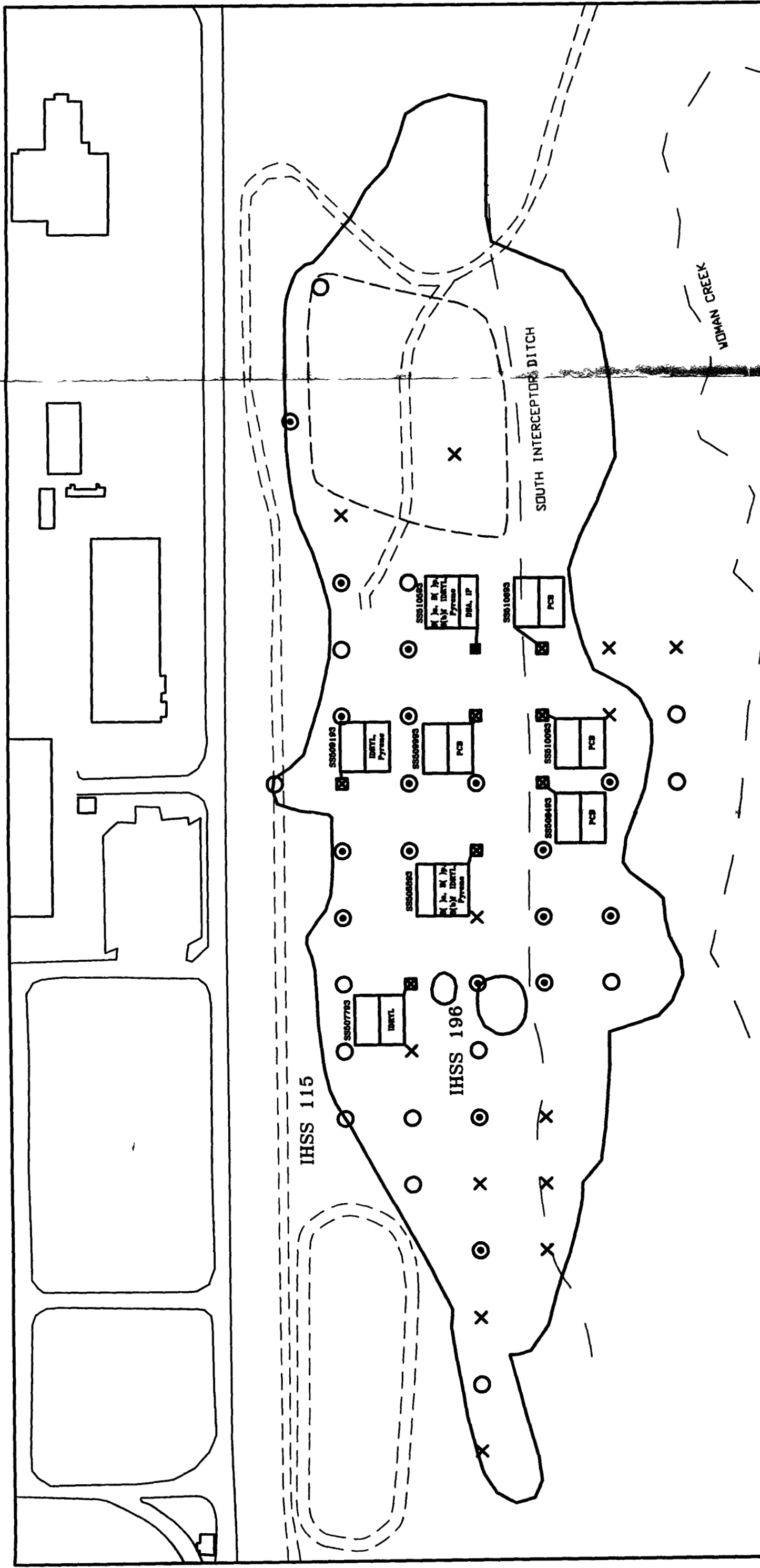
- | | | | |
|----|--|---|---|
| / | STREAMS, DITCHES,
DRAINAGE FEATURES | X | Sample Location |
| == | PAVED ROADS | O | Detectors less than the Reporting Limit (RL) |
| == | DIRT ROADS | ⊙ | Detectors exceeding RL
but less than 10 x RL |
| — | HSS BOUNDARY | ■ | Detectors exceeding 10 x RL
but less than 100 x RL |
| | | ■ | Detectors exceeding 100 x RL |



D	JWH	93095
Ch ck d	709	10/2/95
Appr d	MES	10/11/95
FILE DJS 4 3B DMG		
EXTENT OF ORGANIC COCs IN SURFACE SOIL IHSS 142/209		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OUS-WOMAN CREEK PRIORITY DRAINAGE		
RPT/MI REPORT		
FIGURE 4-3B		



- MAP LEGEND**
- | | |
|----|--|
| X | Sample Location |
| ○ | Detects less than the Reporting Limit (RL) |
| ⊙ | Detects exceeding RL but less than 10 x RL |
| ■ | Detects exceeding 10 x RL but less than 100 x RL |
| ■ | Detects exceeding 100 x RL |
| / | STREAMS, DITCHES, DRAINAGE FEATURES |
| == | PAVED ROADS |
| == | DIRT ROADS |
| — | IHSS BOUNDARY |



Dr wn JWH 10/3/95

Check d 7/7 10/3/95

Appr ed MRS 10/3/95

Date 10/3/95

FILE DUS 4 3C DMG

EXTENT OF ORGANIC COCs
IN SURFACE SOIL
IHSS 115/196

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WIDMAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

FIGURE 4-3C

LOCATION

CONSTITUENTS
100 x 100
100 x 100

CONSTITUENTS
100 x 100
100 x 100

0 75 150

SCALE 1" = 150'

MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

Sample Location

Detectors less than the Reporting Limit (RL)

Detectors exceeding RL
but less than 10 x RL

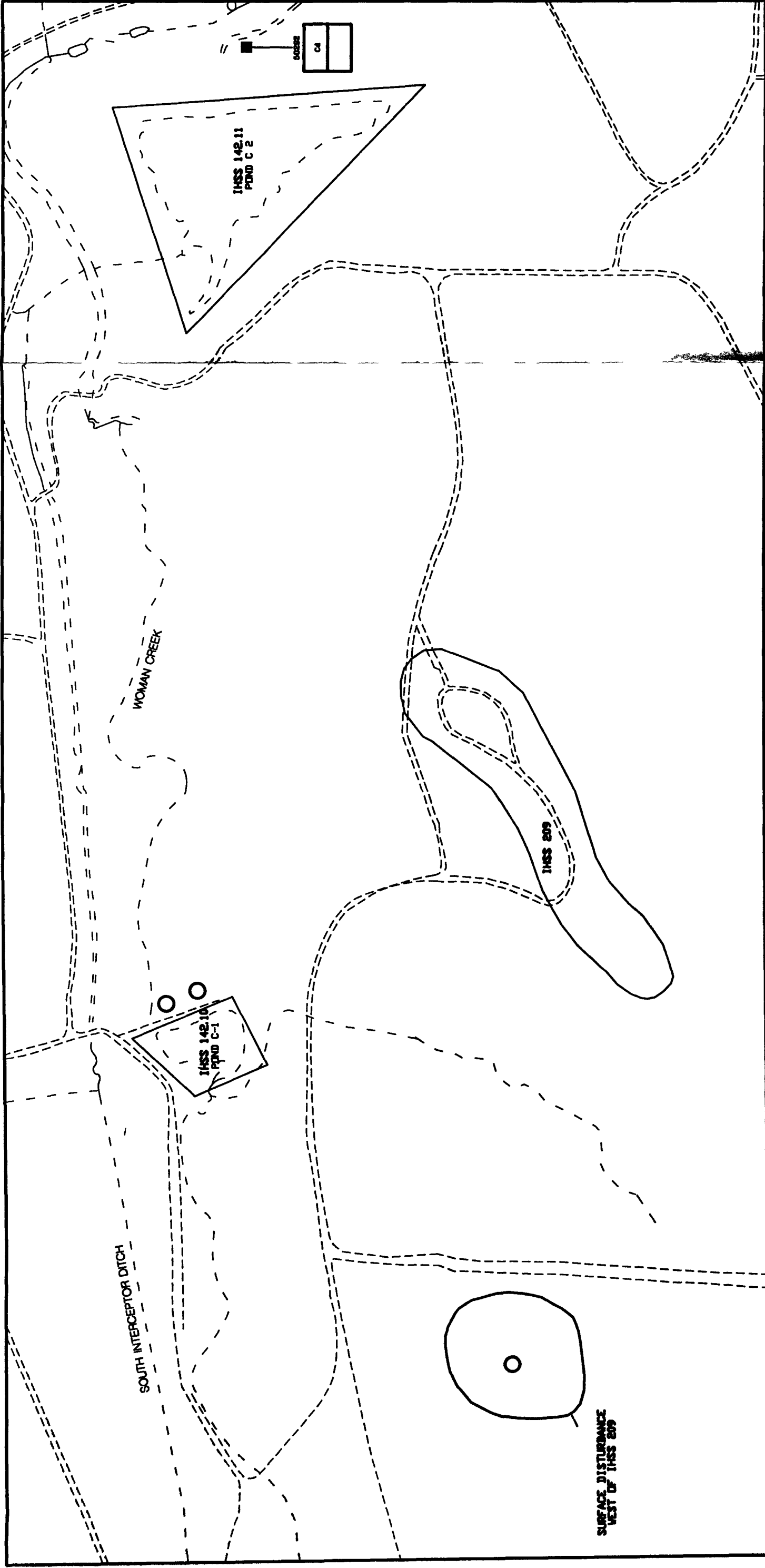
Detectors exceeding 10 x RL
but less than 100 x RL

Detectors exceeding 100 x RL

BACKGROUND DATA

SYMBOL	CONSTITUENT	RL (µg/kg)
DBA	Dibenzo(a,h)anthracene	330
IDRTL	Fluoranthene	330
IP	Indeno(1,2,3-cd)Pyrene	330
Pyrene	Pyrene	330

SYMBOL	CONSTITUENT	RL (µg/kg)
PCB	Aroclor - 1254	160
B(a)a	Benzo(a)anthracene	330
B(a)p	Benzo(a)Pyrene	330
B(b)f	Benzo(b)Fluoranthene	330



Dr n JWH 9/30/98
Ch k d 7/9 9/2/98
Appro d WLS 10/10/98

FILE DUS 4 4B DMG

EXTENT OF METAL COCs
IN SUBSURFACE SOIL
IHSS 142/209

ROCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

RTI/RI REPORT

FIGURE 4-4B

MAP LEGEND

LOCATION

CONSTITUENTS
>BM+3 STD DEV
CONSTITUENTS
>BM+3 STD DEV
AND
CONSTITUENTS
>BM+3 STD DEV

Note: Constituents occurring
in different concentrations
at the same location represent
samples from different depths

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

X < Background Mean (BM)

O > BM and < BM 1 STD DEV

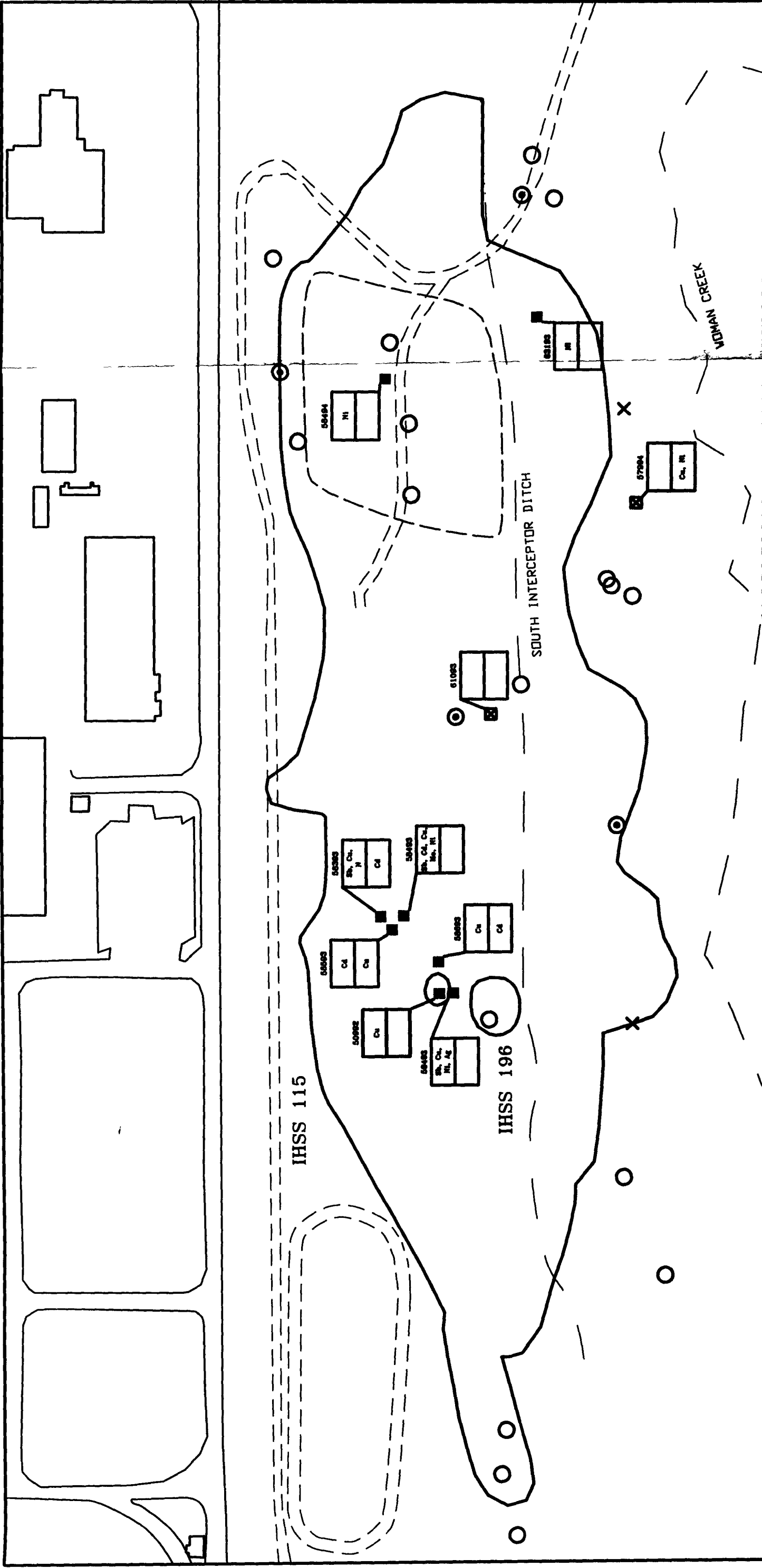
⊙ > BM 1 STD DEV and < BM 2 STD DEV

■ > BM 2 STD DEV and < BM 3 STD DEV

■ > BM 3 STD DEV

BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (mg/kg)	STD. DEV
Sb	Antimony	6.56	2.84
Ba	Barium	4.66	4.77
Ca	Calcium	0.64	0.24
Cu	Copper	12.59	12.77
Mn	Manganese	15.39	9.01
Ni	Nickel	19.81	20.56
Ag	Silver	5.70	9.40



Dr. n. JWH 9/30/95
Checked 7/29 8/2/95
Appr. v. d. MGS 10/10/95

FILE QUS 4 4C DVG

EXTENT OF METAL COCs
IN SUBSURFACE SOIL
IHSS 115/196

ROCKY PLATE ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

ERT/RI REPORT

FIGURE 4-4C

MAP LEGEND

STREAMS, DITCHES, DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

Background Mean (BM)

< BM and > BM 1 STD DEV

> BM 1 STD DEV and < BM 2 STD DEV

> BM 2 STD DEV and < BM 3 STD DEV

> BM 3 STD DEV

LOCATION

CONSTITUENTS > BM+3 STD DEV

CONSTITUENTS BM+2 STD DEV AND < BM-2 STD DEV

CONSTITUENTS < BM-3 STD DEV

BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (mg/kg)	STD. DEV.
Sb	Antimony	6.56	2.84
Be	Beryllium	4.86	4.77
Cd	Cadmium	0.84	0.24
Cu	Copper	12.59	12.77
Mo	Molybdenum	15.39	9.01
Ni	Nickel	19.81	20.56
Ag	Silver	5.70	9.40

Note: Constituents occurring in different concentrations at the same location represent samples from different depths.

INCORRECT LOCATION
OF IHSS 133.1 SHOWN
IN OUS WORK PLAN

133 5
INCINERATOR
AREA

INCINERATOR
LOCATION

TDEM 1

133 6

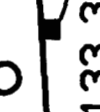
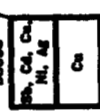
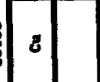
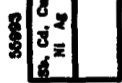
133 4
ASH PIT

TDEM 2

133 1
ASH PIT

133 3
ASH PIT

133 2
ASH PITS



YONAH CREEK

YONAH CREEK

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

- X < Background Mean (BM)
- O > BM and < BM 1 STD DEV
- ⊙ > BM 1 STD DEV and < BM 2 STD DEV
- > BM 2 STD DEV and < BM 3 STD DEV
- > BM 3 STD DEV

MAP LEGEND

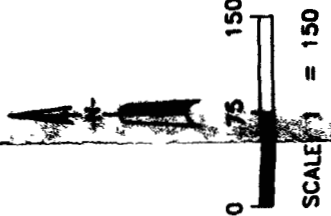
LOCATION
CONSTITUENTS >BM+3 STD DEV
CONSTITUENTS >BM+2 STD DEV
CONSTITUENTS >BM+1 STD DEV
CONSTITUENTS >BM+0 STD DEV

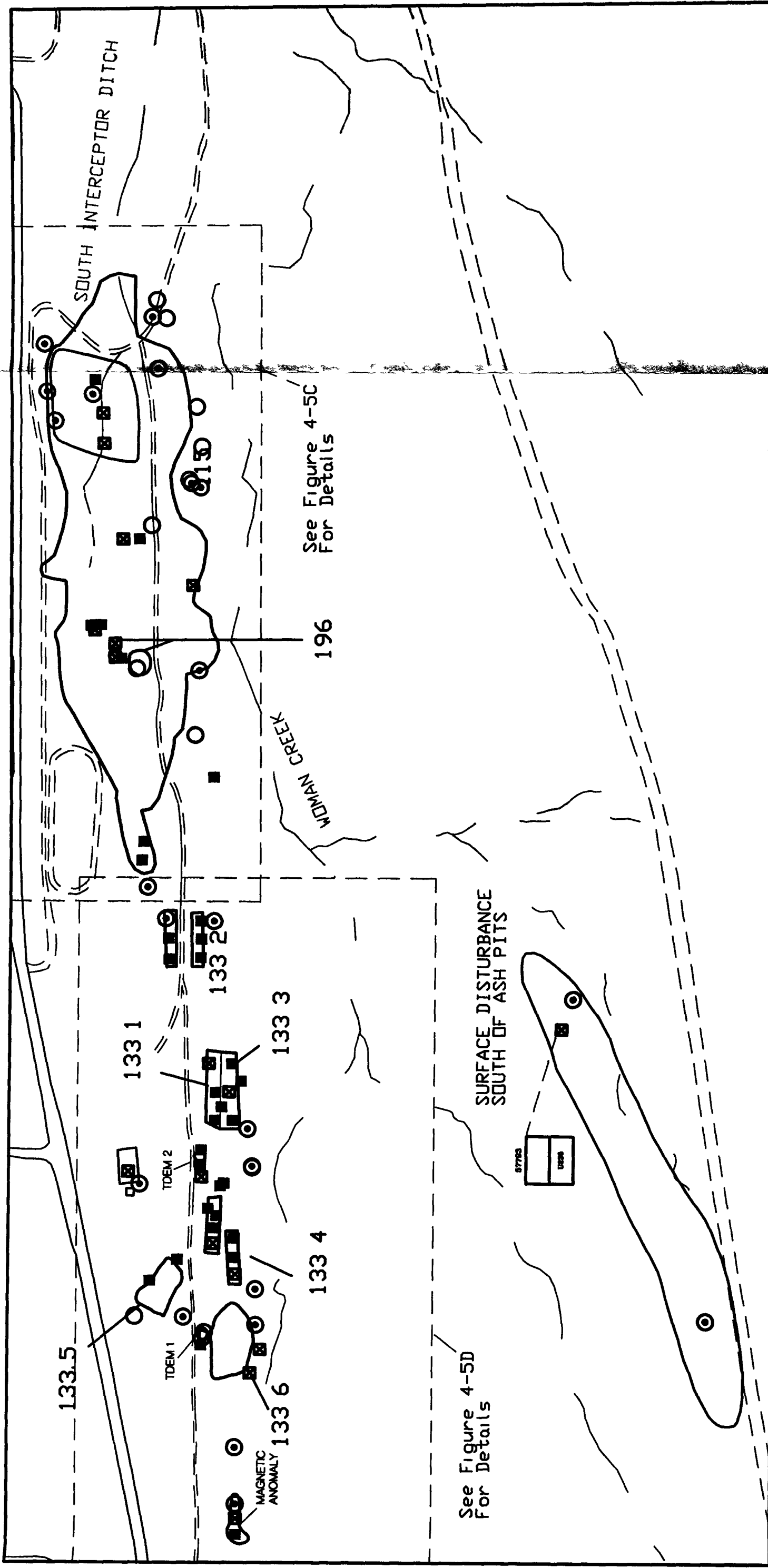
BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (mg/kg)	STD. DEV.
Sb	Antimony	6.56	2.84
Bi	Bismuth	4.66	4.77
Cd	Cadmium	0.64	0.24
Cu	Copper	12.59	12.77
Mn	Manganese	15.39	9.01
Ni	Nickel	19.81	20.56
Ag	Silver	5.70	9.40

Note: Constituents occurring
in different concentrations
at the same location represent
samples from different depths.

Dr. JNH 9/30/95
Check d 7/27 10/10/95
Appr d MGS 10/10/95
Date
FILE OUS 4 4D.DWG
EXTENT OF METAL COCs
IN SUBSURFACE SOIL
IHSS 133
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS-YONAH CREEK PRIORITY DRAINAGE
RPT/RM REPORT
FIGURE 4-4D





Drawn: JWH 9/24/95
Checked: JWH 10/2/95
Approved: JWH 10/2/95

FILE QUS-4 SA DIV

EXTENT OF RADIONUCLIDE
COCs IN SUBSURFACE SOIL

DOCKY PLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS-WOMAN CREEK PROPERTY DRAINAGE
REF/RE REPORT

FIGURE 4-5A

0 1 350
SCALE
= 350

MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

HSS BOUNDARY

LOCATION

CONSTITUENTS
BM-3 STD DEV

CONSTITUENTS
>BM-3 STD DEV
AND
<BM-3 STD DEV

Note: Constituents occurring
in different concentrations
at the same location represent
samples from different depths.

< Background Mean (BM)

> BM and
< BM 1 STD DEV

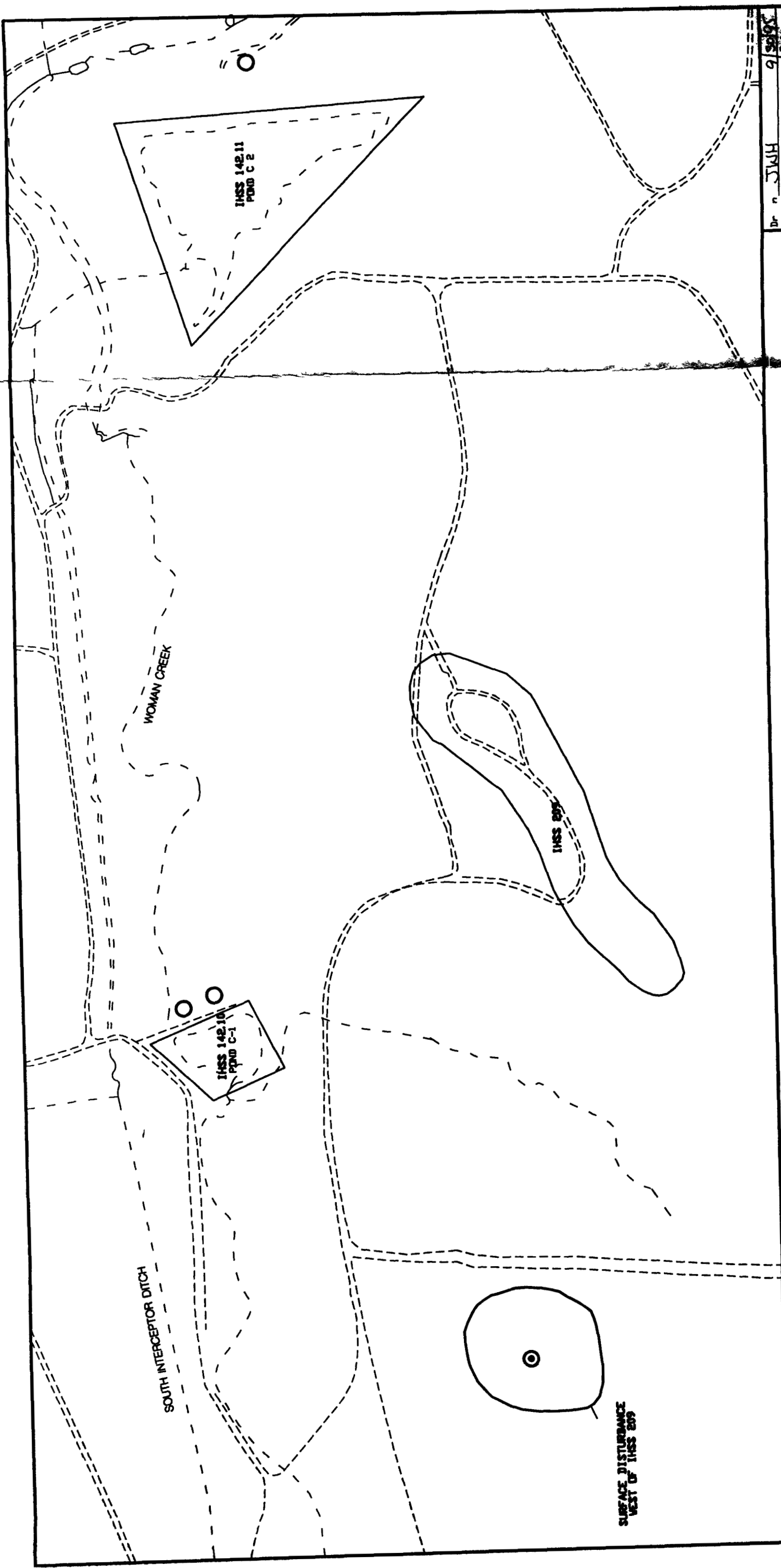
> BM 1 STD DEV and
< BM 2 STD DEV

> BM 2 STD DEV and
< BM 3 STD DEV

> BM 3 STD DEV

BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (pCi/g)	STD. DEV
U235/234	Uranium 235/234	0.779	0.932
U238	Uranium 238	0.022	0.046
U238	Uranium 238	0.733	0.376



Dr n JWH 9/29/85
Ch k d 7-7 1/8/85
Appr d Mew 10/10/85
Date

FILE QUS 4 SB DMG

EXTENT OF RADIONUCLIDE
COCs IN SUBSURFACE SOIL
IHSS 142/209

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

QUS-WOMAN CREEK PRIORITY DRAINAGE

B7/MI REPORT

FIGURE 4-0B

MAP LEGEND

LOCATION
CONSTITUENTS >BM+3 STD DEV
CONSTITUENTS >BM+2 STD DEV
CONSTITUENTS >BM+1 STD DEV
CONSTITUENTS >BM+0 STD DEV

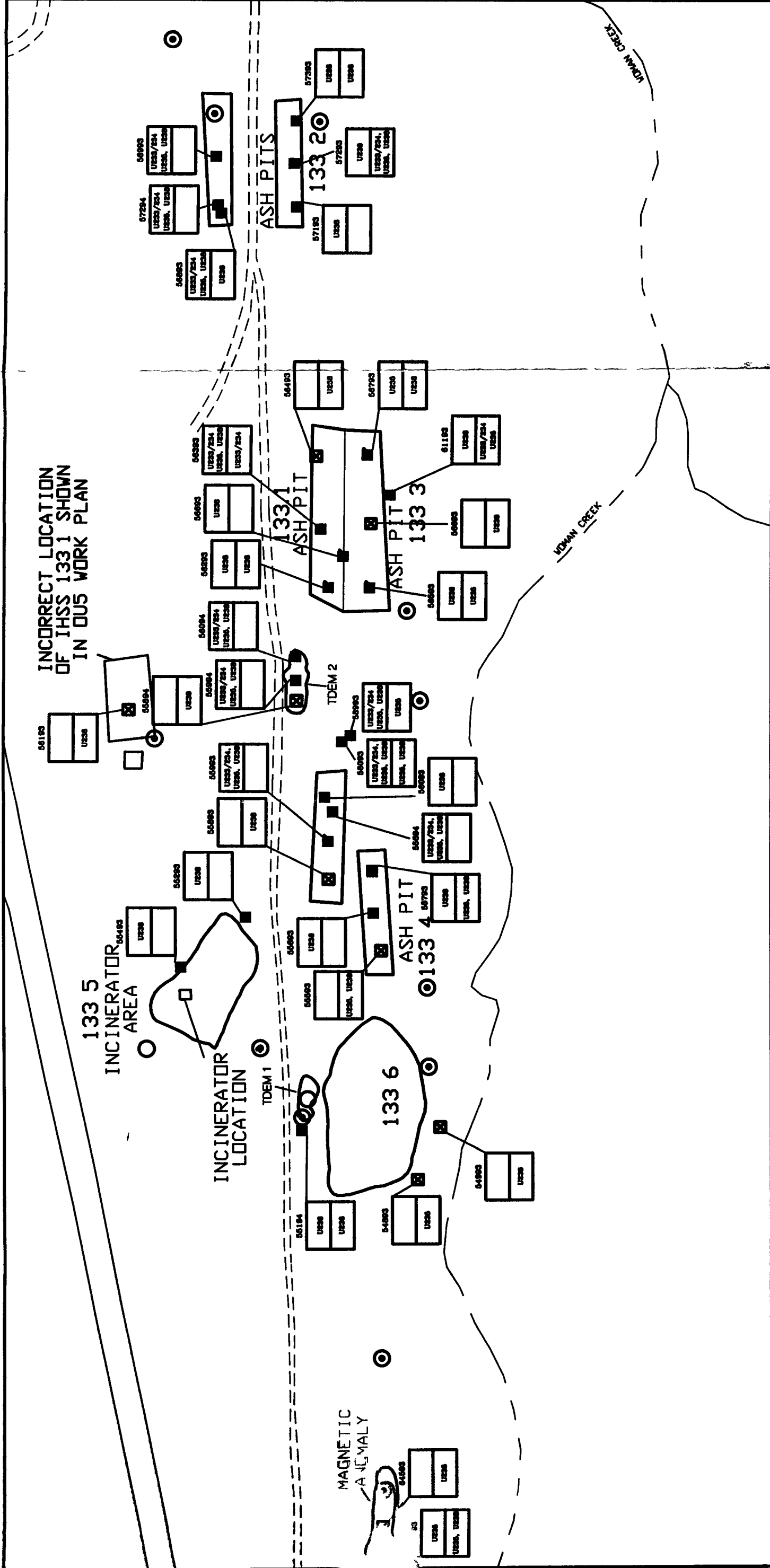
- X < Background Mean (BM)
- > BM and < BM 1 STD DEV
- ⊙ > BM 1 STD DEV and < BM 2 STD DEV
- ⊙ > BM 2 STD DEV and < BM 3 STD DEV
- > BM 3 STD DEV

- STREAMS, DITCHES,
DRAINAGE FEATURES
- == PAVED ROADS
- == DIRT ROADS
- IHSS BOUNDARY

BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (pCi/g)	STD. DEV
UC235/234	Uranium 235/234	0.779	0.932
UC238	Uranium 238	0.022	0.046
UC236	Uranium 236	0.733	0.376

Note: Constituents occurring
in different concentrations
at the same location represent
samples from different depths.



Dr n JWH 9/30/95

Check d 7/2 10/3/95

App ed MRS 10/10/95

FILE DUS 4 SD DUG

EXTENT OF RADIONUCLIDE COCs IN SUBSURFACE SOIL IHSS 133

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

RPT/RI REPORT

FIGURE 4-5D

0 75 150

SCALE 1" = 150

MAP LEGEND

STREAMS, DITCHES, DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

LOCATION

CONSTITUENTS >BM+3 STD DEV

CONSTITUENTS >BM+3 STD DEV AND <BM+3 STD DEV

Notes: Constituents occurring in different concentrations at the same location represent samples from different depths.

Background Mean (BM)

< BM and > BM 1 STD DEV

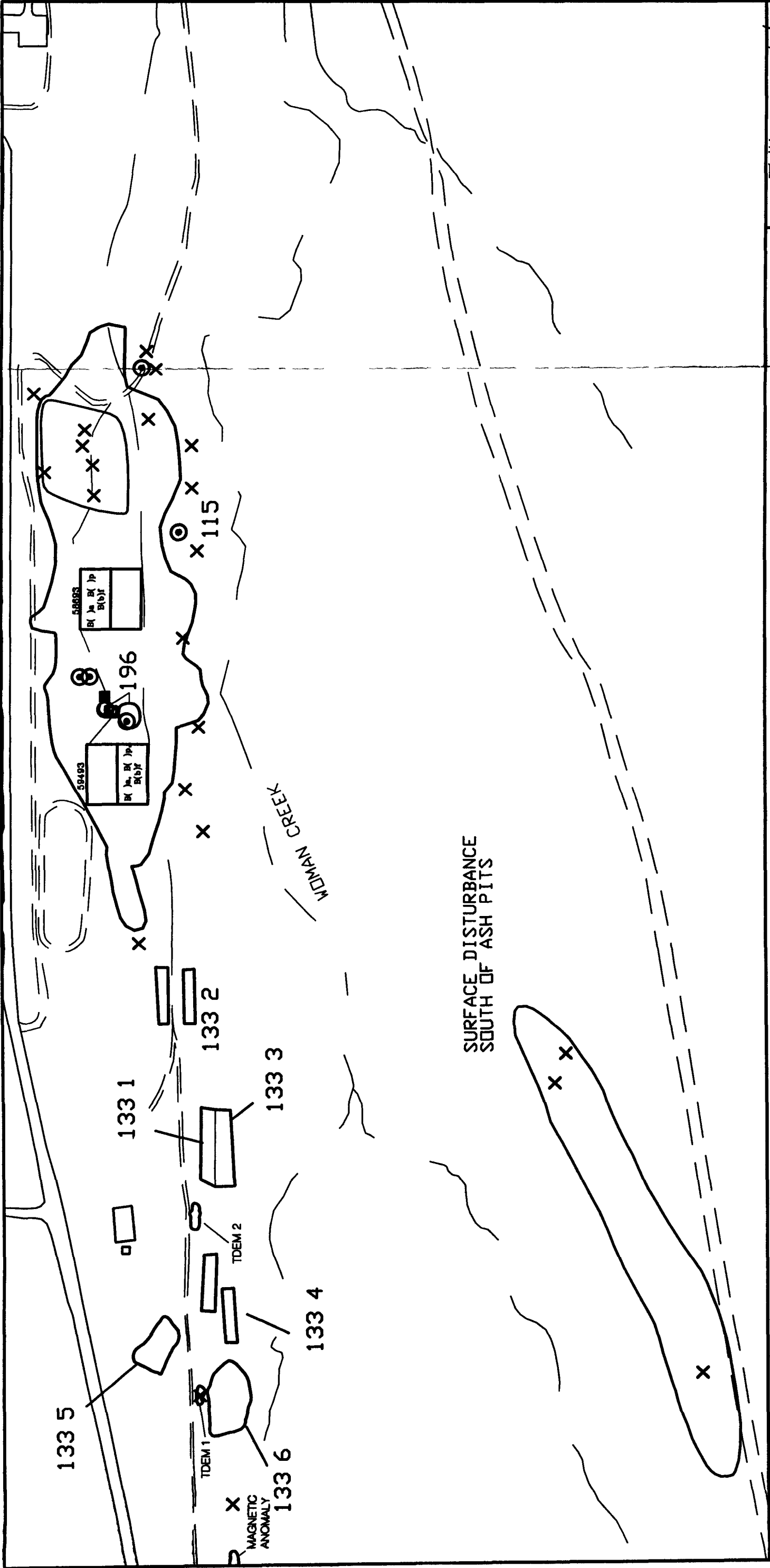
> BM 1 STD DEV and < BM 2 STD DEV

> BM 2 STD DEV and < BM 3 STD DEV

> BM 3 STD DEV

BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (pCi/g)	STD. DEV
U235/234	Uranium 235/234	0.779	0.932
U235	Uranium 235	0.022	0.046
U238	Uranium 238	0.733	0.376



Dr wn JWKH 9/30/95
Check d 7/27 10/13/95
Appr d MES 10/10/95
FILE DJS 4 6A DMG

**EXTENT OF ORGANIC COCs
IN SUBSURFACE SOIL**

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS-WOMAN CREEK PRIORITY DRAINAGE
RPT/RI REPORT
FIGURE 4-6A

0 175 350
SCALE: 1" = 350'

MAP LEGEND

STREAMS, DITCHES, DRAINAGE FEATURES
PAVED ROADS
DIRT ROADS
HSS BOUNDARY

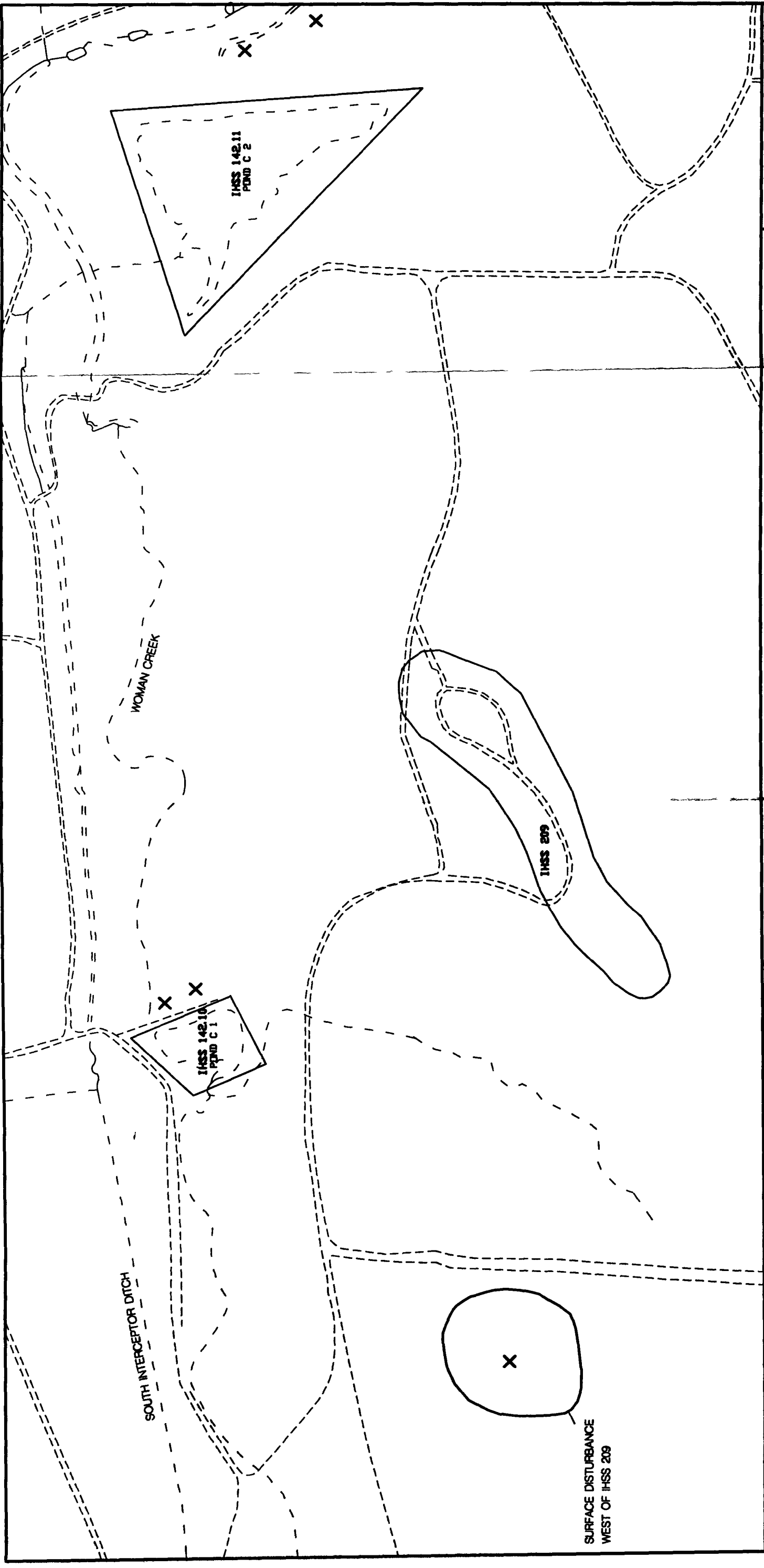
Sample Location
Detects less than the Reporting Limit (RL)
Detects exceeding RL but below 10 x RL
Detects exceeding 10 x RL but below 100 x RL
Detects exceeding 100 x RL

LOCATION
CONSTITUENTS
100 ML
CONCENTRATION
10 ML
= 100 ML

BACKGROUND DATA

SYMBOL	CONSTITUENT	Reporting Limit (RL) µg/kg
PCB	Aroclor-1254	160
B(a)h	Benzo(a)anthracene	330
B(k)h	Benzo(k)fluoranthene	330
B(a)P	Benzo(a)pyrene	330
B(b)F	Benzo(b)fluoranthene	330
B(a)A	Benzo(a)anthracene	330
B(a)P	Benzo(a)pyrene	330
IP	Indeno(1,2,3-cd)pyrene	330
Pyrene	Pyrene	330

Note: Constituents occurring in different concentrations at the same location represent samples from different depths.



D

Ch k d

Appro d

FILE QUS 4 6B DWG

10/2/95

7#7

WES

10/10/95

10/2/95

0/3/95

10/10/95

EXTENT OF ORGANIC COCs
IN SUBSURFACE SOIL
IHSS 142/209

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

RFI/RI REPORT

FIGURE 4-6B

MAP LEGEND

STREAMS, DITCHES,
DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

IHSS BOUNDARY

X

○

⊙

■

■

Sample Location

Detects less than the Reporting Limit (RL)

Detects exceeding RL
but below 10 x RL

Detects exceeding 10 x RL
but below 100 x RL

Detects exceeding 100 x RL

LOCATION

CONSTITUENTS
100 x RL

CONSTITUENTS
10 x RL

CONSTITUENTS
1 x RL

CONSTITUENTS
100 x RL

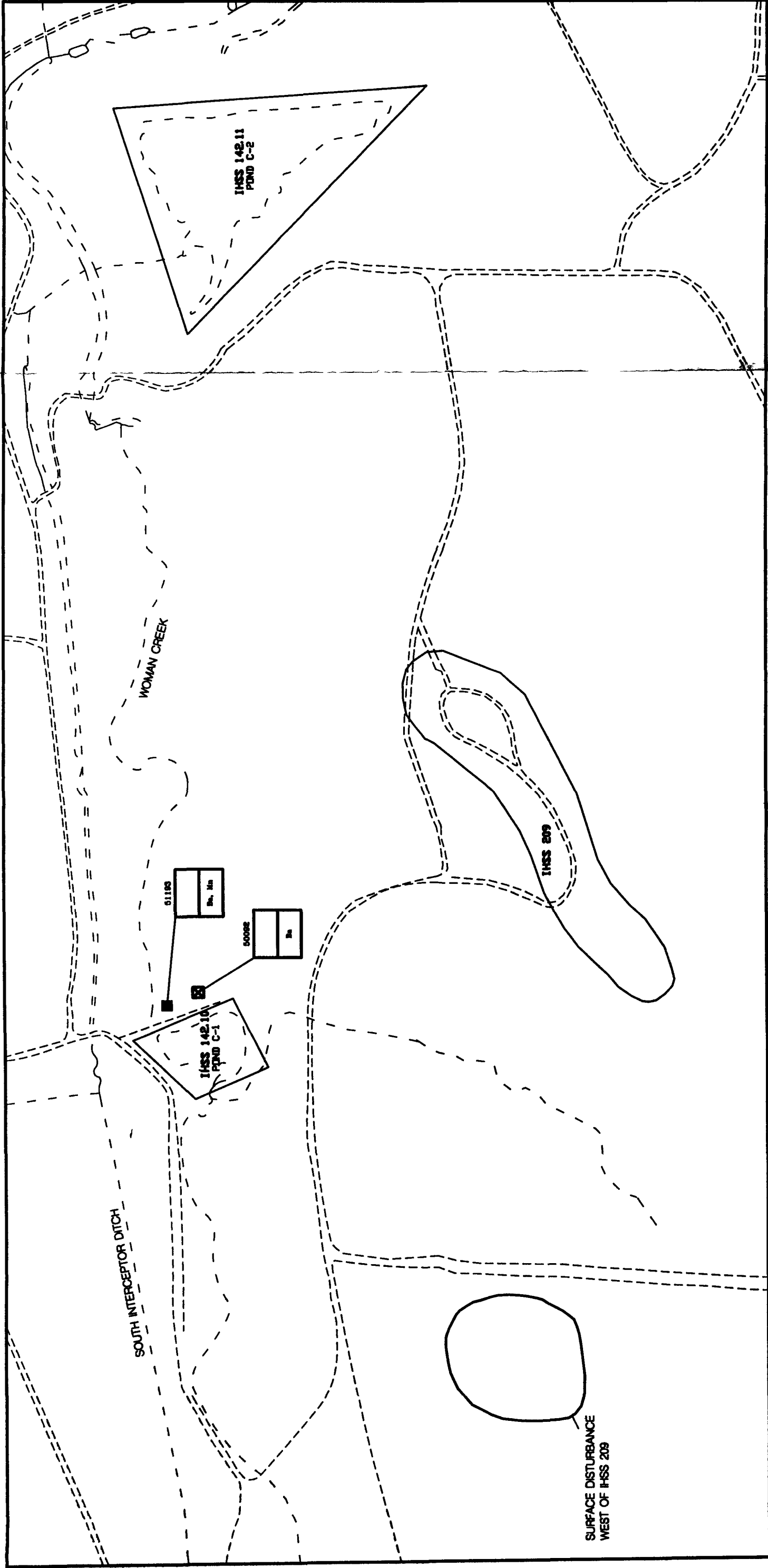
CONSTITUENTS
10 x RL

CONSTITUENTS
1 x RL

BACKGROUND DATA

SYMBOL	CONSTITUENT	Reporting Limit (RL) µg/kg
PCB	Aroclor-1254	160
M 1a	Benzofluoranthene	330
M 1b	Benzofluoranthene	330
M 1c	Benzofluoranthene	330
M 1d	Benzofluoranthene	330
M 1e	Benzofluoranthene	330
M 1f	Benzofluoranthene	330
M 1g	Benzofluoranthene	330
M 1h	Benzofluoranthene	330
M 1i	Benzofluoranthene	330
M 1j	Benzofluoranthene	330
M 1k	Benzofluoranthene	330
M 1l	Benzofluoranthene	330
M 1m	Benzofluoranthene	330
M 1n	Benzofluoranthene	330
M 1o	Benzofluoranthene	330
M 1p	Benzofluoranthene	330
M 1q	Benzofluoranthene	330
M 1r	Benzofluoranthene	330
M 1s	Benzofluoranthene	330
M 1t	Benzofluoranthene	330
M 1u	Benzofluoranthene	330
M 1v	Benzofluoranthene	330
M 1w	Benzofluoranthene	330
M 1x	Benzofluoranthene	330
M 1y	Benzofluoranthene	330
M 1z	Benzofluoranthene	330

Notes: Constituents occurring
in different concentrations
at the same location represent
samples from different depths.



Dr. n. JKH		10/2/95	Date
Checked		727	Date 10/5/95
Approved		MES	Date 10/10/95
FILE DJS 4.7B.DVG			
EXTENT OF DISSOLVED METAL COCs IN GROUNDWATER IHSS 142/209			
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE			
OUS-WOMAN CREEK PRIORITY DRAINAGE			
RPT/RE REPORT			
FIGURE 4-7B			

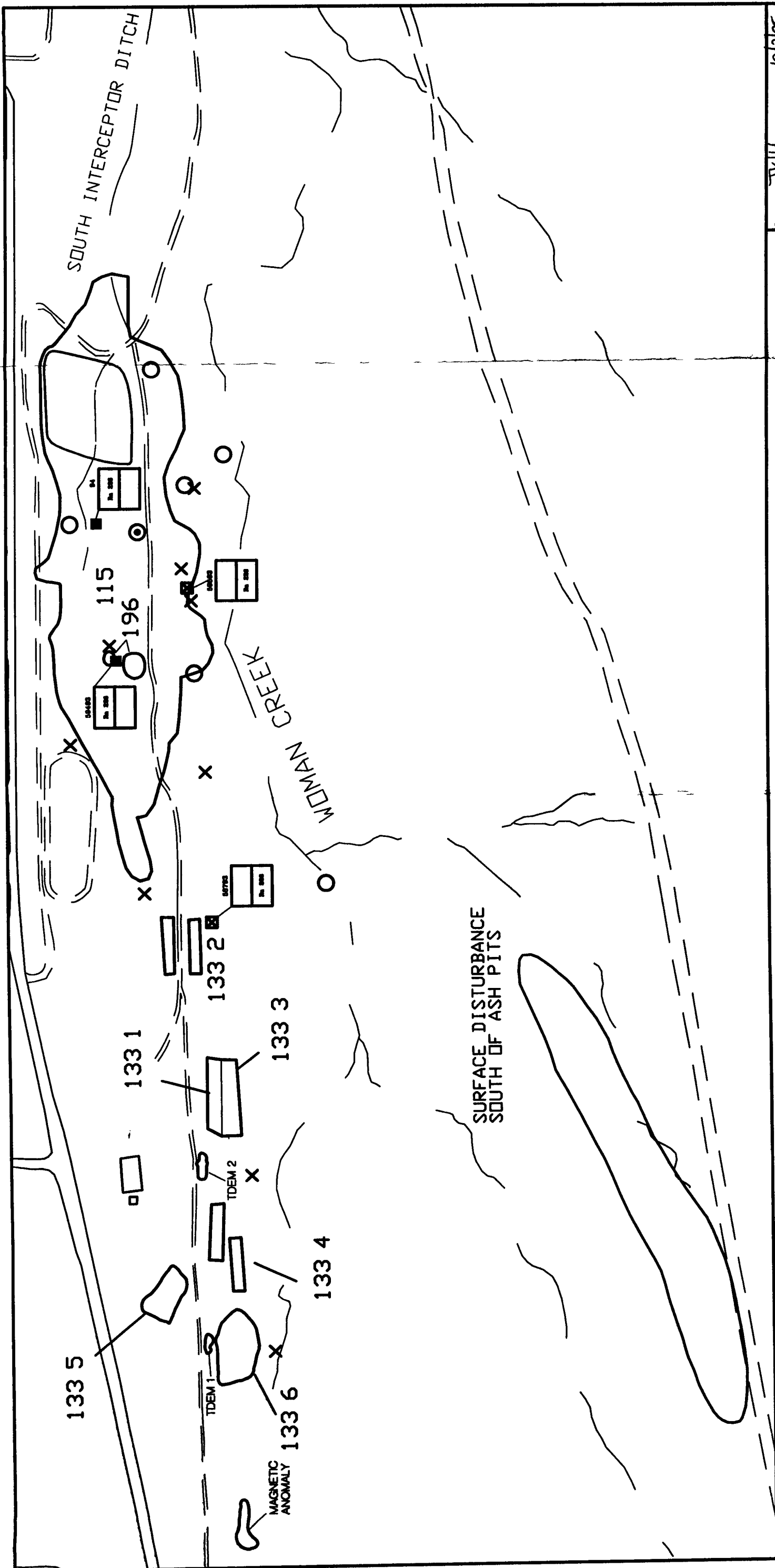
BACKGROUND DATA			
SYMBOL	CONSTITUENT	MEAN (µg/l)	STD DEV
Al	Dissolved Aluminum	113.66	594.80
Ba	Dissolved Barium	84.00	33.10
Mn	Dissolved Manganese	32.66	87.43

LOCATION	
CONSTITUENTS	> BM +3 STD DEV
CONSTITUENTS	> BM +3 STD DEV
CONSTITUENTS	> BM +3 STD DEV
CONSTITUENTS	> BM +3 STD DEV

Note: Constituents occurring in different concentrations at the same location represent samples collected on different dates.

X	< Background Mean (BM)
○	> BM and < BM +1 STD DEV
⊙	> BM +1 STD DEV and < BM +2 STD DEV
■	> BM +2 STD DEV and < BM +3 STD DEV
■	> BM +3 STD DEV

STREAMS, DITCHES, DRAINAGE FEATURES	
—	PAVED ROADS
==	DIRT ROADS
---	HSS BOUNDARY



Drawn by JKH Date 10/2/95

Checked by 729 Date 10/3/95

Approved by HLS Date 10/10/95

FILE DUS 4 8A DVG

EXTENT OF DISSOLVED RADIONUCLIDE COCs IN GROUNDWATER

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

RPT/RM REPORT

FIGURE 4-8A

MAP LEGEND

LOCATION

CONSTITUENTS
>BM+6 STD DEV
<BM+6 STD DEV

CONSTITUENTS
>BM+6 STD DEV
<BM+6 STD DEV
<BM+3 STD DEV

SYMBOL

X < Background Mean (BM)

O > BM and < BM 1 STD DEV

⊙ > BM 1 STD DEV and < BM 2 STD DEV

■ > BM 2 STD DEV and < BM 3 STD DEV

■ > BM 3 STD DEV

STREAMS, DITCHES, DRAINAGE FEATURES

PAVED ROADS

DIRT ROADS

HSS BOUNDARY

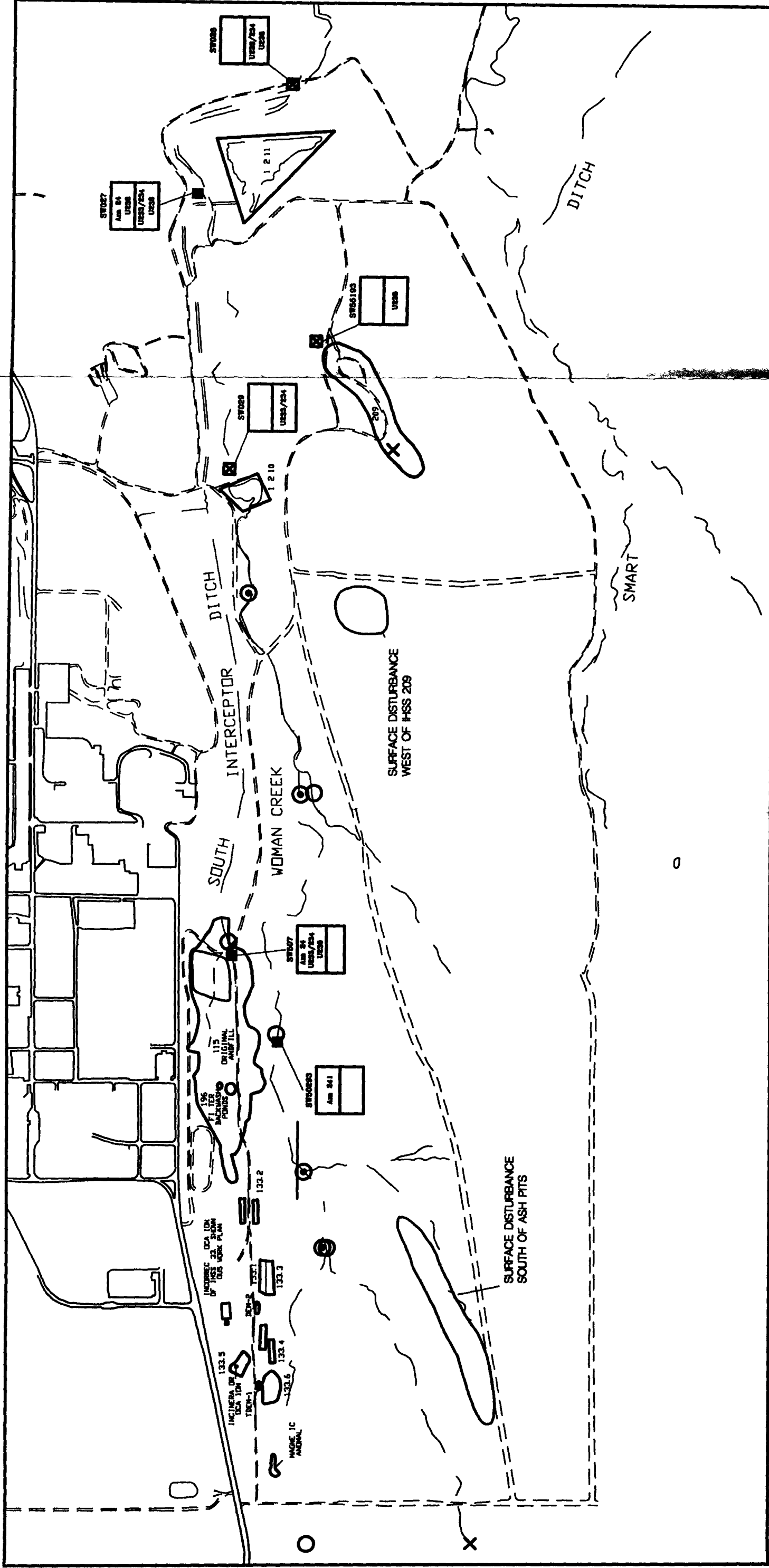
BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (pCi/l)	STD DEV
U233/234	Dissolved U233/234	6.914	25.440
U235	Dissolved U235	0.20	0.640
U238	Dissolved U238	4.832	17.670
Am241	Dissolved Am241	0.011	0.010
Ra226	Dissolved Ra226	0.258	0.110

Note: Constituents occurring in different concentrations at the same location represent samples collected on different dates.

0 175 350

SCALE 1" = 350'



Dr n JWH 10/3/95
Checked 729 10/3/95
Appr ed MRS 10/10/95
FILE DLS 4 10.DWG
EXTENT OF TOTAL RADIONUCLIDE COCs IN SURFACE WATER
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE
OUS-WOMAN CREEK PRIORITY DRAINAGE
RFL/RE REPORT
FIGURE 4-10

MAP LEGEND

STREAMS, DITCHES, DRAINAGE FEATURES
PAVED ROADS
DIRT ROADS
HSS BOUNDARY

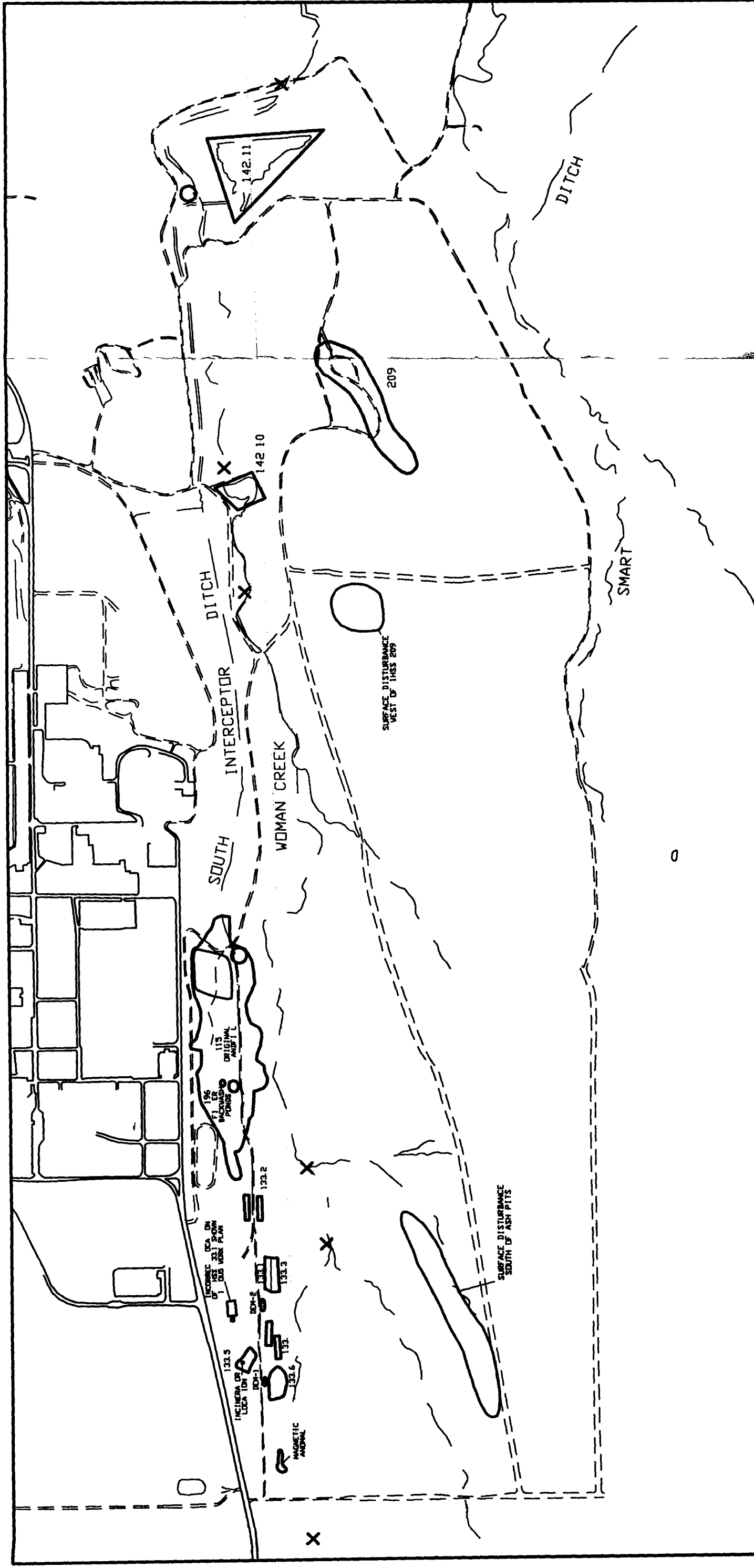
LOCATION

CONSTITUENTS
BM-13 STD DEV
CONSTITUENTS
BM-13 STD DEV
CONSTITUENTS
BM-13 STD DEV
CONSTITUENTS
BM-13 STD DEV

Note: Constituents occurring in different concentrations at the same location represent samples collected on different dates.

BACKGROUND DATA

SYMBOL	CONSTITUENT	MEAN (pCi/l)	STD DEV
Am241	Total Am241	0.0039	0.0060
U233/234	Total U233/234	0.4862	0.5500
U238	Total U238	0.3642	0.4360



Dr. Wm. J. W. H. 10/3/95

Check #	Check d	Date
722	10/3/95	

Approved _____ Date 12/21/05

Date _____

FILE D05 4 12 DMG

EXTENT OF RADIONUCLIDE COCs IN STREAM SEDIMENTS

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OUS-WOMAN CREEK PRIORITY DRAINAGE

REF/DE REPORT

FIGURE 4-12

MAP LEGEND

< Background Mean (BM)

	< BM	= BM	> BM and pure MB	STD DEV
MB	0.0000	0.0000	0.0000	0.0000
BM	0.0000	0.0000	0.0000	0.0000
MB + BM	0.0000	0.0000	0.0000	0.0000
MB - BM	0.0000	0.0000	0.0000	0.0000
MB * BM	0.0000	0.0000	0.0000	0.0000
MB / BM	0.0000	0.0000	0.0000	0.0000
MB ^ BM	0.0000	0.0000	0.0000	0.0000
BM ^ MB	0.0000	0.0000	0.0000	0.0000
MB > BM	0.0000	0.0000	0.0000	0.0000
BM > MB	0.0000	0.0000	0.0000	0.0000
MB < BM	0.0000	0.0000	0.0000	0.0000
BM < MB	0.0000	0.0000	0.0000	0.0000
MB = BM	0.0000	0.0000	0.0000	0.0000
BM = MB	0.0000	0.0000	0.0000	0.0000
MB >= BM	0.0000	0.0000	0.0000	0.0000
BM >= MB	0.0000	0.0000	0.0000	0.0000
MB <= BM	0.0000	0.0000	0.0000	0.0000
BM <= MB	0.0000	0.0000	0.0000	0.0000
MB > BM or pure MB	0.0000	0.0000	0.0000	0.0000
BM > MB or pure MB	0.0000	0.0000	0.0000	0.0000
MB < BM or pure MB	0.0000	0.0000	0.0000	0.0000
BM < MB or pure MB	0.0000	0.0000	0.0000	0.0000
MB = BM or pure MB	0.0000	0.0000	0.0000	0.0000
BM = MB or pure MB	0.0000	0.0000	0.0000	0.0000
MB >= BM or pure MB	0.0000	0.0000	0.0000	0.0000
BM >= MB or pure MB	0.0000	0.0000	0.0000	0.0000
MB <= BM or pure MB	0.0000	0.0000	0.0000	0.0000
BM <= MB or pure MB	0.0000	0.0000	0.0000	0.0000

```
> BM 1 STD DEV and
< BM 2 STD DEV
```

> BM 2 STD DEV and

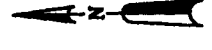
> BM 3 STD DEV

**STREAMS, DITCHES,
DRAINAGE FEATURES**

PAVED ROADS

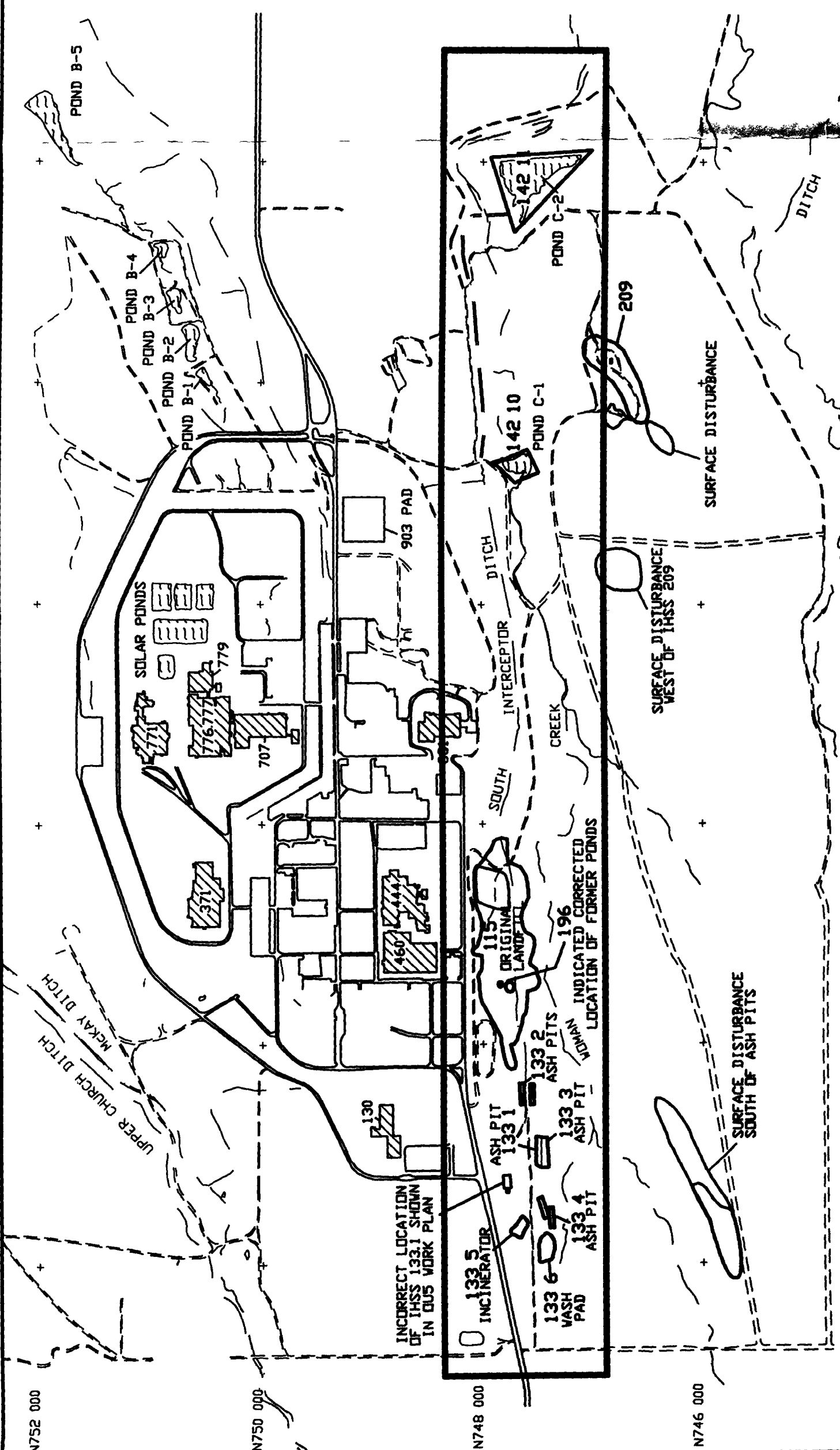
== DIRT ROADS

✓ IHSS BOUNDARY



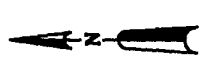
0 400 800

SCALE 1 = 800



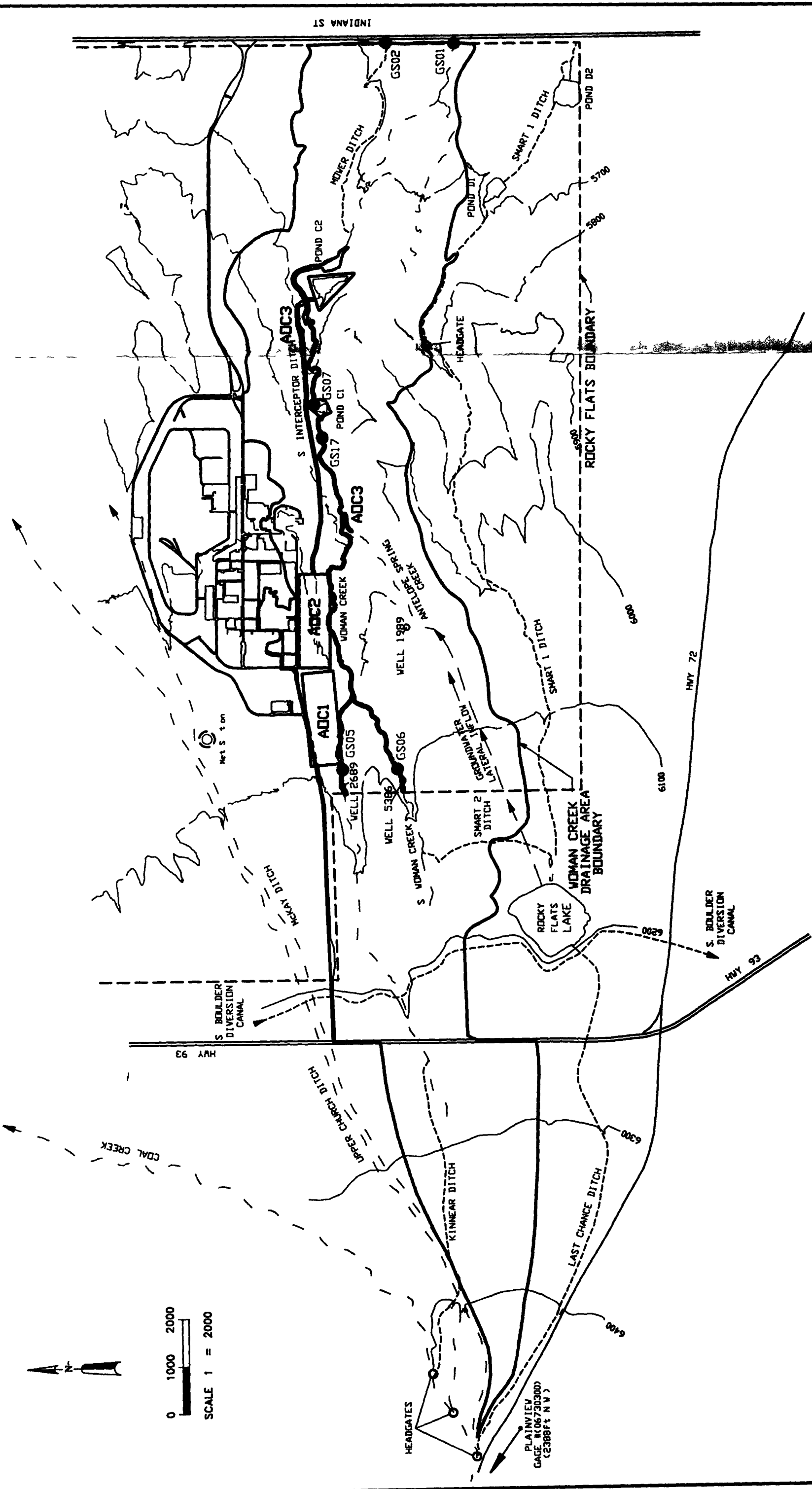
MAP LEGEND

- STREAMS, DITCHES, DRAINAGE FEATURES
- PAVED ROADS
- DIRT ROADS
- SURFACE WATER IMPOUNDMENTS
- BUILDINGS
- INDIVIDUAL HAZARDOUS SUBSTANCE SITES (APPROXIMATE LOCATION)
- MODELED AREA



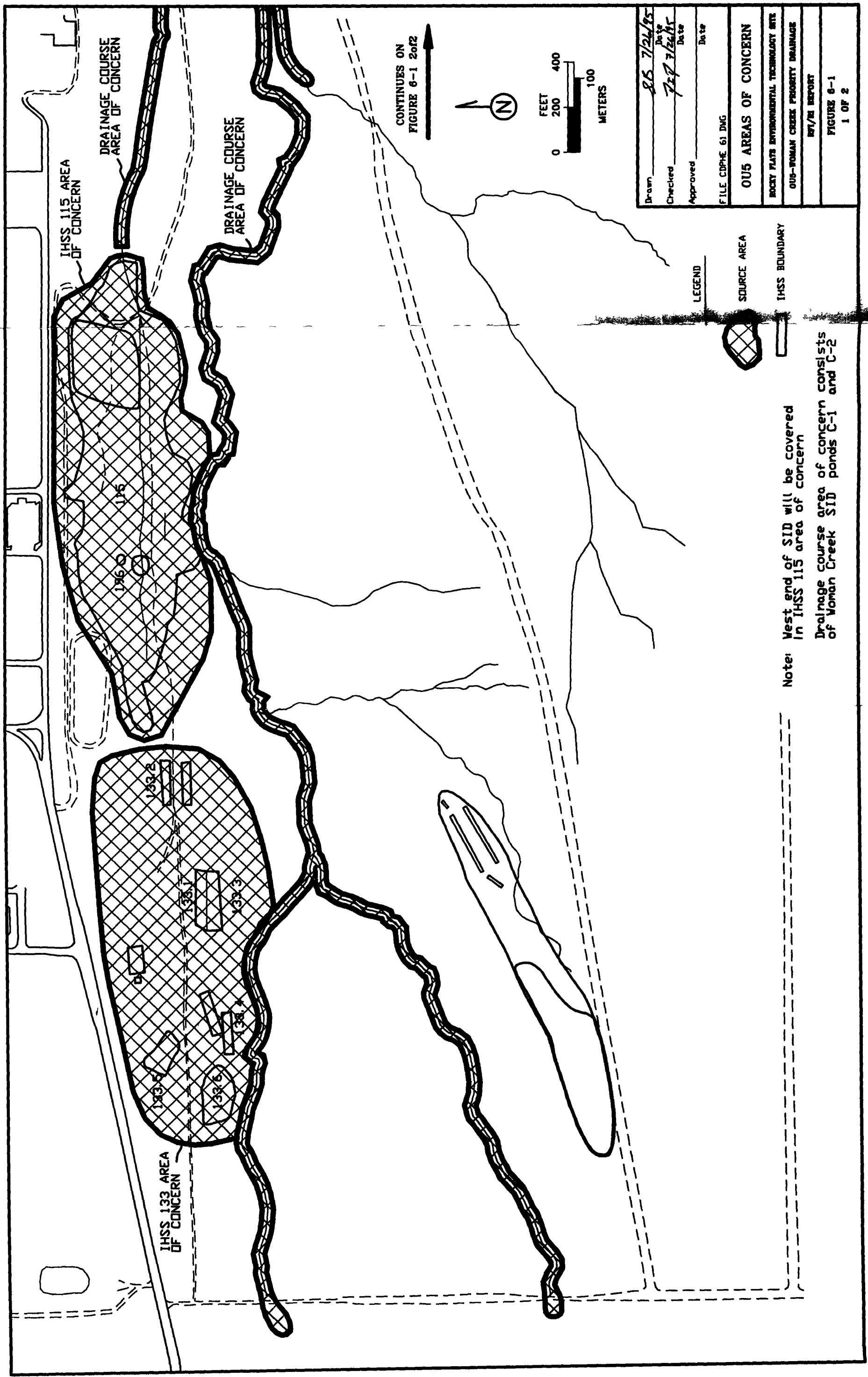
0 500 1000
SCALE 1" = 1000'

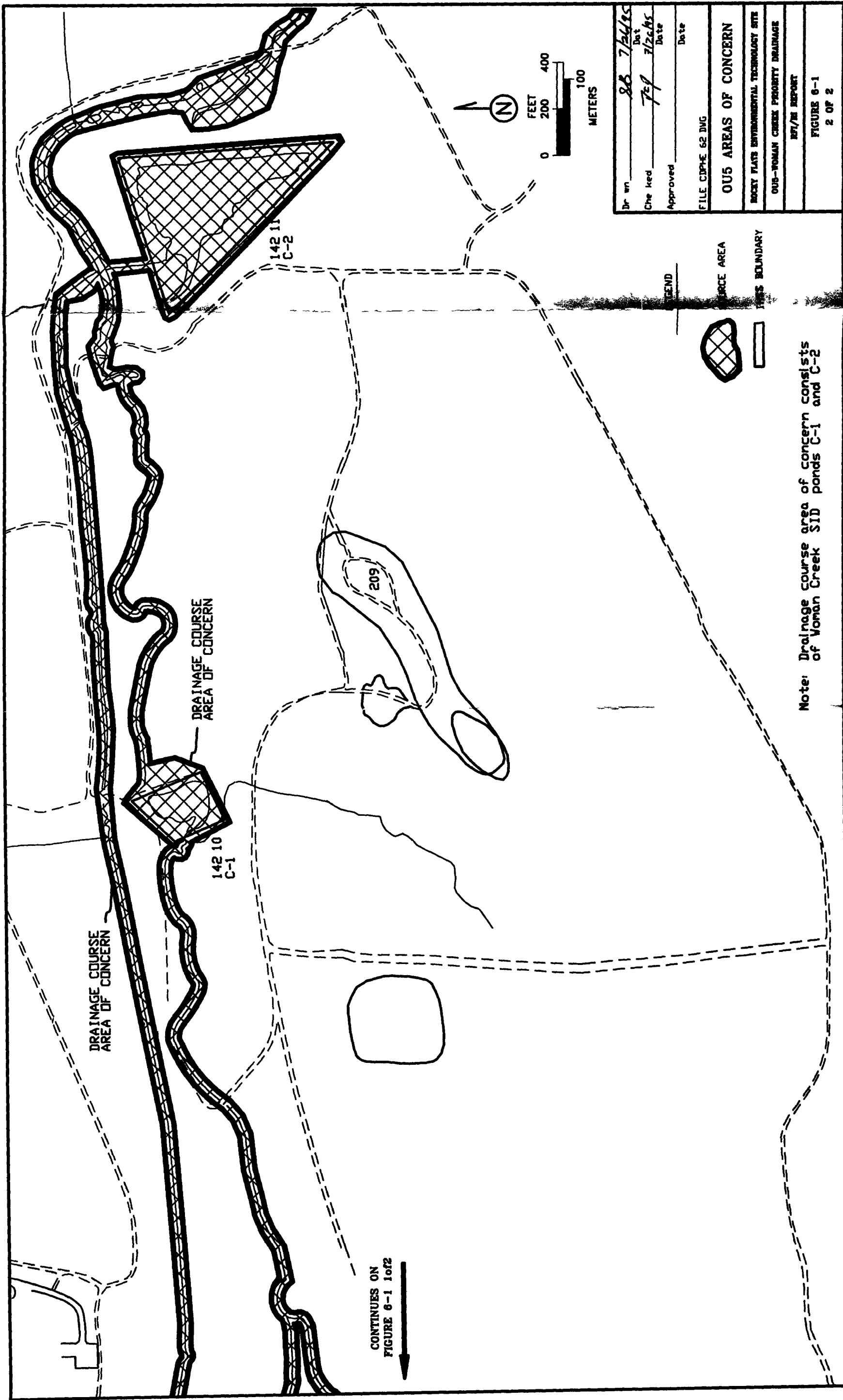
Drawn	11/11/85
Approved	7/27/85
Approved	8/5/85
Date	
Date	
FILE DUS 5 4 DNG	
GROUNDWATER MODEL SITE LOCATION MAP HIGHLIGHTING AREA MODELED	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	
DUS-WOMAN CREEK PRIORITY DRAINAGE	
RPT/RS REPORT	
FIGURE 6-4	



WOMAN CREEK	
PLAINIMETRIC FEATURES	
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE	Drawn NAM 8/75
OU5 - WOMAN CREEK PRIORITY DRAINAGE	Checked Tef
RFI/RI REPORT	Approved
FIGURE 5-16	FILE OUS-3 18 DWG

GS = Gage Station (Surface Water Flow Rate)
AOC = Area Of Concern





CONTINUES ON
FIGURE 6-1 1 of 2

Dr. wn	88	7/24/95
Chg. led	7/29	7/26/95
Approved		
FILE CDPHE 62 DWG		
OU5 AREAS OF CONCERN		
ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE		
OU5-WOMAN CREEK PRIORITY DRAINAGE		
RPT/RE REPORT		
FIGURE 6-1		
2 OF 2		

Note: Drainage course area of concern consists of Voman Creek SID ponds C-1 and C-2

PRIMARY
SOURCE

PRIMARY
RELEASE
MECHANISM

SECONDARY
SOURCE

SECONDARY
RELEASE
MECHANISM

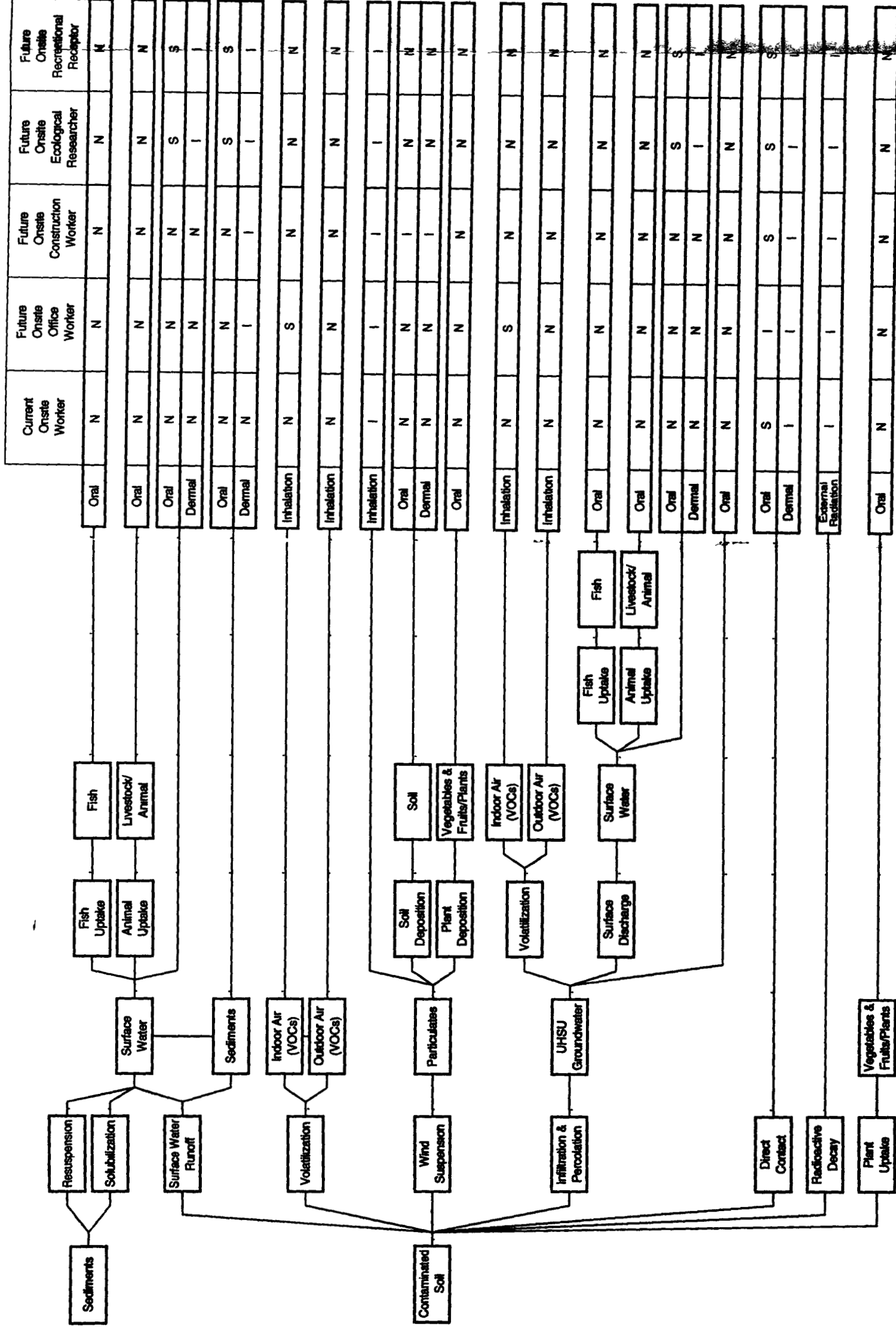
TERTIARY
SOURCE

TERTIARY
RELEASE
MECHANISM

QUATERNARY
SOURCE

EXPOSURE
ROUTE

POTENTIALLY EXPOSED
HUMAN RECEPTOR



S Significant Potential Exposure Pathway
I Insignificant Potential Exposure Pathway
N Negligible or Incomplete Exposure Pathway
UHSU Upper Hydrostratigraphic Unit

NOTES

- 1 Potentially complete dermal pathways will be quantitatively assessed only if investigation demonstrates presence of organic contaminants of concern
- 2 Significant and insignificant potential exposure pathways will be quantitatively evaluated.

CONCEPTUAL SITE MODEL

ROCKY FLATS ENVIRONMENTAL TECHNOLOGY SITE

OU5 WOMAN CREEK PRIORITY DRAINAGE

RF/RJ REPORT

FIGURE 6-3

EXPLANATION

- Watershed Boundary
- Rock Creek Watershed
- Walnut Creek Watershed
- Woman Creek Watershed
- Canals and Ditches
- Security Fences
- Rocky Flats Buffer Zone
- Lakes and Ponds
- Source Areas

- Preble's Meadow Jumping Mouse
- American Kestrel
- Great Blue Heron
- Mallard



U.S. Department of Energy
Rocky Flats Environmental Technology Site
Golden, Colorado

ERAs for Walnut Creek and Woman Creek
Watersheds at RFETS

Hazard Indices
for
Woman Creek Watershed

September 1995

Figure 7 2 2

